This reanalysis of the horizontal directional drill (HDD) installation of a 16-inch diameter pipeline that traverses Waltonville Road, Shopes Church Road, four wetlands (4) wetlands (W-B56 through W-B58 and W-C26), and Streams S-B60 through S-B63 in Derry Township, Dauphin County, Pennsylvania, is in accordance with Condition No. 3 of the Stipulated Order issued under Environmental Hearing Board Docket No. 2017-009-L. Condition No. 3 stipulates, for HDDs initiated after the temporary injunction issued by the Pennsylvania Department of Environmental Protection (PADEP) Environmental Hearing Board on July 25, 2017, a reanalysis must be performed on HDDs for which an inadvertent return (IR) occurs during the installation of one pipe (20-inch or 16-inch diameter) where a second pipe will thereafter be installed in the same right-of-way (ROW).

The 16-inch pipeline HDD is referred to herein as HDD S3-0080-16.

There were two IR events during the installation of the 20-inch pipe which were remediated. The HDD installation of the 20-inch pipeline at this location is complete.

PIPE INFORMATION

16-Inch: 0.438 wall thickness; X-70.

Pipe stress allowances are an integral part of the design calculations performed for each HDD.

ORIGINAL HORIZONTAL DIRECTIONAL DRILL DESIGN SUMMARY: 16-INCH

Horizontal length: 3,870 feet (ft)
Entry/Exit angle: 10 degrees
Maximum depth of cover: 60 ft

Depths below streams and wetlands: 15-40 ft

Pipe design radius: 1,600 ft

ROOT CAUSE ANALYSIS FOR THE 20-INCH PIPELINE INSTALLATION INADVERDENT RETURNS

The occurrence of the IR events in during the installation of the 20-inch diameter pipeline resulted from advancing the drilling tool through rocks within the shallow and weak substrate immediately before the exit point, which allowed drilling fluid to travel through the surrounding wet and soft soils and discharge to the land surface.

GEOLOGIC AND HYDROGEOLOGIC ANALYSIS

The Pennsylvania Department of Conservation and Natural Resources (2000) reported that the S3-0080 HDD site is situated in the Gettysburg-Newark Lowland Section of the Piedmont Physiographic Province. The dominant topography is rolling lowlands, shallow valleys, and isolated hills with low to moderate relief. The rock type generally consists of red shale, siltstone, and sandstone with some conglomerate and diabase. The predominant geologic structure within this physiographic section consists of a half-graben having low, monoclinal, northwest-dipping beds.

The Gettysburg Formation located to the north and south of the site is composed of Reddish-brown shale and soft, red-brown, medium-to fine-grained sandstone; conglomeratic sandstone; minor amounts of

yellowish-brown shale and sandstone; may be metamorphosed by intrusive diabase to dark-purple to black argillite; total thickness is about 16,000 feet (Geyer and Wilshusen, 1982).

The diabase underlying the site is described as a medium- to coarse-grained, quartznormative tholeiitic basalt; composed of labradorite and various pyroxenes; occurs as dikes, sheets, and a few small flows (DCNR, 2001). The diabase is highly resistant to weathering and commonly weathers to form large, massive, spheroidal boulders (Geyer and Wilshusen, 1982; Low, et al., 2002). Joints are well-developed, abundant, and open providing a very low secondary porosity. The overlying soil is thin. Dikes typically form narrow ridges, and larger intrusions form hills of moderate relief. Excavation and/or drilling are slow due to the density and hardness of the rock.

Karst geology is not present in the immediate vicinity of this HDD location.

Attachment 1 provides an extensive discussion on the geology and results of the geotechnical investigation performed at this location.

HYDROGEOLOGY, GROUNDWATER, AND WELL PRODUCTION ZONES

According to Wood (1980) and Low, et al. (2002), groundwater within the elastic rocks of the Gettysburg Formation occurs under both unconfined (i.e., water table) and confined conditions. Groundwater flow paths within the elastic rocks have both local and regional components. Locally, shallow groundwater discharges to the gaining portions of nearby streams and deeper regional groundwater flow is toward points of regional groundwater discharge such as the Susquehanna River. According to the geologic map diabase underlies the entire site.

Based on the geotechnical reports groundwater was encountered in the five borings at depths ranging from 6 to 17 feet bgs.

Well records from the Pennsylvania Department of Conservation and Natural Resources (PADCNR) Pennsylvania Groundwater Information System (PaGWIS) database were reviewed to identify domestic water supply and other wells located within a 0.5-mile radius of the proposed HOD right-of-way (ROW) boundary (PaGWIS, 2019). The search identified 62 wells within the 0.5-mile radius of the HOD. These wells consist of 35 domestic supply wells, 21 geothermal wells, 1 domestic irrigation well, and 1 well identified as "other". Based on this data it appears that the majority of the identified wells were completed as 6-inch-diameter open-rock wells at depths ranging from 55 to 500 feet bgs. Based solely on the PaGWIS database, the depth to bedrock ranges from 0 to 85 feet bgs, and well construction consists of 0 to 105 feet of steel casing with the open-rock portions of the wells ranging from 2 to 500 feet bgs. Reported well yields range from 0 to 80 gpm, Static water level measurements ranged from 2 to 65 feet bgs. Based on the PaGWIS database, the majority of the wells identified above were completed in the Gettysburg Formation.

Attachment 1 provides an extensive discussion on the hydrogeology, and results of the geotechnical investigation performed at this location.

