

Post Construction Stormwater Management/Site Restoration Plans Narrative

Atlantic Sunrise Project Phase 1

Compressor Station 610
Orange Township
Columbia County
Pennsylvania

Prepared For:



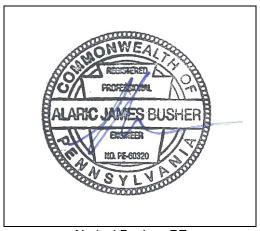
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> Issued: August 2015 Revised: October 2016

BL Project No. 14C4909

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United States Department of Agriculture (USDA) Natural Resources Conservation Service (NRCS) Custom Soil Resource Report



1.0 GENERAL INFORMATION

The following narrative was prepared as a supplement to the Transcontinental Gas Pipe Line Company, LLC.'s (Transco's) Environmental Construction Plan (ECP) provided in Section 4 of the Erosion and Sediment Control General Permit 2 (ESCGP-2) Notice of Intent (NOI), which was prepared for the Atlantic Sunrise Project ("Project"). This narrative is intended to describe the post construction stormwater management/site restoration (PCSM/SR) design for the Compressor Station 610 ("Site") to be constructed as part of the Project, within Orange Township, Columbia County, Pennsylvania. Similar narratives were prepared, under separate cover, for facilities in other affected counties, as well as for the pipeline construction.

The facility proposed to be constructed as part of Phase 1 of the Atlantic Sunrise Project in Columbia County is the following:

Facility Name	Facility Description	Facility Coordinates
Compressor Station 610	Compressor Station	N41°06'24.47", W76°26'57.38"

The Compressor Station 610 will be approximately 33.70 acres in area including a 1,526 linear foot new access road, 286,603 square feet (6.58 acres) of new gravel pad, and 261,861 square feet (6.01 acres) of impervious area. The Site will utilize existing public and private roads for access to the Site during and after construction. Best Management Practices (BMPs), in accordance with the standards and specifications in the Pennsylvania Department of Environmental Protection's (PADEP's) "Erosion and Sediment Pollution Control (E&S) Program Manual," Technical Guidance No. 363-2134-008, as amended and updated (E&S Manual) will be implemented to minimize and/or avoid potential adverse environmental impacts due to the construction, operation and maintenance activities associated with the Site. The proposed practices are designed to maximize volume reduction technologies, eliminate or minimize point source discharges to surface waters, preserve the integrity of stream channels, and protect the physical, biological, and chemical qualities of the receiving surface water. The intent is to keep the post construction runoff volume and flow rate no greater than the preconstruction conditions while maintaining water quality. Impervious areas, land clearing and soil compaction are minimized and natural drainage features and vegetation are protected wherever possible. Heavy equipment will be restricted from infiltration areas. E&SC and PCSM BMP measures will be installed and maintained as needed to control stormwater movement in the Site area.

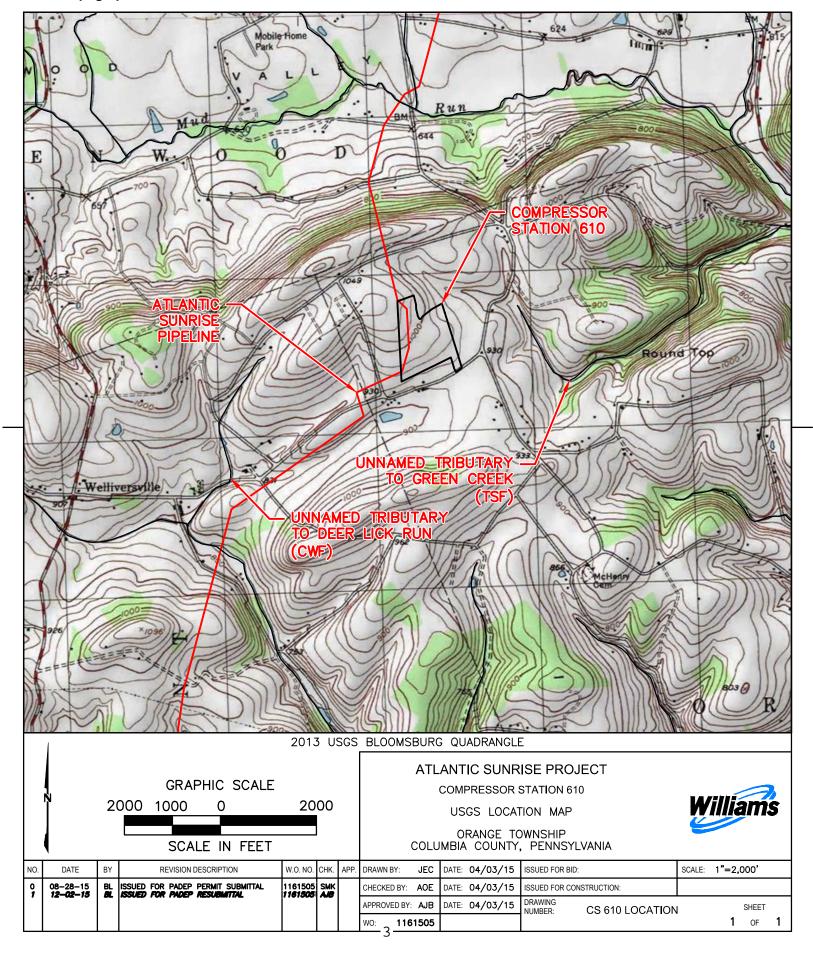
Refer to the ECP (**Section 4 of the ESCGP-2 NOI**) for overall Project information.



There are no impacts to regulated wetlands associated with this proposed Site. Refer to the Wetland Delineation Report provided in **Section 5 of the ESCGP-2 NOI** for information supporting wetland mapping as shown on the Erosion and Sediment Control (E&SC) Plans (**Section 2 of the ESCGP-2 NOI**).



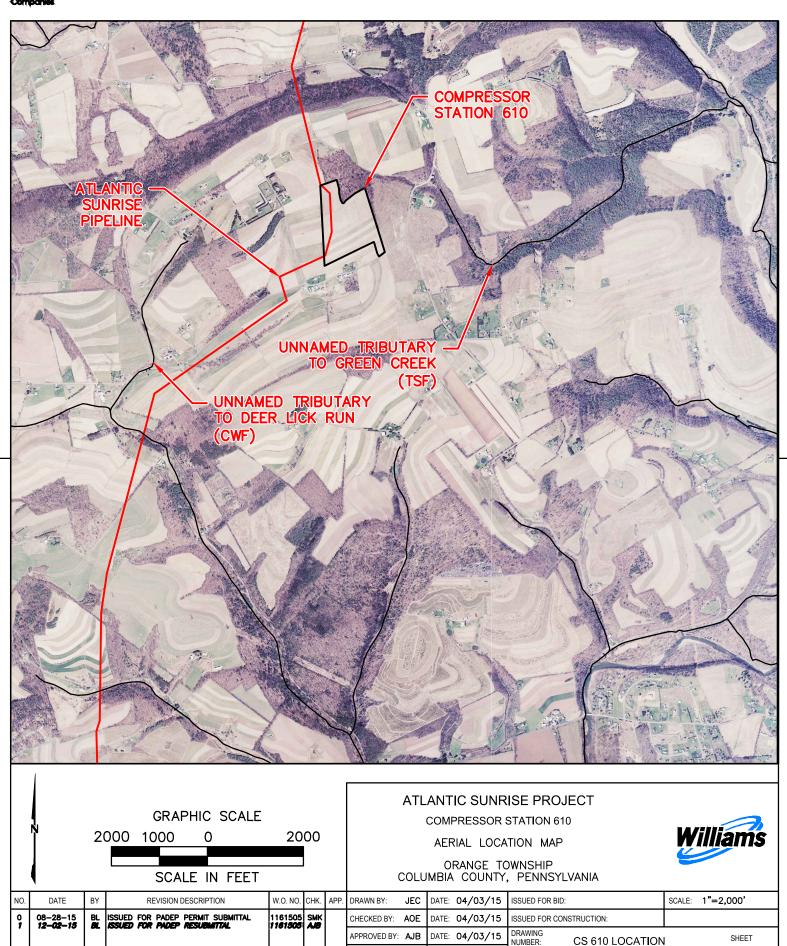
1.1 Topographic Features



CS 610 LOCATION

1 OF 1





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1.2 Soil Characteristics

In addition to the below use limitations and resolutions, refer to Appendix C for the United States Department of Agriculture (USDA) Natural Resources Conservation Service (NRCS) Custom Soil Resource Report for the Site.

Soil Type and Use Limitations

Map Symbol	Soil Name	Slope	Cut Banks Cave	Corrosive to Concrete or Steel	Droughty	Easily Erodible	Flooding	High Water Table	Hydric/Hydric Inclusions	Low Strength	Slow Percolation	Piping	Poor Source of Topsoil	Frost Action	Shrink-Swell	Potential Sinkhole	Ponding	Wetness
AeB2	Allenwood silt loam, moderately eroded	3-12%	Х	C/S					Х	Х	Χ	Х	Х	Х				
HhC3	Hartleton channery silt loam, severely eroded	12-20%	х	С	Х					х	Х	х	х	Х				
HhB2	Hartleton channery silt loam,	3-12%	Х	С	Х					Х	Х	Х	Х	Х				
WbB2	Watson silt loam, , moderately eroded	3-8%	Х	C/S	Х			Х	Х	Х	Х	Х		Х	Х			
WcC2	Weikert channery silt loam, moderately eroded	12-20%	х	C/S	Х				Х	Х	Х	Х	Х	Х				

Source: Appendix E, Table E-1, PADEP, *Erosion and Sediment Pollution Control (E&S) Program Manual* Technical Guidance Number 363-2134-008.



Soil Use Limitations Resolutions

Limitation	Resolution
Cut Banks Cave	Excavations will be properly supported by sheeting and shoring to prevent caves.
Corrosive to Concrete or Steel	No concrete or steel piping is proposed without appropriate coatings and protection.
Droughty	Existing suitable topsoil and soil amendments will be used during construction.
Easily Erodible	Temporary and permanent erosion control BMPs will be employed throughout the Site.
Flooding	Ensure that the Site has proper drainage.
High Water Table	A geotechnical investigation was conducted to minimize conflicts with saturated zones.
Hydric/Hydric Inclusions	A wetland investigation was completed to determine no wetlands are present in the development area.
Low Strength	A maximum of 3:1 slopes are proposed.
Slow Percolation	A field investigation of percolation rates at the infiltration areas was performed to verify the soils percolation capacity.
Piping	Watertight pipe, antiseep collars, clay cores through basin berms, and concrete endwalls will be used to minimize the danger of piping.
Poor Source of Topsoil	Existing topsoil, which has proven to be suitable, will be reused on the Site.
Frost Action	Pavement subbase will be provided to minimize frost effects.
Shrink-Swell	Stone base will be provided to prevent shrink-swell from effecting pavement.
Potential Sinkhole	Geotechnical engineer of record recommendations will be followed for any potential occurrences.
Ponding	Surface grading and drainage facilities will be provided to minimize ponding affects.
Wetness	Wet weather construction recommendations, per the geotechnical engineer's recommendations, will be employed to minimize the effects of wetness during construction, surface grading. Surface grading and drainage will be provided to minimize wetness affects after construction.



1.3 Earth Disturbance Activity Characterization

Proposed Improvements and Land Use

The proposed Compressor Station 610 will be constructed in Orange Township, Columbia County, Pennsylvania. The Project will involve the construction of a natural gas compressor station. The earthmoving activity will involve the stripping and stockpiling of top soil, Site grading, Site excavation, placement of fill, trenching and backfill, construction of buildings and equipment with gravel pad/parking lot, construction of an asphalt access drive, construction of a stormwater management system, finish grading, and stabilization of disturbed surfaces. Approximately 261,861 square feet (6.01 acres) of additional impervious area and 286,603 square feet (6.58 acres) of additional gravel surface will result on-site. Areas outside the Site LOD may be used for staging of equipment and materials, but no earth disturbance will occur in these areas.

Present/Past Land Use

This section identifies the land requirements for construction and operation of the proposed CPL North, CPL South, and Associated Facilities. Table 1.3.1 summarizes the land requirements for the proposed Compressor Station 610 associated with the CPL North and CPL South mainlines.

The characterization of land use within the proposed CPL North, CPL South, and Associated Facilities project areas is based on interpretation of aerial photographs taken in the spring of 2014 and information gathered from field surveys conducted during 2014 and 2015. Transco classified land uses within the proposed CPL North, CPL South, and Associated Facilities project areas into the following eight broad types:

- <u>Agricultural Land</u> land associated with active cultivation of row and field crops; areas of grasses planted for livestock grazing or for the production of hay crops; orchards; and specialty crops, including vineyards, Christmas trees, and fruits and vegetables.
- <u>Upland Forest/Woodland</u> includes upland deciduous forest, evergreen forest, and mixed (deciduous and evergreen) forest, but does not include forested wetlands.
- <u>Industrial/Commercial Land</u> land used for mines or quarries and associated processing plants; manufacturing or other industrial facilities; and land developed for commercial or retail uses, including malls, strip plazas, business parks, and medical facilities.



- <u>Transportation Land</u> land used for transportation purposes, including interstate highways; state, county, and local highways and roads; and railroad lines.
- Residential Land residential areas, including yards of individual residences.
- Open Land non-forested and undeveloped land not classified for another use, including land maintained as utility ROWs for overhead and underground electric transmission, natural gas transmission, and oil transmission facilities.
- Wetlands includes wetlands covered with emergent, scrub-shrub, and forested vegetation.
- Open Water include rivers, streams, creeks, canals, and other linear waterbodies, as well as lakes, ponds, and other non-flowing waterbodies.

New MLVs will be wholly located within the permanent ROWs for the proposed CPL North and CPL South mainlines. Construction will primarily occur within the proposed CPL North and CPL South construction ROWs. Land uses appear to have been similar over the past 50 years.

Table 1.3.1
Land Requirements for the New Aboveground Facilities^a

Facility	Facility Milepost (Agricultural Land (acres)		Upland Forest / Woodland (acres)		Open Land (acres)		Total (acres)	
			Cons	Op	Cons	Op	Cons	Op	Cons	Op
New Compressor Station 610	CPL South 112.5	Columbia	32.8	32.8	0.7	0.7	0.0	0.0	33.5	33.5
Compressor Station 610 Subtotal			32.8	32.8	0.7	0.7	0.0	0.0	33.5	33.5

Notes:

Kev:

Cons = Construction

L = Leidy Line system milepost

Op = Operation

Please refer to the PCSM/SR Plans and Detail Sheets, as provided in **Section 3 of the ESCGP-2 NOI**, and Section 1.2 and Appendix C of this PCSM/SR Narrative for information on the Site soils

Land use acreages for construction and operation are provided for reference only. Acreages provided were calculated by using kmz files and prepared as part of the June 8, 2015 FERC Supplement. Refer to plans and ESCGP-2 NOI for actual site conditions.



1.4 Stormwater Management Calculation Methodology & Net Change in Volume and Rate of Runoff

Runoff volume and rate calculations have been performed for the Site are included in Appendix A.

Pre-development and Post Development runoff hydrographs were developed for the 1-, 2-, 10-, 25-, 50-, and 100-year storm events using the Soil Conservation Service's TR-55 Method. The PCSM/SR BMPs will meet the volume reduction and water quality requirements of Control Guideline 1 (CG 1). Water Quality Worksheet #4 was used to complete the CG 1 volume analysis for the 2-year storm event. Stormwater models were created using the HydroCAD Version 7.10 computer program produced by HydroCAD Software Solutions, LLC. Stormwater conveyance calculations were performed using Worksheet 11 of the Pennsylvania Erosion and Sediment Pollution Control (E&S) Program Manual. (Analysis of rates and flows at each point of interest (POI) were completed to meet CG 1 Requirements.) National Oceanic Atmospheric Administration (NOAA) Atlas 14 rainfall intensities were used in the calculations. See Appendix A for calculations and results.

Drainage Area Summary:

The proposed Compressor Station 610 will be located at a highpoint that drains into two primary drainage areas. The first drainage area is comprised of Drainage Area A and Drainage Area C, with a combined POI located at POI C. The combined drainage area flows to an unnamed tributary to Deer Lick Run. However, Drainage Areas A and C were analyzed separately to demonstrate that there will be no increase in discharge from the site to the roadside swale at the adjacent property line. The second drainage area discharges to POI B and drains to the east to an unnamed tributary of Green Creek. The peak rate discharges for all three drainage areas have been analyzed to demonstrate that there will be no increase in runoff from the site for the 1, 2, 5, 10, 25, 50 and 100 year storm events. A list of the POIs is given below:

POI Summary:

POI A: Roadside swale south of the Site; Combines with POI C.

POI B: Offsite point of convergence of roadside swales east of the Site.

POI C: Roadside swale south of the Site; Combines with POI A.

Overall Site: Susquehanna River Watershed



Volume Summary Table

WATERSHED	2- YR PRE	2- YR POST	2- YR VOLUME INCREASE	2- YR STRUCTURAL AND NONSTRUCTURAL CREDITS	REDUCTION
	(FT³)		(FT³)	(FT³)	(FT³)
UNT. to Deer Lick Run	17711	79745	62034	62156	122
UNT. To Green Creek	12395	8413	-3982	0	3982

^{*}See Appendix A for calculations.

Runoff Rate Summary Table

STORM	POINT OF INTEREST A			POI	NT OF INTE	REST B	POINT OF INTEREST C		
EVENT	PRE	POST	REDUCTION	PRE	POST	REDUCTION	PRE	POST	REDUCTION
	(CFS)	(CFS)	(CFS)	(CFS)	(CFS)	(CFS)	(CFS)	(CFS)	(CFS)
1-yr	0.44	0.40	0.04	2.41	2.28	0.13	0.54	0.44	0.10
2-yr	1.57	1.05	0.52	8.96	8.49	0.47	1.68	1.35	0.33
5-yr	4.46	2.61	1.85	24.74	23.45	1.29	4.59	3.69	0.90
10-yr	8.15	5.51	2.64	44.21	41.91	2.30	8.11	6.51	1.60
25-yr	14.70	11.10	3.60	78.97	74.85	4.12	14.11	11.33	2.78
50-yr	20.90	15.82	5.08	112.40	106.54	5.86	19.79	15.89	3.90
100-yr	28.09	21.13	6.96	151.36	143.47	7.89	26.37	21.17	5.20

^{*}See Appendix A.1 for Pre-Development Calculations with Mapping and Appendix A.2 for Post Development Calculations with Mapping.

Act 167 Summary

The Site is not located within a current, PADEP approved Act 167 Stormwater Management Watershed Plan. Therefore, the Site was designed to meet CG 1 requirements.

1.5 Surface Water Classification

The PCSM/SR drawings in **Section 3 of the ESCGP-2 NOI** depict the locations of the streams and wetlands in and near the LOD for the Site. The Site area surface water runoff drains in two directions. To the east runoff drains to an unnamed tributary (UNT) to Green Creek, which is designated as Trout Stocking (TSF) under PA Code 25



Chapter 93. To the south, runoff drains to an UNT to Deer Lick Run, which is designated as Cold Water Fishery (CWF) under PA Code 25 Chapter 93. Both of these receiving waters are part of the Fishing Creek Watershed. The Site's watersheds are not listed as impaired in the PADEP Chapter 93 Integrated List.

1.6 BMP Description Narrative

The structural PCSM BMPs listed below are to be used for this Site. The calculations used to design the PCSM BMPs are included in Appendix A. The locations of the PCSM BMPs are shown on the PCSM/SR Plans and Detail Sheets (**Section 3 of the ESCGP-2 NOI**).

<u>Vegetated Swales with Earthen Check Dams</u>: Three vegetated swales will be utilized to infiltrate post construction stormwater runoff from the proposed facilities. This BMP is proposed to meet both volume reduction and nitrate removal.

<u>Infiltration Basin</u>: An infiltration basin will be utilized to infiltrate post construction stormwater runoff volume and provide runoff rate control. This BMP is proposed to meet volume reduction requirements.

<u>Infiltration Berms and Retentive Grading</u>: Infiltration berms will be used to increase the surface area available for infiltration as well as increasing the volume infiltrated and providing rate control. This BMP is proposed to meet volume reduction requirements.

<u>Protect Sensitive and Special Value Features</u>: Sensitive and special value features will be protected to reduce stormwater impacts. Construction activities will be conducted in a manner that avoids affecting and encroaching upon areas with important stormwater functions or stormwater impact sensitivities wherever practical so that the valuable functions are preserved. This BMP is proposed to meet non-structural volume credits

Minimize Soil Compaction in Disturbed Areas: Soil compaction within the LOD will be minimized to the extent practicable in order to protect soil quality, preserve permeability and protect the soil from damage where possible. Minimum compaction areas will be surrounded by orange construction fence for the duration of construction activities to ensure minimum compaction. This BMP is proposed to meet volume reduction credits and nitrate removal.

<u>Soil Amendment and Restoration</u>: Soil amendments shall be added to infiltration areas after construction in order to restore soil porosity and enhance long term infiltration. This BMP is proposed to meet non-structural volume reduction credit.

<u>Street Sweeping</u>: Street Sweeping of the site impervious surfaces will be performed on a regular schedule. This BMP is being proposed to meet the nitrate removal credit.



Reduce parking impervious area: Impervious parking areas will be minimized to the maximum extent practicable. Overflow parking will be on gravel areas.

<u>Disconnected Non-Roof Impervious Areas</u>: Non-roof impervious areas will be directed to vegetated areas rather than being directly connected to storm sewers. This BMP is proposed to meet required volume reduction credits

1.7 BMP Installation Sequence Narrative

- 1. At least 7 days prior to starting any earth disturbance activities, including clearing and grubbing, the owner and/or operator shall invite all contractors, Environmental Inspectors, the landowner, appropriate municipal officials, the E&S plan preparer, the PCSM plan preparer, the licensed professional responsible for oversight of critical stages of implementation of the PCSM plan, and a representative from the local conservation district to an on-site preconstruction meeting.
- 2. At least 3 days prior to starting any earth disturbance activities, or expanding into an area previously unmarked, the Pennsylvania One Call System Inc. shall be notified at 1-800-242-1776 for the location of existing underground utilities.
- Install orange construction fence around areas to be protected. These include woodland area at the north east corner of the site, minimum compaction area north of infiltration basin #1 and minimum compaction/soil amendment areas of infiltration basins and berms.
- 4. Locate staging areas and access points including construction entrances. Field locate limits of disturbance.
- 5. Install rock construction entrances (RCEs).
- 6. Remove brush to effectively install perimeter controls, level side cuts to grant access for vehicles and workers to safely perform the installation of sediment barriers on the Site as shown on the construction drawings.
- 7. The Compliance Manager shall provide PADEP and CCD at least three days' notice prior to bulk earth disturbance and upon completed installation of perimeter erosion controls.
- 8. Install compost filter sock 2, 3 and 4. Install swale 1 and immediately seed and stabilize.



- 9. * Install Sediment Basin 1 berm including clay core, outfall structure, aprons, and antiseep collars immediately after installing compost filter sock 3 and 4 and prior to any other disturbance on site.
- 10. Install CFS Sediment Trap 1.
- 11. * Install remainder of Sediment Basin 1 including slope liners, cleanout stake, and associated improvements. Install Filter Sock Diversions 1 and 2 only after basin is completed.
- 12. Install vegetated roadside swales, culverts and riprap outlet protection.
- 13. * Install Earthen Check Dams and drainage channel aprons as soon as swale grading is complete.
- 14. Begin construction staking for grading.
- 15. Begin grading and strip and stockpile topsoil within the area of improvements and install sediment barriers around stockpiles.
- 16. Upon temporary cessation of an earth disturbance activity or any stage of an activity where the cessation of earth disturbance activities will exceed four days, the site shall be immediately seeded, mulched, or otherwise protected from accelerated erosion and sedimentation pending future earth disturbance activities. For an earth disturbance activity or any stage of an activity to be considered temporarily stabilized, the disturbed areas shall be covered with one of the following: A minimum uniform coverage of mulch and seed, with a density capable of resisting accelerated erosion and sedimentation, or an acceptable BMP which temporarily minimizes accelerated erosion and sedimentation. Temporary stabilization will not occur on active vehicular travel ways within the ROW. The onsite Environmental Inspector will log daily activity within the LOD and notify the contractor of areas requiring temporary stabilization (i.e., areas where work has ceased for at least four days).
- Grade the compressor station pads and access roads, including stormwater runoff conveyance features as shown on the E&SC and PCSM/SR Plans (Sections 2 and 3 of the ESCGP-2 NOI).
- 18. Immediately stabilize side slopes with erosion control matting when slopes are 3:1 or greater. See PCSM/SR Plans and Detail Sheets, as provided in **Section 3 of**



the ESCGP-2 NOI, (patterns differ by slope category). Install rip rap slope stabilization where shown on the PCSM/SR Plans.

- 19. Remove FSD 2. Maintain drainage to the sediment basin while placing fill.
- 20. Construct facility including access roads.
- 21. Establish final grade.
- 22. Spread topsoil and construct infiltration berm 2 including amended soil.
- 23. Surface Stabilization, apply permanent stabilization measures immediately to any disturbed areas where work has reached final grade.
- 24. Upon completion of all earthwork activities and permanent stabilization of all disturbed areas, the Owner and/or Operators shall contact the local CCD for an inspection prior to the removal/conversion of the E&SC BMPs.
- 25. * Install Vegetated Swale 3. Remove FSD 1.
- 26. * After all upslope disturbed areas are stabilized, remove accumulated sediments and raise Basin 1 bottom to final grade, convert sediment basin to proposed infiltration management basin 1, including construction of Infiltration Berm 1 and placement of amended soil. Remove temporary skimmer from permanent outlet structure and install watertight plug in orifice. Remove temporary plate over permanent 36"x6" orifice in outlet structure and install top grate.
- 27. All material removed from temporary basins, traps and infiltration berms to be removed from site.
- 28. After finish grading and topsoil placement is completed, disturbed areas shall be fertilized, seeded, and mulched. Seed mixtures, fertilizer and mulch applications rates and dates shall conform to the tables provided on the PCSM/SR Plans and Detail Sheets (Section 3 of the ESCGP-2 NOI), land owner agreements and/or the ECP (Section 4 of the ESCGP-2 NOI).
- 29. After seeding, fertilizing and mulching is complete, install ECBs as required or ordered or on slopes of than 3:1 or greater.



- 30. After the Site is permanently stabilized and upon PADEP or local CCD and Owner approval of stabilization and re-vegetation, remove temporary erosion and sediment control measures and stabilize areas disturbed by removal.
- 31. Complete Site stabilization. Including seed application, ECB and mulching.
- 32. Upon completion of all earth disturbance activities and permanent stabilization of all disturbed areas, the Owner and/or Operators shall contact the local CCD for a final inspection.
- 33. Maintain E&SC BMPs until Site work is complete and uniform 70% perennial vegetative cover is established.
- 34. Remove and properly dispose/recycle E&SC BMPs. Remove orange construction fence. Repair and permanently stabilize areas disturbed during E&SC BMP removal upon establishment of uniform 70% vegetative cover.

1.8 Supporting Calculations

Supporting calculations are included in Appendix A.

1.9 Plan Drawings

PCSM/SR Plans, including sensitive resource mapping, are included in **Section 3 of the ESCGP-2 NOI**.

1.10 Long Term Operation and Maintenance Schedule

Monitoring

Transco's personnel (Operations) will perform visual inspections on an annual basis after permit closure, by qualified personnel, trained and experienced in PCSM/SR, to ascertain that the BMPs are functioning and operating effectively to ensure Compressor Station 610 is causing no undue burden on the property owner or adjacent owners. Repairs of deficiencies will be initiated within ten business days of discovery.

Maintenance

^{*} indicates a critical stage of PCSM installation to be observed by a licensed professional or designee. Contractor to provide three working days' notice to Design Engineer.



The Contractor will be responsible for the maintenance of the system during construction. After construction, the stormwater management facilities will be owned and maintained by Transco.

Where maintenance of the storm system after acceptance by the Owner will primarily consist of routine cleaning of accumulated sediment and debris by facility staff or private contractors, the specific maintenance steps and schedule are listed below:

1. Detention/Infiltration Facility

Inspect detention/infiltration facility annually and inspect soil, repair eroded areas and remove litter and debris as needed. Inspect twice a year for sediment buildup, erosion and vegetative conditions. Remove and replace dead and diseased vegetation. Any litter, debris, sediment, vegetation, or other items removed during maintenance activities will be disposed of in a manner consistent with the ESCGP-2 requirements. *Compaction of the basin bottom shall be prevented.*

2. Vegetated Swales with Earthen Check Dams

Vegetated swales with Earthen Check Dams are to be inspected annually for sediment, build-up, erosion debris, and damage due to traffic. Ditches should be maintained to ensure that the specified design dimensions and vegetative lining are available at all times. No more than one-third of the shoot (grass leaf) shall be removed in any mowing. Grass height shall be maintained between 3 and 6 inches unless otherwise specified. Excess vegetation shall be removed from permanent channels to ensure sufficient channel capacity. Any litter, debris, sediment, vegetation, or other items removed during maintenance activities will be disposed of in a manner consistent with the ESCGP-2 requirements.

3. Infiltration Berms/Retentive Grading

All berms must be kept free of obstructions such as fill, fallen leaves & woody debris, accumulated sediment, and construction material/wastes. Any disturbance to the berms shall be immediately repaired and stabilized. Compaction of the berm bottoms shall be prevented.

4. Protect Sensitive/Special Value Features



Protected areas shall remain undisturbed after construction activities cease. Orange construction fence will be used to protect special value/sensitive areas during construction.

- 5. Minimize Soil Compaction
 - Protected areas restrict vehicle access, do not clear vegetation. Avoid earth disturbance.
 - Minimum disturbance areas Restrict vehicle access.
- 6. Soil Amendment and Restoration

Restrict vehicle access. Monitor water drawdown time in infiltration areas and replace amended soils if dewatering time increases to more than three days. Maintain Infiltration areas and vegetated swales as indicated on the PCSM/SR Plans.

7. Reduce Parking Area Imperviousness

Gravel areas will be maintained in good condition and will not be paved without obtaining prior approval from the PADEP or the County Conservation District.

8. Street Sweeping

Paved areas will be swept as required but at a minimum of annually.

9. Annual Records of Maintenance Procedures

The facility shall maintain a checklist whenever the storm system is inspected and cleaned. An annual list of inspections and major cleaning operations and repairs (pumping, sweeping parking lots, cleaning catch basin, etc.) shall be maintained. The local CCD or enforcement officials shall have access to those records.

10.ESCGP-2

The facility Owner and Operator shall ensure compliance with ESCGP-2 requirements by meeting all ongoing record, keeping maintenance, and other applicable ESCGP-2 and PADEP permit conditions.



1.11 Material Recycling and Disposal

The restoration of the temporary gravel will require the removal of the temporary materials. The temporary materials include, but may not be limited to, stone surface and associated geotextiles. The contractors are required to dispose of materials at suitable disposals or recycling sites and in compliance with local, state and federal regulations.

Transco has prepared a Spill Plan for Oil and Hazardous Materials to assist in prevention of any spills that may occur at the Site and to respond to any spills that do occur. The Contractor will be required to become familiar with the Spill Plan for Oil and Hazardous Materials and its contents prior to commencing any construction-related activities. The Spill Plan for Oil and Hazardous Materials is included as **Attachment 9** to the ECP provided as **Section 4** of the ESCGP-2 NOI.

Contractors are required to inventory and manage their construction site materials. The goal is to be aware of the materials on-site; ensure they are properly maintained, used, and disposed of; and to make sure the materials are not exposed to stormwater.

Silt, sediment, trash, construction wastes and all other wastes generated during operation and maintenance activities shall be properly managed and disposed of in accordance with local, state and federal requirements.

Materials Covered

The following materials or substances are expected to be present on-site during construction (Note: this list is not an all-inclusive list and the Materials Management Practices can be modified to address additional materials used on-site):

- Acids
- Detergents
- Fertilizers (nitrogen/phosphorus)
- Hydroseeding mixtures
- Petroleum based products
- Sanitary wastes
- Soil stabilization additives
- Solder
- Solvents
- Other



These materials must be stored as appropriate and shall not contact storm or nonstormwater discharges. Contractor shall provide a weather proof container to store chemicals or erodible substances that must be kept on the Site. Contractor is responsible for reading, maintaining, and making employees and subcontractors aware of safety data sheets (SDSs).

Material Management Practices

The following are material management practices that will be used to reduce the risk of spills or other accidental exposure of materials and substances to stormwater runoff.

1. Good Housekeeping Practices

The following good housekeeping practices will be followed on Site during construction:

- Store only enough material required to do the job.
- Store materials in a neat, orderly manner.
- Store chemicals in watertight containers or in a storage shed, under a roof, completely enclosed, with appropriate secondary containment to prevent spill or leakage. Drip pans shall be provided under dispensers.
- Substances will not be mixed with one another unless recommended by the Manufacturer.
- Manufacturer's recommendations for proper use and disposal will be followed.
- Inspections will be performed to ensure proper use and disposal of materials.
- Cover and berm loose stockpiled construction materials that are not actively being used (i.e. Soil, spoils, aggregate, etc.).
- Minimize exposure of construction materials to precipitation.
- Minimize the potential for off-site tracking of loose construction and landscape materials.



2. Hazardous Products

These practices will be used to reduce the risks associated with hazardous materials. SDSs for each substance with hazardous properties that is used on the job site(s) will be obtained and used for the proper management of potential wastes that may result from these products. A SDS will be posted in the immediate area where such product is stored and/or used and another copy of each SDS will be maintained in a file at the job site construction trailer office. Each employee, who must handle a substance with hazardous properties, will be instructed on the use of SDS and the specific information in the applicable SDS for the product he/she is using, particularly regarding spill control techniques.

- Products will be kept in original containers with the original labels in legible condition.
- Original labels and SDSs will be produced and used for each material.
- If surplus product must be disposed of, manufacturers or local/state/federal recommended methods for proper disposal will be followed.

3. Hazardous Wastes

All hazardous waste materials will be disposed of by the Contractor in the manner specified by local, state, and/or federal regulations and by the manufacturer of such products. Site personnel will be instructed.

4. Concrete and Other Wash Waters

Prevent disposal of rinse, wash waters, or materials on impervious or pervious surfaces, into streams, wetlands or other water bodies.

Concrete trucks will be allowed to wash out or discharge surplus concrete or drum wash water on the Site, but only in either (1) specifically designated diked areas which have been prepared to prevent contact between the concrete and/or washout and soil and stormwater having the potential to be discharged from the Site; or (2) in locations where waste concrete can be poured into forms to make riprap or other useful concrete products.

The hardened residue from the concrete washout diked areas will be disposed of in the same manner as other non-hazardous construction waste materials or may be broken up and used on the Site as deemed appropriate by the Contractor and



Owner or Owner's representative. The Contractor will be responsible for seeing that these procedures are followed.

All concrete washout areas will be located in an area where the likelihood of the area contributing to stormwater discharge is negligible. If required, additional E&SC BMPs must be implemented to prevent concrete wastes from contributing to stormwater discharges. The location of the concrete washout area(s) must be identified, by the Contractor/Job Site Superintendent, on the job site copy of the E&SC Plans (Section 2 of the ESCGP-2 NOI) and in the E&SC Narrative.

5. Sanitary Wastes

All sanitary waste units will be located in an area where the likelihood of the unit contributing to stormwater discharges is negligible. Additional E&SC BMPs must be implemented, such as containment trays (provided by the rental company) or special containment created with 2" x 4" lumber, impervious plastic, and gravel. The location of the sanitary waste units must be identified on the job site copy of the E&SC Plans (Section 2 of the ESCGP-2 NOI), in the E&SC Narrative, by the Contractor/Job Site Superintendent.

Solid and Construction Wastes

All waste materials will be collected and stored in a securely lidded metal dumpster. The dumpster will comply with all local and state solid waste management regulations. The dumpster/container lids shall be closed at the end of every business day and during rain events. Appropriate measures shall be taken to prevent discharges from waste disposal containers to the receiving water.

7. Construction Access

A stabilized construction exit will be provided to help reduce vehicle tracking of sediments. The paved roads adjacent to the Site entrance will be inspected daily and swept as necessary to remove any excess mud, dirt, or rock tracked from the Site. Dump trucks hauling material from the construction site will be covered with a tarpaulin as necessary.

8. Petroleum Products

On-site vehicles will be monitored for leaks and receive regular preventative maintenance. Petroleum products will be stored in tightly sealed containers which are clearly labeled. Petroleum storage tanks on-site will have a dike or berm containment structure constructed around it to contain spills which may occur



(containment volume to be 110% of volume stored). The dike or bermed area shall be lined with an impervious material such as a heavy duty plastic sheet. Drip pans shall be provided for all dispensers. Any asphalt substances used on the Site will be applied according to the manufacturer's recommendations.

9. Fertilizers and Landscape Materials

Fertilizers will be applied only in the minimum amounts recommended by the manufacturer. Once applied, fertilizer will be worked into the soil to minimize the potential for exposure to stormwater. Storage will be under cover. The contents of any partially used bags of fertilizer will be transferred to a sealable plastic bin to minimize the potential for spills. The bin shall be labeled appropriately.

Contain stockpiled materials, such as but not limited to, mulches, top soil, rocks and gravel, and decomposed granite, when they are not actively being used.

Apply erodible landscape material at quantities and application rates according to the manufacturer's recommendations or based on written specifications by knowledgeable and experienced field personnel. Discontinue the application of any erodible landscape material within two days prior to a forecasted rain event or during periods of precipitation.

10. Paints, Paint Solvents and Cleaning Solvents

Containers will be tightly sealed and stored when not in use. Excess paint and solvents will be properly disposed of according to the manufacturer's recommendations or local, state, and/or federal regulations.

11. Contaminated Soils

Any contaminated soils (resulting from spills of materials with hazardous properties) which may result from construction activities will be contained and cleaned up immediately in accordance with applicable local, state and federal regulations.

1.12 Soil Conditions and Geologic Formations

There are no naturally occurring geologic formations or soils on-site that are expected that may have the potential to cause pollution during earth disturbance activities. See E&SC Detail Sheets (**Section 2 of the ESCGP-2 NOI**) for Acid-Producing Soils and Bedrock Control Plan should any unexpected acid runoff producing soils be encountered.



1.13 Thermal Impacts

Thermal impacts associated with CPL North, CPL South, and Associated Facilities will be avoided to the maximum extent practicable. The following provisions related to thermal impacts are included in the **E&SC Plan** within **Section 2 of the ESCGP-2 NOI**:

- The minimum permanent changes in land cover, necessary to construct the required facilities are being proposed.
- Runoff from the permanent impervious areas will be collected as part of the Post Construction Stormwater Management/Site Restoration (PCSM/SR) Plan and routed to PCSM/SR BMPs. In addition, impervious areas will be gravel instead of asphalt wherever practical.
- PCSM/SR BMPs incorporate the use of infiltration facilities such as basins and vegetated swales with Rock Filter Check Dams.
- The removal of vegetation, especially tree cover, will be limited to only that necessary for construction.
- The amount of impervious surfaces will be limited to only that necessary to support the construction of CPL North, CPL South, and Associated Facilities and/or operation of the pipeline.

1.14 Riparian Forest Buffer Management Plan

There are no regulated riparian buffers within the Site area.

1.15 Antidegradation Requirements

The Site is not located in a special protection or siltation impaired watershed; therefore, no antidegradation analysis is necessary.

1.16 Preparedness Prevention and Contingency Plan

See Attachment 9 of the **ECP** within **Section 4 of the ESCGP-2 NOI** for the Preparedness Prevention and Contingency Plan provided.



APPENDICES

Appendix A Compressor Station 610 Supporting Calculations

A.1 Pre-Development CalculationsA.2 Post Development Calculations

A.3 Conveyance CalculationsA.4 PCSM BMP CalculationsA.5 Water Quality Worksheets

A.6 Site Characterization Assessment

A.7 Supporting Documentation

Appendix B Preparer Qualifications

Appendix C United States Department of Agriculture (USDA) Natural

Resources Conservation Service (NRCS) Custom Soil

Resource Report



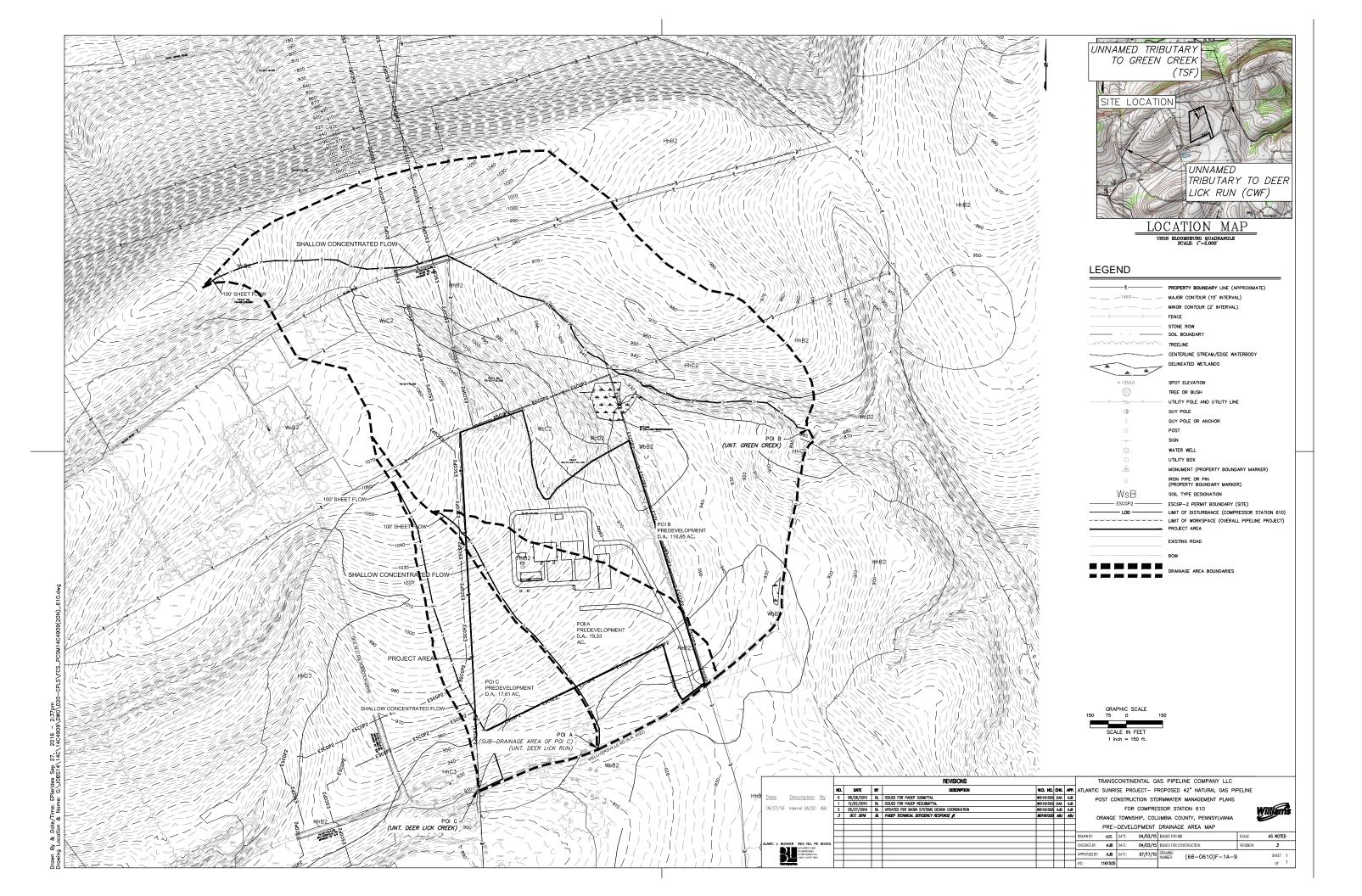
APPENDIX A

Compressor Station 610 Supporting Calculations

- A.1 Pre-Development Calculations
- A.2 Post Development Calculations
- A.3 Conveyance Calculations
- A.4 PCSM BMP Calculations
- A.5 Water Quality Worksheets
- A.6 Site Characterization Assessment
- A.7 Supporting Documentation



A.1 Pre-Development Calculations





Point of Interest A Pre-Development Calculations

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Summary for Subcatchment 1: PREDEVELOPMENT DRAINAGE AREA TO POI A

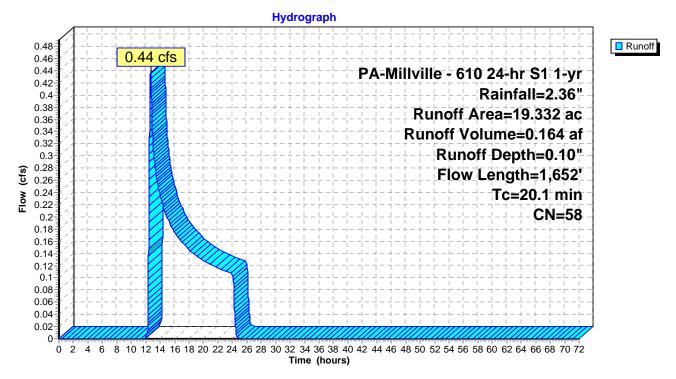
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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs PA-Millville - 610 24-hr S1 1-yr Rainfall=2.36"

Area	(ac) C	N Des	cription				
19.332 58 Meadow, non-grazed, HSG B							
19.	.332	100.	00% Pervi	ous Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
6.4	100	0.0500	0.26		Sheet Flow, SHT 1		
1.1	111	0.0633	1.76		Range n= 0.130 P2= 2.83" Shallow Concentrated Flow, SCF 1 Short Grass Pasture Kv= 7.0 fps		
4.6	561	0.0835	2.02		Shallow Concentrated Flow, SCF 2		
3.2	363	0.0730	1.89		Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, SCF 3 Short Grass Pasture Kv= 7.0 fps		
2.1	230	0.0686	1.83		Shallow Concentrated Flow, SCF 4		
1.5	177	0.0811	1.99		Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, SCF 5 Short Grass Pasture Kv= 7.0 fps		
1.2	110	0.0489	1.55		Shallow Concentrated Flow, SCF 6 Short Grass Pasture Kv= 7.0 fps		
20.1	1,652	Total			·		

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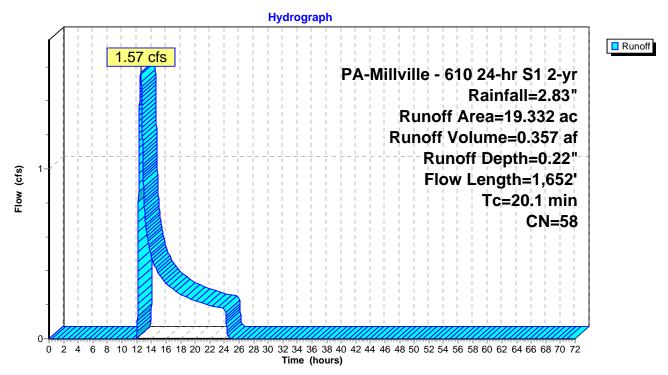
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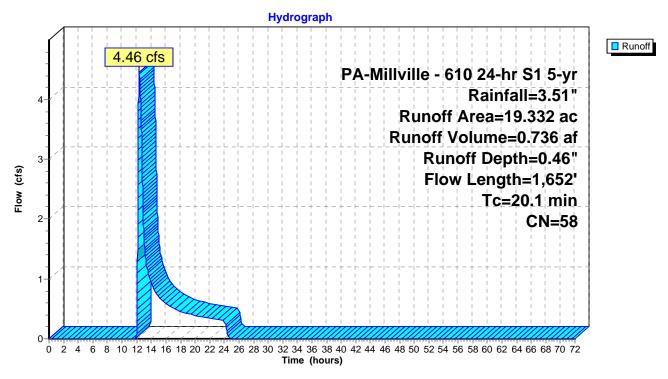
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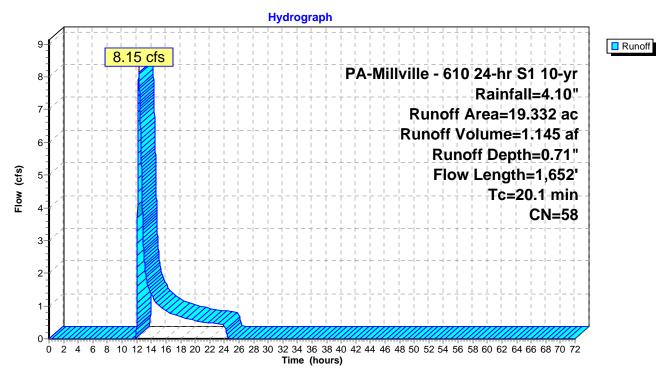
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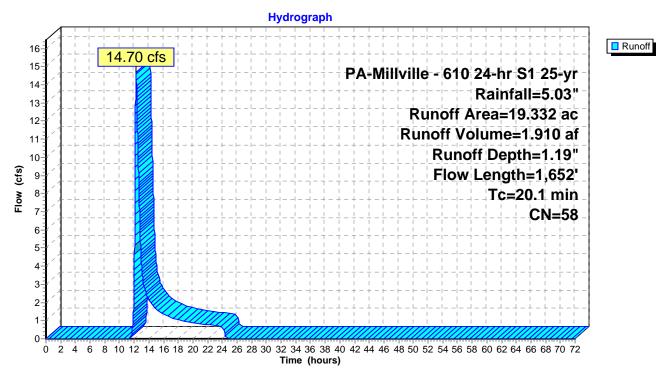
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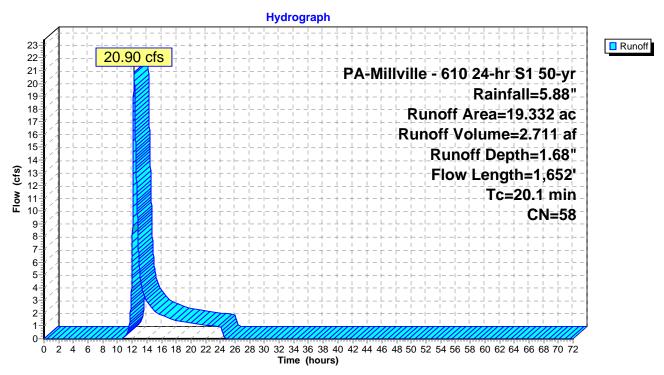
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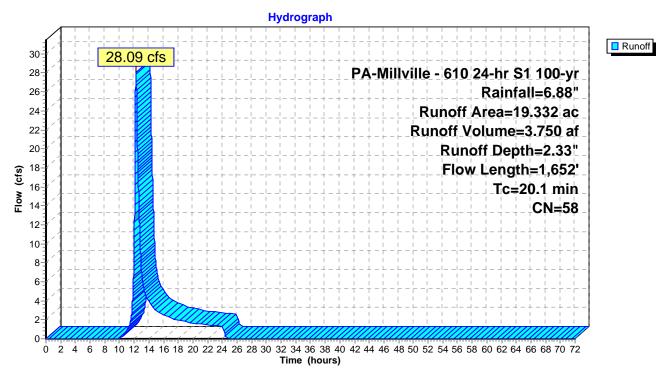
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Point of Interest B Pre-Development Calculations

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Summary for Subcatchment 7: PREDEVELOPMENT DRAINAGE AREA TO POI B

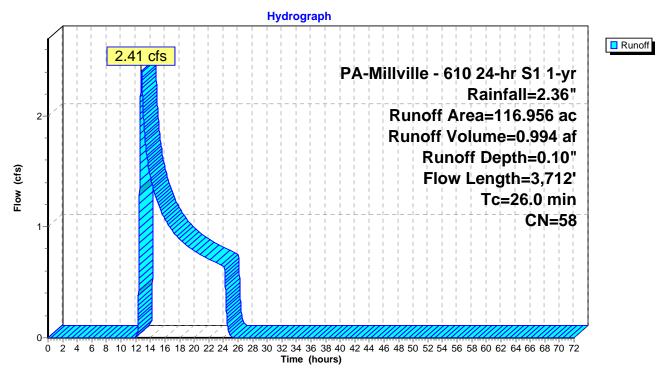
Runoff = 2.41 cfs @ 12.77 hrs, Volume= 0.994 af, Depth= 0.10"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs PA-Millville - 610 24-hr S1 1-yr Rainfall=2.36"

	Area	(ac) C	N Desc	cription		
	1.	818	55 Woo	ds, Good,	HSG B	
	113.	882	58 Mea	dow, non-g	grazed, HS	G B
*	1.	256	98 Impe	ervious, HS	SG D	
116.956 58 Weighted Average						
	115.700 98.93% Pervious Area					
	1.	256	1.07	% Impervi	ous Area	
	Тс	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	5.8	100	0.0650	0.29		Sheet Flow, SHT 1
						Range n= 0.130 P2= 2.83"
	8.2	1,084	0.0990	2.20		Shallow Concentrated Flow, SCF 1
						Short Grass Pasture Kv= 7.0 fps
	1.6	262	0.0340	2.77		Shallow Concentrated Flow, SCF 2
						Grassed Waterway Kv= 15.0 fps
	1.4	487	0.7000	5.86		Shallow Concentrated Flow, SCF 3
						Short Grass Pasture Kv= 7.0 fps
	9.0	1,779	0.0480	3.29		Shallow Concentrated Flow, SCF 4
						Grassed Waterway Kv= 15.0 fps
	26.0	3,712	Total			

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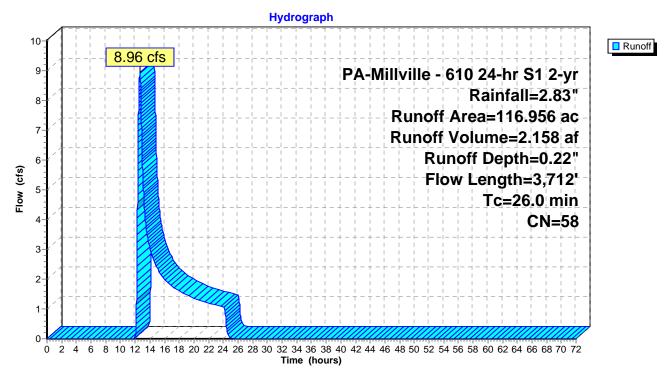
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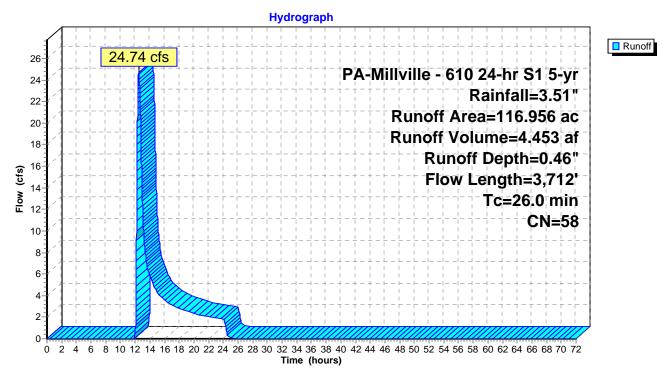
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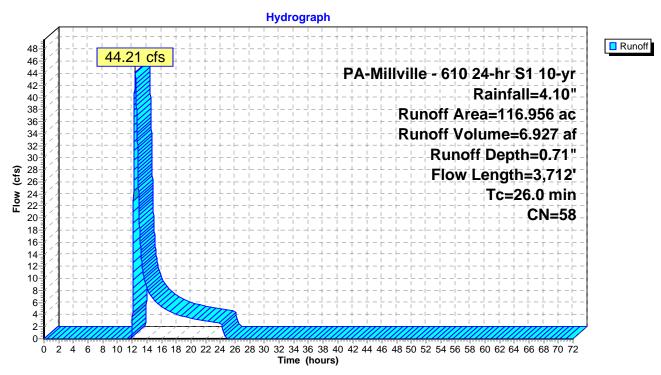
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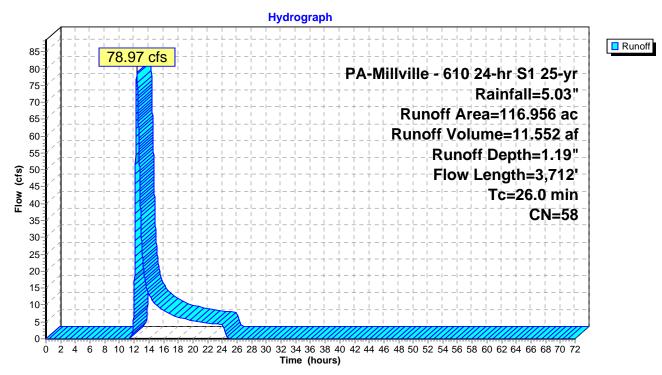
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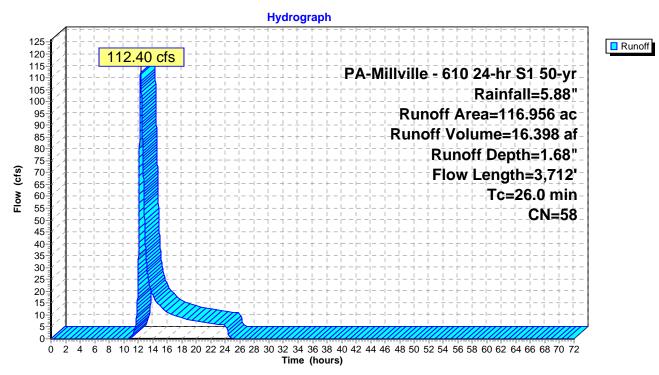
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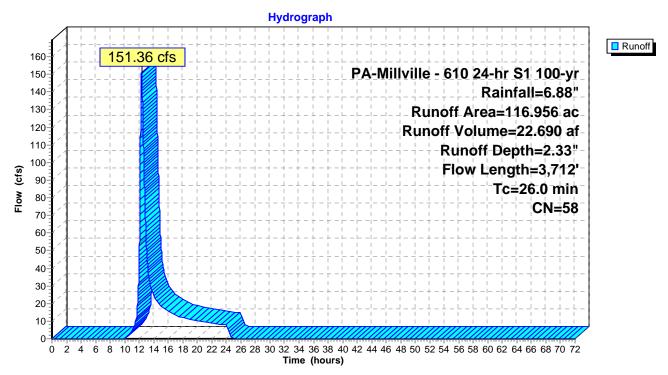
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Point of Interest C Pre-Development Calculations

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Summary for Subcatchment 11S: PREDEVELOPMENT DRAINAGE AREA TO POI C

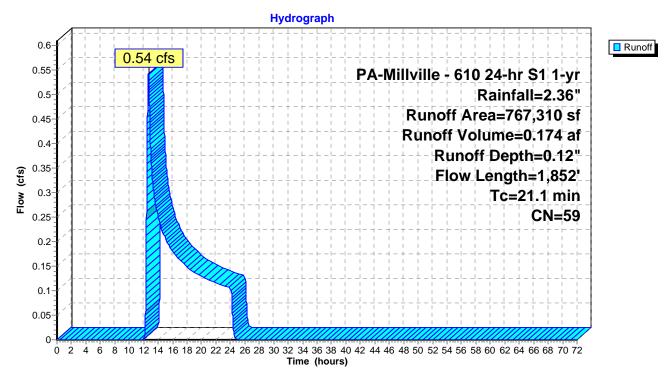
Runoff = 0.54 cfs @ 12.67 hrs, Volume= 0.174 af, Depth= 0.12"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs PA-Millville - 610 24-hr S1 1-yr Rainfall=2.36"

A	rea (sf)	CN D	Description		
7	757,073	58 N	leadow, no	on-grazed,	HSG B
*	10,237	98 lı	mpervious,	HSG B	
7	67,310	59 V	Veighted A	verage	
7	757,073	9	8.67% Per	vious Area	
	10,237	1	.33% Impe	ervious Area	a
_					
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
6.7	100	0.0450	0.25		Sheet Flow, SHT 1
					Range n= 0.130 P2= 2.83"
13.7	1,660	0.0830	2.02		Shallow Concentrated Flow, SCF 1
					Short Grass Pasture Kv= 7.0 fps
0.7	92	0.0200	2.12		Shallow Concentrated Flow, SCF 2
					Grassed Waterway Kv= 15.0 fps
21.1	1,852	Total			

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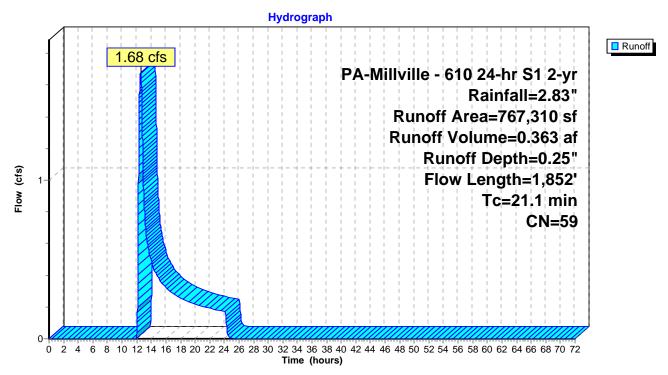
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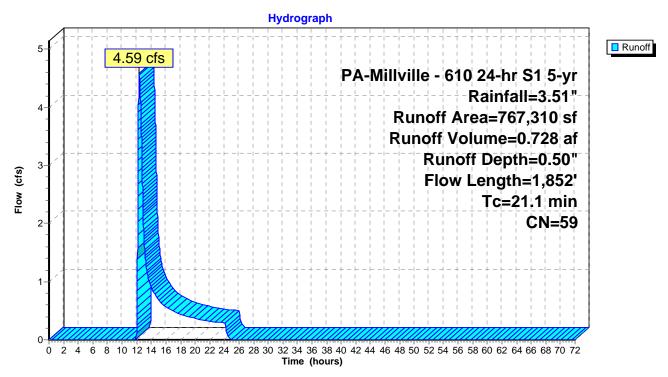
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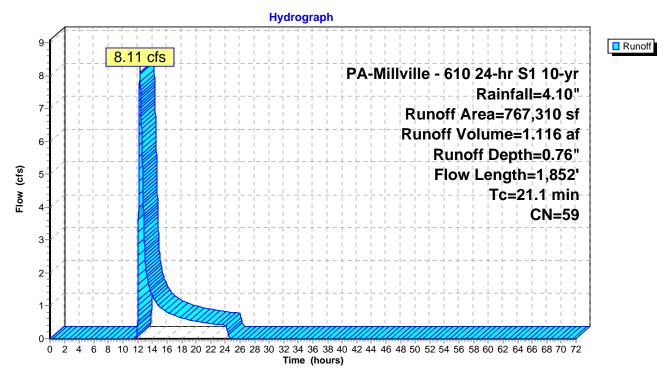


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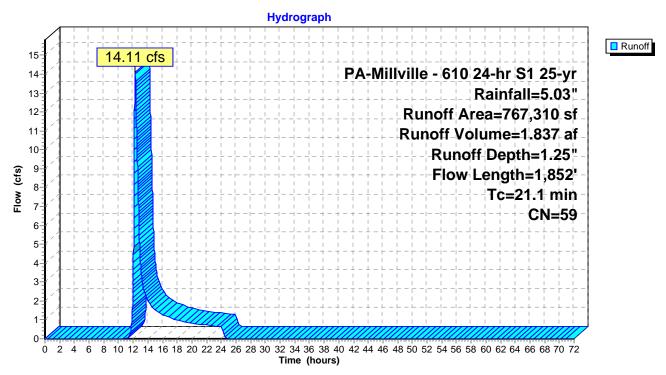


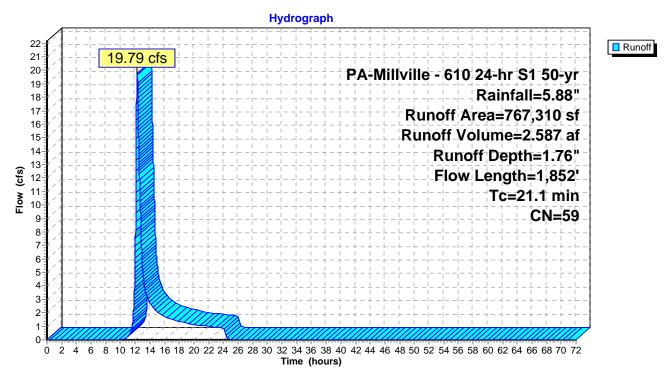
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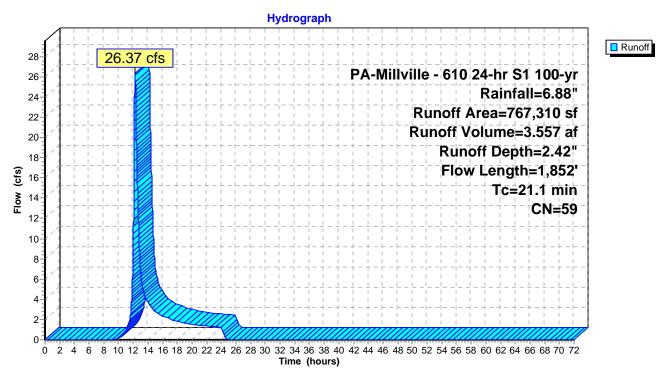
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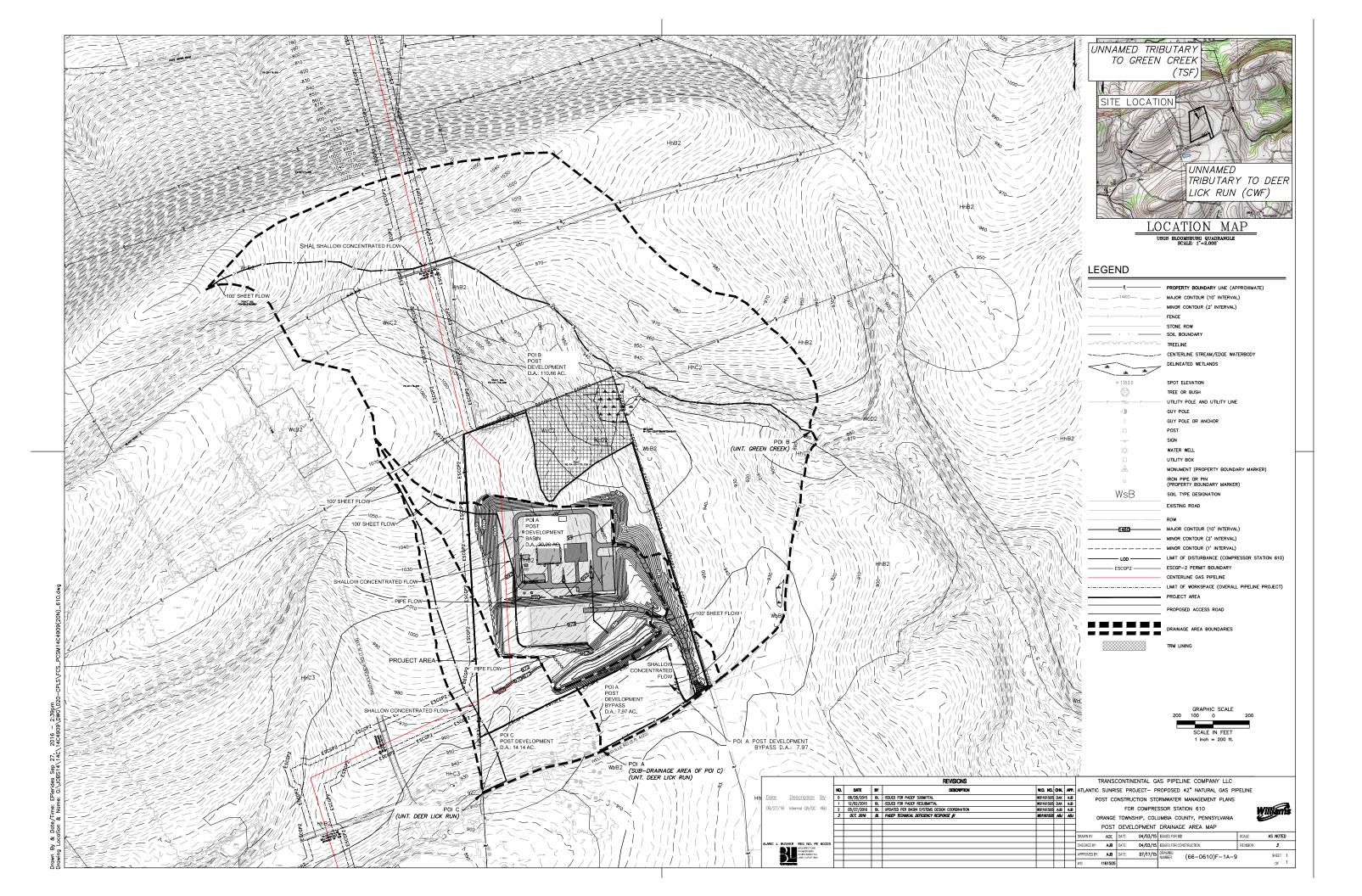


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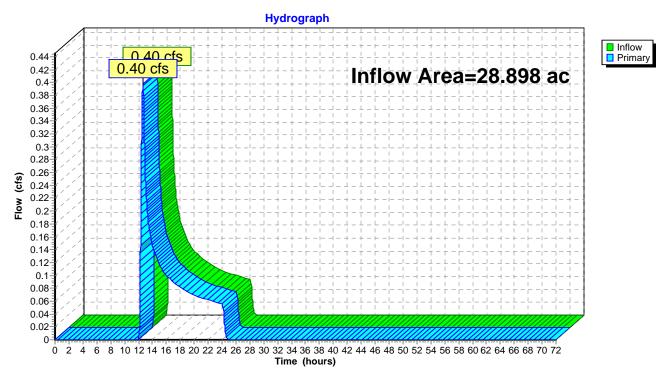
A.2 Post Development Calculations



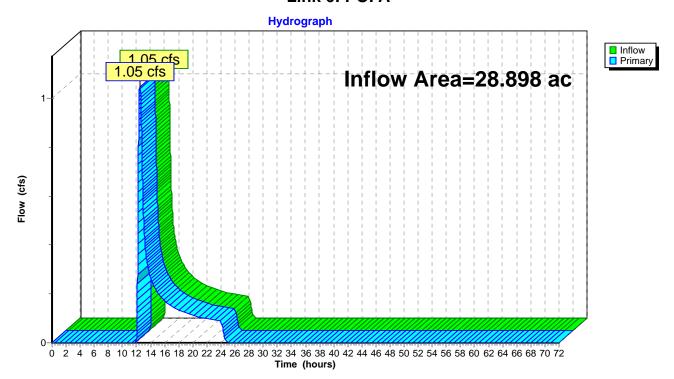


Point of Interest A

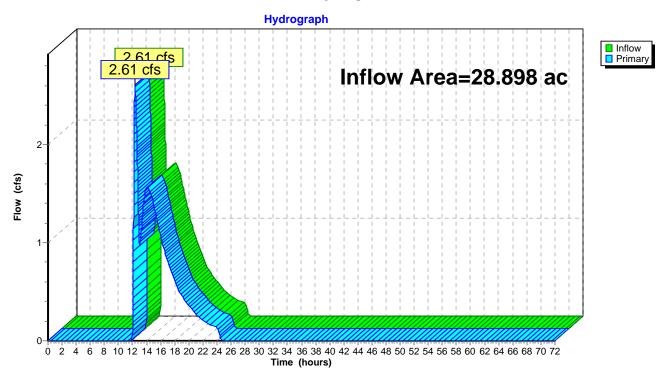
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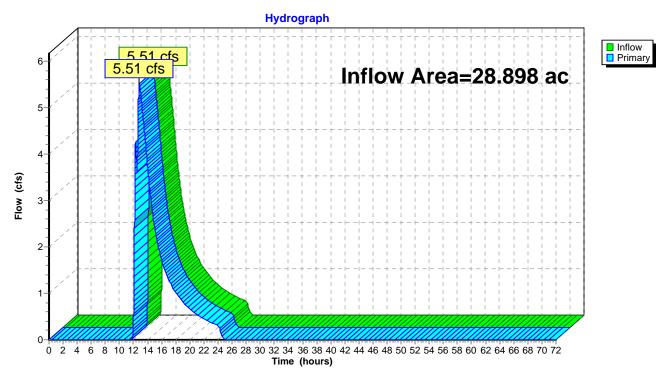
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Link 6: POI A

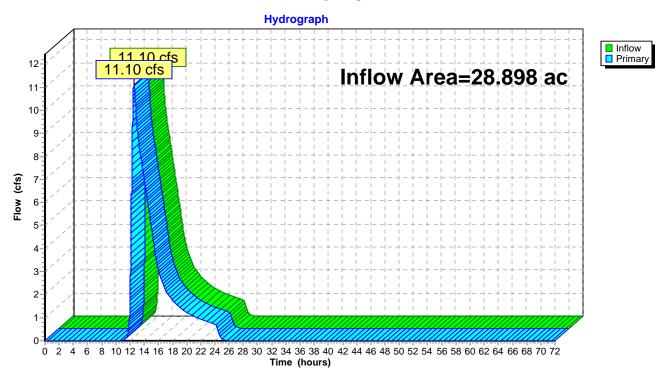


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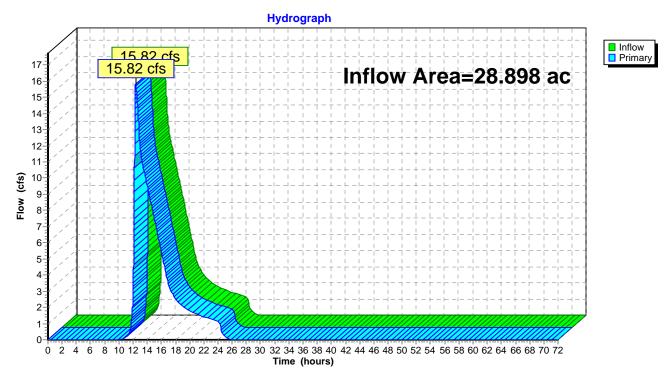
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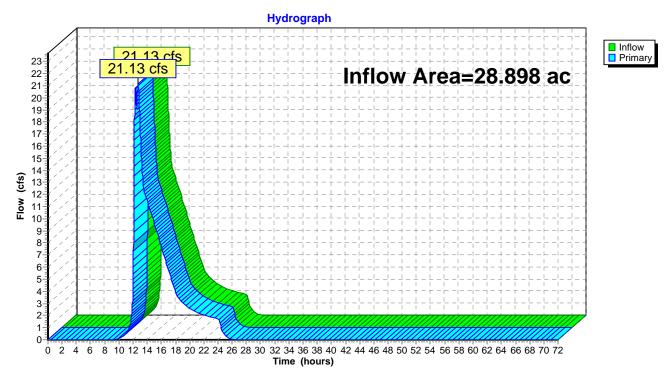
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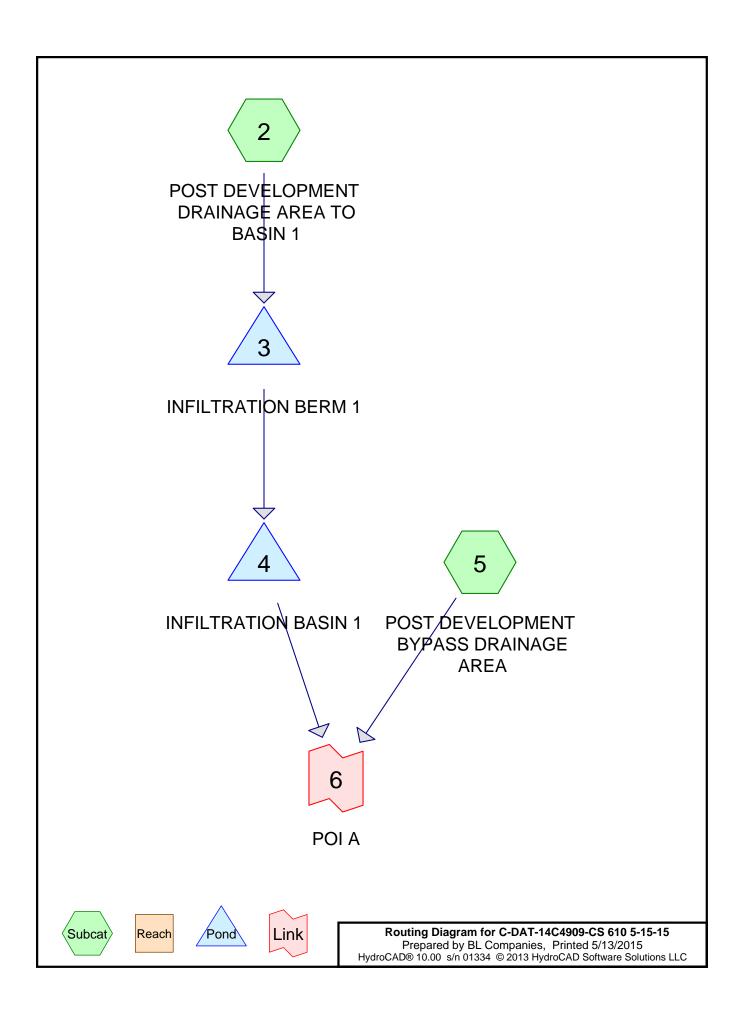
Link 6: POI A



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Link 6: POI A







Point of Interest A Post Development Drainage Area to Basin 1

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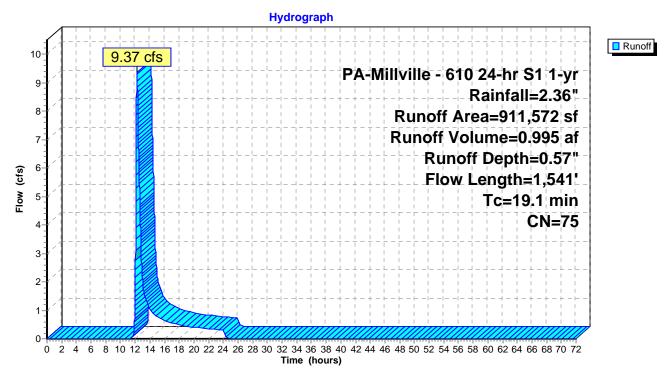
Summary for Subcatchment 2: POST DEVELOPMENT DRAINAGE AREA TO BASIN 1

Runoff = 9.37 cfs @ 12.25 hrs, Volume= 0.995 af, Depth= 0.57"

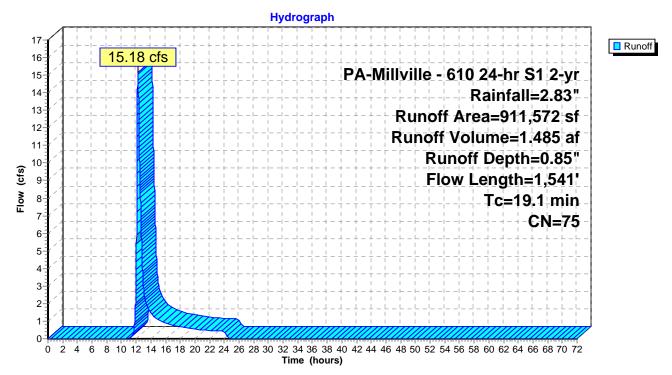
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs PA-Millville - 610 24-hr S1 1-yr Rainfall=2.36"

A	rea (sf)	CN D	escription				
	290,973 61 >75% Grass cover, Good, HSG B						
* 2	86,581		iravel area	,			
1	79,293			ing, HSG B			
1	54,725	58 N	leadow, no	on-grazed,	HSG B		
9	11,572	75 V	/eighted A	verage			
7	32,279	8	0.33% Per	vious Area			
1	79,293	1	9.67% lmp	pervious Are	ea		
Tc	Length	Slope	Velocity	Capacity	Description		
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)			
6.7	100	0.0453	0.25		Sheet Flow, SHT 1		
					Range n= 0.130 P2= 2.83"		
2.3	223	0.0549	1.64		Shallow Concentrated Flow, SHT 1		
					Short Grass Pasture Kv= 7.0 fps		
0.5	111	0.3000	3.83		Shallow Concentrated Flow, SHT 2		
					Short Grass Pasture Kv= 7.0 fps		
2.8	327	0.0150	1.97		Shallow Concentrated Flow, SHT 3		
					Unpaved Kv= 16.1 fps		
0.9	157	0.0300	2.79		Shallow Concentrated Flow, SHT 4		
					Unpaved Kv= 16.1 fps		
0.0	53	0.1480	30.01	94.28	Pipe Channel,		
					24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'		
		0.0400	4.04		n= 0.012		
5.9	570	0.0100	1.61		Shallow Concentrated Flow, SHT 5		
					Unpaved Kv= 16.1 fps		
19.1	1,541	Total					

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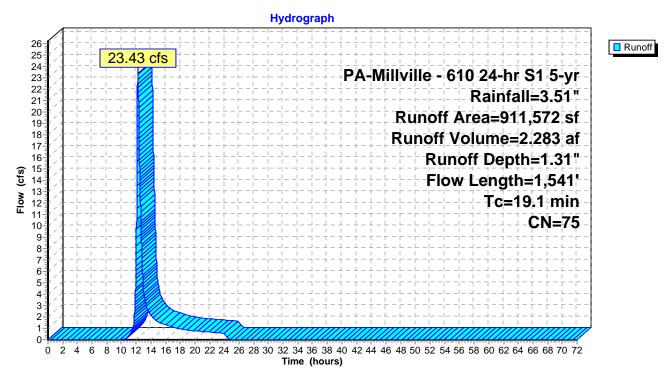


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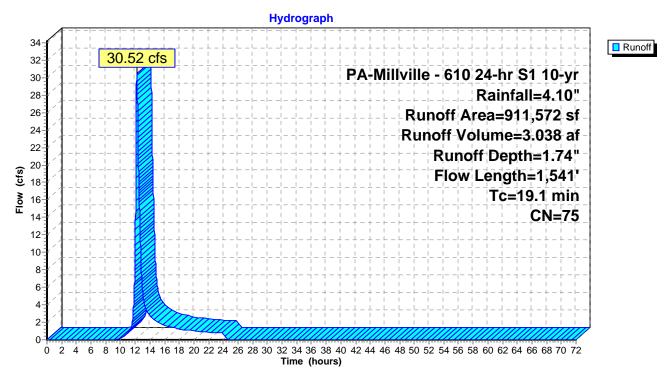
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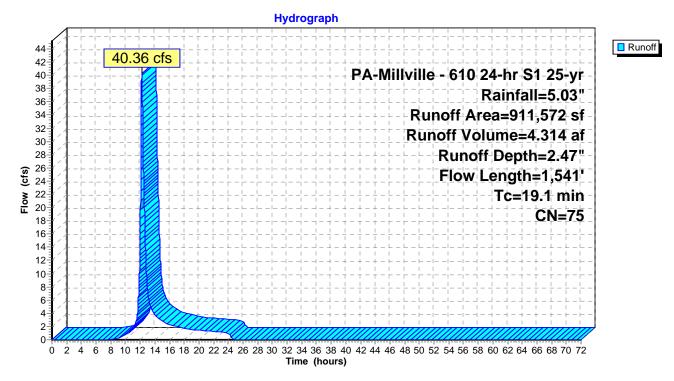


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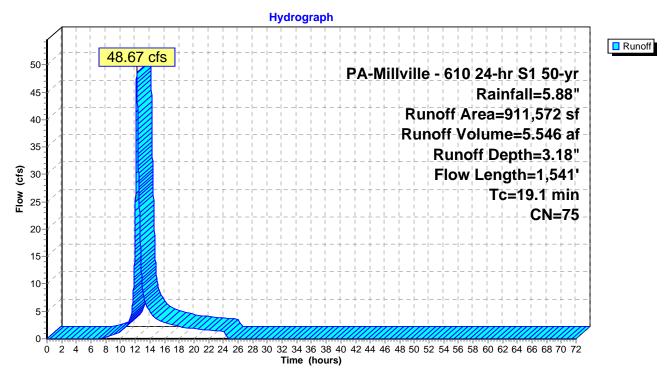


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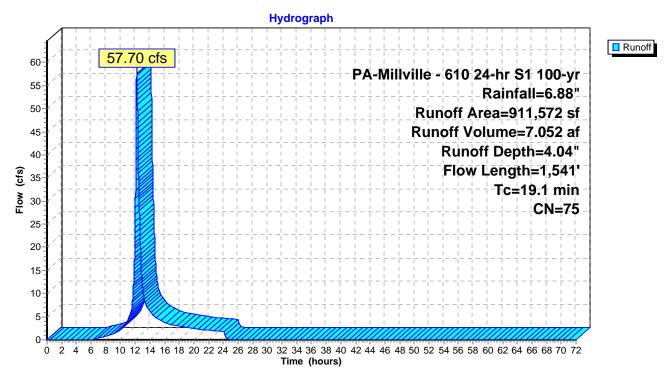
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Point of Interest A Post Development Infiltration Berm 1

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Page 1

Summary for Pond 3: INFILTRATION BERM 1

Inflow Area = 20.927 ac, 19.67% Impervious, Inflow Depth = 0.57" for 1-yr event
Inflow = 9.37 cfs @ 12.25 hrs, Volume= 0.995 af
Outflow = 1.55 cfs @ 13.26 hrs, Volume= 0.995 af, Atten= 83%, Lag= 61.0 min
Discarded = 0.32 cfs @ 13.26 hrs, Volume= 0.779 af
Primary = 1.23 cfs @ 13.26 hrs, Volume= 0.216 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 960.01' @ 13.26 hrs Surf.Area= 17,218 sf Storage= 20,148 cf

Plug-Flow detention time= 642.2 min calculated for 0.995 af (100% of inflow) Center-of-Mass det. time= 642.1 min (1,539.7 - 897.6)

Volume	Invert	Avail.Stor	age Storage	Description	
#1	958.00'	24,76	88 cf Custom	Stage Data (P	rismatic)Listed below (Recalc)
Elevation (fee		ırf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
958.0 960.0 960.2	00	2,915 17,103 20,894	0 20,018 4,750	0 20,018 24,768	
Device	Routing	Invert	Outlet Device	S	
#1	Discarded	958.00'		diltration over	
#2	Primary	960.00'	Head (feet) 0 2.50 3.00 3.5	.20 0.40 0.60 50 a) 2.54 2.61 2.	70ad-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 1.80 2.00 61 2.60 2.66 2.70 2.77 2.89 2.88

Discarded OutFlow Max=0.32 cfs @ 13.26 hrs HW=960.01' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.32 cfs)

Primary OutFlow Max=0.82 cfs @ 13.26 hrs HW=960.01' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 0.82 cfs @ 0.22 fps)

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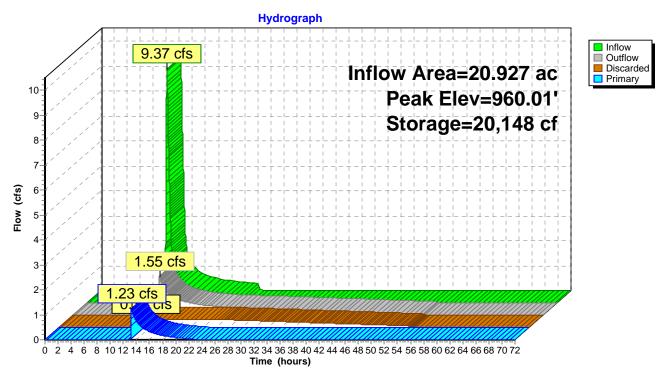
Stage-Discharge for Pond 3: INFILTRATION BERM 1

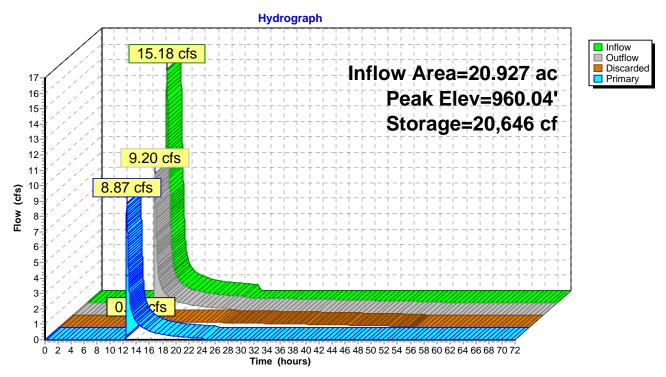
Elevation	Discharge	Discarded	Primary
(feet)	(cfs)	(cfs)	(cfs)
958.00	0.00	0.00	0.00
958.05	0.06	0.06	0.00
958.10	0.07	0.07	0.00
958.15	0.07	0.07	0.00
958.20	0.08	0.08	0.00
958.25	0.09	0.09	0.00
958.30	0.09	0.09	0.00
958.35	0.10	0.10	0.00
958.40	0.11	0.11	0.00
958.45	0.11	0.11	0.00
958.50	0.12	0.12	0.00
958.55	0.13	0.13	0.00
958.60	0.13	0.13	0.00
958.65	0.14	0.14	0.00
958.70	0.15	0.15	0.00
958.75	0.15	0.15	0.00
958.80	0.16	0.16	0.00
958.85	0.17	0.17	0.00
958.90	0.17	0.17	0.00
958.95	0.18	0.18	0.00
959.00	0.19	0.19	0.00
959.05	0.19	0.19	0.00
959.10	0.20	0.20	0.00
959.15	0.21	0.21	0.00
959.20	0.21	0.21	0.00
959.25	0.22	0.22	0.00
959.30	0.23	0.23	0.00
959.35	0.23	0.23	0.00
959.40	0.24	0.24	0.00
959.45	0.25	0.25	0.00
959.50	0.25	0.25	0.00
959.55	0.26 0.27	0.26 0.27	0.00 0.00
959.60 959.65		0.27	0.00
959.03	0.27 0.28	0.27	0.00
959.75	0.28	0.28	0.00
959.80	0.29	0.29	0.00
959.85	0.29	0.29	0.00
959.90	0.30	0.30	0.00
959.95	0.31	0.31	0.00
960.00	0.31	0.32	0.00
960.05	14.25	0.33	13.92
960.10	39.71	0.35	39.36
960.15	72.67	0.36	72.30
960.20	111.70	0.38	111.32
960.25	157.04	0.39	156.65
550.20	.51104	0.00	. 55.55

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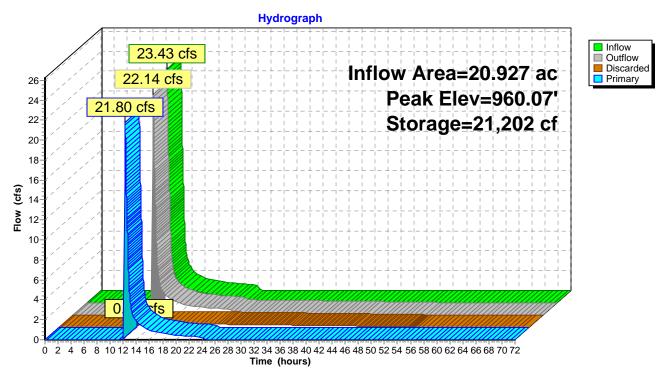
Stage-Area-Storage for Pond 3: INFILTRATION BERM 1

Elevation	Surface	Storage
(feet)	(sq-ft)	(cubic-feet)
958.00	2,915	0
958.05	3,270	155
958.10 958.15	3,624 3,979	327 517
958.20	4,334	725
958.25	4,689	950
958.30	5,043	1,194
958.35	5,398	1,455
958.40	5,753	1,734
958.45	6,107	2,030
958.50	6,462	2,344
958.55 958.60	6,817 7,171	2,676 3,026
958.65	7,526	3,393
958.70	7,881	3,779
958.75	8,236	4,181
958.80	8,590	4,602
958.85	8,945	5,040
958.90	9,300	5,497
958.95 959.00	9,654 10,009	5,970 6,462
959.05	10,364	6,971
959.10	10,718	7,498
959.15	11,073	8,043
959.20	11,428	8,606
959.25	11,783	9,186
959.30	12,137	9,784
959.35 959.40	12,492 12,847	10,400 11,033
959.45	13,201	11,684
959.50	13,556	12,353
959.55	13,911	13,040
959.60	14,265	13,744
959.65	14,620	14,466
959.70	14,975	15,206
959.75 959.80	15,330 15,684	15,964 16,739
959.85	16,039	17,532
959.90	16,394	18,343
959.95	16,748	19,172
960.00	17,103	20,018
960.05	17,861	20,892
960.10	18,619	21,804
960.15 960.20	19,378 20,136	22,754 23,742
960.25	20,130 20,894	24,768
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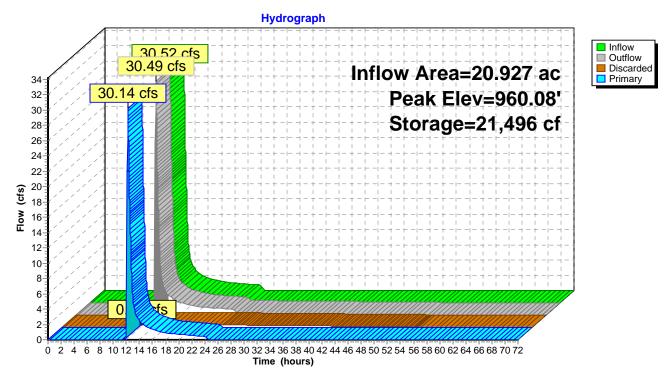




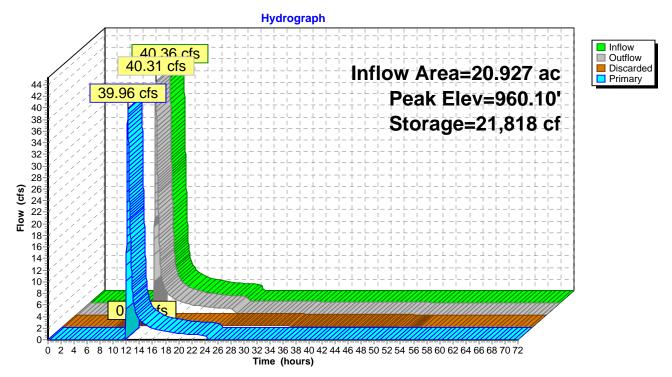
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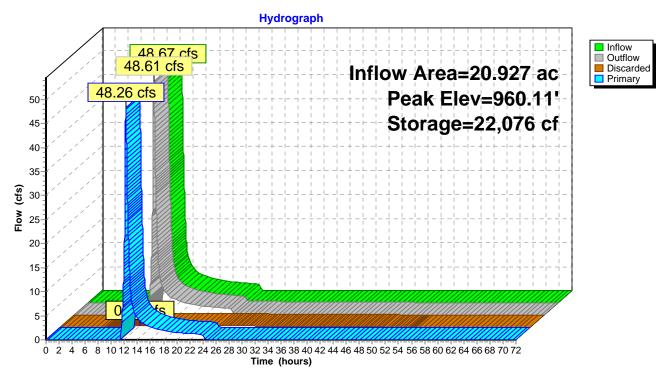
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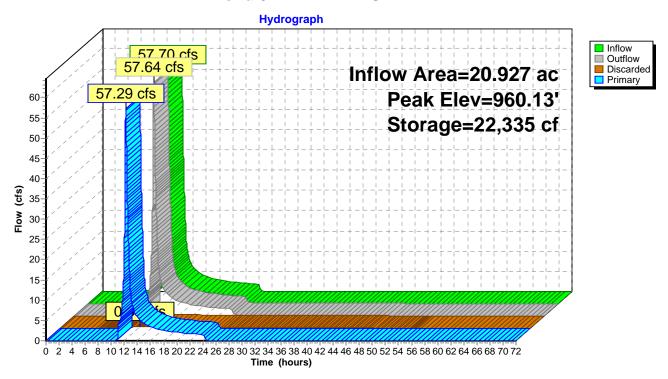


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Point of Interest A Post Development Infiltration Basin 1

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Page 1

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Summary for Pond 4: INFILTRATION BASIN 1

Inflow Area = 20.927 ac, 19.67% Impervious, Inflow Depth = 0.12" for 1-yr event

Inflow 1.23 cfs @ 13.26 hrs. Volume= 0.216 af

0.21 cfs @ 17.30 hrs, Volume= Outflow 0.216 af, Atten= 83%, Lag= 242.3 min

0.21 cfs @ 17.30 hrs, Volume= Discarded = 0.216 af 0.00 cfs @ 0.00 hrs, Volume= Primary = 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 954.51' @ 17.30 hrs Surf.Area= 11,215 sf Storage= 4,747 cf

Plug-Flow detention time= 269.3 min calculated for 0.216 af (100% of inflow)

Center-of-Mass det. time= 269.4 min (1,200.5 - 931.2)

Volume	Invert	Avail.Storage	Storage Description
#1	954.00'	168,903 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
954.00	7,235	0	0
956.00	22,706	29,941	29,941
958.00	36,022	58,728	88,669
960.00	44,212	80,234	168,903

Device	Routing	Invert	Outlet Devices
#1	Primary	953.00'	24.0" Round Culvert
			L= 40.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 953.00' / 951.00' S= 0.0500 '/' Cc= 0.900
			n= 0.012, Flow Area= 3.14 sf
#2	Discarded	954.00'	0.810 in/hr Exfiltration over Surface area
#3	Device 1	956.00'	36.0" W x 6.0" H Vert. Orifice/Grate C= 0.600
#4	Device 1	958.25'	24.0" x 48.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#5	Primary	958.75'	15.0' long x 18.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Discarded OutFlow Max=0.21 cfs @ 17.30 hrs HW=954.51' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.21 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=954.00' (Free Discharge)

-1=Culvert (Passes 0.00 cfs of 5.35 cfs potential flow)

-3=Orifice/Grate (Controls 0.00 cfs) 4=Orifice/Grate (Controls 0.00 cfs)

-5=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Page 2

Stage-Discharge for Pond 4: INFILTRATION BASIN 1

Elevation Discharge Discarded Primary (feet) Cirls								
954.00 0.00 0.00 0.00 959.30 52.12 0.78 51.34 954.10 0.15 0.15 0.00 959.50 62.13 0.79 61.34 954.30 0.18 0.18 0.00 959.50 62.13 0.79 61.34 954.40 0.19 0.19 0.00 959.50 67.60 0.80 66.80 954.50 0.21 0.21 0.21 0.00 959.70 73.48 0.81 72.68 954.60 0.22 0.22 0.00 959.80 79.73 0.81 78.92 954.60 0.22 0.22 0.00 959.80 79.73 0.81 78.92 954.60 0.22 0.22 0.00 959.90 86.35 0.82 85.53 954.70 0.24 0.24 0.00 959.90 86.35 0.82 85.53 0.955.00 0.25 0.00 955.00 0.27 0.27 0.00 955.00 0.28 0.28 0.00 955.10 0.30 0.30 0.00 955.50 0.32 0.32 0.00 955.50 0.32 0.32 0.00 955.50 0.34 0.34 0.34 0.00 955.50 0.34 0.34 0.34 0.00 955.50 0.37 0.37 0.00 955.60 0.40 0.40 0.00 955.80 0.40 0.40 0.00 955.80 0.40 0.41 0.41 0.00 956.00 0.43 0.43 0.34 0.00 955.80 0.40 0.44 0.30 956.10 0.74 0.44 0.30 956.10 0.74 0.44 0.30 956.60 0.43 0.35 0.48 2.44 956.50 3.89 0.49 3.40 956.60 4.67 0.50 4.17 956.70 5.29 0.51 4.78 956.70 5.29 0.51 4.78 956.70 5.29 0.51 4.78 956.70 5.29 0.51 4.78 956.70 5.29 0.51 4.78 956.70 5.29 0.51 4.78 956.70 5.29 0.51 4.78 956.70 7.97 0.59 7.38 957.00 6.78 0.55 6.23 957.10 7.20 0.56 6.63 957.20 7.59 0.58 7.02 957.30 7.97 0.59 7.38 957.50 8.67 0.61 8.06 9.57 9957.00 8.67 0.61 8.06 957.50 9.01 0.62 8.98 957.90 9.93 0.66 9.27 958.00 10.22 0.68 9.55 958.10 10.50 0.68 9.82 957.90 9.93 0.66 9.27 958.00 10.22 0.68 9.55 988.20 10.77 0.69 10.08 9.82 958.80 10.25 0.68 9.82 958.20 10.77 0.69 10.08 9.82 958.80 10.25 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.68 9.82 958.80 10.20 0.20 0.68 9.82 958.80 10.20 0.20 0.68 9.82 958								
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957.20 7.59 0.58 7.02 957.30 7.97 0.59 7.38 957.40 8.33 0.60 7.73 957.50 8.67 0.61 8.06 957.60 9.01 0.63 8.38 957.70 9.32 0.64 8.69 957.80 9.63 0.65 8.98 957.90 9.93 0.66 9.27 958.00 10.22 0.68 9.55 958.10 10.50 0.68 9.82 958.20 10.77 0.69 10.08 958.30 11.47 0.70 10.77 958.40 13.57 0.71 12.86 958.50 16.45 0.71 15.73 958.60 19.91 0.72 19.19	957.00	6.78	0.55	6.23				
957.30 7.97 0.59 7.38 957.40 8.33 0.60 7.73 957.50 8.67 0.61 8.06 957.60 9.01 0.63 8.38 957.70 9.32 0.64 8.69 957.80 9.63 0.65 8.98 957.90 9.93 0.66 9.27 958.00 10.22 0.68 9.55 958.10 10.50 0.68 9.82 958.20 10.77 0.69 10.08 958.30 11.47 0.70 10.77 958.40 13.57 0.71 12.86 958.50 16.45 0.71 15.73 958.60 19.91 0.72 19.19	957.10	7.20	0.56	6.63				
957.40 8.33 0.60 7.73 957.50 8.67 0.61 8.06 957.60 9.01 0.63 8.38 957.70 9.32 0.64 8.69 957.80 9.63 0.65 8.98 957.90 9.93 0.66 9.27 958.00 10.22 0.68 9.55 958.10 10.50 0.68 9.82 958.20 10.77 0.69 10.08 958.30 11.47 0.70 10.77 958.40 13.57 0.71 12.86 958.50 16.45 0.71 15.73 958.60 19.91 0.72 19.19	957.20							
957.50 8.67 0.61 8.06 957.60 9.01 0.63 8.38 957.70 9.32 0.64 8.69 957.80 9.63 0.65 8.98 957.90 9.93 0.66 9.27 958.00 10.22 0.68 9.55 958.10 10.50 0.68 9.82 958.20 10.77 0.69 10.08 958.30 11.47 0.70 10.77 958.40 13.57 0.71 12.86 958.50 16.45 0.71 15.73 958.60 19.91 0.72 19.19	957.30							
957.60 9.01 0.63 8.38 957.70 9.32 0.64 8.69 957.80 9.63 0.65 8.98 957.90 9.93 0.66 9.27 958.00 10.22 0.68 9.55 958.10 10.50 0.68 9.82 958.20 10.77 0.69 10.08 958.30 11.47 0.70 10.77 958.40 13.57 0.71 12.86 958.50 16.45 0.71 15.73 958.60 19.91 0.72 19.19								
957.70 9.32 0.64 8.69 957.80 9.63 0.65 8.98 957.90 9.93 0.66 9.27 958.00 10.22 0.68 9.55 958.10 10.50 0.68 9.82 958.20 10.77 0.69 10.08 958.30 11.47 0.70 10.77 958.40 13.57 0.71 12.86 958.50 16.45 0.71 15.73 958.60 19.91 0.72 19.19								
957.80 9.63 0.65 8.98 957.90 9.93 0.66 9.27 958.00 10.22 0.68 9.55 958.10 10.50 0.68 9.82 958.20 10.77 0.69 10.08 958.30 11.47 0.70 10.77 958.40 13.57 0.71 12.86 958.50 16.45 0.71 15.73 958.60 19.91 0.72 19.19								
957.90 9.93 0.66 9.27 958.00 10.22 0.68 9.55 958.10 10.50 0.68 9.82 958.20 10.77 0.69 10.08 958.30 11.47 0.70 10.77 958.40 13.57 0.71 12.86 958.50 16.45 0.71 15.73 958.60 19.91 0.72 19.19								
958.00 10.22 0.68 9.55 958.10 10.50 0.68 9.82 958.20 10.77 0.69 10.08 958.30 11.47 0.70 10.77 958.40 13.57 0.71 12.86 958.50 16.45 0.71 15.73 958.60 19.91 0.72 19.19								
958.10 10.50 0.68 9.82 958.20 10.77 0.69 10.08 958.30 11.47 0.70 10.77 958.40 13.57 0.71 12.86 958.50 16.45 0.71 15.73 958.60 19.91 0.72 19.19								
958.20 10.77 0.69 10.08 958.30 11.47 0.70 10.77 958.40 13.57 0.71 12.86 958.50 16.45 0.71 15.73 958.60 19.91 0.72 19.19								
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958.50								
958.60 19.91 0.72 19.19								
95870 2387 073 235 E	958.70	23.87	0.72	23.15				
958.80 28.72 0.74 27.98								
958.90 35.40 0.74 34.65								
959.00 39.61 0.75 38.86								
959.10 43.29 0.76 42.53								
959.20 47.49 0.77 46.72								

Storage (cubic-feet)

138,958

143,113

147,309

151,546

155,824

160,142

164,502

168,903

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Stage-Area-Storage for Pond 4: INFILTRATION BASIN 1

Surface

(sq-ft)

41,345

41,755

42,165

42,574

42,984

43,393

43,802

44,212

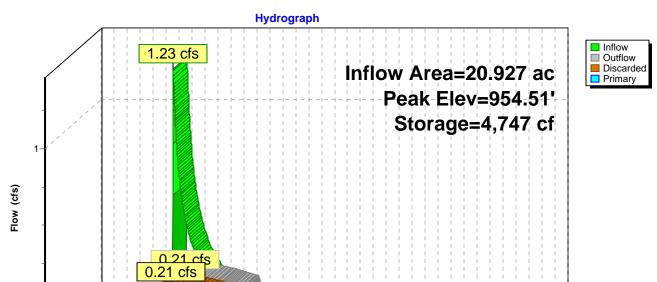
Elevation	Surface	Storage	Elevation
(feet)	(sq-ft)	(cubic-feet)	(feet)
954.00	7,235	0	959.30
954.10	8,009	762	959.40
954.20	8,782	1,602	959.50
954.30	9,556	2,519	959.60
954.40	10,329	3,513	959.70
954.50	11,103	4,584	959.80
954.60	11,876	5,733	959.90
954.70	12,650	6,960	960.00
954.80	13,423	8,263	
954.90 955.00	14,197	9,644	
955.00 955.10	14,971 15,744	11,103 12,638	
955.20	16,518	14,252	
955.30	17,291	15,942	
955.40	18,065	17,710	
955.50	18,838	19,555	
955.60	19,612	21,477	
955.70	20,385	23,477	
955.80	21,159	25,555	
955.90	21,932	27,709	
956.00	22,706	29,941	
956.10	23,372	32,245	
956.20	24,038	34,615	
956.30	24,703	37,052	
956.40	25,369	39,556	
956.50	26,035	42,126	
956.60	26,701	44,763	
956.70	27,367	47,466	
956.80	28,032	50,236	
956.90	28,698	53,073	
957.00	29,364	55,976	
957.10	30,030	58,946	
957.20	30,696	61,982	
957.30 057.40	31,361 32,027	65,085 68,254	
957.40 957.50	32,693	71,490	
957.60	33,359	74,793	
957.70	34,025	78,162	
957.80	34,690	81,598	
957.90	35,356	85,100	
958.00	36,022	88,669	
958.10	36,432	92,292	
958.20	36,841	95,955	
958.30	37,250	99,660	
958.40	37,660	103,405	
958.50	38,070	107,192	
958.60	38,479	111,019	
958.70	38,889	114,888	
958.80	39,298	118,797	
958.90	39,707	122,747	
959.00	40,117	126,739	
959.10	40,527	130,771	
959.20	40,936	134,844	

0.00 cfs

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Page 1

Pond 4: INFILTRATION BASIN 1



0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72

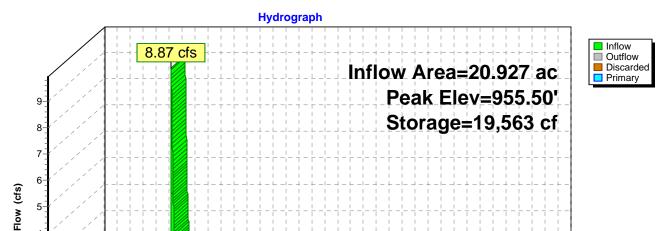
0.35 cfs 0.35 cfs

0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 Time (hours)

0.00 cfs

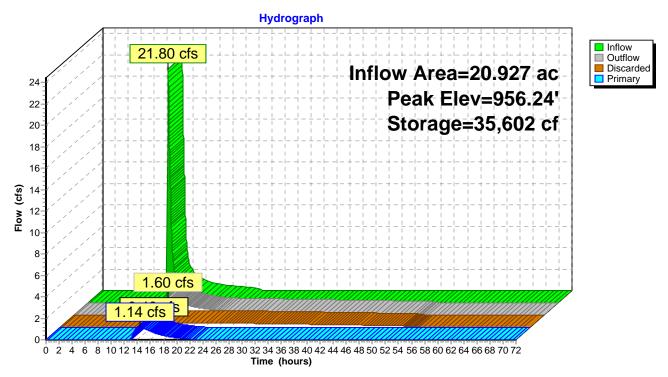
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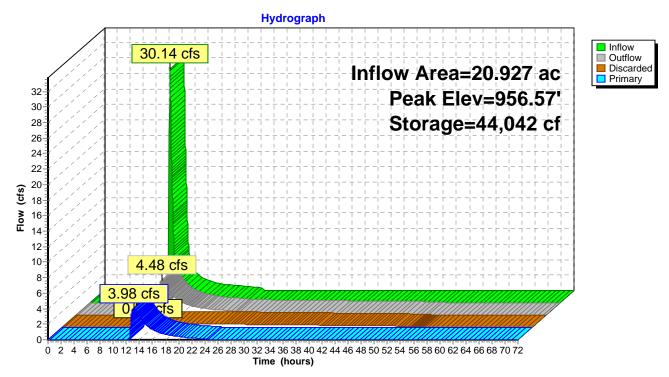


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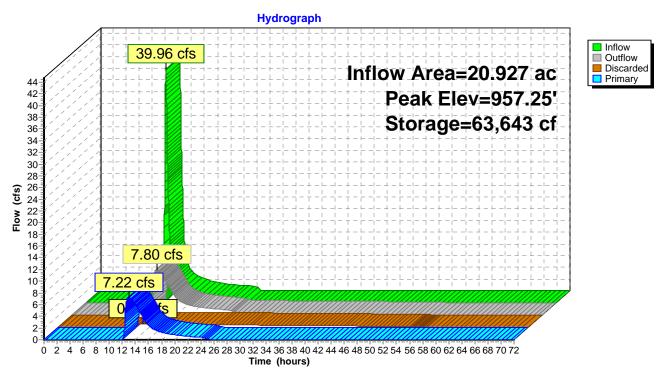
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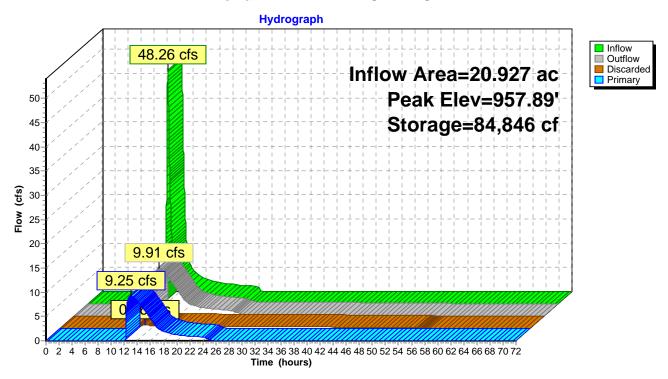


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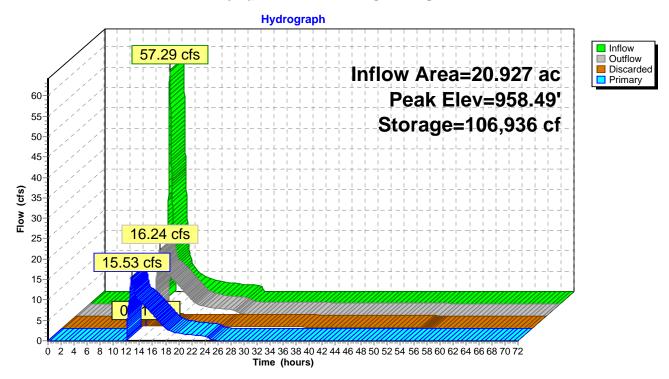


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Point of Interest A Post Development Bypass Drainage Area

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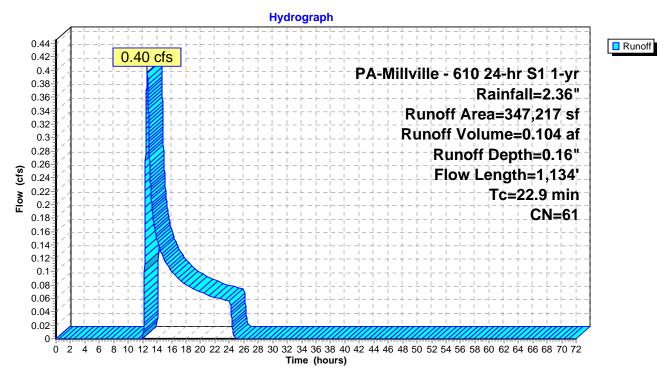
Summary for Subcatchment 5: POST DEVELOPMENT BYPASS DRAINAGE AREA

Runoff 0.40 cfs @ 12.64 hrs, Volume= 0.104 af, Depth= 0.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs PA-Millville - 610 24-hr S1 1-yr Rainfall=2.36"

_	Α	rea (sf)	CN E	Description					
		58,825	61 >	>75% Grass cover, Good, HSG B					
		25,788	98 F	Paved park	ing, HSG B				
_	2	62,604	58 N	/leadow, no	on-grazed,	HSG B			
	3	47,217	61 V	Veighted A	verage				
	3	21,429	9	2.57% Per	vious Area				
		25,788	7	'.43% Impe	ervious Area	a			
	Tc	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	6.0	100	0.0605	0.28		Sheet Flow, SHT 1			
						Range n= 0.130 P2= 2.83"			
4.9 433 0.0451 1.49				1.49		Shallow Concentrated Flow, SCF 1			
Short Grass Pasture Kv= 7.0 fps					Short Grass Pasture Kv= 7.0 fps				
12.0 601 0.0143 0.84 Shallow Concentrated Flow, SCF 2									
_						Short Grass Pasture Kv= 7.0 fps			
	22.9	1.134	Total						

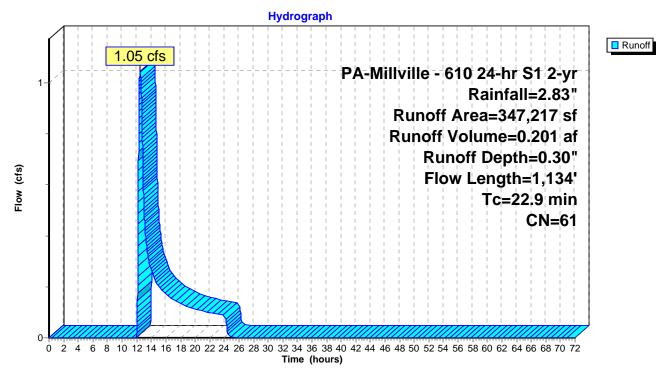
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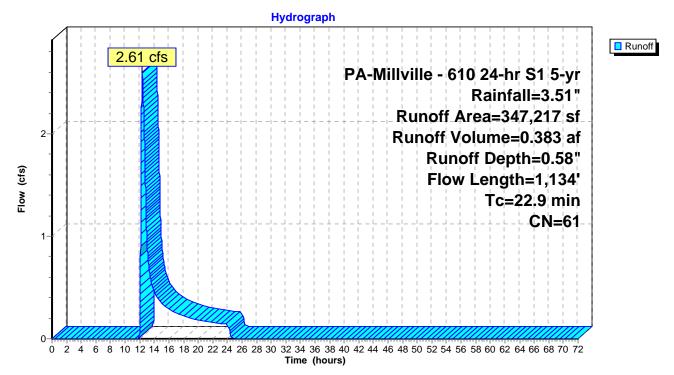
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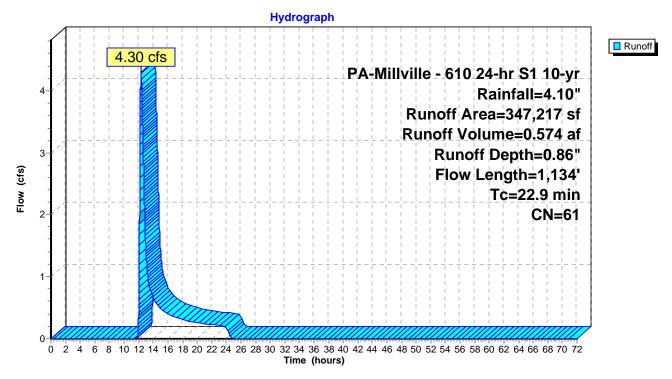
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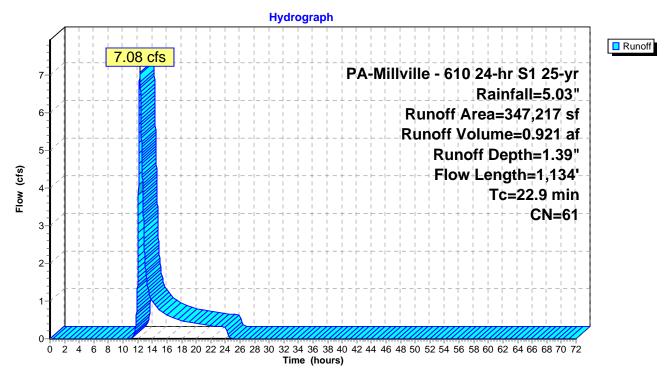
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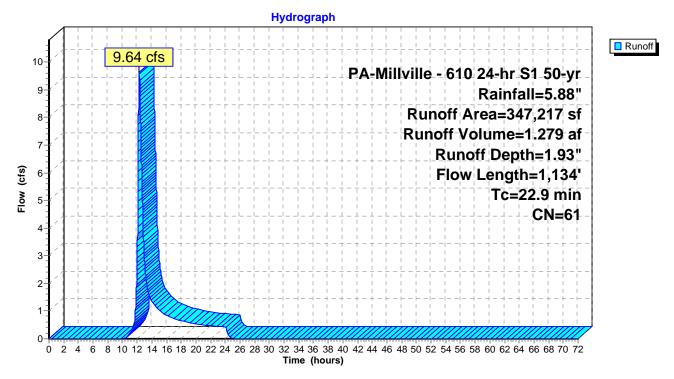
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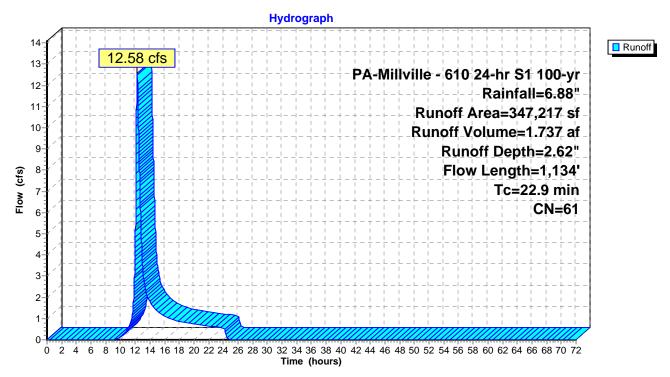


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Point of Interest B Post Development Calculations

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Summary for Subcatchment 8: POST DEVELOPMENT DRAINAGE AREA TO POI B

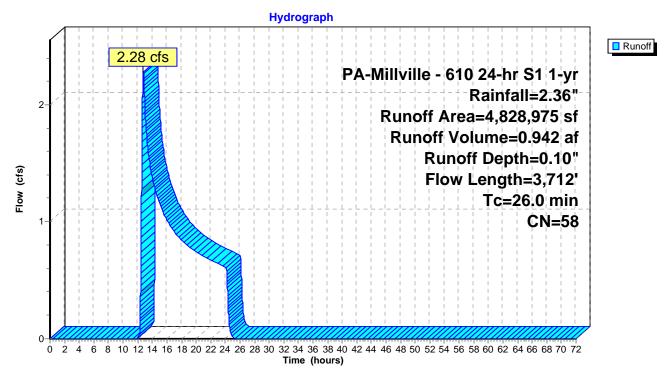
Runoff 2.28 cfs @ 12.77 hrs, Volume= 0.942 af, Depth= 0.10"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs PA-Millville - 610 24-hr S1 1-yr Rainfall=2.36"

	Α	rea (sf)	CN D	escription				
	7	92,008		Woods, Good, HSG B				
	3,980,165 58 Meadow, non-grazed, HSG B 56,802 98 Impervious, HSG B							
*								
	4,8	28,975	58 V	Veighted A	verage			
	4,7	72,173	9	8.82% Per	vious Area			
		56,802	1	.18% Impe	ervious Area	a		
				•				
	Tc	Length	Slope	Velocity	Capacity	Description		
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	5.8	100	0.0650	0.29		Sheet Flow, SHT 1		
						Range n= 0.130 P2= 2.83"		
	8.2	1,084	0.0990	2.20		Shallow Concentrated Flow, SCF 1		
						Short Grass Pasture Kv= 7.0 fps		
	1.6	262	0.0340	2.77		Shallow Concentrated Flow, SCF 2		
						Grassed Waterway Kv= 15.0 fps		
	1.4	487	0.7000	5.86		Shallow Concentrated Flow, SCF 3		
						Short Grass Pasture Kv= 7.0 fps		
	9.0	1,779	0.0480	3.29		Shallow Concentrated Flow, SCF 4		
						Grassed Waterway Kv= 15.0 fps		
	26.0	3,712	Total					

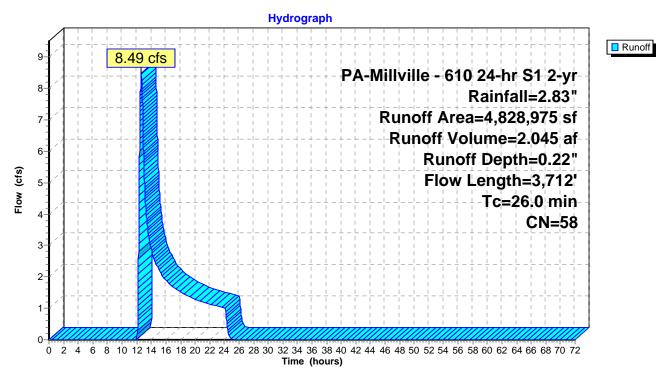
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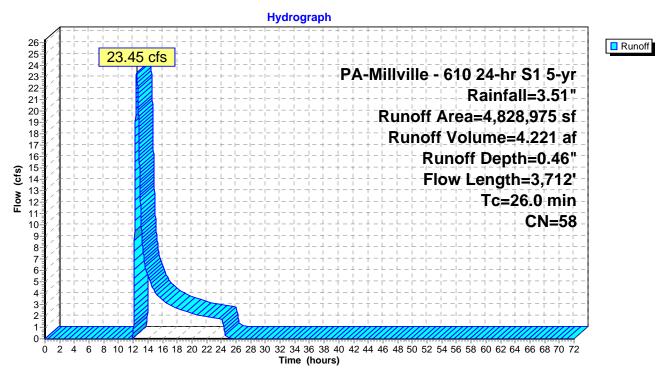


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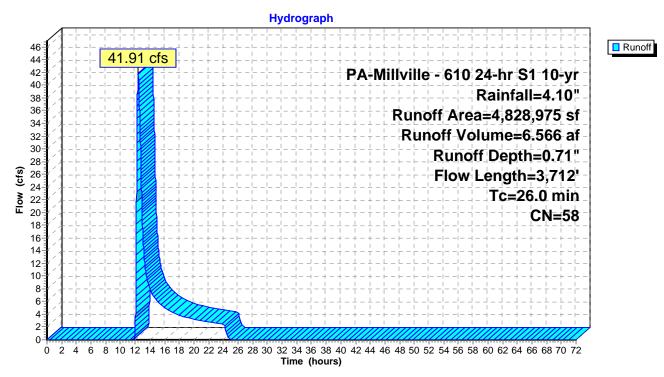
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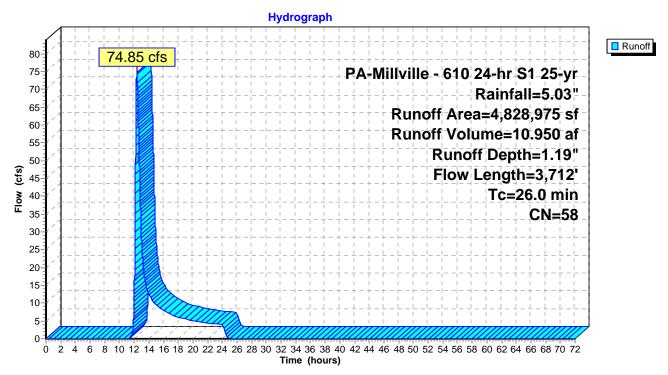
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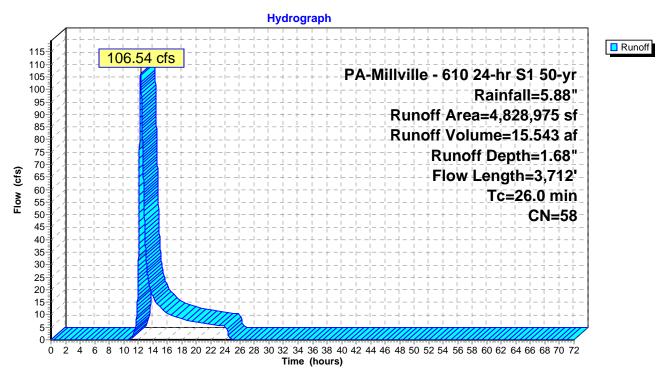
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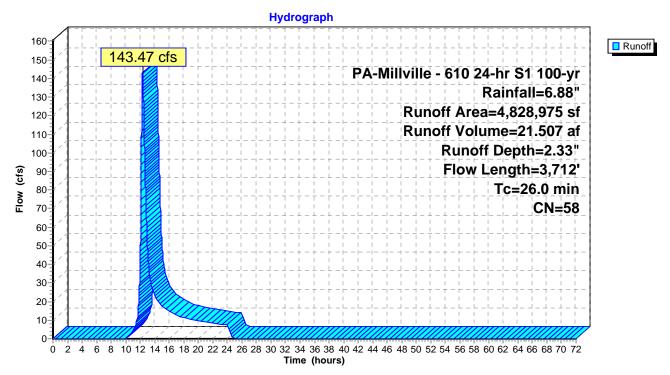
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Point of Interest C Post Development Calculations

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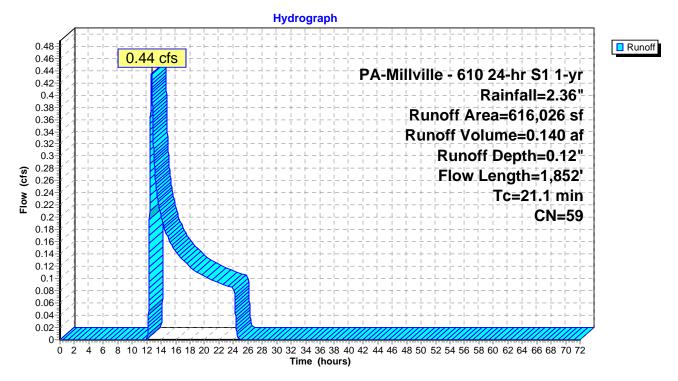
Summary for Subcatchment 13S: POST DEVELOPMENT DRAINAGE AREA TO POI C

Runoff 0.44 cfs @ 12.67 hrs, Volume= 0.140 af, Depth= 0.12" =

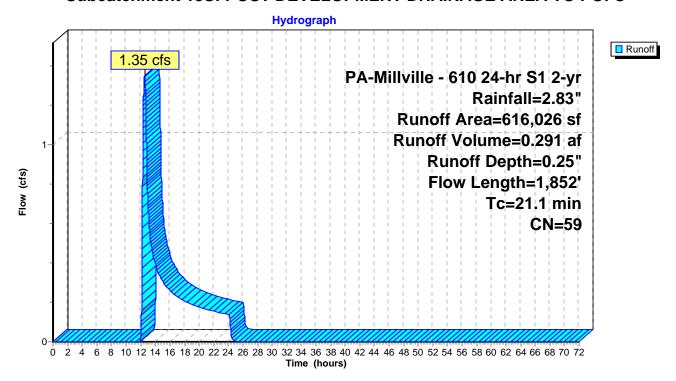
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs PA-Millville - 610 24-hr S1 1-yr Rainfall=2.36"

	Α	rea (sf)	CN D	Description					
_	6	05,789	58 N	Meadow, non-grazed, HSG B					
*		10,237		mpervious,	•				
616,026 59 Weighted Average									
	6	05,789	9	8.34% Per	vious Area				
		10,237	1	.66% Impe	ervious Area	a			
	Тс	Length	Slope	Velocity	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	6.7	100	0.0450	0.25		Sheet Flow, SHT 1			
						Range n= 0.130 P2= 2.83"			
	13.7	1,660	0.0830	2.02		Shallow Concentrated Flow, SCF 1			
						Short Grass Pasture Kv= 7.0 fps			
	0.7	92	0.0200	2.12		Shallow Concentrated Flow, SCF 2			
_						Grassed Waterway Kv= 15.0 fps			
	21.1	1,852	Total						

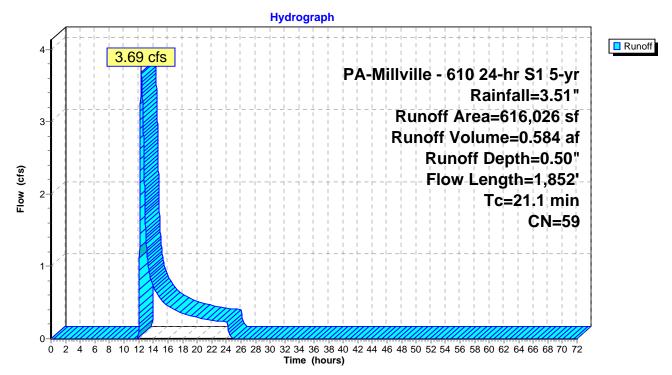
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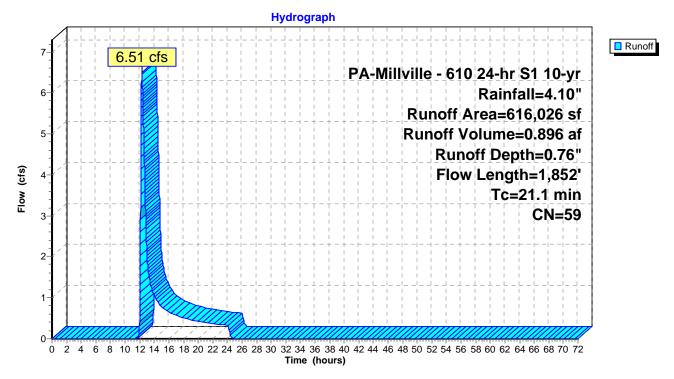
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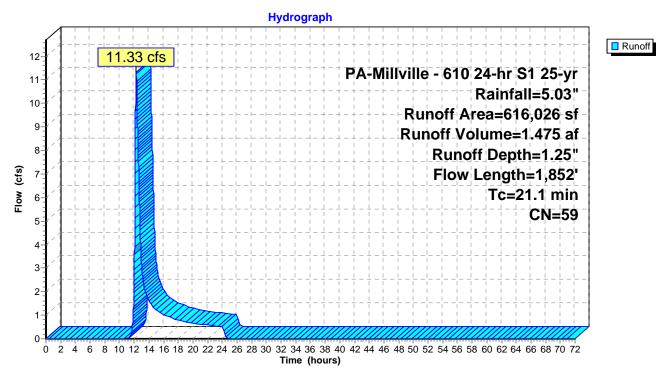
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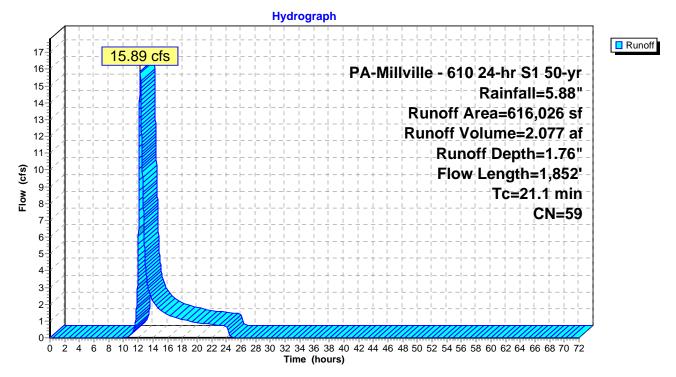
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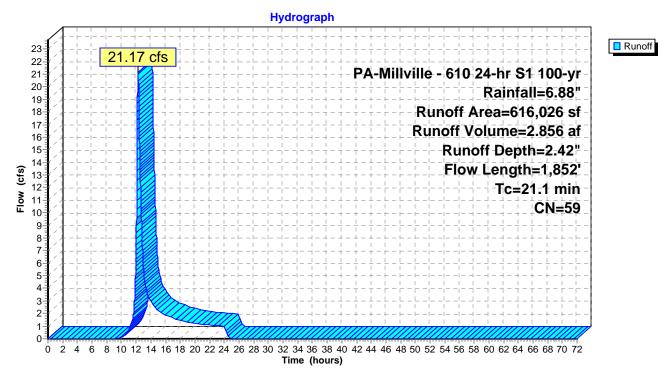
Subcatchment 13S: POST DEVELOPMENT DRAINAGE AREA TO POI C



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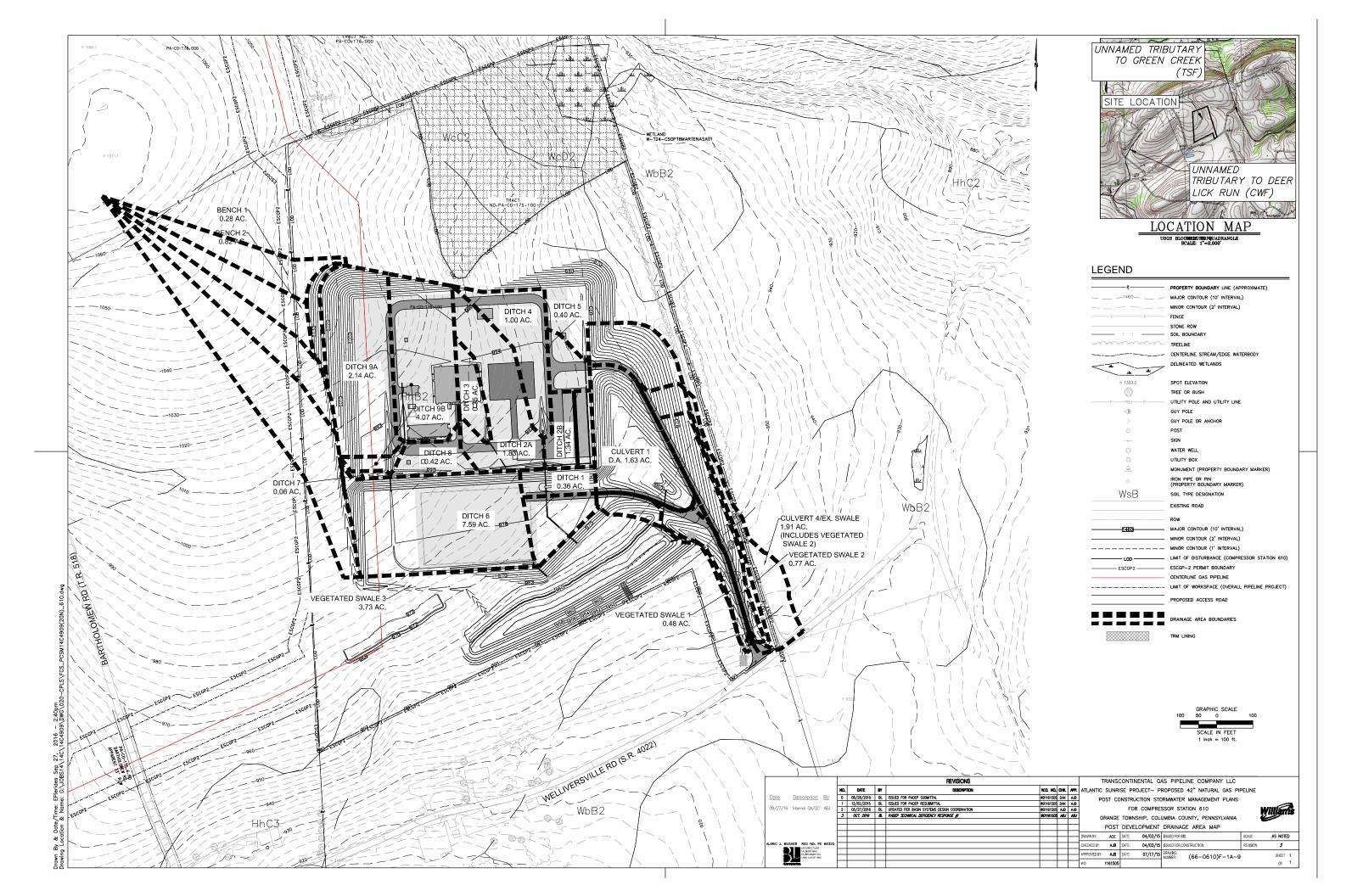
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Subcatchment 13S: POST DEVELOPMENT DRAINAGE AREA TO POI C





A.3 Conveyance Calculations



Channel Design Data

PROJECT NAME: ___ATLANTIC SUNRISE PROJECT - COMPRESSOR STATION 610

LOCATION: ORANGE TOWNSHIP, COLUMBIA COUNTY, PENNSYLVANIA

 PREPARED BY:
 AOE
 DATE:
 08/17/2015

 CHECKED BY:
 AJB
 DATE:
 08/17/2015

ONLONED D1			. D/(IL0	J/ 17/2010		
CHANNEL OR CHANNEL SECTION		SWALE 1	VEGETATED SWALE 1	SWALE 1	VEGETATED SWALE 1	
		MAX LINING	MAX GRASS	MIN LINING	MIN GRASS	
TEMPORARY OR PERMANENT?	(T OR P)	P	P	P	P	
DESIGN STORM	(2, 5, OR 10 YR)	10	10	10	10	
ACRES	(AC)	THE REQUIRED	CAPACITY (Qr) OF	THIS SWALE IS T	THE DISCHARGE	
MULTIPLIER ¹	(1.6, 2.25, or 2.75) ¹		ATION BASIN 1 CC ERLAND DRAINA			
Qr (REQUIRED CAPACITY)	(CFS)		.98 (BASIN) +1.16			
Q (CALCULATED AT FLOW DEPTH d)	(CFS)	5.27	5.22	5.28	5.15	
PROTECTIVE LINING ²		SC250	GRASS/ SC250	SC250	GRASS/ SC250	
n (MANNING'S COEFFICIENT) ²		0.04	0.088	0.04	0.092	
Va (ALLOWABLE VELOCITY)	(FPS)	N/A	N/A	N/A	N/A	
V (CALCULATED AT FLOW DEPTH d)	(FPS)	4.26	2.40	3.61	1.96	
та (MAX ALLOWABLE SHEAR STRESS)	(LB/FT ²)	2.50	8.00	2.50	8.00	
тd (CALC'D SHEAR STRESS AT FLOW DI	EPTH d) (LB/FT ²)	1.78	2.64	1.26	1.89	
CHANNEL BOTTOM WIDTH	(FT)	2	2	2	2	
CHANNEL SIDE SLOPES	(H:V)	3	3	3	3	
D (TOTAL DEPTH)	(FT)	2.0	2.0	2.0	2.0	
CHANNEL TOP WIDTH @ D	(FT)	14	14	14	14	
d (CALCULATED FLOW DEPTH)	(FT)	0.39	0.58	0.44	0.66	
CHANNEL TOP WIDTH @ FLOW DEPTH	d (FT)	4.34	5.48	4.64	5.96	
BOTTOM WIDTH: FLOW DEPTH RATIO	(12:1 MAX)	5.13	3.45	4.55	3.03	
d50 STONE SIZE	(IN)	N/A	N/A	N/A	N/A	
A (CROSS-SECTIONAL AREA)	(SQ. FT.)	1.24	2.17	1.46	2.63	
R (HYDRAULIC RADIUS)		0.28	0.38	0.31	0.43	
S (BED SLOPE) ³	(FT/FT)	0.073	0.073	0.046	0.046	
Sc (CRITICAL SLOPE)	(FT/FT)	0.037	0.161	0.036	0.170	
.7Sc	(FT/FT)	0.026	0.112	0.025	0.119	
1.3Sc	(FT/FT)	0.048	0.209	0.046	0.221	
STABLE FLOW?	(Y/N)	Y	Y	N	Y	
FREEBOARD BASED ON UNSTABLE FLO	OW (FT)	0.12	0.10	0.12	0.10	
FREEBOARD BASED ON STABLE FLOW	(FT)	0.50	0.50	0.50	0.50	
MINIMUM REQUIRED FREEBOARD ⁴	(FT)	0.50	0.50	0.50	0.50	
DESIGN METHOD FOR PROTECTIVE LIN PERMISSIBLE VELOCITY (V) OR SHEAR		S	S	S	S	

^{1.} Use 1.6 for Temporary Channels; 2.25 for Temporary Channels in Special Protection (HQ or EV) Watersheds; 2.75 for Permanent Channels. For Rational Method, enter "N/A" and attach E&S Worksheets 9 and 10. For TR-55 enter "N/A" and attach appropriate Worksheets.

^{2.} Adjust "n" value for changes in channel liner and flow depth. For vegetated channels, provide data for manufactured linings without vegetation and with vegetation in separate columns.

^{3.} Slopes may not be averaged.

^{4.} Minimum Freeboard is 0.5 ft. or 1/4 Total Channel Depth, whichever is greater

^{5.} Permissible velocity lining design method is not acceptable for channels with a bed slope of 10% or greater. Shear stress lining design method is required for channels with a bed slope of 10% or greater. Shear stress lining design method may be used for any channel bed slope.

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Page 1

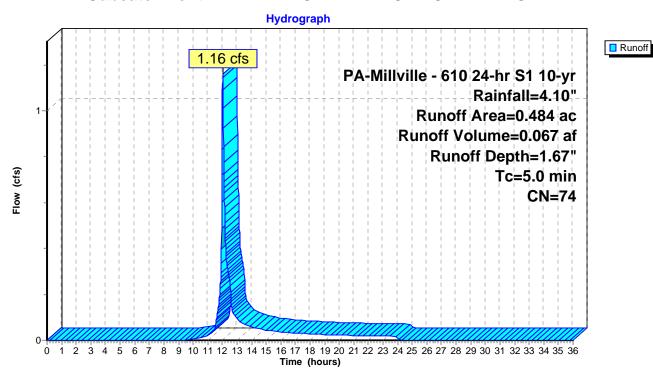
Summary for Subcatchment 11: DRAINAGE AREA TO VEGETATED SWALE 1

Runoff = 1.16 cfs @ 12.03 hrs, Volume= 0.067 af, Depth= 1.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs PA-Millville - 610 24-hr S1 10-yr Rainfall=4.10"

	Area	(ac)	CN	Desc	ription					
	0.	320	61	Past	asture/grassland/range, Good, HSG B					
*	0.	164	98	Impe	rvious, HS	SG B				
	0.	484	74	Weig	hted Aver	age				
	0.	320		66.1	2% Pervio	us Area				
	0.	164		33.8	8% Imperv	ious Area				
	Тс	Leng	th	Slope	Velocity	Capacity	Description			
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)				
	5.0						Direct Entry,			

Subcatchment 11: DRAINAGE AREA TO VEGETATED SWALE 1



For discharge velocities exceeding Maximum Allowable for Riprap indicated, increase d50 stone size and/or provide velocity reduction device.

Channel Design Data

PROJECT NAME: ___ATLANTIC SUNRISE PROJECT - COMPRESSOR STATION 610

LOCATION: ORANGE TOWNSHIP, COLUMBIA COUNTY, PENNSYLVANIA

 PREPARED BY:
 JEC
 DATE:
 06/15/2015

 CHECKED BY:
 AJB
 DATE:
 06/15/2015

OTILOTED DT		B/(TE: 06/19/2010				
		VEGETATED SWALE 2	VEGETATED SWALE 2	VEGETATED SWALE 2	VEGETATED SWALE 2	
CHANNEL OR CHANNEL SECTION		MAX	MAX	MIN	MIN	
		LINING	GRASS	LINING	GRASS	
TEMPORARY OR PERMANENT?	(T OR P)	Р	Р	Р	Р	
DESIGN STORM	(2, 5, OR 10 YR)	10	10	10	10	
ACRES	(AC)	0.77	0.77	0.77	0.77	
MULTIPLIER ¹	(1.6, 2.25, or 2.75) ¹	2.75	2.75	2.75	2.75	
Qr (REQUIRED CAPACITY)	(CFS)	2.12	2.12	2.12	2.12	
Q (CALCULATED AT FLOW DEPTH d)	(CFS)	2.12	2.12	2.17	2.17	
PROTECTIVE LINING ²		SC250	GRASS/ SC250	SC250	GRASS/ SC250	
n (MANNING'S COEFFICIENT) ²		0.04	0.126	0.04	0.129	
Va (ALLOWABLE VELOCITY)	(FPS)	N/A	N/A	N/A	N/A	
V (CALCULATED AT FLOW DEPTH d)	(FPS)	3.08	1.36	2.86	1.24	
та (MAX ALLOWABLE SHEAR STRESS)	(LB/FT ²)	2.50	8.00	2.50	8.00	
тd (CALC'D SHEAR STRESS AT FLOW D	DEPTH d) (LB/FT ²)	0.97	1.78	0.83	1.53	
CHANNEL BOTTOM WIDTH	(FT)	2	2	2	2	
CHANNEL SIDE SLOPES	(H:V)	3	3	3	3	
D (TOTAL DEPTH)	(FT)	2.0	2.0	2.0	2.0	
CHANNEL TOP WIDTH @ D	(FT)	14	14	14	14	
d (CALCULATED FLOW DEPTH)	(FT)	0.25	0.46	0.27	0.50	
CHANNEL TOP WIDTH @ FLOW DEPTH	d (FT)	3.50	4.76	3.62	5.00	
BOTTOM WIDTH: FLOW DEPTH RATIO	(12:1 MAX)	8.00	4.35	7.41	4.00	
d50 STONE SIZE	(IN)	N/A	N/A	N/A	N/A	
A (CROSS-SECTIONAL AREA)	(SQ. FT.)	0.69	1.55	0.76	1.75	
R (HYDRAULIC RADIUS)		0.19	0.32	0.20	0.34	
S (BED SLOPE) ³	(FT/FT)	0.062	0.062	0.049	0.049	
Sc (CRITICAL SLOPE)	(FT/FT)	0.041	0.350	0.040	0.359	
.7Sc	(FT/FT)	0.029	0.245	0.028	0.251	
1.3Sc	(FT/FT)	0.054	0.455	0.053	0.466	
STABLE FLOW?	(Y/N)	Υ	Y	N	Y	
FREEBOARD BASED ON UNSTABLE FL	OW (FT)	0.06	0.05	0.06	0.05	
FREEBOARD BASED ON STABLE FLOW	/ (FT)	0.50	0.50	0.50	0.50	
MINIMUM REQUIRED FREEBOARD ⁴	(FT)	0.50	0.50	0.50	0.50	
DESIGN METHOD FOR PROTECTIVE LI PERMISSIBLE VELOCITY (V) OR SHEAF		S	S	S	S	

^{1.} Use 1.6 for Temporary Channels; 2.25 for Temporary Channels in Special Protection (HQ or EV) Watersheds; 2.75 for Permanent Channels. For Rational Method, enter "N/A" and attach E&S Worksheets 9 and 10. For TR-55 enter "N/A" and attach appropriate Worksheets.

^{2.} Adjust "n" value for changes in channel liner and flow depth. For vegetated channels, provide data for manufactured linings without vegetation and with vegetation in separate columns.

^{3.} Slopes may not be averaged.

^{4.} Minimum Freeboard is 0.5 ft. or 1/4 Total Channel Depth, whichever is greater

^{5.} Permissible velocity lining design method is not acceptable for channels with a bed slope of 10% or greater. Shear stress lining design method is required for channels with a bed slope of 10% or greater. Shear stress lining design method may be used for any channel bed slope.

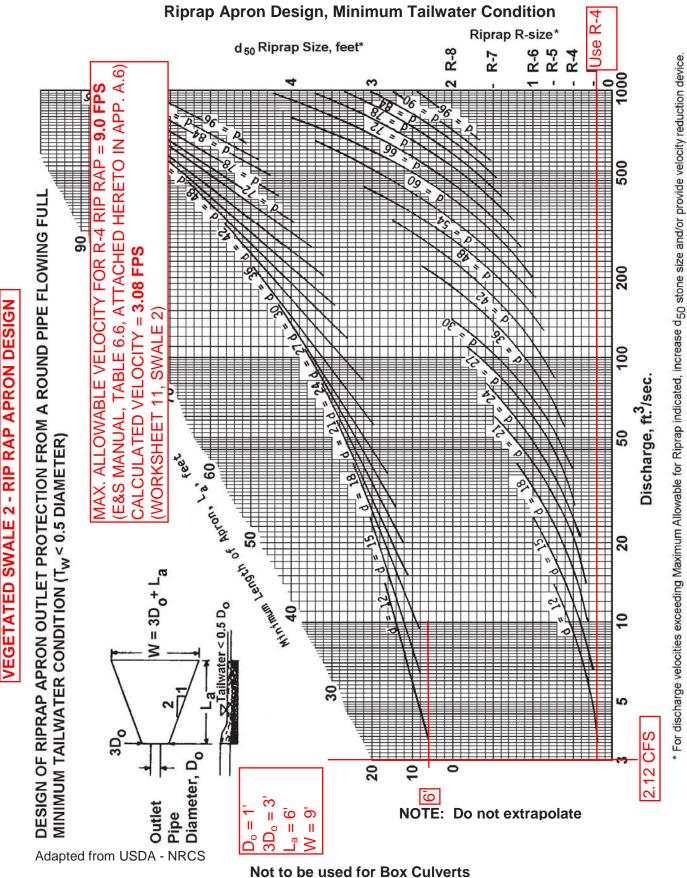


FIGURE 9.3

Channel Design Data

PROJECT NAME: __ATLANTIC SUNRISE PROJECT - COMPRESSOR STATION 610

LOCATION: ORANGE TOWNSHIP, COLUMBIA COUNTY, PENNSYLVANIA

 PREPARED BY:
 JEC
 DATE:
 06/15/2015

 CHECKED BY:
 AJB
 DATE:
 06/15/2015

OHEORED D1			D/(1L0	<u> </u>		
CHANNEL OR CHANNEL SECTION		SWALE 3	VEGETATED SWALE 3			
TEMPORARY OR PERMANENT?	(T OR P)	LINING P	GRASS P			
DESIGN STORM	(2, 5, OR 10 YR)	10	10			
ACRES	(AC)	3.73	3.73			
4	.6, 2.25, or 2.75) ¹	2.75	2.75			
Qr (REQUIRED CAPACITY)	(CFS)	10.26	10.26			
Q (CALCULATED AT FLOW DEPTH d)	(CFS)	10.20	10.20			
PROTECTIVE LINING ²	(010)	W3000	GRASS/ W3000			
n (MANNING'S COEFFICIENT) ²		0.065	0.065			
Va (ALLOWABLE VELOCITY)	(FPS)	N/A	N/A			
V (CALCULATED AT FLOW DEPTH d)	(FPS)	4.44	4.44		1	
та (MAX ALLOWABLE SHEAR STRESS)	(LB/FT ²)	16.00	16.00			
тd (CALC'D SHEAR STRESS AT FLOW DEP		4.90	4.90			
CHANNEL BOTTOM WIDTH	(FT)	2	2			
CHANNEL SIDE SLOPES	(H:V)	3	3			
D (TOTAL DEPTH)	(FT)	1.5	1.5			
CHANNEL TOP WIDTH @ D	(FT)	11	11			
d (CALCULATED FLOW DEPTH)	(FT)	0.60	0.60			
CHANNEL TOP WIDTH @ FLOW DEPTH d	(FT)	5.60	5.60			
BOTTOM WIDTH: FLOW DEPTH RATIO	(12:1 MAX)	3.33	3.33			
d50 STONE SIZE	(IN)	N/A	N/A			
A (CROSS-SECTIONAL AREA)	(SQ. FT.)	2.28	2.28			
R (HYDRAULIC RADIUS)		0.39	0.39			
S (BED SLOPE) ³	(FT/FT)	0.131	0.131			
Sc (CRITICAL SLOPE)	(FT/FT)	0.087	0.087			
.7Sc	(FT/FT)	0.061	0.061			
1.3Sc	(FT/FT)	0.113	0.113			
STABLE FLOW?	(Y/N)	Y	Y			
FREEBOARD BASED ON UNSTABLE FLOW	/ (FT)	0.20	0.20			
FREEBOARD BASED ON STABLE FLOW	(FT)	0.50	0.50			
MINIMUM REQUIRED FREEBOARD ⁴	(FT)	0.50	0.50			
DESIGN METHOD FOR PROTECTIVE LININ PERMISSIBLE VELOCITY (V) OR SHEAR S		S	S			

^{1.} Use 1.6 for Temporary Channels; 2.25 for Temporary Channels in Special Protection (HQ or EV) Watersheds; 2.75 for Permanent Channels. For Rational Method, enter "N/A" and attach E&S Worksheets 9 and 10. For TR-55 enter "N/A" and attach appropriate Worksheets.

^{2.} Adjust "n" value for changes in channel liner and flow depth. For vegetated channels, provide data for manufactured linings without vegetation and with vegetation in separate columns.

^{3.} Slopes may not be averaged.

^{4.} Minimum Freeboard is 0.5 ft. or 1/4 Total Channel Depth, whichever is greater

^{5.} Permissible velocity lining design method is not acceptable for channels with a bed slope of 10% or greater. Shear stress lining design method is required for channels with a bed slope of 10% or greater. Shear stress lining design method may be used for any channel bed slope.

For discharge velocities exceeding Maximum Allowable for Riprap indicated, increase d₅₀ stone size and/or provide velocity reduction device.

FIGURE 9.3

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Channel Design Data

PROJECT NAME: <u>ATLANTIC SUNRISE PIPELINE - COMPRESSOR STATION 610</u>

LOCATION: ORANGE TOWNSHIP, COLUMBIA COUNTY, PENNSYLVANIA

PREPARED BY: <u>JEC</u> DATE: <u>06/15/2015</u>

CHECKED BY: AJB DATE: 06/15/2015

CHANNEL OR CHANNEL SECTION		BENCH 1 LINING	BENCH 1 GRASS	BENCH 2 LINING	BENCH 2 GRASS
TEMPORARY OR PERMANENT?	(T OR P)	Р	Р	Р	Р
DESIGN STORM	(2, 5, OR 10 YR)	10	10	10	10
ACRES	(AC)	0.28	0.28	0.82	0.82
MULTIPLIER ¹ (1.6, 2.25, or 2.75) ¹	2.75	2.75	2.75	2.75
Qr (REQUIRED CAPACITY)	(CFS)	0.77	0.77	2.26	2.26
Q (CALCULATED AT FLOW DEPTH d)	(CFS)	0.76	0.77	2.30	2.22
PROTECTIVE LINING ²		SC250	GRASS/ SC250	SC250	GRASS/ SC250
n (MANNING'S COEFFICIENT) ²		0.04	0.25	0.04	0.155
Va (ALLOWABLE VELOCITY)	(FPS)	N/A	N/A	N/A	N/A
V (CALCULATED AT FLOW DEPTH d)	(FPS)	1.55	0.39	2.05	0.73
та (MAX ALLOWABLE SHEAR STRESS)	(LB/FT ²)	2.50	8.00	2.50	8.00
td (CALC'D SHEAR STRESS AT FLOW DEP	TH d) (LB/FT ²)	0.41	0.82	0.62	1.02
CHANNEL BOTTOM WIDTH	(FT)	0	0	0	0
CHANNEL SIDE SLOPES	(H:V)	6 3	6 3	6 3	6 3
D (TOTAL DEPTH)	(FT)	1.00	1.00	1.00	1.00
CHANNEL TOP WIDTH @ D	(FT)	9.00	9.00	9.00	9.00
d (CALCULATED FLOW DEPTH)	(FT)	0.33	0.66	0.50	0.82
CHANNEL TOP WIDTH @ FLOW DEPTH d	(FT)	2.97	5.94	4.50	7.38
BOTTOM WIDTH: FLOW DEPTH RATIO	(12:1 MAX)	0.00	0.00	0.00	0.00
d50 STONE SIZE	(IN)	N/A	N/A	N/A	N/A
A (CROSS-SECTIONAL AREA)	(SQ. FT.)	0.49	1.96	1.13	3.03
R (HYDRAULIC RADIUS)		0.16	0.32	0.24	0.40
S (BED SLOPE) ³	(FT/FT)	0.02	0.02	0.02	0.02
Sc (CRITICAL SLOPE)	(FT/FT)	0.044	1.365	0.038	0.488
.7Sc	(FT/FT)	0.031	0.955	0.027	0.342
1.3Sc	(FT/FT)	0.057	1.774	0.050	0.634
STABLE FLOW?	(Y/N)	Y	Y	Y	Y
FREEBOARD BASED ON UNSTABLE FLOW	(FT)	0.04	0.02	0.08	0.05
FREEBOARD BASED ON STABLE FLOW	(FT)	0.50	0.50	0.50	0.50
MINIMUM REQUIRED FREEBOARD⁴	(FT)	0.50	0.50	0.50	0.50
DESIGN METHOD FOR PROTECTIVE LININ PERMISSIBLE VELOCITY (V) OR SHEAR ST		S	S	S	S

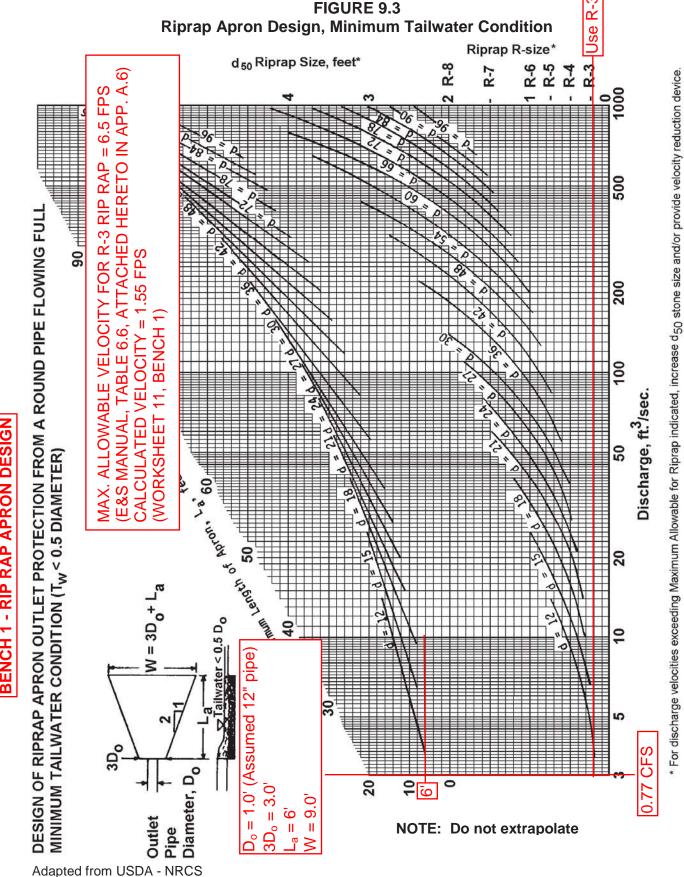
^{1.} Use 1.6 for Temporary Channels; 2.25 for Temporary Channels in Special Protection (HQ or EV) Watersheds; 2.75 for Permanent Channels. For Rational Method, enter "N/A" and attach E&S Worksheets 9 and 10. For TR-55 enter "N/A" and attach appropriate Worksheets.

^{2.} Adjust "n" value for changes in channel liner and flow depth. For vegetated channels, provide data for manufactured linings without vegetation and with vegetation in separate columns.

^{3.} Slopes may not be averaged.

^{4.} Minimum Freeboard is 0.5 ft. or $\frac{1}{4}$ Total Channel Depth, whichever is greater

^{5.} Permissible velocity lining design method is not acceptable for channels with a bed slope of 10% or greater. Shear stress lining design method is required for channels with a bed slope of 10% or greater. Shear stress lining design method may be used for any channel bed slope.



Not to be used for Box Culverts

Channel Design Data

PROJECT NAME: ___ATLANTIC SUNRISE PROJECT - COMPRESSOR STATION 610

LOCATION: ___ORANGE TOWNSHIP, COLUMBIA COUNTY, PENNSYLVANIA

PREPARED BY: ______ DATE: _____11/13/2015

CHECKED BY: <u>AJB</u>			DATE:1	1/13/2015		
CHANNEL OR CHANNEL SECTION		EX. ROAD SWALE MAX SLOPE	EX. ROAD SWALE MIN SLOPE			
TEMPORARY OR PERMANENT?	(T OR P)	P	P			
DESIGN STORM	(2, 5, OR 10 YR)	10	10			
ACRES	(AC)				IS THE COMBINE	
MULTIPLIER ¹ (1	.6, 2.25, or 2.75) ¹				SYPASS FLOW WI EA TO CULVERT 4	
Qr (REQUIRED CAPACITY)	(CFS)	1		LE 1) + 4.30 (BYP)		
Q (CALCULATED AT FLOW DEPTH d)	(CFS)	9.45	9.45			
PROTECTIVE LINING ²		GRASS	GRASS			
n (MANNING'S COEFFICIENT) ²		0.082	0.084			
Va (ALLOWABLE VELOCITY)	(FPS)	3	3			
V (CALCULATED AT FLOW DEPTH d)	(FPS)	1.53	1.14			
та (MAX ALLOWABLE SHEAR STRESS)	(LB/FT ²)	N/A	N/A			
τd (CALC'D SHEAR STRESS AT FLOW DEF	PTH d) (LB/FT ²)	N/A	N/A			
CHANNEL BOTTOM WIDTH	(FT)	1	1			
CHANNEL SIDE SLOPES	(H:V)	VARIES SEE C	HANNEL REPO	DRT		
D (TOTAL DEPTH)	(FT)	1.31	1.31			
CHANNEL TOP WIDTH @ D	(FT)	14.90	17.56			
d (CALCULATED FLOW DEPTH)	(FT)	1.03	1.16			
CHANNEL TOP WIDTH @ FLOW DEPTH d	(FT)	14.90	14.90			
BOTTOM WIDTH: FLOW DEPTH RATIO	(12:1 MAX)	1.03:1	1.16:1			
d50 STONE SIZE	(IN)	N/A	N/A			
A (CROSS-SECTIONAL AREA)	(SQ. FT.)	6.17	6.17			
R (HYDRAULIC RADIUS)		0.40	0.40			
S (BED SLOPE) ³	(FT/FT)	0.025	0.012			
Sc (CRITICAL SLOPE)	(FT/FT)	0.138	0.144			
.7Sc	(FT/FT)	0.096	0.101			
1.3Sc	(FT/FT)	0.179	0.188			
STABLE FLOW?	(Y/N)	Y	Y			
FREEBOARD BASED ON UNSTABLE FLOV	V (FT)	0.12	0.10			
FREEBOARD BASED ON STABLE FLOW	(FT)	0.50	0.50			
MINIMUM REQUIRED FREEBOARD ⁴	(FT)	0.50	0.50			
DESIGN METHOD FOR PROTECTIVE LININ PERMISSIBLE VELOCITY (V) OR SHEAR S		V	V			

- 1. Use 1.6 for Temporary Channels; 2.25 for Temporary Channels in Special Protection (HQ or EV) Watersheds; 2.75 for Permanent Channels. For Rational Method, enter "N/A" and attach E&S Worksheets 9 and 10. For TR-55 enter "N/A" and attach appropriate Worksheets.
- 2. Adjust "n" value for changes in channel liner and flow depth. For vegetated channels, provide data for manufactured linings without vegetation and with vegetation in separate columns.
- 3. Slopes may not be averaged.
- 4. Minimum Freeboard is 0.5 ft. or $\frac{1}{4}$ Total Channel Depth, whichever is greater
- 5. Permissible velocity lining design method is not acceptable for channels with a bed slope of 10% or greater. Shear stress lining design method is required for channels with a bed slope of 10% or greater. Shear stress lining design method may be used for any channel bed slope.

Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

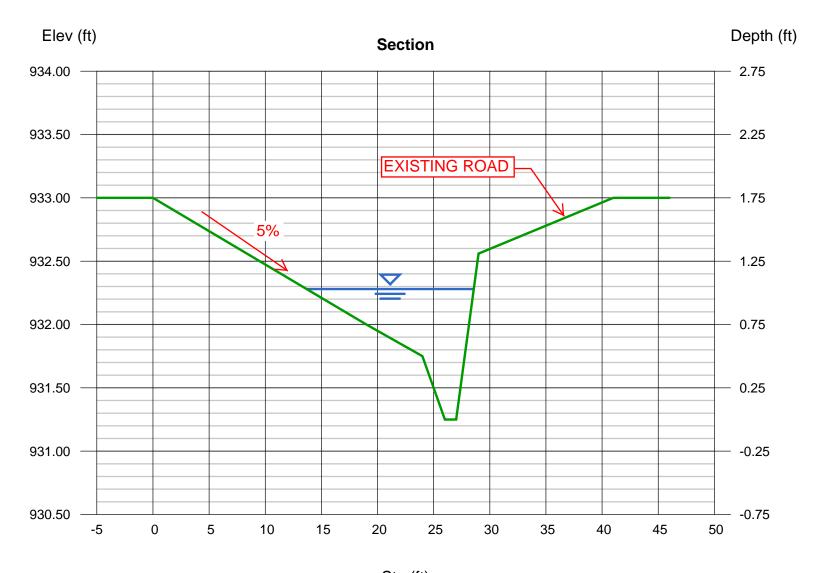
Friday, Nov 13 2015

EXISTING ROAD SWALE MAXIMUM SLOPE

User-defined		Highlighted	
Invert Elev (ft)	= 931.25	Depth (ft)	= 1.03
Slope (%)	= 2.50	Q (cfs)	= 9.450
N-Value	= 0.082	Area (sqft)	= 6.17
		Velocity (ft/s)	= 1.53
Calculations		Wetted Perim (ft)	= 15.28
Compute by:	Known Q	Crit Depth, Yc (ft)	= 0.77
Known Q (cfs)	= 9.45	Top Width (ft)	= 14.89
		EGL (ft)	= 1.07

(Sta, El, n)-(Sta, El, n)...

(0.00, 933.00)-(19.00, 932.00, 0.090)-(24.00, 931.75, 0.080)-(26.00, 931.25, 0.060)-(27.00, 931.25, 0.060)-(29.00, 932.56, 0.100)-(41.00, 933.00, 0.015)



Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

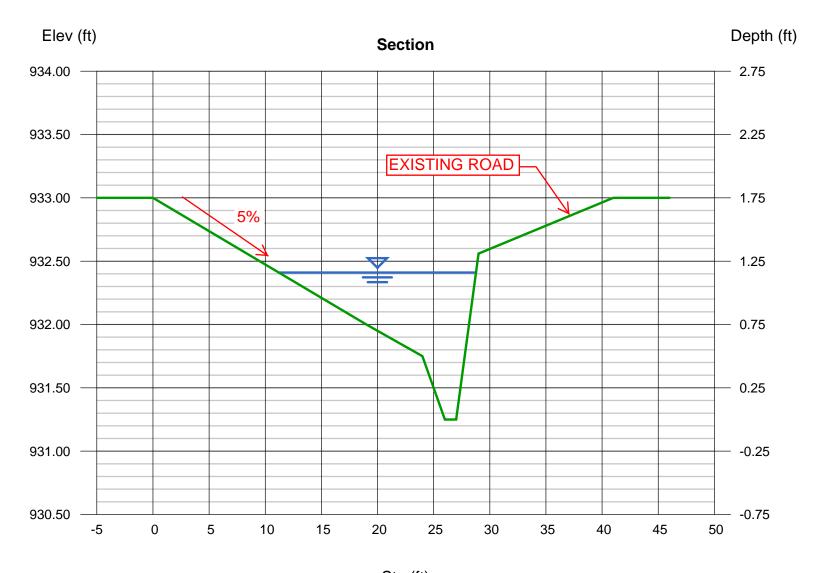
Friday, Nov 13 2015

EXISTING ROAD SWALE MINIMUM SLOPE

User-defined		Highlighted	
Invert Elev (ft)	= 931.25	Depth (ft)	= 1.16
Slope (%)	= 1.20	Q (cfs)	= 9.450
N-Value	= 0.084	Area (sqft)	= 8.28
		Velocity (ft/s)	= 1.14
Calculations		Wetted Perim (ft)	= 17.99
Compute by:	Known Q	Crit Depth, Yc (ft)	= 0.77
Known Q (cfs)	= 9.45	Top Width (ft)	= 17.56
		EGL (ft)	= 1.18

(Sta, El, n)-(Sta, El, n)...

(0.00, 933.00)-(19.00, 932.00, 0.090)-(24.00, 931.75, 0.080)-(26.00, 931.25, 0.060)-(27.00, 931.25, 0.060)-(29.00, 932.56, 0.100)-(41.00, 933.00, 0.015)



Channel Design Data

PROJECT NAME: __ATLANTIC SUNRISE PROJECT - COMPRESSOR STATION 610

LOCATION: ORANGE TOWNSHIP, COLUMBIA COUNTY, PENNSYLVANIA

 PREPARED BY:
 AOE
 DATE:
 03/07/16

 CHECKED BY:
 AJB
 DATE:
 03/07/16

CHANNEL OR CHANNEL SECTION		DITCH 1 R-4 RIP RAP	DITCH 2A R-4 RIP RAP	DITCH 2B R-4 RIP RAP	DITCH 3 R-4 RIP RAP	DITCH 4 R-4 RIP RAP
TEMPORARY OR PERMANENT?		LINING	LINING	LINING	LINING	LINING
	(T OR P)	Р	Р	Р	Р	Р
DESIGN STORM	(2, 5, OR 10 YR)	10	10	10	10	10
ACRES	(AC)	0.36	1.83	1.34	0.35	1.00
,	.6, 2.25, or 2.75) ¹	2.75	2.75	2.75	2.75	2.75
Qr (REQUIRED CAPACITY)	(CFS)	0.99	5.03	3.69	0.96	2.75
Q (CALCULATED AT FLOW DEPTH d)	(CFS)	1.00	5.06	3.72	1.00	2.77
PROTECTIVE LINING ²		R-4 RIP RAP	R-4 RIP RAP	R-4 RIP RAP	R-4 RIP RAP	R-4 RIP RAP
n (MANNING'S COEFFICIENT) ²		0.064	0.059	0.063	0.064	0.064
Va (ALLOWABLE VELOCITY)	(FPS)	9	9	9	9	9
V (CALCULATED AT FLOW DEPTH d)	(FPS)	0.99	2.64	2.42	1.76	2.55
та (MAX ALLOWABLE SHEAR STRESS)	(LB/FT ²)	N/A	N/A	N/A	N/A	N/A
td (CALC'D SHEAR STRESS AT FLOW DEP	TH d) (LB/FT ²)	0.23	1.35	1.30	0.78	1.53
CHANNEL BOTTOM WIDTH	(FT)	2	2	2	2	2
CHANNEL SIDE SLOPES	(H:V)	2	2	2	2	2
D (TOTAL DEPTH)	(FT)	2.0	2.0	2.0	2.0	2.0
CHANNEL TOP WIDTH @ D	(FT)	10	10	10	10	10
d (CALCULATED FLOW DEPTH)	(FT)	0.37	0.60	0.51	0.23	0.39
CHANNEL TOP WIDTH @ FLOW DEPTH d	(FT)	3.48	4.40	4.04	2.92	3.56
BOTTOM WIDTH: FLOW DEPTH RATIO	(12:1 MAX)	5.41	3.33	3.92	8.70	5.13
d50 STONE SIZE	(IN)	6	6	6	6	6
A (CROSS-SECTIONAL AREA)	(SQ. FT.)	1.01	1.92	1.54	0.57	1.08
R (HYDRAULIC RADIUS)		0.28	0.41	0.36	0.19	0.29
S (BED SLOPE) ³	(FT/FT)	0.01	0.036	0.041	0.054	0.063
Sc (CRITICAL SLOPE)	(FT/FT)	0.096	0.073	0.086	0.108	0.095
.7Sc	(FT/FT)	0.067	0.051	0.060	0.076	0.066
1.3Sc	(FT/FT)	0.125	0.094	0.112	0.141	0.123
STABLE FLOW?	(Y/N)	Υ	Y	Y	Y	Υ
FREEBOARD BASED ON UNSTABLE FLOW	/ (FT)	0.03	0.12	0.09	0.03	0.07
FREEBOARD BASED ON STABLE FLOW	(FT)	0.50	0.50	0.50	0.50	0.50
MINIMUM REQUIRED FREEBOARD ⁴	(FT)	0.50	0.50	0.50	0.50	0.50
DESIGN METHOD FOR PROTECTIVE LININ PERMISSIBLE VELOCITY (V) OR SHEAR S		V	V	V	V	V

^{1.} Use 1.6 for Temporary Channels; 2.25 for Temporary Channels in Special Protection (HQ or EV) Watersheds; 2.75 for Permanent Channels. For Rational Method, enter "N/A" and attach E&S Worksheets 9 and 10. For TR-55 enter "N/A" and attach appropriate Worksheets.

^{2.} Adjust "n" value for changes in channel liner and flow depth. For vegetated channels, provide data for manufactured linings without vegetation and with vegetation in separate columns.

^{3.} Slopes may not be averaged.

^{4.} Minimum Freeboard is 0.5 ft. or ¼ Total Channel Depth, whichever is greater

^{5.} Permissible velocity lining design method is not acceptable for channels with a bed slope of 10% or greater. Shear stress lining design method is required for channels with a bed slope of 10% or greater. Shear stress lining design method may be used for any channel bed slope.

Channel Design Data

PROJECT NAME: __ATLANTIC SUNRISE PROJECT - COMPRESSOR STATION 610

LOCATION: ORANGE TOWNSHIP, COLUMBIA COUNTY, PENNSYLVANIA

 PREPARED BY:
 AOE
 DATE:
 02/05/17

 CHECKED BY:
 AJB
 DATE:
 02/05/17

CHANNEL OR CHANNEL SECTION		DITCH 5 R-4 RIP RAP	DITCH 6 R-4 RIP RAP	DITCH 7 R-4 RIP RAP	DITCH 8 R-4 RIP RAP	
TEMPODADY OD DEDMANENTO		LINING	LINING	LINING	LINING	
TEMPORARY OR PERMANENT?	(T OR P)	Р	Р	Р	Р	
	(2, 5, OR 10 YR)	10	10	10	10	
ACRES	(AC)	0.40	7.59	0.06	0.42	
· ·	6, 2.25, or 2.75) ¹	2.75	2.75	2.75	2.75	
Qr (REQUIRED CAPACITY)	(CFS)	1.10	20.87	0.17	1.16	
Q (CALCULATED AT FLOW DEPTH d)	(CFS)	1.15	20.91	0.21	1.19	
PROTECTIVE LINING ²		R-4 RIP RAP	R-4 RIP RAP	R-4 RIP RAP	R-4 RIP RAP	
n (MANNING'S COEFFICIENT) ²		0.064	0.045	0.064	0.064	
Va (ALLOWABLE VELOCITY)	(FPS)	9	9	9	9	
V (CALCULATED AT FLOW DEPTH d)	(FPS)	0.99	3.04	1.20	1.52	
та (MAX ALLOWABLE SHEAR STRESS)	(LB/FT ²)	N/A	N/A	N/A	N/A	
td (CALC'D SHEAR STRESS AT FLOW DEPT	H d) (LB/FT ²)	0.23	0.97	0.44	0.56	
CHANNEL BOTTOM WIDTH	(FT)	2	2	2	2	
CHANNEL SIDE SLOPES	(H:V)	2	2	2	2	
D (TOTAL DEPTH)	(FT)	2.0	2.0	2.0	2.0	
CHANNEL TOP WIDTH @ D	(FT)	10	10	10	10	
d (CALCULATED FLOW DEPTH)	(FT)	0.41	1.42	0.08	0.30	
CHANNEL TOP WIDTH @ FLOW DEPTH d	(FT)	3.64	7.68	2.32	3.20	
BOTTOM WIDTH: FLOW DEPTH RATIO	(12:1 MAX)	4.88	1.41	25.00	6.67	
d50 STONE SIZE	(IN)	6	6	6	6	
A (CROSS-SECTIONAL AREA)	(SQ. FT.)	1.16	6.87	0.17	0.78	
R (HYDRAULIC RADIUS)		0.30	0.82	0.07	0.23	
S (BED SLOPE) ³	(FT/FT)	0.009	0.011	0.088	0.030	
Sc (CRITICAL SLOPE)	(FT/FT)	0.094	0.034	0.145	0.101	
.7Sc	(FT/FT)	0.066	0.024	0.101	0.071	
1.3Sc	(FT/FT)	0.122	0.044	0.188	0.131	
STABLE FLOW?	(Y/N)	Y	Y	Y	Y	
FREEBOARD BASED ON UNSTABLE FLOW	(FT)	0.03	0.32	0.01	0.03	
FREEBOARD BASED ON STABLE FLOW	(FT)	0.50	0.50	0.50	0.50	
MINIMUM REQUIRED FREEBOARD⁴	(FT)	0.50	0.50	0.50	0.50	
DESIGN METHOD FOR PROTECTIVE LINING PERMISSIBLE VELOCITY (V) OR SHEAR ST		V	V	V	V	

^{1.} Use 1.6 for Temporary Channels; 2.25 for Temporary Channels in Special Protection (HQ or EV) Watersheds; 2.75 for Permanent Channels. For Rational Method, enter "N/A" and attach E&S Worksheets 9 and 10. For TR-55 enter "N/A" and attach appropriate Worksheets.

^{2.} Adjust "n" value for changes in channel liner and flow depth. For vegetated channels, provide data for manufactured linings without vegetation and with vegetation in separate columns.

^{3.} Slopes may not be averaged.

^{4.} Minimum Freeboard is 0.5 ft. or ¼ Total Channel Depth, whichever is greater

^{5.} Permissible velocity lining design method is not acceptable for channels with a bed slope of 10% or greater. Shear stress lining design method is required for channels with a bed slope of 10% or greater. Shear stress lining design method may be used for any channel bed slope.

Channel Design Data

PROJECT NAME: __ATLANTIC SUNRISE PROJECT - COMPRESSOR STATION 610

LOCATION: ORANGE TOWNSHIP, COLUMBIA COUNTY, PENNSYLVANIA

 PREPARED BY:
 AOE
 DATE:
 02/05/17

 CHECKED BY:
 AJB
 DATE:
 02/05/17

CHECKED BT. AJB			DATE02/	00/11	
CHANNEL OR CHANNEL SECTION		DITCH 9A R-4 RIP RAP LINING	DITCH 9B R-4 RIP RAP LINING		
TEMPORARY OR PERMANENT?	(T OR P)	Р	Р		
DESIGN STORM (2, 5, OR 10 YR)	10	10		
ACRES	(AC)	2.14	4.07		
	, 2.25, or 2.75) ¹	2.75	2.75		
Qr (REQUIRED CAPACITY)	(CFS)	5.89	11.19		
Q (CALCULATED AT FLOW DEPTH d)	(CFS)	5.96	11.38		
PROTECTIVE LINING ²		R-4 RIP RAP	R-4 RIP RAP		
n (MANNING'S COEFFICIENT) ²		0.058	0.047		
Va (ALLOWABLE VELOCITY)	(FPS)	9	9		
V (CALCULATED AT FLOW DEPTH d)	(FPS)	2.90	2.13		
та (MAX ALLOWABLE SHEAR STRESS)	(LB/FT ²)	N/A	N/A		
td (CALC'D SHEAR STRESS AT FLOW DEPT	H d) (LB/FT ²)	1.57	0.53		
CHANNEL BOTTOM WIDTH	(FT)	2	2		
CHANNEL SIDE SLOPES	(H:V)	2	2		
D (TOTAL DEPTH)	(FT)	2.0	2.0		
CHANNEL TOP WIDTH @ D	(FT)	10	10		
d (CALCULATED FLOW DEPTH)	(FT)	0.63	1.21		
CHANNEL TOP WIDTH @ FLOW DEPTH d	(FT)	4.52	6.84		
BOTTOM WIDTH: FLOW DEPTH RATIO	(12:1 MAX)	3.17	1.65		
d50 STONE SIZE	(IN)	6	6		
A (CROSS-SECTIONAL AREA)	(SQ. FT.)	2.05	5.35		
R (HYDRAULIC RADIUS)		0.43	0.72		
S (BED SLOPE) ³	(FT/FT)	0.040	0.007		
Sc (CRITICAL SLOPE)	(FT/FT)	0.069	0.039		
.7Sc	(FT/FT)	0.049	0.027		
1.3Sc	(FT/FT)	0.090	0.051		
STABLE FLOW?	(Y/N)	Y	Y		
FREEBOARD BASED ON UNSTABLE FLOW	(FT)	0.14	0.19		
FREEBOARD BASED ON STABLE FLOW	(FT)	0.50	0.50		
MINIMUM REQUIRED FREEBOARD ⁴	(FT)	0.50	0.50		
DESIGN METHOD FOR PROTECTIVE LINING PERMISSIBLE VELOCITY (V) OR SHEAR STR		V	V		

^{1.} Use 1.6 for Temporary Channels; 2.25 for Temporary Channels in Special Protection (HQ or EV) Watersheds; 2.75 for Permanent Channels. For Rational Method, enter "N/A" and attach E&S Worksheets 9 and 10. For TR-55 enter "N/A" and attach appropriate Worksheets.

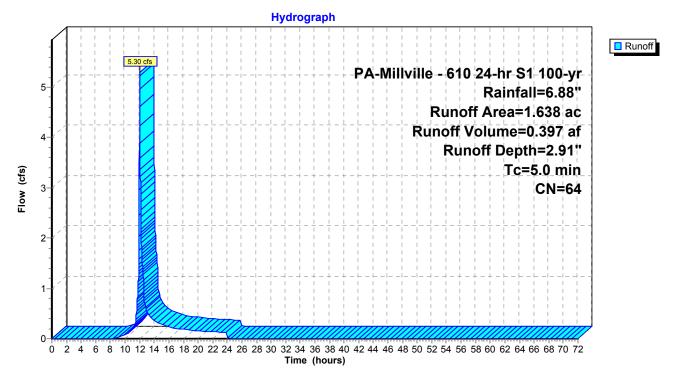
- 3. Slopes may not be averaged.
- 4. Minimum Freeboard is 0.5 ft. or ¼ Total Channel Depth, whichever is greater
- 5. Permissible velocity lining design method is not acceptable for channels with a bed slope of 10% or greater. Shear stress lining design method is required for channels with a bed slope of 10% or greater. Shear stress lining design method may be used for any channel bed slope.

^{2.} Adjust "n" value for changes in channel liner and flow depth. For vegetated channels, provide data for manufactured linings without vegetation and with vegetation in separate columns.

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Page 1

Subcatchment 10S: DRAINAGE AREA TO CULVERT 1



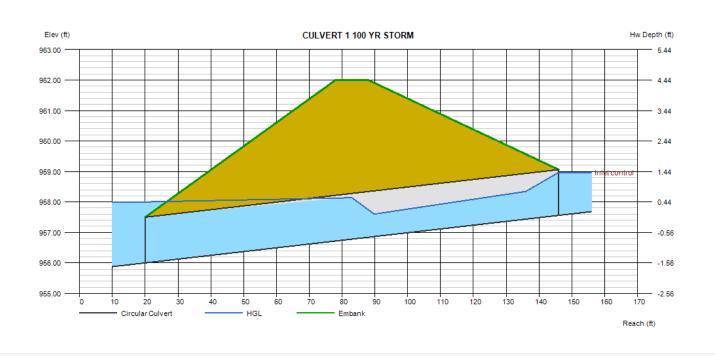
Culvert Report

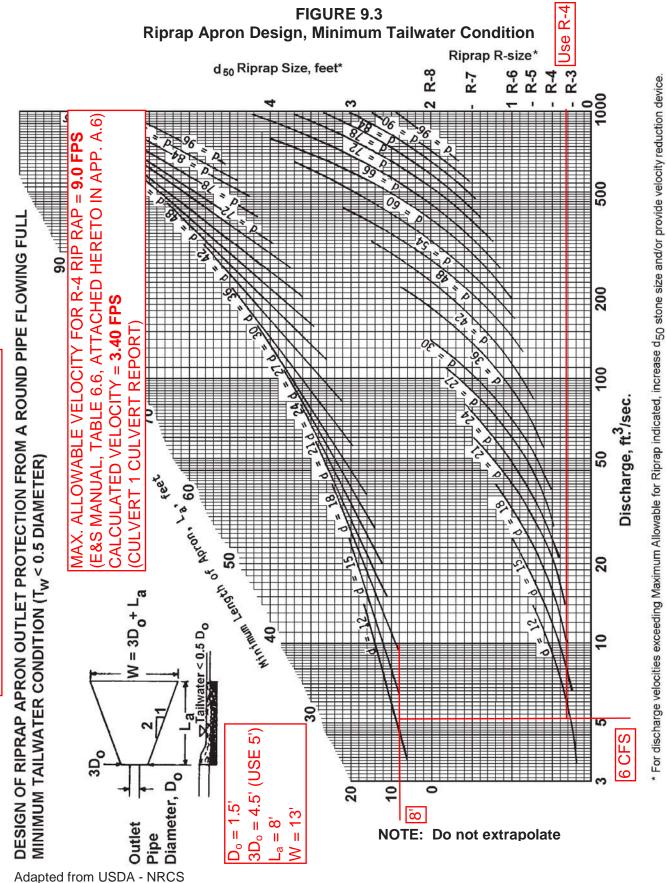
Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Wednesday, Aug 19 2015

CULVERT 1 100 YR STORM

Invert Elev Dn (ft)	= 956.00	Calculations	
Pipe Length (ft)	= 126.00	Qmin (cfs)	= 6.00
Slope (%)	= 1.24	Qmax (cfs)	= 6.00
Invert Elev Up (ft)	= 957.56	Tailwater Elev (ft)	= 958
Rise (in)	= 18.0		
Shape	= Circular	Highlighted	
Span (in)	= 18.0	Qtotal (cfs)	= 6.00
No. Barrels	= 1	Qpipe (cfs)	= 6.00
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	Circular Culvert	Veloc Dn (ft/s)	= 3.40
Culvert Entrance	= Smooth tapered inlet throat	Veloc Up (ft/s)	= 5.12
Coeff. K,M,c,Y,k	= 0.534, 0.555, 0.0196, 0.9, 0.2	HGL Dn (ft)	= 958.00
		HGL Up (ft)	= 958.51
Embankment		Hw Elev (ft)	= 958.97
Top Elevation (ft)	= 962.00	Hw/D (ft)	= 0.94
Top Width (ft)	= 10.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



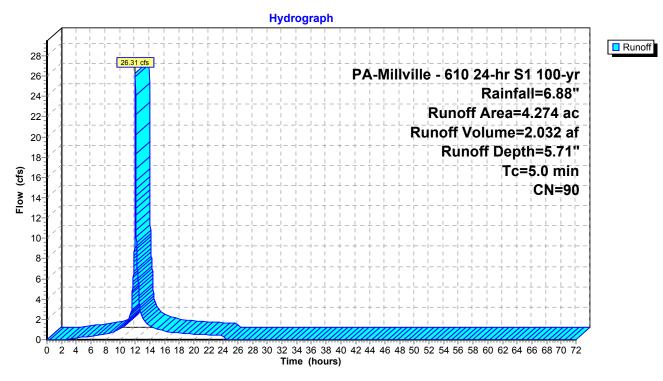


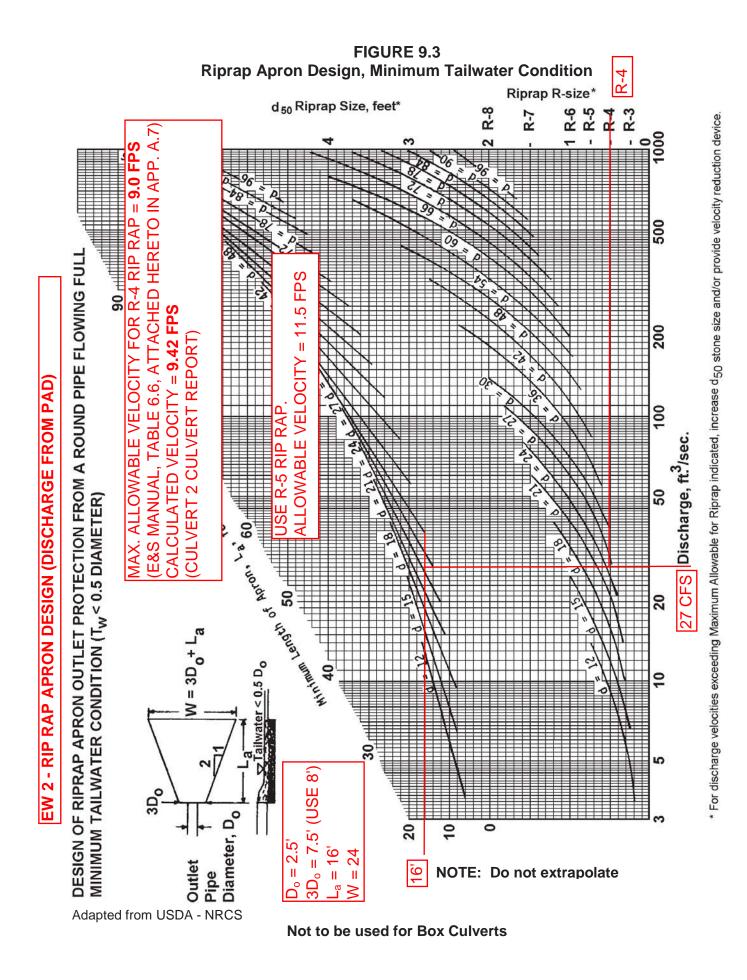
Not to be used for Box Culverts

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Page 1

Subcatchment 7S: DRAINAGE AREA TO EW 2





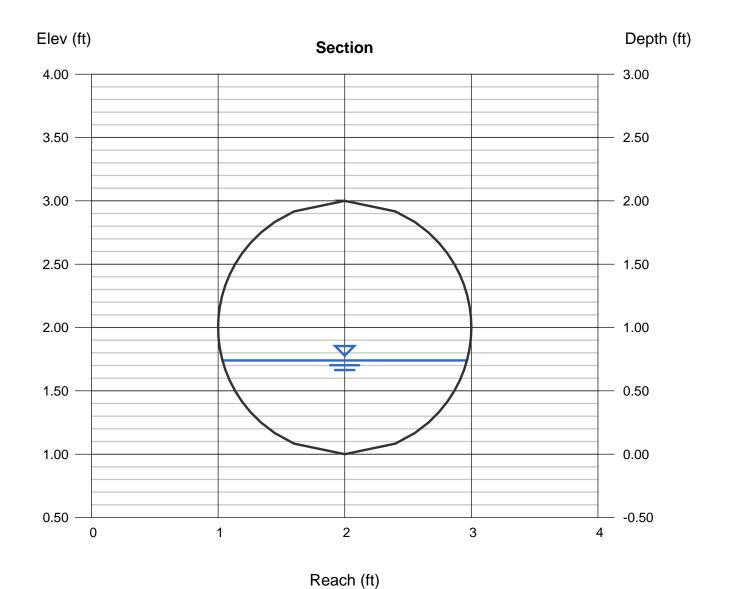
Channel Report

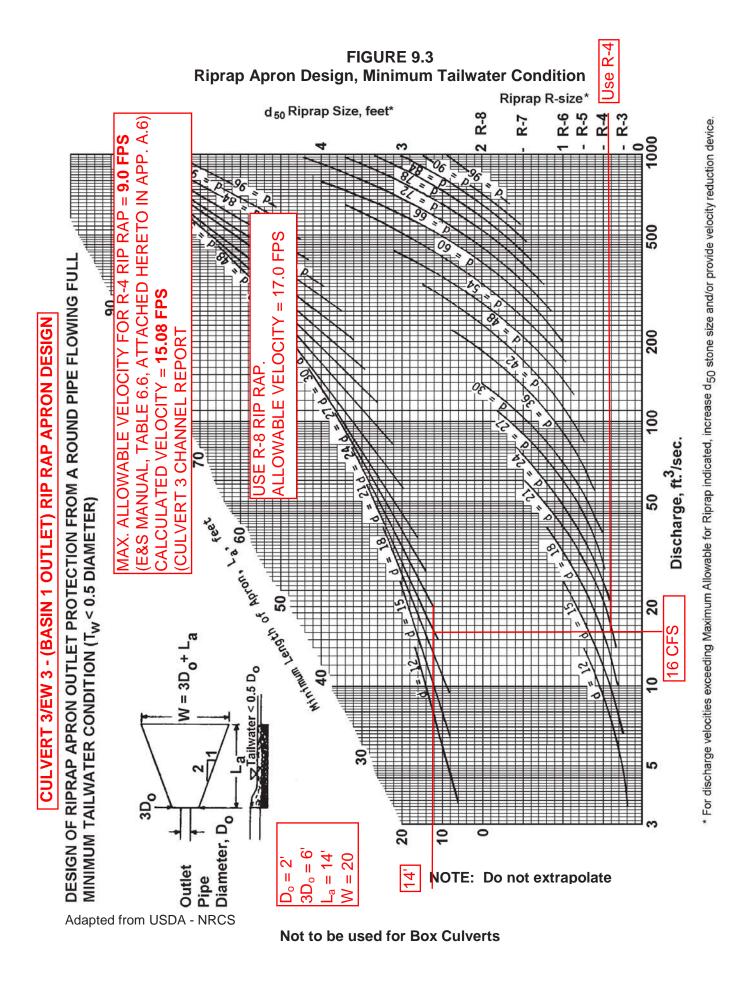
Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Saturday, Oct 17 2015

CULVERT 3

Circular		Highlighted	
Diameter (ft)	= 2.00	Depth (ft)	= 0.74
		Q (cfs)	= 16.00
		Area (sqft)	= 1.06
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 15.08
Slope (%)	= 5.00	Wetted Perim (ft)	= 2.62
N-Value	= 0.012	Crit Depth, Yc (ft)	= 1.44
		Top Width (ft)	= 1.93
Calculations		EGL (ft)	= 4.28
Compute by:	Known Q		
Known Q (cfs)	= 16.00		

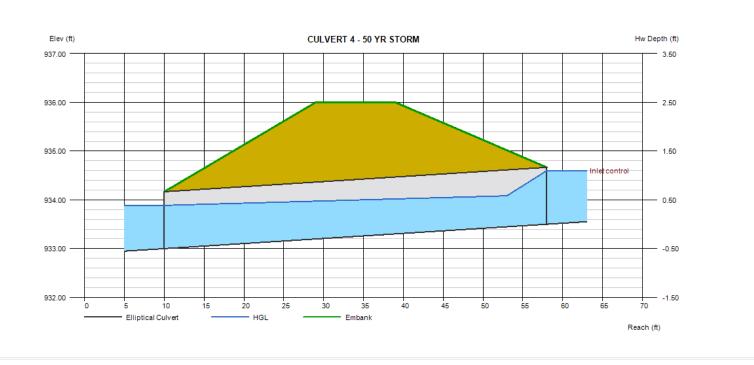




Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

CULVERT 4 - 50 YR STORM

= 933.00	Calculations	
= 48.00	Qmin (cfs)	= 4.77
= 1.04	Qmax (cfs)	= 4.77
= 933.50	Tailwater Elev (ft)	= (dc+D)/2
= 14.0		
Elliptical	Highlighted	
= 23.0	Qtotal (cfs)	= 4.77
= 1	Qpipe (cfs)	= 4.77
= 0.012	Qovertop (cfs)	= 0.00
 Horizontal Ellipse Concrete 	Veloc Dn (ft/s)	= 3.25
Square edge w/headwall (H)	Veloc Up (ft/s)	= 5.22
= 0.01, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 933.89
	HGL Up (ft)	= 934.11
	Hw Elev (ft)	= 934.60
= 936.00	Hw/D (ft)	= 0.94
= 10.00	Flow Regime	= Inlet Control
= 20.00		
	= 48.00 = 1.04 = 933.50 = 14.0 = Elliptical = 23.0 = 1 = 0.012 = Horizontal Ellipse Concrete = Square edge w/headwall (H) = 0.01, 2, 0.0398, 0.67, 0.5	= 48.00 Qmin (cfs) = 1.04 Qmax (cfs) = 933.50 Tailwater Elev (ft) = 14.0 = Elliptical Highlighted = 23.0 Qtotal (cfs) = 1 Qpipe (cfs) = 0.012 Qovertop (cfs) = Horizontal Ellipse Concrete Veloc Dn (ft/s) = Square edge w/headwall (H) Veloc Up (ft/s) = 0.01, 2, 0.0398, 0.67, 0.5 HGL Dn (ft) HGL Up (ft) HW Elev (ft) = 936.00 Hw/D (ft) = 10.00 Flow Regime



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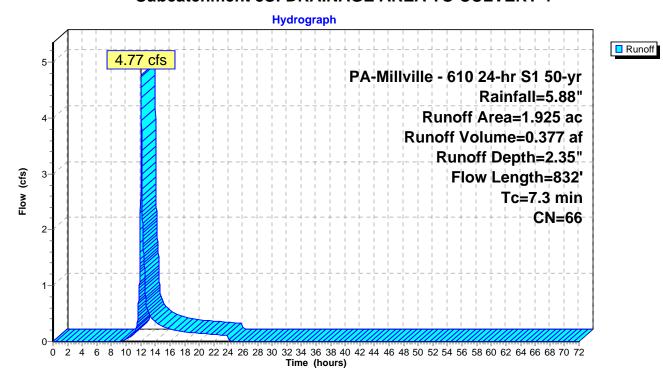
Summary for Subcatchment 8S: DRAINAGE AREA TO CULVERT 4

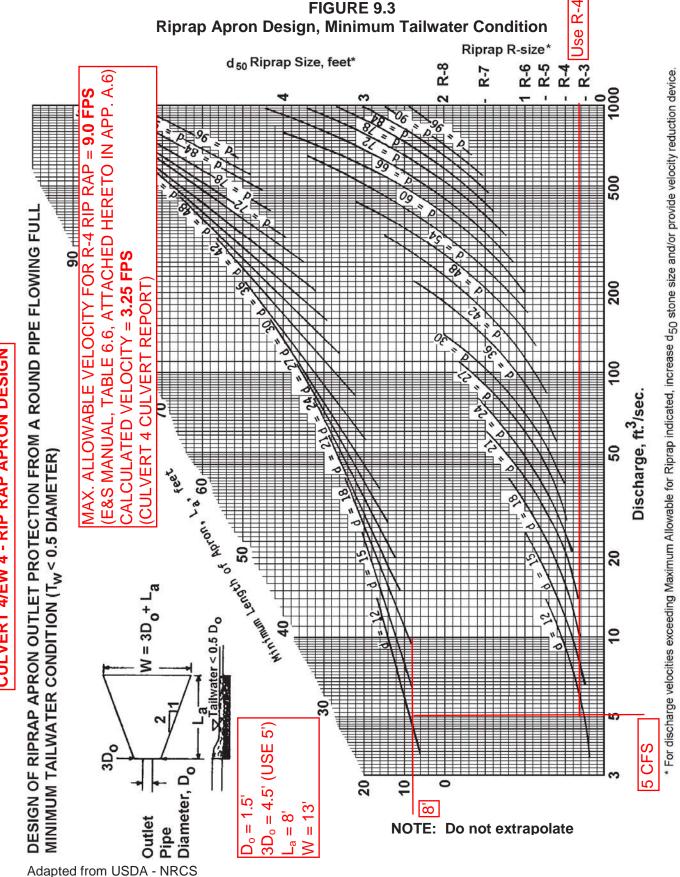
Runoff = 4.77 cfs @ 12.06 hrs, Volume= 0.377 af, Depth= 2.35"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs PA-Millville - 610 24-hr S1 50-yr Rainfall=5.88"

	Area	(ac) C	N Des	cription			
						Good, HSG B	
*	0.	<u> 261 </u>	98 Impe	ervious, HS	SG B		
	1.	925	66 Weig	ghted Aver	age		
	1.	664	86.4	4% Pervio	us Area		
	0.	261	13.5	6% Imperv	ious Area		
				•			
	Tc	Length	Slope	Velocity	Capacity	Description	
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·	
	3.0	87	0.3300	0.48		Sheet Flow, SHT 1	
						Grass: Short n= 0.150 P2= 2.83"	
	3.6	610	0.0350	2.81		Shallow Concentrated Flow, SCF 1	
						Grassed Waterway Kv= 15.0 fps	
	0.7	135	0.0420	3.07		Shallow Concentrated Flow, SCF 2	
						Grassed Waterway Kv= 15.0 fps	
	7.3	832	Total			•	

Subcatchment 8S: DRAINAGE AREA TO CULVERT 4





Not to be used for Box Culverts

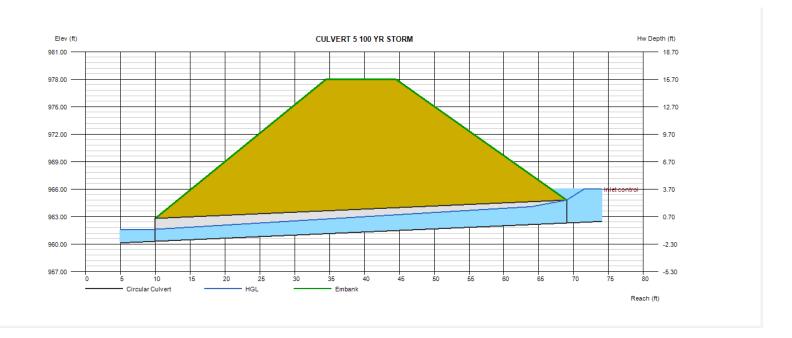
Culvert Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Monday, Sep 26 2016

CULVERT 5 100 YR STORM

Invert Elev Dn (ft)	= 960.30	Calculations	
Pipe Length (ft)	= 59.00	Qmin (cfs)	= 35.40
Slope (%)	= 3.39	Qmax (cfs)	= 35.40
Invert Elev Up (ft)	= 962.30	Tailwater Elev (ft)	= 0.00
Rise (in)	= 30.0		
Shape	= Circular	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 35.40
No. Barrels	= 1	Qpipe (cfs)	= 35.40
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	Circular Concrete	Veloc Dn (ft/s)	= 13.57
Culvert Entrance	Square edge w/headwall (C)	Veloc Up (ft/s)	= 8.34
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 961.61
		HGL Up (ft)	= 964.32
Embankment		Hw Elev (ft)	= 966.00
Top Elevation (ft)	= 978.00	Hw/D (ft)	= 1.48
Top Width (ft)	= 10.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



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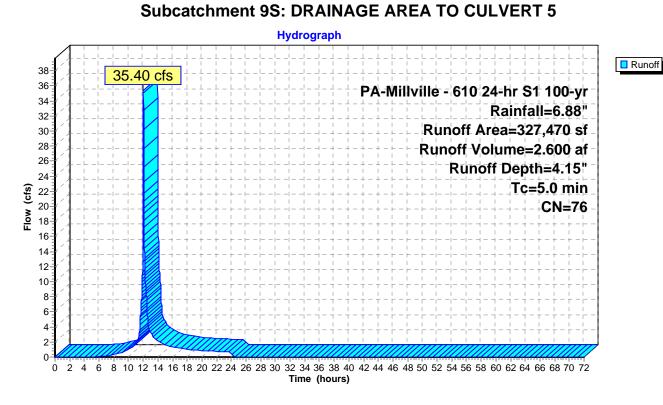
Page 1

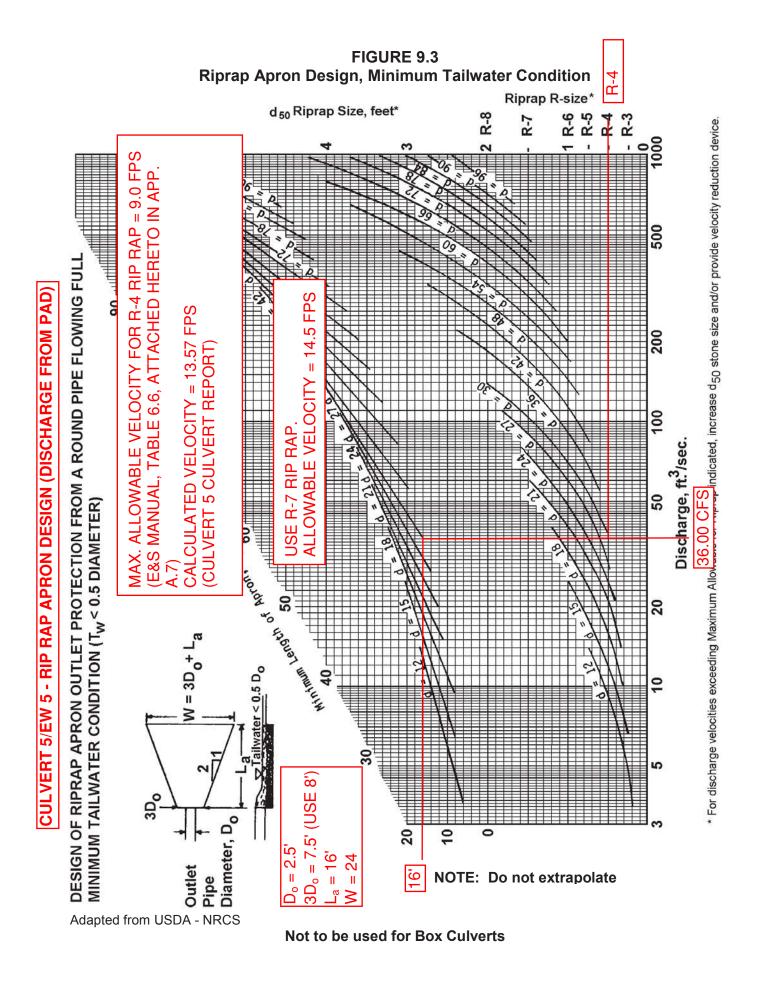
Summary for Subcatchment 9S: DRAINAGE AREA TO CULVERT 5

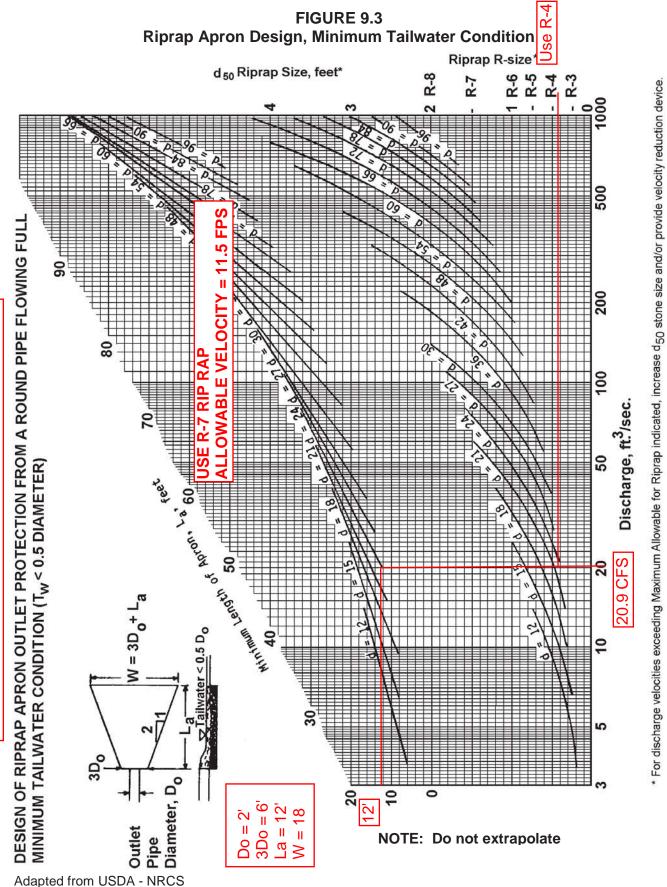
Runoff = 35.40 cfs @ 12.03 hrs, Volume= 2.600 af, Depth= 4.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs PA-Millville - 610 24-hr S1 100-yr Rainfall=6.88"

	Α	rea (sf)	CN	Description				
	1	66,277	85	Gravel road	ls, HSG B			
*		34,702	98	Impervious,	HSG B			
	1	26,491	58	Meadow, no	on-grazed,	HSG B		
	3	327,470	76 Weighted Average					
	2	292,768		89.40% Pervious Area				
		34,702		10.60% Imp	ervious Ar	ea		
	Тс	Length	Slope	,	Capacity	Description		
	(min)	(feet)	(ft/ft) (ft/sec)	(cfs)			
	5.0					Direct Entry,		







Not to be used for Box Culverts



A.4 PCSM BMP Calculations

E&S WORKSHEET #11

Channel Design Data

PROJECT NAME: <u>ATLANTIC SUNRISE PROJEC</u>	T - COMPRESSOR STATION 610
LOCATION: ORANGE TOWNSHIP, COLUMBIA C	OUNTY, PENNSYLVANIA
PREPARED BY: AOE	DATE: <u>08/17/2015</u>
OLIFOKED DV	DATE: 00/47/0045

CHECKED BY: AJB			DATE: _	<u>08/17/2015</u>	
CHANNEL OR CHANNEL SECTION		EMERGENCY SPILLWAY LINING/GRASS			
TEMPORARY OR PERMANENT?	(T OR P)	Р			
DESIGN STORM	(2, 5, OR 10 YR)	100			
ACRES	(AC)	NA			
MULTIPLIER ¹ (*	1.6, 2.25, or 2.75) ¹	NA			
Qr (REQUIRED CAPACITY)	(CFS)	15.66			
Q (CALCULATED AT FLOW DEPTH d)	(CFS)	16.20			
PROTECTIVE LINING ²		GRASS/ W3000			
n (MANNING'S COEFFICIENT) ²		0.085			
Va (ALLOWABLE VELOCITY)	(FPS)	N/A			
V (CALCULATED AT FLOW DEPTH d)	(FPS)	3.95			
та (MAX ALLOWABLE SHEAR STRESS)	(LB/FT ²)	16.00			
тd (CALC'D SHEAR STRESS AT FLOW DEF	PTH d) (LB/FT ²)	5.35			
CHANNEL BOTTOM WIDTH	(FT)	15			
CHANNEL SIDE SLOPES	(H:V)	3			
D (TOTAL DEPTH)	(FT)	1.3			
CHANNEL TOP WIDTH @ D	(FT)	22.5			
d (CALCULATED FLOW DEPTH)	(FT)	0.26			
CHANNEL TOP WIDTH @ FLOW DEPTH d	(FT)	16.56			
BOTTOM WIDTH: FLOW DEPTH RATIO	(12:1 MAX)	57.69			
d50 STONE SIZE	(IN)	N/A			
A (CROSS-SECTIONAL AREA)	(SQ. FT.)	4.10			
R (HYDRAULIC RADIUS)		0.25			
S (BED SLOPE) ³	(FT/FT)	0.33			
Sc (CRITICAL SLOPE)	(FT/FT)	0.169			
.7Sc	(FT/FT)	0.118			
1.3Sc	(FT/FT)	0.219			
STABLE FLOW?	(Y/N)	Y			
FREEBOARD BASED ON UNSTABLE FLOW	V (FT)	0.08			
FREEBOARD BASED ON STABLE FLOW	(FT)	0.50			
MINIMUM REQUIRED FREEBOARD ⁴	(FT)	0.50			
DESIGN METHOD FOR PROTECTIVE LINII PERMISSIBLE VELOCITY (V) OR SHEAR S		S			

^{1.} Use 1.6 for Temporary Channels; 2.25 for Temporary Channels in Special Protection (HQ or EV) Watersheds; 2.75 for Permanent Channels. For Rational Method, enter "N/A" and attach E&S Worksheets 9 and 10. For TR-55 enter "N/A" and attach appropriate Worksheets.

Source: 363-2134-008 / March 31, 2012 / Page 382

^{2.} Adjust "n" value for changes in channel liner and flow depth. For vegetated channels, provide data for manufactured linings without vegetation and with vegetation in separate columns.

^{3.} Slopes may not be averaged.

^{4.} Minimum Freeboard is 0.5 ft. or 1/4 Total Channel Depth, whichever is greater

^{5.} Permissible velocity lining design method is not acceptable for channels with a bed slope of 10% or greater. Shear stress lining design method is required for channels with a bed slope of 10% or greater. Shear stress lining design method may be used for any channel bed slope.

Weir Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Tuesday, Aug 18 2015

BASIN 1 EMERGENCY SPILLWAY WEIR - 100 YR DISCHARGE

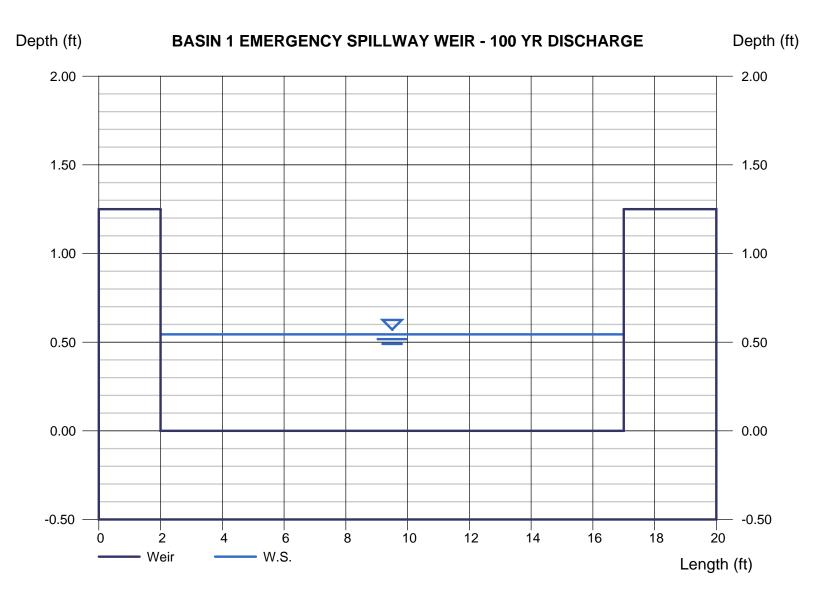
Rectangular Weir
Crest = Broad
Bottom Length (ft) = 15.00

Total Depth (ft) = 1.25

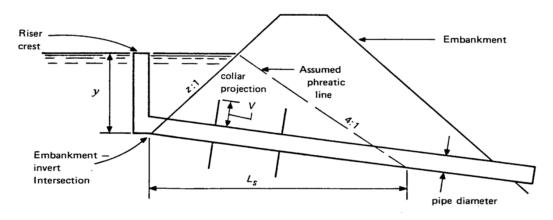
Calculations

Weir Coeff. Cw = 2.60 Compute by: Known Q Known Q (cfs) = 15.66 Highlighted

Depth (ft) = 0.54 Q (cfs) = 15.66 Area (sqft) = 8.16 Velocity (ft/s) = 1.92 Top Width (ft) = 15.00



WORKSHEET #18 Anti-seep Collar Design

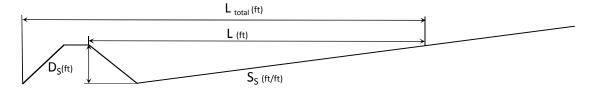


BASIN NO.	TEMP. OR PERM.	Y (FT)	z	Ls (FT)	Lf (FT)	V (IN)	BARRELL DIA. (IN)	COLLAR SIZE (IN)	NO. COLLARS	COLLAR SPACING (FT)	DISTANCE TO 1 ST COLLAR (FT)
1	Р	5.49	3	48	55.2	22	24	68	2	10	15

Source: 363-2134-008 / March 31, 2012 / Page 389

ATLANTIC SUNRISE NATURAL GAS PIPELINE PROJECT COMPRESSOR STATION 610 VEGETATED SWALE INFILTRATION VOLUME ROCK FILTER VOLUME AND SPACING

Per the Pennsylvania Stormwater BMP Manual (pg 94), the minimum spacing of rock filter is determined by the length of the storage volume (L). The length of the storage volume is calculated by dividing the height of the rock filter (D_S) by the slope of the channel (S_S):



$$L = D_S/S_S$$

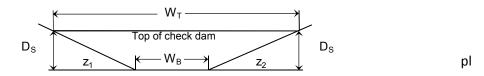
Where:

L = Storage Length

S_S = Channel slope

D_S = Height of the rock filter

The volume of runoff that will be stored upstream of a rock filter is dependent on the height of the check dam, the slope of the upstream channel and the dimensions of the upstream channel. The storage volume (V_S) can be calculated with:



$$V_S = 0.25 \times L \times D_S \times (W_T + W_B)$$

Where:

L = Storage Length

D_S = Height of rock filter

 W_T = rock filter top width

 W_B = rock filter bottom width

The rock filter top width (W_T) is given by:

$$W_T = W_B + z_1 + z_2$$

Where: $W_B = \text{rock filter bottom width}$

 z_1 = side slope

 z_2 = side slope

ATLANTIC SUNRISE PROJECT COMPRESSOR STATION 610 VEGETATED SWALE INFILTRATION VOLUME

5/29/2015

TOTAL REACH VOLUME = 1,879 CF

TOTAL REACH AREA = 1,843 SF

VEGETATED SWALE 1- 6.	3% VEGETATED	SWALE 1 - 3.6%	VEGETATED SWALE 1 - 0.57%
Input data	Input data		Input data
S = 0.063 ft/ft	S =	0.036 ft/ft	S = 0.057 ft/ft
H = 1 ft	H =	1 ft	H = 1 ft
$W_B = 2$	$W_B =$	2	$W_B = 2$
$z_1 = 3$	z ₁ =	3	z ₁ = 3
z ₂ = 3	z ₂ =	3	z ₂ = 3
Output data	Output data	1	Output data
L = 16 ft	L =	28 ft	L= 18 ft
$L_{total} = 21$ ft	$L_{total} =$	33 ft	$L_{total} = 23$ ft
$W_T = 8$ ft	$W_T =$	8 ft	$W_T = 8$ ft
$W_T + W_B = 10$ ft	$W_T + W_B =$	10 ft	$W_T + W_B = 10$ ft
V = 40 cf	V =	69 cf	V = 44 cf
No. of check dams =	3 No. of che	eck dams = 4	No. of check dams = 4
Subreach Volume =	119 CF Subreach	volume = 278 CF	Subreach Volume = 175 CF

Sub Reach Area = 262 SF

Sub Reach Area = 180 SF

VEGETATED SWALE 2

Input data

S = 0.044 ft/ft

Sub Reach Area =

125 SF

H = 1 ft

 $W_B = 2$

 $z_1 = 3$

 $z_2 = 3$

Output data

L = 23 ft

 $L_{total} = 28$ ft

 $W_T = 8$ ft

 $W_T + W_B = 10$ ft

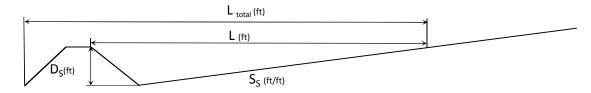
V = 57 cf

No. of check dams = 23 Subreach Volume = 1,307 CF

Sub Reach Area = 1,275 SF

ATLANTIC SUNRISE NATURAL GAS PIPELINE PROJECT COMPRESSOR STATION 610 VEGETATED SWALE INFILTRATION VOLUME ROCK FILTER VOLUME AND SPACING

Per the Pennsylvania Stormwater BMP Manual (pg 94), the minimum spacing of rock filter is determined by the length of the storage volume (L). The length of the storage volume is calculated by dividing the height of the rock filter (D_S) by the slope of the channel (S_S):



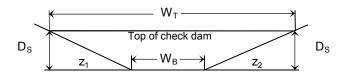
$$L = D_S/S_S$$

Where: L = Storage Length

S_S = Channel slope

D_S = Height of the rock filter

The volume of runoff that will be stored upstream of a rock filter is dependent on the height of the check dam, the slope of the upstream channel and the dimensions of the upstream channel. The storage volume (V_S) can be calculated with:



$$V_S = 0.25 \times L \times D_S \times (W_T + W_B)$$

Where:

L = Storage Length

 D_S = Height of rock filter

 W_T = rock filter top width

 W_B = rock filter bottom width

The rock filter top width (W_T) is given by:

$$W_T = W_B + z_1 + z_2$$

Where: $W_B = \text{rock filter bottom width}$

 z_1 = side slope

 z_2 = side slope



INFILTRATION RATE/DEWATERING TIME

Note: the infiltration tests were performed with a double ring infiltrometer. Therefore, no reduction factors were applied.

INFILTRATION BASIN 1

Note: Due to the slopes on site, there is variation in the elevation of the infiltration testing. However, the depth to the limiting layer and the infiltration rates at the various test locations are similar. It follows that the infiltration rates and depth to limiting layers are also similar at the locations of the infiltration areas that are in close proximity to the test pit and infiltration locations. Therefore, the average infiltration rates at the closest test pits are used for the dewatering calulations for the infiltration berms and basin.

INFILTRATION BASIN 1 AND INFILTRATION BERM 1

Test pit 1	3.63	in/hr	<u>Limiting Layer</u>
Test pit 2	3.63	in/hr	The limiting layer is 36 inches deep in the area of
Test pit 3	1.25	in/hr	Infiltration Basin 1. Therefore, the cut in this area is
Average	2.83	in/hr	held to 1' depth.
Safety factor	3.50		
Adjusted rate	0.81	in/hr	

Dewatering time

Infiltration depth	24	in
Dewatering time	29.6	hr

INFILTRATION BERM 2 & 3

Infiltration Rate

Test pit 4	5.25	in/hr	<u>Limiting Layer</u>
Test pit 5	1.06	in/hr	The limiting layer is 27 inches deep in the area of
Average	3.16	in/hr	Infiltration Berms 2 and 3. Therefore, the infiltration
Safety factor	3.00		area is at the existing ground surface.
Adjusted rate	1.05	in/hr	4.04.04.05.05.05.05.05.05.05.05.05.05.05.05.05.

Dewatering time

Infiltration depth	24	in
Dewatering time	22.8	hr



COMPRESSOR STATION 610 INFILTRATION BASIN OUTLET STRUCTURE FLOTATION CALCULATIONS

Assumptions

24" X 48" concrete inlet box riser

Total area of 24" x 48" inlet box = 10 sf

6" concrete wall thickness

6" thick bottom

Density of water = 62.4 lb/cf

Density of concrete = 150 lb/cf

Area of concrete in a 2' X 4' inlet box with a 6" thick wall = 3.5 sf

Volume of concrete per vertical foot of inlet box = $1' \times 3.5 \text{ sf} = 3.5 \text{ cf}$.

Weight of concrete per vertical foot of inlet box = 3.5 cf X 150 lb/cf = 525 Lbs

Buoyant force from water per vertical foot of inlet box = 62.4lb/cf X 10 sf X 1 ft = 624 lb.

Volume of bottom of inlet = 10 sf X 0.5 ft = 5 cf

Weight of bottom of inlet = 150 lb/cf X 5 cf = 750 lb

Buoyant force on bottom of inlet = 62.4 lb/cf X 5 = 312 lb

CS 610 outlet structure height = 5.25 ft

Weight of outlet structure = 5.25 X 525 + 750 = 3,506 lb

Buoyant force = 312 + 624 X 5.25 = 3,588 lb

Weight of outlet structure with 6 inches of concrete below invert:

 $3,506 + 10 \times 150 = 5,006 \text{ lb}$ OK

ATLANTIC SUNRISE PROJECT COMPRESSOR STATION 610 INFILTRATION VOLUME

9/23/2016

BASIN 1

Elevation	Surface Area (S.F.)	Inc. Storage (C.F.)	Cumulative Storage (C.F.)
954	7235	0	0
956	22706	29941	29941
958	36022	58728	88669
960	44212	80234	168903

BERM 1

Elevation	Surface Area (S.F.)	Inc. Storage (C.F.)	Cumulative Storage (C.F.)		
958	2915	0	0		
960	17103	20018	20018		
960.25	20894	4750	24768		

BERM 2

Elevation	Surface Area (S.F.)	Inc. Storage (C.F.)	Cumulative Storage (C.F.)
959.75	0	0	0
960	767	96	96
962	7220	7987	8083

RUNOFF VOLUME FOR 2-YR STORM EVENT

PROJECT: Atlantic Sunrise Project - Compressor Station 610- Deer Lick Run

DA: Infiltration Berm 1

2-Year Rainfall: 2.83 in

Total Contributing Area: 4.95 acres

Developed Conditions:

Cover Type	Soil Type	Area (sf)	Area (ac)	CN	S	la (0.2*S)	Q Runoff ¹ (in)	Runoff Volume ² (ft ³)
Grass	В	290,980.00	6.68	61	6.39	1.28	0.30	7,345
Meadow	В	154,725.00	3.55	58	7.24	1.45	0.22	2,855
Impervious	В	179,292.00	4.12	98	0.20	0.04	2.60	38,832
Gravel Road	В	286,581.00	6.58	85	1.76	0.35	1.45	34,546
TOTAL:		911,578.00	20.93					83,577

Berm 1 Available Volume (ft ³)	24,768
Actual 2-Year Volume runoff (ft ³)	83,577

If 2-Year Volume Runnoff is less than Available Berm Volume, use 2-year volume in Worksheet 5

1. Runoff (in) = Q = $(P - 0.2S)^2 / (P + 0.8S)$ where

P = 2-Year Rainfall (in)

S = (1000/CN)-10

2. Runoff Volume (CF) = Q x Area x 1/12

Q = Runoff (in)

Area = Land use area (sq. ft.)

Note: Runoff Volume must be calculated for EACH land use type/condition and HSGI. The use of a weighted CN value for volume calculations is not acceptable.

RUNOFF VOLUME FOR 2-YR STORM EVENT

PROJECT: Atlantic Sunrise Project - Compressor Station 610- Deer Lick Run

DA: Infiltration Berm 2

2-Year Rainfall: 2.83 in

Total Contributing Area: 4.95 acres

Developed Conditions:

Cover Type	Soil Type	Area (sf)	Area (ac)	CN	s	la (0.2*S)	Q Runoff ¹ (in)	Runoff Volume ² (ft ³)
Grass	В	-	0.00	61	6.39	1.28	0.30	-
Meadow	В	215,529.00	4.95	58	7.24	1.45	0.22	3,977
Impervious	В	-	0.00	98	0.20	0.04	2.60	-
Gravel Road	В	-	0.00	85	1.76	0.35	1.45	-
TOTAL:		215,529.00	4.95					3,977

Berm 2 Available Volume (ft ³)	8,083
Actual 2-Year Volume runoff (ft ³)	3,977

If 2-Year Volume Runnoff is less than Available Berm Volume, use 2-year volume in Worksheet 5

1. Runoff (in) = Q = $(P - 0.2S)^2 / (P + 0.8S)$ where

P = 2-Year Rainfall (in)

S = (1000/CN)-10

2. Runoff Volume (CF) = Q x Area x 1/12

Q = Runoff (in)

Area = Land use area (sq. ft.)

Note: Runoff Volume must be calculated for EACH land use type/condition and HSGI. The use of a weighted CN value for volume calculations is not acceptable.

Criteria and Credits for BMP 5.4.1 Protect Sensitive/Special Value Features

To receive credit, the proposed areas:

☑ Shall include natural areas of floodplains, mapped wetlands, mapped woodlands, and natural slopes over 15% and 25%.
 ☐ May include other areas of significant natural resources that the applicant demonstrates are of special natural value. N/A
 ☑ Shall not be disturbed during project construction (i.e., cleared or graded) except for temporary impacts associated with mitigation and reforestation efforts. Utility disturbance is discouraged and should be kept to a minimum.
 ☑ Shall be protected by having the limits of disturbance clearly shown on all construction drawings and delineated in the field.
 ☑ Shall be located within an acceptable land preservation/protection agreement or other enforceable instrument, such as a deed restriction, that ensures perpetual protection of the proposed areas. The preservation agreement shall clearly specify how the natural area shall be managed and boundaries will be marked with permanent survey markers.
 ☑ Managed turf is not considered an acceptable form of vegetation management.

CREDITS

Volume and Quality

Protected Area is not to be included in Runoff Volume calculation

Stormwater Management Area = (Total Area – Protected Area)

Peak Rate and Channel Protection

Shall be located on the development project.

Runoff from the Protected Area may be excluded from Peak Rate calculations and Channel Protection calculations for rate control, provided that the runoff from the protected area is not conveyed to and/or through stormwater management control structures. If necessary, runoff from Protected Areas should be directed around BMPs and stormwater pipes and inlets by means of vegetated swales or low berms that direct flow to natural drainage ways.

Criteria and Credits for BMP 5.6.2 Minimize Soil Compaction in Disturbed Areas

To receive credit, areas of Minimal Soil Compaction must meet the following criteria:

Area shall NOT be stripped of existing topso	X	Area shal	I NOT	be stripp	ed of exi	isting to	psoil
----------------------------------------------	---	-----------	-------	-----------	-----------	-----------	-------

- Area shall not be subject to excessive equipment movement. Vehicles movement, storage, or equipment/material laydown shall not be permitted in areas of Minimized Disturbance/Grading.
- The area shall be protected by having the limits of disturbance and access clearly shown on the Stormwater Management Plan, all construction drawings and delineated in the field.
- \square The use of soil amendments and additional topsoil is permitted. Light grading may be done with tracked vehicles that prevent compaction. $_{N/A}$
- ☑ Lawn and turf grass are acceptable uses. Planted Meadow is an encouraged use.
- Area shall be located on the development project.

CREDITS

Volume and Quality

A Volume Reduction may be credited based upon the area of Minimal Soil Compaction.

For Lawn Areas:

Volume Reduction (ft3) = Area of Min. Soil Compaction (ft2) x 1/4" / 12

For Meadow Areas:

Volume Reduction (ft³) = Area of Min. Soil Compaction (ft²) \times 1/3" / 12

Note: The applicant may request a greater volume credit if calculations support a greater numerical value to Minimizing Soil Compaction.

Peak Rate and Channel Protection

The Peak Rate for flood protection and channel protection will be reduced by the reduction in runoff volume provided above.

Criteria and Credits for BMP 5.8.2 Disconnection from Storm Sewers

To receive credit, the following must be met: Runoff from the non-rooftop impervious cover shall be directed to pervious areas where it is infiltrated into the soil. May include Vegetated Swales as outlined in BMP 6.8. May include check dams, low berms, native vegetation, and limited grading to improve natural drainage features. Shall be designed such that flows after development are non-erosive. ☐ Shall be protected from compaction or unintended disturbance during construction by having the limits of disturbance clearly shown on all construction drawings and delineated in the field. N/A Shall be noted on stormwater management plans as part of stormwater management system and included in any municipal easement requirements for stormwater systems. ☑ Shall be located on the development project. ☑ Runoff cannot originate from a designated hotspot. The maximum contributing impervious flow path length shall be 75 feet. The disconnection shall drain continuously through a vegetated swale or filter strip, or planted area to the property line or BMP. The length of the disconnection area must be at the least the length of the contributing area. The entire vegetated "disconnection" area shall have a maximum slope of 5%. The contributing impervious area to any one discharge point shall not exceed 1000 ft². ☐ Disconnections are encouraged on relatively well-draining soils (HSG A & B). ☐ If the site cannot meet the required disconnect length, a level-spreading device, recharge garden, infiltration trench, or other storage device may be needed for compensation.

CREDITS

Volume and Quality

Volume Reduction (ft³) = Contributing Impervious Area (ft²) x 1/4" / 12

Note: A greater volume credit may be requested by the applicant if calculations support a greater numerical value to Minimizing Soil Compaction.

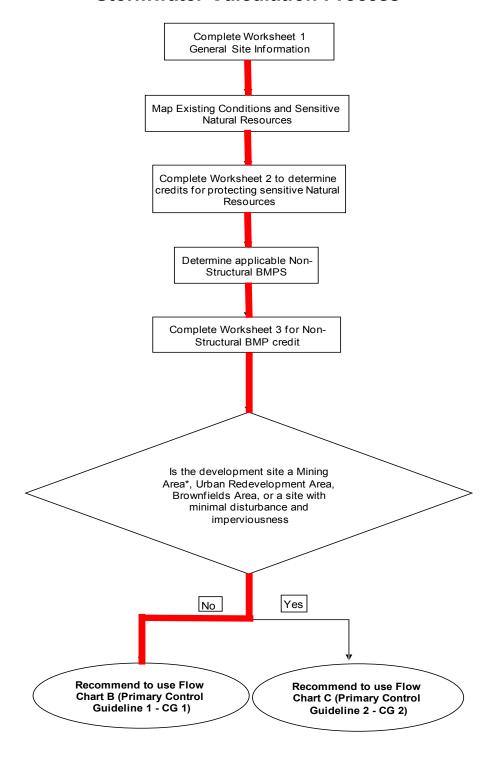
Peak Rate and Channel Protection

The Peak Rate for flood protection and channel protection will be reduced by the reduction in runoff volume provided above.



A.5 Water Quality Worksheets

FLOW CHART A (Green Creek POI) Stormwater Calculation Process



	Worksheet 1. General Site Information	,	
RUCTIONS: Fill out Wo	rksheet 1 for each watershed		
Date:	25-Oct-15		_
Project Name:	Atlantic Sunrise Project - Compressor Station 610 - Green Cr	reek	_
Municipality:	Orange Township		_
County:	Columbia County		_
Total Area (acres):	13.36		
Major River Basin:	Susquehanna River		_
	pa.us/dep/depupdate/watermgt/wc/default.htm#newtopics		
Watershed:	Fishing Creek - Columbia Co.		_
Sub-Basin:	Green Creek		_
-			
Nearest Surface Wa		ek	_
Nearest Surface Wa Chapter 93 - Design http://www.pacode.co	nated Water Use: pm/secure/data/025/chapter93/chap93toc.html g to Chapter 303(d) List?	Yes	
Nearest Surface Wa Chapter 93 - Design http://www.pacode.co	nated Water Use: pm/secure/data/025/chapter93/chap93toc.html g to Chapter 303(d) List? pa.us/dep/deputate/watermgt/wqp/wqstandards/303d-Report	Yes	X
Nearest Surface Watchest Surface Surfac	nated Water Use: pm/secure/data/025/chapter93/chap93toc.html g to Chapter 303(d) List? pa.us/dep/deputate/watermgt/wqp/wqstandards/303d-Report pairment: N/A n, or part of: g Storm Sewer System (MS4) Requirements? pa.us/dep/deputate/watermgt/wc/Subjects/Stormwate palPermits/default.htm I drinking water supply?	Yes	x x
Nearest Surface Watchest Surface	nated Water Use: Dem/secure/data/025/chapter93/chap93toc.html TSF	Yes rt.htn No Yes No Yes	X
Nearest Surface Watchest Surface Surfac	nated Water Use: Dem/secure/data/025/chapter93/chap93toc.html TSF	Yes rt.htn No Yes No Yes	X
Chapter 93 - Design http://www.pacode.co Impaired according http://www.dep.state. List Causes of Impaired subject to Municipal Separate http://www.dep.state.rManagement/General Existing or planned If yes, distance from Approved Act 167 P	nated Water Use: Dem/secure/data/025/chapter93/chap93toc.html	Yes rt.htn No Yes No Yes No	X
Chapter 93 - Design http://www.pacode.co Impaired according http://www.dep.state. List Causes of Impaired subject to Municipal Separate http://www.dep.state.rManagement/General Existing or planned If yes, distance from Approved Act 167 Phttp://www.dep.state.p	nated Water Use: Dem/secure/data/025/chapter93/chap93toc.html It o Chapter 303(d) List? Dea.us/dep/deputate/watermgt/wqp/wqstandards/303d-Report Deairment:	Yes rt.htn No Yes No Yes No Yes	X

Worksheet 2. Sensitive Natural Resources

INSTRUCTIONS: (Green Creek)

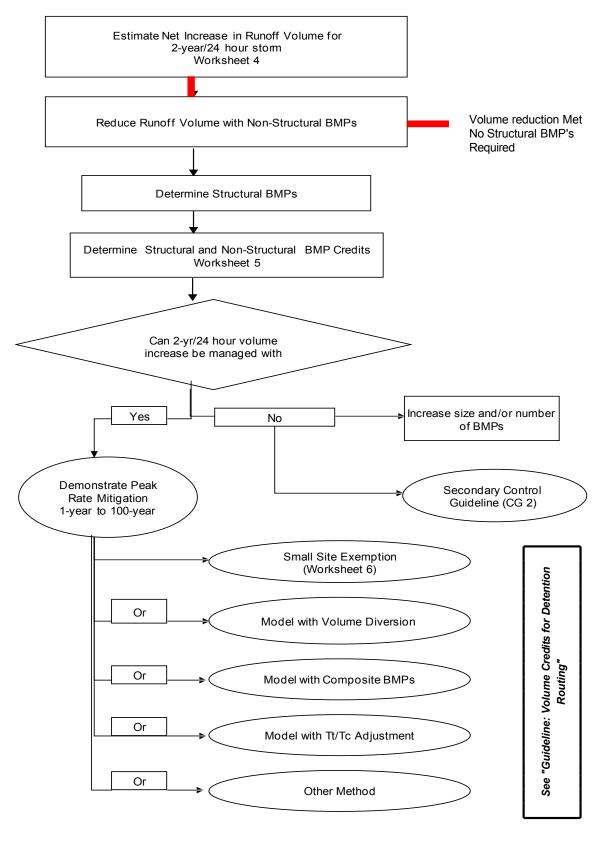
- 1. Provide Sensitive Resources Map according to non-structural BMP 5.4.1 in Chapter 5. This map should identify wetlands, woodlands, natural drainage ways, steep slopes, and other sensitive natural areas.
- 2. Summarize the existing extent of each sensitive resource in the Existing Sensitive Resources Table (below, using Acres). If none present, insert 0.
- 3. Summarize Total Protected Area as defined under BMPs in Chapter 5.
- 4. Do not count any area twice. For example, an area that is both a floodplain and a wetland may only be considered once.

NOTE: NO DEVELOPMENT WILL TAKE PLACE WITHIN THE

EXISTING NATURAL SENSITIVE RESOURCE	MAPPED? yes/no/n/a	TOTAL AREA (Ac.)	PROTECTED AREA (Ac.)
Waterbodies	N/A	0.00	0.00
Floodplains	N/A	0.00	0.00
Riparian Areas	N/A	0.00	0.00
Wetlands	Y	0.00	0.00
Woodlands	Y	5.63	5.63
Natural Drainage Ways	N/A	0.00	0.00
Steep Slopes, 15% - 25%	N/A	0.00	0.00
Steep Slopes, over 25%	N/A	0.00	0.00
Other:			
Other:			
TOTAL EXISTING:		5.63	5.63

1	Norksheet 3.	Nons	tructural B	MP Credits			
PROTECTED AREA (Green Cr	eek)						
1.1 Area of Protected Ser	nsitive/Spec	ial Valu	ie Feature	s (see WS 2)		5.63	Ac.
1.2 Area of Riparian Fore	est Buffer Pro	tection	1			-	Ac.
3.1 Area of Minimum Dis	turbance/Re	duced (Grading			-	Ac.
NOTE: NO DEVELOPM	ENT WILL	TAKE I	PLACE W	ITHIN THE			
GREEN CREEK WATER					TOTAL	5.63	Ac.
Site Area minu	Protected	=	Stormwat	er Managemer	nt Area]
13.36 -	Area	ר =		13.36			
	is the area that	_	_	13.30			
	stormwater mar		/	,]
VOLUME CREDITS	,						
3.1 Minimum Soil Compa							
Lawn	ft²	x 1/4"	x 1/12	=		0	_ft³
Meadow	ft²	x 1/3"	x 1/12	=			ft³
3.3 Protect Existing Trees	2						
For Trees within 100 fee		us area.	:				
Tree Canopy	ft ²		x 1/12	=			ft³
For Trees within 00 fee							-
For Trees within 20 feet Tree Canopy	t ot imperviou	s area:	x 1/12	=			ft³
пее Сапору			X 1/12	-			."
5.1 Disconnect Roof Lead	_						
For Runoff directed to a	•			5.8.2			_
Roof Area	ft²		x 1/12	=			_ft³
For all other disconnect	ted roof areas	;					
Roof Area	ft²		x 1/12	=			ft³
5 O Discours of New Deaf			4-41 4				-
5.2 Disconnect Non-Roof For Runoff directed to a	-	_					
Impervious Area	•		x 1/12	=		_	ft³
impervious Area	—"	X 1/3	X 1/12	_			٠''
For all other disconnect							
Impervious Area	ft²	x 1/4"	x 1/12	=			_ft³
							-
	TOTAL NO	ON-STR	UCTURAL	VOLUME CR	EDIT*		ft³
	* For use on	Workshe	eet 5				

FLOW CHART B (Green Creek POI) Control Guideline 1 Process



WORKSHEET 4. CHANGE IN RUNOFF VOLUME FOR 2-YR STORM EVENT

PROJECT: Atlantic Sunrise Project - Compressor Station 610 - Green Creek

DA: Green Creek

2-Year Rainfall: 2.83 in

Total Site Area:13.36acresProtected Site Area:5.63acresManaged Area7.73acres

Existing Conditions:

Cover Type	Soil Type	Area (sf)	Area (ac)	CN	S	la (0.2*S)	Q Runoff (in)	Runoff Volume ² (ft³)
Woods	В	-	0.00	55	8.18	1.64	0.15	-
Meadow	В	565,283.00	12.98	58	7.24	1.45	0.22	10,430
Meadow 20%	В	2,221.00	0.05	58	7.24	1.45	0.22	40.98
Impervious	В	8,885.00	0.20	98	0.20	0.04	2.60	1,924.36
TOTAL:		576,389.00	13.23					12,395

Developed Conditions:

Cover Type	Soil Type	Area (sf)	Area (ac)	CN	s	la (0.2*S)	Q Runoff (in)	Runoff Volume ² (ft³)
Woods	В	-	0.00	55	8.18	1.64	0.15	-
Meadow	В	325,614.00	7.48	58	7.24	1.45	0.22	6,008
Impervious	В	11,107.00	0.25	98	0.20	0.04	2.60	2,406
TOTAL:		336,721.00	7.73					8,413

2-Year Volume Increase (ft ³) (3,982)

2-Year Volume Increase = Developed Conditions Runoff Volume - Existing Conditions Runoff Volume

1. Runoff (in) = Q = $(P - 0.2S)^2 / (P + 0.8S)$ where

P = 2-Year Rainfall (in)

S = (1000/CN)-10

NOTE: NO DEVELOPMENT WILL TAKE PLACE WITHIN THE GREEN CREEK WATERSHED.

2. Runoff Volume (CF) = $Q \times Area \times 1/12$

Q = Runoff (in)

Area = Land use area (sq. ft.)

Note: Runoff Volume must be calculated for EACH land use type/condition and HSGI. The use of a weighted CN value for volume calculations is not acceptable.

WORKSHEET 5. STRUCTURAL BMP VOLUME CREDITS

PROJECT: SUB-BASIN:	Atlantic Sunrise Project - Compressor Station 610 - Green Creek						
Required	Control Volume (ft³) - from Worksheet 4:		(3,982)				
Non-structural		0					
	Structural Volume Reqmt (ft³)		(3,982)				
(Required Con	trol Volume minus Non-structural Credit)						

	Proposed BMP	Area (ft²)	Storage Volume (ft³)
6.4.1	Porous Pavement		
6.4.2	Infiltration Basin		
6.4.3	Infiltration Bed		
6.4.4	Infiltration Trench		
6.4.5	Rain Garden/Bioretention	NOTE: NO D	EVELOPMENT
6.4.6	Dry Well / Seepage Pit	WILL TAKE	PLACE WITHIN
6.4.7	Constructed Filter	THE GRE	EN CREEK
6.4.8	Vegetated Swale	WATE	RSHED.
6.4.9	Vegetated Filter Strip		
6.4.10	Berm		
6.5.1	Vegetated Roof		
6.5.2	Capture and Re-use		
6.6.1	Constructed Wetlands		
6.6.2	Wet Pond / Retention Basin		
6.6.3	Dry Extended Detention Basin		
6.6.4	Water Quality Filters		
6.7.1	Riparian Buffer Restoration		
6.7.2	Landscape Restoration / Reforestation		
6.7.3	Soil Amendment		
6.8.1	Level Spreader		
6.8.2	Special Storage Areas		
Other	Check Dams in Vegetated Swales		

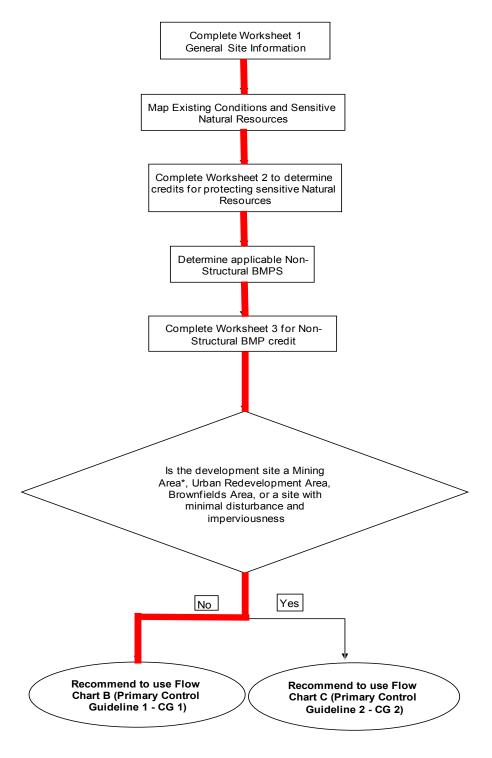
Total Structural Volume (ft³): 0
Structural Volume Requirement (ft³) -3,982

DIFFERENCE 3,982

	WORKSHEET 10. WATER QUALITY COMPLIAN	ICE FC	R NITR	ATE
achieved if at l	design incorporate the following BMPs to address nitrate pollution? least 2 Primary BMPs for nitrate are provided across the site or 4 sec ss the site (or the			
PRIMARY BMF	Ps FOR NITRATE:			
NS	S BMP 5.4.2 - Protect / Conserve / Enhance Riparian Buffers		YES	NO
NS.	S BMP 5.5.4 - Cluster Uses at Each Site			
NS	S BMP 5.6.1 - Minimize Total Disturbed Area			
NS	S BMP 5.6.3 - Re-Vegetate / Re-Forest Disturbed Areas (Native			
NS	S BMP 5.9.1 - Street Sweeping / Vacuuming			
St	tructural BMP 6.7.1 - Riparian Buffer Restoration			
St	tructural BMP 6.7.2 - Landscape Restoration			
SECONDARY	BMPs FOR NITRATE:	_	_	EVELOPMENT
	BMPs FOR NITRATE: S BMP 5.4.1 - Protect Sensitive / Special Value Features	WILL T	AKE PLA	EVELOPMENT ACE WITHIN THE (WATERSHED.
NS		WILL T	AKE PLA	CE WITHIN THE
NS NS	S BMP 5.4.1 - Protect Sensitive / Special Value Features	WILL T	AKE PLA	CE WITHIN THE
NS NS	S BMP 5.4.1 - Protect Sensitive / Special Value Features S BMP 5.4.3 - Protect / Utilize Natural Drainage Features	WILL T	AKE PLA	CE WITHIN THE
NS NS St	S BMP 5.4.1 - Protect Sensitive / Special Value Features S BMP 5.4.3 - Protect / Utilize Natural Drainage Features S BMP 5.6.2 - Minimize Soil Compaction	WILL T	AKE PLA	CE WITHIN THE
NS NS St	S BMP 5.4.1 - Protect Sensitive / Special Value Features S BMP 5.4.3 - Protect / Utilize Natural Drainage Features S BMP 5.6.2 - Minimize Soil Compaction tructural BMP 6.4.5 - Rain Garden / Bioretention	WILL T	AKE PLA	CE WITHIN THE
NS NS St St	S BMP 5.4.1 - Protect Sensitive / Special Value Features S BMP 5.4.3 - Protect / Utilize Natural Drainage Features S BMP 5.6.2 - Minimize Soil Compaction tructural BMP 6.4.5 - Rain Garden / Bioretention tructural BMP 6.4.8 - Vegetated Swale	WILL T	AKE PLA	CE WITHIN THE
NS NS St St St	S BMP 5.4.1 - Protect Sensitive / Special Value Features S BMP 5.4.3 - Protect / Utilize Natural Drainage Features S BMP 5.6.2 - Minimize Soil Compaction tructural BMP 6.4.5 - Rain Garden / Bioretention tructural BMP 6.4.8 - Vegetated Swale tructural BMP 6.4.9 - Vegetated Filter Strip	WILL T	AKE PLA	CE WITHIN THE
NS NS St St St St	S BMP 5.4.1 - Protect Sensitive / Special Value Features S BMP 5.4.3 - Protect / Utilize Natural Drainage Features S BMP 5.6.2 - Minimize Soil Compaction tructural BMP 6.4.5 - Rain Garden / Bioretention tructural BMP 6.4.8 - Vegetated Swale tructural BMP 6.4.9 - Vegetated Filter Strip	WILL T	AKE PLA	CE WITHIN THE

L

FLOW CHART A (Deer Lick Run POI) Stormwater Calculation Process



	Worksheet 1. General Site Information		
RUCTIONS: Fill out Wo	rksheet 1 for each watershed		
Date:	1-Jul-15		
Project Name:	Atlantic Sunrise Project - Compressor Station 610- Deer Lick	Run	_
Municipality:	Orange Township		_
County:	Columbia County		_
Total Area (acres):	25.85		
Major River Basin:	Susquehanna River		
http://www.dep.state.	pa.us/dep/depupdate/watermgt/wc/default.htm#newtopics		_
Watershed:	Fishing Creek - Columbia Co.	,	_
Sub-Basin:	Deer Lick Run		
_			
Nearest Surface Wa	ater(s) to Receive Runoff: UNTs to Deer Lick F	Run	
		Run	_
Chapter 93 - Design	nated Water Use: CWF	Run	_
Chapter 93 - Design		Run	_ _
Chapter 93 - Design	nated Water Use: CWF	Run	_ _ _
Chapter 93 - Design	nated Water Use: Dm/secure/data/025/chapter93/chap93toc.html	Yes	_ _ _ _ _ _ _
Chapter 93 - Design http://www.pacode.co	pated Water Use: CWF pm/secure/data/025/chapter93/chap93toc.html g to Chapter 303(d) List?	Yes	
Chapter 93 - Design http://www.pacode.co	nated Water Use: DM/secure/data/025/chapter93/chap93toc.html To Chapter 303(d) List? pa.us/dep/deputate/watermgt/wqp/wqstandards/303d-Report Dairment:	Yes	
Chapter 93 - Design http://www.pacode.co Impaired according http://www.dep.state.l List Causes of Imp	nated Water Use: cm/secure/data/025/chapter93/chap93toc.html g to Chapter 303(d) List? pa.us/dep/deputate/watermgt/wqp/wqstandards/303d-Report pairment: N/A n, or part of:	Yes r <u>t.htn</u> No	
Chapter 93 - Design http://www.pacode.co Impaired according http://www.dep.state. List Causes of Imp Is project subject to Municipal Separate	nated Water Use: Dem/secure/data/025/chapter93/chap93toc.html	Yes rt.htn No Yes	
Chapter 93 - Design http://www.pacode.co Impaired according http://www.dep.state. List Causes of Imp Is project subject to Municipal Separate	nated Water Use: Dem/secure/data/025/chapter93/chap93toc.html	Yes r <u>t.htn</u> No	
Chapter 93 - Design http://www.pacode.co Impaired according http://www.dep.state. List Causes of Imp Is project subject to Municipal Separate http://www.dep.state. rManagement/General	nated Water Use: Dem/secure/data/025/chapter93/chap93toc.html	Yes rt.htn No Yes	
Chapter 93 - Design http://www.pacode.co Impaired according http://www.dep.state. List Causes of Imp Is project subject to Municipal Separate http://www.dep.state. rManagement/General	nated Water Use: Dem/secure/data/025/chapter93/chap93toc.html	Yes rt.htn No Yes No	X
Chapter 93 - Design http://www.pacode.co Impaired according http://www.dep.state. List Causes of Imp Is project subject to Municipal Separate http://www.dep.state. rManagement/General Existing or planned	nated Water Use: Dem/secure/data/025/chapter93/chap93toc.html	Yes rt.htn No Yes No Yes	X
Chapter 93 - Design http://www.pacode.co Impaired according http://www.dep.state. List Causes of Imp Is project subject to Municipal Separate http://www.dep.state. rManagement/General Existing or planned	nated Water Use: Dem/secure/data/025/chapter93/chap93toc.html Dem/secure/data/0	Yes rt.htn No Yes No Yes	×
Chapter 93 - Design http://www.pacode.co Impaired according http://www.dep.state. List Causes of Imp Is project subject to Municipal Separate http://www.dep.state. rManagement/General Existing or planned If yes, distance from Approved Act 167 P	nated Water Use: Dem/secure/data/025/chapter93/chap93toc.html	Yes rt.htn No Yes No Yes No	×
Chapter 93 - Design http://www.pacode.co Impaired according http://www.dep.state. List Causes of Imp Is project subject to Municipal Separate http://www.dep.state. rManagement/General Existing or planned If yes, distance from Approved Act 167 P http://www.dep.state.p	nated Water Use: Dem/secure/data/025/chapter93/chap93toc.html It o Chapter 303(d) List? Dea.us/dep/deputate/watermgt/wqp/wqstandards/303d-Report Deairment:	Yes rt.htn No Yes No Yes No Yes	

Worksheet 2. Sensitive Natural Resources

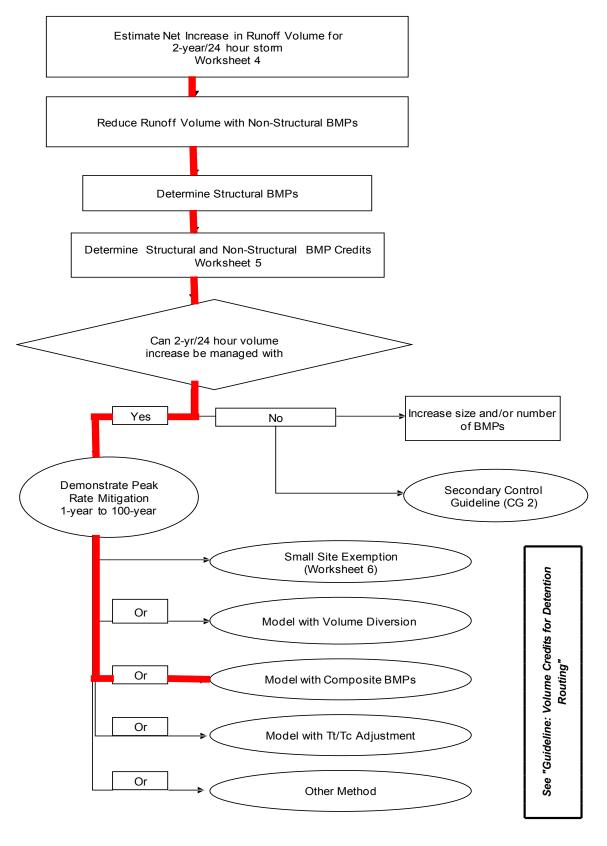
INSTRUCTIONS: (Deer Lick Run POI)

- 1. Provide Sensitive Resources Map according to non-structural BMP 5.4.1 in Chapter 5. This map should identify wetlands, woodlands, natural drainage ways, steep slopes, and other sensitive natural areas.
- 2. Summarize the existing extent of each sensitive resource in the Existing Sensitive Resources Table (below, using Acres). If none present, insert 0.
- 3. Summarize Total Protected Area as defined under BMPs in Chapter 5.
- 4. Do not count any area twice. For example, an area that is both a floodplain and a wetland may only be considered once.

EXISTING NATURAL SENSITIVE RESOURCE	MAPPED? yes/no/n/a	TOTAL AREA (Ac.)	PROTECTED AREA (Ac.)
Waterbodies	N/A	0.00	0.00
Floodplains	N/A	0.00	0.00
Riparian Areas	N/A	0.00	0.00
Wetlands	N/A	0.00	0.00
Woodlands	N/A	0.00	0.00
Natural Drainage Ways	N/A	0.00	0.00
Steep Slopes, 15% - 25%	N/A	0.00	0.00
Steep Slopes, over 25%	N/A	0.00	0.00
Other:			
Other:			
TOTAL EXISTING:		0.00	0.00

Worksheet 3. Nonstructural BMP Credits	
PROTECTED AREA (Deer Lick Run POI)	
1.1 Area of Protected Sensitive/Special Value Features (see WS 2)	5.41_Ac.
1.2 Area of Riparian Forest Buffer Protection	Ac.
3.1 Area of Minimum Disturbance/Reduced Grading	0.69_ Ac.
TOTAL	6.10_Ac.
Site Area minus Protected Area = Stormwater Management Area 25.85 = 25.85 This is the area that requires	ו
stormwater management /	
VOLUME CREDITS	
3.1 Minimum Soil Compaction	
Lawnft ² x 1/4" x 1/12 =	0ft³
Meadow 49725 ft ² x 1/3" x 1/12 =	1381ft³
3.3 Protect Existing Trees For Trees within 100 feet of impervious area: Tree Canopy ft ² x 1/12 =	ft³
For Trees within 20 feet of impervious area:	e.2
Tree Canopy x 1/12 =	ft³
5.1 Disconnect Roof Leaders to Vegetated Areas	
For Runoff directed to areas protected under 5.8.1 and 5.8.2	_
Roof Area ft ² x 1/12 =	ft³
For all other disconnected roof areas	
Roof Area ft ² x 1/4" x 1/12 =	ft³
5.2 Disconnect Non-Roof impervious to Vegetated Areas For Runoff directed to areas protected under 5.8.1 and 5.8.2	612
Impervious Area ft ² x 1/3" x 1/12 =	ft³
For all other disconnected roof areas	
Impervious Area 9125 ft^2 x 1/4" x 1/12 =	190ft³
TOTAL NON-STRUCTURAL VOLUME CREDIT*	1,571 ft ³
* For use on Worksheet 5	

FLOW CHART B (Deer Lick Run POI) Control Guideline 1 Process



WORKSHEET 4. CHANGE IN RUNOFF VOLUME FOR 2-YR STORM EVENT

PROJECT: Atlantic Sunrise Project - Compressor Station 610- Deer Lick Run

DA: Deer Lick Run

2-Year Rainfall: 2.83 in

Total Site Area:25.85acresProtected Site Area:0.00acresManaged Area25.85acres

Existing Conditions:

Cover Type	Soil Type	Area (sf)	Area (ac)	CN	s	la (0.2*S)	Q Runoff (in)	Runoff Volume ² (ft³)
Meadow	В	883,590.00	20.28	58	7.24	1.45	0.22	16,302
Impervious	В	6,503.00	0.15	98	0.20	0.04	2.60	1,408
TOTAL:		890,093.00	20.43					17,711

Developed Conditions:

Cayen Tyma	So:I	A ====	A ====	CNI	s	la la	Q Runoff	
Cover Type	Soil Type	Area (sf)	Area (ac)	CN	.	la (0.2*S)	(in)	Runoff Volume ² (ft³)
Grass	В	349,798.00	8.03	61	6.39	1.28	0.30	8,830
Meadow	В	351,890.00	8.08	58	7.24	1.45	0.22	6,492
Impervious	В	137,948.00	3.17	98	0.20	0.04	2.60	29,877
Gravel Road	В	286,581.00	6.58	85	1.76	0.35	1.45	34,546
TOTAL:		1,126,217.00	25.85					79,745

2-Year Volume Increase (ft ³) 62,03

2-Year Volume Increase = Developed Conditions Runoff Volume - Existing Conditions Runoff Volume

1. Runoff (in) = Q = $(P - 0.2S)^2 / (P + 0.8S)$ where

P = 2-Year Rainfall (in)

S = (1000/CN)-10

2. Runoff Volume (CF) = Q x Area x 1/12

Q = Runoff (in)

Area = Land use area (sq. ft.)

Note: Runoff Volume must be calculated for EACH land use type/condition and HSGI. The use of a weighted CN value for volume calculations is not acceptable.

WORKSHEET 5. STRUCTURAL BMP VOLUME CREDITS

PROJECT: SUB-BASIN:	Atlantic Sunrise Project - Compressor Station 610- Deer Lic	k Run	
	Required Control Volume (ft³) - from Worksheet 4:		62,034
No	n-structural Volume Credit (ft³) - from Worksheet 3:		1,571
	Structural Volume Reqmt (ft ³)		60,463
(Req	uired Control Volume minus Non-structural Credit)		

	Proposed BMP	Area (ft²)	Volume Reduction Permanently Removed (ft ³)
6.4.1	Porous Pavement		
6.4.2	Infiltration Basin	39,809	29,941
6.4.3	Infiltration Bed		
6.4.4	Infiltration Trench		
6.4.5	Rain Garden/Bioretention		
6.4.6	Dry Well / Seepage Pit		
6.4.7	Constructed Filter		
6.4.8	Vegetated Swale		
6.4.9	Vegetated Filter Strip		
6.4.10	Berm	34,611	28,745
6.5.1	Vegetated Roof		
6.5.2	Capture and Re-use		
6.6.1	Constructed Wetlands		
6.6.2	Wet Pond / Retention Basin		
6.7.1	Riparian Buffer/Riparian Forest Buffer Restoration		
6.7.2	Landscape Restoration / Reforestation		
6.7.3	Soil Amendment		
6.8.1	Level Spreader		
6.8.2	Special Storage Areas		
Other	Check Dams in Vegetated Swales	1,879	1,879

Total Structural Volume (ft³): 60,565
Structural Volume Requirement (ft³): 60,463

DIFFERENCE 102

WORKSHEET 10. WATER QUALITY COMPLIANCE FOR NITRATE

Does the site design incorporate the following BMPs to address nitrate pollution? A summary "yes" rating is

YES NO
X
X
X



A.6 Site Characterization Assessment



Field Observation Report

Project Number:	14C4909			
Project Name:	Atlantic Sunrise Project –	Compressor Sta	ation 610	
Date of Field Visit:	March 10, 2015			
Weather Conditions:	Overcast	Tem	perature:	Approximately 26-45°F
Prepared By:	Krystal Bealing, APSS an	d Joseph Kemp	f	
Copies of Report Ha	ve Been Sent To: 🛛 C	lient 🗌 Co	ontractor	Other
Client:		Contracto	r:	
Transcontinen Company, LL0	tal Gas Pipe Line		BL Com	panies rlisle Pike, Suite 260
2800 Post Oal				ill, PA 17011
Houston, TX 7	7251			

Five soil pits were excavated by backhoe and described to varying depths. Additionally, infiltration tests using the double ring infiltrometer method were conducted at each pit location, at depths ranging from 27 to 36 inches.

Infiltration testing did not appear to be hindered by weather conditions.

The test pit location map, soil profile descriptions, infiltration worksheet and photographs are attached. Determined limiting layer depths are listed below:

Pit #1: 60 inches deep, Limiting Layer observed at 36 inches

Infiltration conducted at 36 inches, Infiltration Rate = 22.594 inches/hour

Pit #2: 58 inches deep, Limiting Layer observed at 36 inches

Infiltration conducted at 36 inches, Infiltration Rate = 3.625 inches/hour

Pit #3: 59 inches deep, Limiting Layer observed at 30 inches

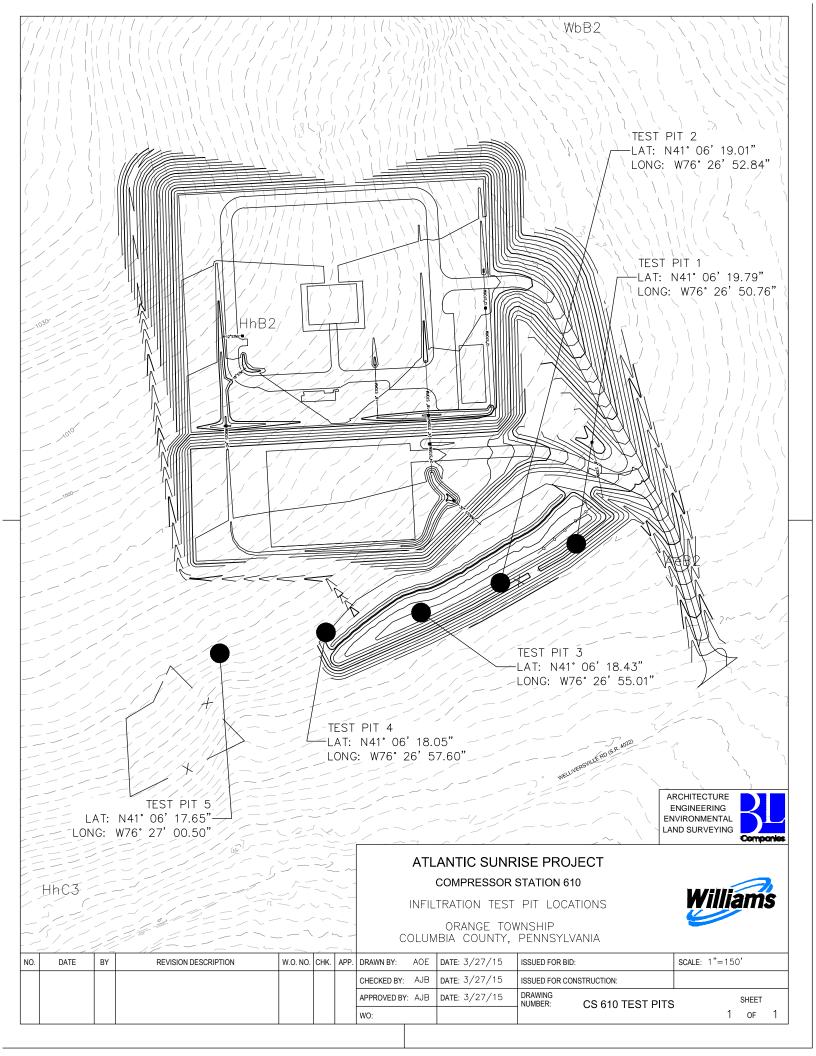
Infiltration conducted at 30 inches, Infiltration Rate = 1.250 inches/hour

Pit #4: 59 inches deep, Limiting Layer observed at 27 inches

Infiltration conducted 27 inches, Infiltration Rate = 5.250 inches/hour

Pit #5: 58 inches deep, Limiting Layer observed at 27 inches

Infiltration conducted at 27 inches, Infiltration Rate = 1.063 inches/hour



Project 14C4909-A Atlantic Sunrise Project - Compressor Station 610	Elevation 955 AMSL
Test Pit # 1	Soil Type Hartleton channery silt loam, 3-12% slopes
Name Krystal Bealing, APSS	Geology Trimmers Rock Formation
Date March 10, 2015	Landscape Position/Slope Hillslope bench, 0-3%
Weather 26-45°F; Overcast	Land Use Agriculture
Equipment Mini Excavator	Additional Comments Approximately 12" snow; Approximiately 6" frozen soil

Horizon	Upper Boundary (inches)	Lower Boundary (inches)	Soil Textural Class	Type, Size, Coarse Fragments, etc.	Soil Matrix Color	Color Patterns	Pores, Roots, Structure	Depth to Bedrock	Depth to Water	Comments
Ар	0	12	SiL	1	10YR 4/3	-	Roots present; Weak, Granular	-	1	-
Bt	12	36	SiL	15-35% Channery	7.5YR 4/6	-	Roots present; Weak, Subangular Blocky	1	-	-
С	36	60+	CL	35-60% Channery	5YR 5/8	-	Stong, Subangular Blocky	-	-	Limiting Layer - Restrictive Soil Horizon

Project 14C4909-A Atlantic Sunrise Project - Compressor Station 610

Test Pit # 2

Name Krystal Bealing, APSS

March 10, 2015

Weather 26-45°F; Overcast

Equipment Mini Excavator

Elevation 956 AMSL

Soil Type Hartleton channery silt loam, 3-12% slopes

Geology Trimmers Rock Formation

Landscape Position/Slope Hillslope bench, 0-3%

Land Use Agriculture

Additional Comments Approximately 12" snow; Approximiately 6" frozen soil

Horizon	Upper Boundary (inches)	Lower Boundary (inches)	Soil Textural Class	Type, Size, Coarse Fragments, etc.	Soil Matrix Color	Color Patterns	Pores, Roots, Structure	Depth to Bedrock	Depth to Water	Comments
Ар	0	13	SiL	-	10YR 4/3	-	Roots present; Weak, Granular	-	-	-
Bt	13	36	SiL	15-35% Channery	7.5YR 4/6	-	Roots present; Weak, Subangular Blocky	-	-	-
С	36	58+	CL	35-60% Channery	5YR 5/8	-	Stong, Subangular Blocky	-	-	Limiting Layer - Restrictive Soil Horizon

Project 14C4909-A Atlantic Sunrise Project - Compressor Station 610

Test Pit # 3

Name Krystal Bealing, APSS

March 10, 2015

Weather 26-45°F; Overcast

Equipment Mini Excavator

Elevation 959 AMSL

Bartleton channery silt loam, 3-12% slopes

Flat Bealing, APSS

Geology Trimmers Rock Formation

Landscape Position/Slope Hillslope bench, 0-3%

Land Use Agriculture

Additional Comments Approximately 12" snow; Approximiately 6" frozen soil

Horizon	Upper Boundary (inches)	Lower Boundary (inches)	Soil Textural Class	Type, Size, Coarse Fragments, etc.	Soil Matrix Color	Color Patterns	Pores, Roots, Structure	Depth to Bedrock	Depth to Water	Comments
Ар	0	12	SiL	-	10YR 4/3	-	Roots present; Weak, Granular	-	-	-
Bt	12	30	SiL	15-35% Channery	7.5YR 5/6	-	Roots present; Weak, Subangular Blocky	1	-	-
С	30	59+	CL	35-60% Channery	5YR 5/6	-	Stong, Subangular Blocky	-	-	Limiting Layer - Restrictive Soil Horizon

Project 14C4909-A Atlantic Sunrise Project - Compressor Station 610

Test Pit # 4

Name Krystal Bealing, APSS

March 10, 2015

Weather 26-45°F; Overcast

Equipment Mini Excavator

Flevation 964 AMSL

Soil Type Hartleton channery silt loam, 3-12% slopes

Geology Trimmers Rock Formation

Landscape Position/Slope Hillslope bench, 0-3%

Land Use Agriculture

Additional Comments Approximately 12" snow; Approximiately 6" frozen soil

Horizon	Upper Boundary (inches)	Lower Boundary (inches)	Soil Textural Class	Type, Size, Coarse Fragments, etc.	Soil Matrix Color	Color Patterns	Pores, Roots, Structure	Depth to Bedrock	Depth to Water	Comments
Ар	0	13	SiL	-	10YR 4/4	-	Roots present; Weak, Granular	-	-	-
Bt	13	27	SiL	15-35% Channery	7.5YR 5/6	-	Roots present; Weak, Subangular Blocky	1	-	-
С	27	59+	CL	35-60% Channery	5YR 5/8	-	Stong, Subangular Blocky	-	-	Limiting Layer - Restrictive Soil Horizon

Project 14C4909-A Atlantic Sunrise Project - Compressor Station 610

Test Pit # 5

Name Krystal Bealing, APSS

Date March 10, 2015

Weather 26-45°F; Overcast

Equipment Mini Excavator

Elevation 973 AMSL

Soil Type Hartleton channery silt loam, 3-12% slopes

Trimmers Rock Formation

Landscape Position/Slope Hillslope bench, 0-3%

Land Use Agriculture

Additional Comments Approximately 12" snow; Approximiately 6" frozen soil

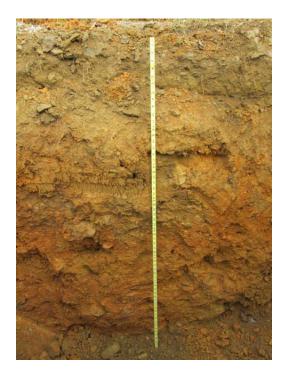
Horizon	Upper Boundary (inches)	Lower Boundary (inches)	Soil Textural Class	Type, Size, Coarse Fragments, etc.	Soil Matrix Color	Color Patterns	Pores, Roots, Structure	Depth to Bedrock	Depth to Water	Comments
Ар	0	12	SiL	-	10YR 4/3	-	Roots present; Weak, Granular	-	1	-
Bt	12	27	SiL	15-35% Channery	7.5YR 5/6	-	Roots present; Weak, Subangular Blocky	-	-	-
С	27	58+	CL	35-60% Channery	5YR 5/6	-	Stong, Subangular Blocky	-	-	Limiting Layer - Restrictive Soil Horizon

	ATLANTIC SUNRISE PROJECT - COMPRESSOR STATION 610												
				SOIL INI	FILTRATIO	N WORKS	HEET - DO	UBLE RIN	G INFILTR	OMETER	METHOD		
Hole Number	Drop >2 inches after 30 minute presoak? ¹	Reading Interval (minutes)	Reading 1 (Inches of Drop)	Reading 2 (Inches of Drop)	Reading 3 (Inches of Drop)	Reading 4 (Inches of Drop)	_	Reading 6 (Inches of Drop)	Reading 7 (Inches of Drop)	Reading 8 (Inches of Drop)	Average Stabilized Reading ² (Inches of Drop)	Infiltration Rate ³ (in/hr)	Comments
1	Yes	10	4.375	3.250	3.875	3.750	3.750	3.688			3.766	22.594	Approximately 26-45 degrees, overcast, approximately 12" snow cover. Frozen layer approximately 6" deep. Test done at 36" below surface.
2	No	30	1.500	1.750	1.875	1.875	1.750				1.813	3.625	Approximately 26-45 degrees, overcast, approximately 12" snow cover. Frozen layer approximately 6" deep. Test done at 36" below surface.
3	No	30	0.625	0.563	0.563	0.750					0.625	1.250	Approximately 26-45 degrees, overcast, approximately 12" snow cover. Frozen layer approximately 6" deep. Test done at 30" below surface.
4	Yes	10	0.875	0.875	0.750	1.000					0.875	5.250	Approximately 26-45 degrees, overcast, approximately 12" snow cover. Frozen layer approximately 6" deep. Test done at 27" below surface.
5	No	30	0.500	0.563	0.563	0.500					0.531	1.063	Approximately 26-45 degrees, overcast, approximately 12" snow cover. Frozen layer approximately 6" deep. Test done at 27" below surface.

¹Inches of drop greater than 2 inches after the 30 minute presoak? Yes, use 10 minute interval; No, use 30 minute interval.

²Calculated as the average of the last four stabilized (less than 0.25-inch difference overall) readings.

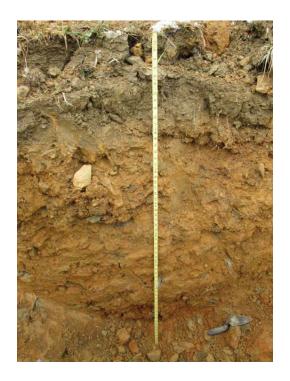
³Calculated as the average stabilized reading x 2 for 30 minute intervals; x 6 for 10 minute intervals.



View of Pit #1.



View of Pit #2.



View of Pit #3.



View of Pit #4.



View of Pit #5.



A.7 Supporting Documentation

TABLE 6.6
Riprap Gradation, Filter Blanket Requirements, Maximum Velocities

	Percent Passing (Square Openings)											
Class, Size NO.												
Rock Size (Inches)	R-8	R-7	R-6	R-5	R-4	R-3						
42	100											
30		100										
24	15-50		100									
18		15-50		100								
15	0-15											
12		0-15	15-50		100							
9				15-50								
6			0-15		15-50	100						
4				0-15								
3					0-15	15-50						
2						0-15						
Nominal Placement Thickness (inches)	63	45	36	27	18	9						
Filter	AASHTO #1	AASHTO #1	AASHTO #1	AASHTO #3	AASHTO #3	AASHTO #57						
V _{max} (ft/sec)	17.0	14.5	13.0	11.5	9.0	6.5						
Adapted from F	Adapted from PennDOT Pub. 408, Section 703.2(c), Table C											

¹ This is a general standard. Soil conditions at each site should be analyzed to determine actual filter size. A suitable woven or non-woven geotextile underlayment, used according to the manufacturer's recommendations, may be substituted for the filter stone for gradients < 10%.

TABLE 6.7
Comparison of Various Gradations of Coarse Aggregates

	Total Percent Passing														
AASHTO NUMBER	6 1/2	4"	3 ½"	2 1/2	2"	1 ½ "	1"	3/4 "	1/2"	3/8"	#4	#8	#16	#30	#100
1		100	90-100	25-60		0-15		0-5							
3				100	90-100	35-70	0-15		0-5						
5						100	90-100	20-55	0-10	0-5					
57						100	90-100		25-60		0-10	0-5			
67							100	90-100		20-55	0-10	0-5			
7								100	90-100	40-70	0-15	0-5			
8									100	85-100	10-30	0-10	0-5		
10										100	75-100				10-30

PennDOT Publication 408, Section 703.2(c), Table C

Tables 6.6 and 6.7 should be placed on the plan drawings of all sites where riprap channel linings are proposed.



NOAA Atlas 14, Volume 2, Version 3 Location name: Millville, Pennsylvania, US* Latitude: 41.1067°, Longitude: -76.4493° Elevation: 998 ft*

NORR

* source: Google Maps

POINT PRECIPITATION FREQUENCY ESTIMATES

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M.Yekta, and D. Riley NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

	PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹ Average recurrence interval (years)									
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	0.334	0.396	0.460	0.506 (0.457-0.559)	0.562	0.604	0.647 (0.579-0.715)	0.690	0.750	0.795
10-min	0.520	0.619	0.715	0.781 (0.706-0.863)	0.859	0.916 (0.823-1.01)	0.973 (0.872-1.08)	1.03 (0.918-1.14)	1.10 (0.977-1.23)	1.16 (1.02-1.29)
15-min	0.637	0.756	0.878 (0.793-0.971)	0.961 (0.868-1.06)	1.06 (0.956-1.17)	1.13 (1.02-1.25)	1.21 (1.08-1.34)	1.28 (1.14-1.42)	1.38 (1.22-1.53)	1.45 (1.27-1.62)
30-min	0.843 (0.762-0.930)	1.01 (0.917-1.12)	1.20 (1.09-1.33)	1.33 (1.21-1.48)	1.50 (1.35-1.66)	1.62 (1.46-1.79)	1.75 (1.56-1.93)	1.87 (1.67-2.07)	2.04 (1.81-2.27)	2.17 (1.91-2.42)
60-min	1.03 (0.930-1.14)	1.24 (1.13-1.37)	1.51 (1.36-1.67)	1.70 (1.53-1.88)	1.94 (1.75-2.15)	2.14 (1.92-2.36)	2.33 (2.09-2.58)	2.54 (2.26-2.81)	2.82 (2.50-3.14)	3.04 (2.68-3.40)
2-hr	1.19 (1.07-1.32)	1.44 (1.29-1.59)	1.76 (1.58-1.95)	2.02 (1.81-2.25)	2.41 (2.15-2.67)	2.73 (2.42-3.04)	3.10 (2.73-3.45)	3.51 (3.07-3.92)	4.13 (3.58-4.64)	4.67 (4.00-5.27)
3-hr	1.29 (1.16-1.45)	1.55 (1.40-1.73)	1.91 (1.71-2.14)	2.21 (1.98-2.47)	2.65 (2.36-2.96)	3.04 (2.69-3.40)	3.48 (3.05-3.90)	3.99 (3.46-4.47)	4.77 (4.07-5.37)	5.46 (4.60-6.18)
6-hr	1.62 (1.45-1.82)	1.94 (1.74-2.18)	2.37 (2.13-2.67)	2.75 (2.45-3.08)	3.30 (2.92-3.69)	3.78 (3.33-4.24)	4.33 (3.79-4.86)	4.96 (4.29-5.57)	5.93 (5.05-6.69)	6.80 (5.72-7.70)
12-hr	2.00 (1.79-2.26)	2.39 (2.15-2.71)	2.95 (2.64-3.33)	3.42 (3.05-3.85)	4.13 (3.65-4.64)	4.77 (4.18-5.36)	5.50 (4.78-6.18)	6.33 (5.44-7.13)	7.65 (6.47-8.66)	8.84 (7.36-10.1)
24-hr	2.36 (2.15-2.63)	2.83 (2.59-3.15)	3.51 (3.20-3.90)	4.10 (3.72-4.54)	5.03 (4.53-5.54)	5.88 (5.25-6.45)	6.88 (6.09-7.51)	8.06 (7.07-8.76)	9.96 (8.60-10.8)	11.7 (9.98-12.6)
2-day	2.78 (2.49-3.15)	3.33 (2.99-3.77)	4.11 (3.69-4.66)	4.80 (4.29-5.42)	5.89 (5.22-6.62)	6.88 (6.06-7.71)	8.05 (7.03-8.99)	9.43 (8.16-10.5)	11.7 (9.94-12.9)	13.7 (11.5-15.2)
3-day	2.95 (2.65-3.34)	3.53 (3.18-4.00)	4.34 (3.90-4.91)	5.05 (4.52-5.69)	6.16 (5.49-6.92)	7.18 (6.35-8.04)	8.38 (7.35-9.36)	9.79 (8.51-10.9)	12.1 (10.3-13.4)	14.2 (12.0-15.6)
4-day	3.13 (2.82-3.54)	3.73 (3.37-4.22)	4.56 (4.11-5.16)	5.29 (4.76-5.96)	6.44 (5.75-7.22)	7.49 (6.64-8.38)	8.72 (7.67-9.71)	10.2 (8.87-11.3)	12.5 (10.7-13.8)	14.6 (12.4-16.1)
7-day	3.67 (3.35-4.11)	4.38 (3.99-4.90)	5.31 (4.82-5.93)	6.12 (5.54-6.82)	7.37 (6.64-8.20)	8.51 (7.61-9.44)	9.83 (8.73-10.9)	11.4 (10.0-12.5)	13.8 (12.0-15.2)	16.0 (13.8-17.6)
10-day	4.24 (3.89-4.69)	5.04 (4.62-5.58)	6.04 (5.53-6.68)	6.91 (6.30-7.63)	8.23 (7.46-9.06)	9.41 (8.49-10.3)	10.8 (9.64-11.8)	12.3 (10.9-13.5)	14.7 (13.0-16.1)	16.9 (14.7-18.4)
20-day	5.79 (5.40-6.27)	6.83 (6.36-7.38)	7.98 (7.41-8.61)	8.96 (8.29-9.65)	10.4 (9.61-11.2)	11.7 (10.7-12.5)	13.1 (12.0-14.1)	14.7 (13.4-15.8)	17.1 (15.5-18.3)	19.2 (17.2-20.6)
30-day	7.21 (6.76-7.77)	8.45 (7.91-9.11)	9.72 (9.09-10.5)	10.8 (10.1-11.6)	12.3 (11.5-13.3)	13.7 (12.7-14.7)	15.2 (14.0-16.3)	16.8 (15.4-18.0)	19.2 (17.5-20.6)	21.2 (19.3-22.7)
45-day	9.12 (8.58-9.75)	10.6 (10.0-11.4)	12.0 (11.3-12.9)	13.2 (12.4-14.1)	14.9 (14.0-15.9)	16.3 (15.3-17.4)	17.9 (16.7-19.0)	19.5 (18.1-20.8)	21.9 (20.3-23.4)	23.9 (22.0-25.5)
60-day	11.0 (10.4-11.7)	12.8 (12.1-13.6)	14.3 (13.5-15.2)	15.6 (14.8-16.6)	17.5 (16.5-18.6)	19.1 (18.0-20.3)	20.8 (19.5-22.1)	22.6 (21.2-24.1)	25.3 (23.6-26.9)	27.4 (25.5-29.2)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

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PF graphical

Please refer to NOAA Atlas 14 document for more information.



APPENDIX B

Preparer Qualifications

STANDARD E&S WORKSHEET # 22 PLAN PREPARER RECORD OF TRAINING AND EXPERIENCE IN EROSION AND SEDIMENT POLLUTION CONTROL METHODS AND TECHNIQUES

NAME OF PLAN PRE	Alaric J. Bush	er, PE, CF	PESC			
FORMAL EDUCATIO						
Name of Colle	ge or Technical Institute	e: The Per	nnsylvania Sta	te University		
Curriculum or	Program: Civil Engineer	ring				
Dates of Atten		5	To:_	5/1999		
Degree Receiv	ved Bachelor of Science	- Civil Eng	gineering			
OTHER TRAINING: Name of Training:	Annual Oil and Gas Train	ning	Chapter 102 L the Regulated	Jpdate Training for Community		
Presented By:	PADEP		PADEP			
Date:	7/10/2013		11/12/2010			
EMPLOYMENT HIST Current Employer: Telephone:	ORY: BL Companies 717-651-9850					
Former Employer: Telephone:	N/A					
	S PREPARED: stitution Pipeline, Access Roads Meter Station (ES, PCSM)	Reynolds Al (E&S, PCSN	ford Pipeline //)	Annville Medical Office (E&S, PCSM)		
County:	Susquehanna	Susqueh	nanna	Lebanon		
Municipality:	Multiple	Brooklyr	n, Harford	Annville Twp		
Permit Number:	ESG0011540002	ESX13-11	5-0152(01)	PAG-02-0038-15-010		
Approving Agency:	Susquehanna CCD	PADEP (O&G)	Lebanon CCD		



APPENDIX C

United States Department of Agriculture (USDA)
Natural Resources Conservation Service (NRCS)
Custom Soil Resource Report



Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Columbia County, Pennsylvania

Compressor Station 610



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (http://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil scientists classified and named the soils in the survey area, they compared the

individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

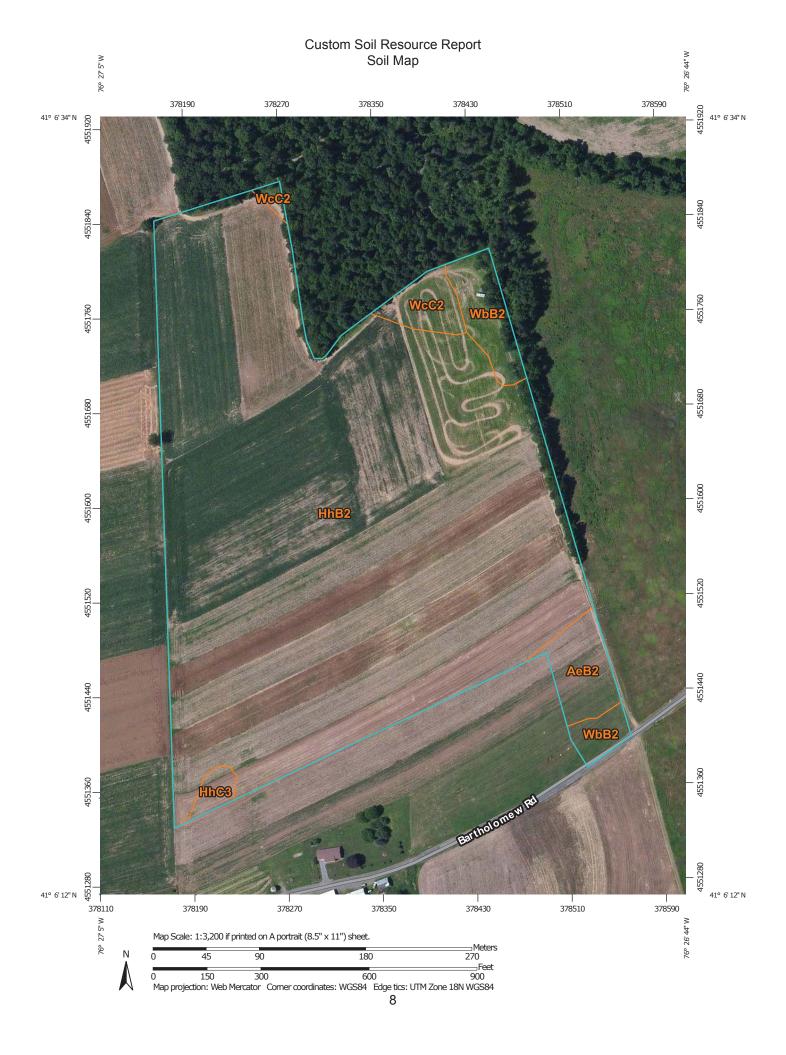
While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



misunderstanding of the detail of mapping and accuracy of soil line Albers equal-area conic projection, should be used if more accurate This product is generated from the USDA-NRCS certified data as of Soil map units are labeled (as space allows) for map scales 1:50,000 Apr 14, 2011—Sep 18, imagery displayed on these maps. As a result, some minor shifting The soil surveys that comprise your AOI were mapped at 1:20,000. placement. The maps do not show the small areas of contrasting Maps from the Web Soil Survey are based on the Web Mercator distance and area. A projection that preserves area, such as the The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background Enlargement of maps beyond the scale of mapping can cause Web Soil Survey URL: http://websoilsurvey.nrcs.usda.gov Coordinate System: Web Mercator (EPSG:3857) projection, which preserves direction and shape but distorts Natural Resources Conservation Service soils that could have been shown at a more detailed scale. Please rely on the bar scale on each map sheet for map Columbia County, Pennsylvania Version 7, Sep 15, 2014 MAP INFORMATION Warning: Soil Map may not be valid at this scale. calculations of distance or area are required. Date(s) aerial images were photographed: the version date(s) listed below. Soil Survey Area: Survey Area Data: Source of Map: measurements. or larger. Special Line Features Streams and Canals Interstate Highways Aerial Photography Very Stony Spot Major Roads Local Roads Stony Spot **US Routes** Spoil Area Wet Spot Other Rails Water Features **Fransportation** Background MAP LEGEND W 8 ŧ Soil Map Unit Polygons Severely Eroded Spot Area of Interest (AOI) Miscellaneous Water Soil Map Unit Points Soil Map Unit Lines Closed Depression Marsh or swamp Perennial Water Mine or Quarry Rock Outcrop Special Point Features **Gravelly Spot** Saline Spot Sandy Spot Slide or Slip Sodic Spot Lava Flow **Borrow Pit** Gravel Pit Clay Spot Area of Interest (AOI) Sinkhole Blowout Landfill 9 Soils

of map unit boundaries may be evident

Map Unit Legend

Columbia County, Pennsylvania (PA037)						
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI			
AeB2	Allenwood silt loam, 3 to 12 percent slopes, moderately eroded	1.0	2.9%			
HhB2	Hartleton channery silt loam, 3 to 12 percent slopes, moderately eroded	30.8	90.1%			
HhC3	Hartleton channery silt loam, 12 to 20 percent slopes, severely eroded	0.3	0.8%			
WbB2	Watson silt loam, 3 to 8 percent slopes, moderately eroded	1.3	3.9%			
WcC2	Weikert channery silt loam, 12 to 20 percent slopes, moderately eroded	0.8	2.3%			
Totals for Area of Interest		34.1	100.0%			

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been

observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An association is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Columbia County, Pennsylvania

AeB2—Allenwood silt loam, 3 to 12 percent slopes, moderately eroded

Map Unit Setting

National map unit symbol: 13b8

Mean annual precipitation: 36 to 46 inches Mean annual air temperature: 44 to 57 degrees F

Frost-free period: 130 to 180 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Allenwood and similar soils: 90 percent

Minor components: 8 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Allenwood

Setting

Landform: Valley sides

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Linear

Parent material: Old till derived from sedimentary rock

Typical profile

H1 - 0 to 8 inches: silt loam
H2 - 8 to 58 inches: silty clay loam

H3 - 58 to 70 inches: very gravelly silt loam

Properties and qualities

Slope: 3 to 12 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.60 to 2.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Moderate (about 8.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: B

Minor Components

Watson

Percent of map unit: 8 percent

HhB2—Hartleton channery silt loam, 3 to 12 percent slopes, moderately eroded

Map Unit Setting

National map unit symbol: 13cj Elevation: 500 to 1,500 feet

Mean annual precipitation: 36 to 46 inches Mean annual air temperature: 45 to 55 degrees F

Frost-free period: 140 to 175 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Hartleton, moderately deep, and similar soils: 90 percent

Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hartleton, Moderately Deep

Settina

Landform: — error in exists on —

Landform position (two-dimensional): Shoulder, backslope

Landform position (three-dimensional): Side slope

Down-slope shape: Linear, concave Across-slope shape: Linear, concave

Parent material: Residuum weathered from sandstone and shale

Typical profile

H1 - 0 to 8 inches: channery silt loam
H2 - 8 to 30 inches: channery silt loam
H3 - 30 to 35 inches: very channery loam
R - 35 to 39 inches: weathered bedrock

Properties and qualities

Slope: 3 to 12 percent

Depth to restrictive feature: 20 to 40 inches to lithic bedrock

Natural drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.60 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Low (about 3.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: B

Minor Components

Allenwood

Percent of map unit: 5 percent

Watson

Percent of map unit: 5 percent

HhC3—Hartleton channery silt loam, 12 to 20 percent slopes, severely eroded

Map Unit Setting

National map unit symbol: 13cl Elevation: 500 to 1,500 feet

Mean annual precipitation: 36 to 46 inches Mean annual air temperature: 45 to 55 degrees F

Frost-free period: 140 to 175 days

Farmland classification: Not prime farmland

Map Unit Composition

Hartleton, moderately deep, and similar soils: 90 percent

Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hartleton, Moderately Deep

Setting

Landform: — error in exists on —

Landform position (two-dimensional): Shoulder, backslope

Landform position (three-dimensional): Side slope

Down-slope shape: Linear, concave Across-slope shape: Linear, concave

Parent material: Residuum weathered from sandstone and shale

Typical profile

H1 - 0 to 5 inches: channery silt loam
H2 - 5 to 30 inches: channery silt loam
H3 - 30 to 35 inches: very channery loam
R - 35 to 39 inches: weathered bedrock

Properties and qualities

Slope: 12 to 20 percent

Depth to restrictive feature: 20 to 40 inches to lithic bedrock

Natural drainage class: Well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.60 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Very low (about 2.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: B

Minor Components

Allenwood

Percent of map unit: 8 percent

Watson

Percent of map unit: 2 percent

WbB2—Watson silt loam, 3 to 8 percent slopes, moderately eroded

Map Unit Setting

National map unit symbol: 13gb

Mean annual precipitation: 36 to 46 inches Mean annual air temperature: 40 to 60 degrees F

Frost-free period: 130 to 180 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Watson and similar soils: 80 percent Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Watson

Setting

Landform: Valley sides

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Linear Across-slope shape: Linear

Parent material: Old till derived from sedimentary rock

Typical profile

H1 - 0 to 9 inches: silt loam

H2 - 9 to 27 inches: gravelly silty clay loam H3 - 27 to 45 inches: gravelly clay loam H4 - 45 to 61 inches: channery loam

Properties and qualities

Slope: 3 to 8 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Moderately well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to

moderately high (0.06 to 0.20 in/hr)

Depth to water table: About 18 to 33 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Moderate (about 7.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C

Minor Components

Allenwood

Percent of map unit: 10 percent

Shelmadine

Percent of map unit: 5 percent Landform: Drainageways Down-slope shape: Concave Across-slope shape: Concave

Alvira

Percent of map unit: 5 percent

Landform: Hillslopes

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Interfluve

Down-slope shape: Concave Across-slope shape: Concave

WcC2—Weikert channery silt loam, 12 to 20 percent slopes, moderately eroded

Map Unit Setting

National map unit symbol: 13gf Elevation: 500 to 1,600 feet

Mean annual precipitation: 36 to 50 inches
Mean annual air temperature: 46 to 57 degrees F

Frost-free period: 120 to 200 days

Farmland classification: Not prime farmland

Map Unit Composition

Weikert and similar soils: 95 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Weikert

Setting

Landform: Hills

Landform position (two-dimensional): Backslope, shoulder Landform position (three-dimensional): Side slope, crest

Down-slope shape: Convex

Across-slope shape: Convex

Parent material: Residuum weathered from shale and siltstone

Typical profile

H1 - 0 to 8 inches: channery silt loam H2 - 8 to 20 inches: very channery silt loam H3 - 20 to 24 inches: weathered bedrock

Properties and qualities

Slope: 12 to 20 percent

Depth to restrictive feature: 10 to 20 inches to lithic bedrock Natural drainage class: Somewhat excessively drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Very low (about 1.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: D

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