INADVERTENT RETURN (IR) DISCUSSION

Two IRs occurred during the pilot hole phase for installation of the 20-inch pipeline. The first IR occurred subsequent to a 20 percent loss of returns (LOR) at a drilling tool trajectory length of 3,693.95 feet and depth of 17.86 feet bgs, approximate 75 feet from the eastern exit point. The second IR occurred at a drilling tool trajectory length of 3,720.95 feet, approximately 128 feet

from the eastern exit point. Both of these IRs are considered "Punch Out" IR's and resulted from the shallow depth of cover and weak substrate while the drilling tool was still advancing through rocks within the substrate before exiting.

Punch out IRs are difficult to prevent. Regardless, SPLP drilling specialists have modified the profile for the 16-inch pipeline to increase the depth of profile, and increase the angles of entry and exit to reduce the potential for IR events during the drilling phases for completion of the second pipeline installation.

ADJACENT FEATURES ANALYSIS

The crossing of Waltonville Road is located in Dauphin County, approximately 2.8 miles southeast of the borough of Hummelstown, Pennsylvania, and approximately 3.7 miles northeast of the borough of Middletown, Pennsylvania. This HDD location is set under these two (2) roads as well as Wetlands W-B56 through W-B58 and W-C26, and Stream S-B60 through S-B63. This HDD avoids surficial impacts to the streams, wetlands, and minimizes potential expanded surficial impacts by avoiding the need to cross under two (2) pipelines perpendicular to the HDD by other construction methods.

SPLP performed a preconstruction survey of all landowners within 450 ft and greater from the HDD S3-0080-16 alignment. Through this outreach effort twelve landowners provided their well location and well data if known. As a result, six water wells were identified within the 450-foot buffer of the alignment. Well locations and limited information regarding depth to water, well yield and pump setting are in the Hydrogeologic Report in Attachment 1.

To further avoid and mitigate any adverse effects from the HDD to private water wells, and in accordance with the requirements of the Stipulated Order, SPLP will transmit a copy of this HDD analysis to all landowners having a property line within 450 ft in any direction of this HDD location. SPLP previously informed these landowners that SPLP will conduct pre-, during, and post-construction sampling of their private water wells to ensure that mitigating actions are taken, if necessary.

ALTERNATIVES ANALYSIS

As part of the PADEP Chapter 105 permit process for the Mariner II East Project, SPLP developed and submitted for review a project-wide Alternatives Analysis. During the development and siting of the project, SPLP considered a number of different routings, locations, and designs to determine whether there was a practicable alternative to the proposed route. SPLP performed this determination through a sequential review of routes and design techniques, which concluded with an alternative that has the least environmental impacts, taking into consideration cost, existing technology and logistics. The baseline route provided for the pipeline construction was to cross every wetland and stream on the project by open cut construction procedures. The Alternatives Analysis submitted to PADEP conceptually analyzed the potential feasibility of any alternative to baseline route trenched resource crossings (e.g., reroute, conventional bore, HDD). The decision-making processes for selection of the HDD instead of an open cut crossing methodology is discussed thoroughly in the submitted alternatives analysis and was an important part of the overall PADEP approval of HDD plans as currently permitted. As described below, the open cut and re-route analyses have confirmed the conclusions reached in the previously submitted Alternatives Analysis.

Using the HDD method avoids direct impacts to Streams S-B60 through S-B63 and Wetlands W-B56 through W-B58 and W-C26 and their associated floodways, associated forested woodlands and riparian habitats; and existing underground utilities. Alteration of the current permitted route and plans for

installation would require major modifications of the state Chapter 102 and Chapter 105 permits, and Section 404, Section 408, and easement authorizations, and associated National Environmental Policy Act (NEPA) Environmental Assessment and Finding of No Significant Impact (FONSI) issued by the USACE.

Open-cut and Conventional Bore Analysis

The pipeline route is within an existing SPLP pipeline easement. SPLP specifications require a minimum of 48 inches of cover over the installed pipelines below ground and below the bottom of watercourses. To meet this cover requirement, construction through Streams S-B60 through S-B63 and Wetlands W-B56 through W-B58 and W-C26 would require a minimum authorized open cut work space 50 ft in width to accommodate the 16-inch diameter pipeline, allowing for the pipeline to be installed with sufficient separation for integrity management and in consideration of the effects of trenching in open water on construction workspace. The assessed area of impact by this open cut plan would directly affect 0.08 acres of state water bottoms, and 2.3 acres of forested wetland.

Re-Route Analysis

The pipeline route as currently permitted follows an existing SPLP easement and this HDD bypasses or avoids direct impacts to forested woodlands, multiple stream channels, and floodway.

No practicable re-route option lies immediately to the north or south of the proposed route that would not transect the same resources transected by the proposed route or encroach upon residential or commercial structures. Shifting the pipeline route north would cross Streams S-B61, S-B64 and S-BB36; Wetlands W-BB36 and W-C26; forested woodlands; Waltonville Road; Shopes Church Road; have additional direct effects on underground utilities; require a new utility corridor requiring consent of newly-affected landowners or the use of eminent domain/condemnation; and create a new land encumbrance on every private property crossed. Shifting the pipeline route south to follow an existing overhead utility corridor would add 0.4 miles of pipe length; require crossing Streams S-B60 and S-B61; Wetlands W-B57, W-C26, and W-J34; forested woodlands; Cedardel Lane; Waltonville Road; three (3) private residential driveways; have additional direct effects on underground utilities; require new utility corridor requiring consent of newly-affected landowners or the use of eminent domain/condemnation; and create a new land encumbrance on every private property crossed. Given site conditions and features north and south of the proposed pipeline alignment, no practicable re-route exists that would result in less impacts to environmental resources.

In summary, due to the woodlands and resources to the north and south of the proposed HDD, additional direct effects to infrastructure, and creation of a new "greenfield" corridor for any shift north or south, there is no identifiable alternative route that would result in less impacts to aquatic and forested woodland resources and existing residences and associated infrastructure in the vicinity of HDD S3-0080.

This re-route analysis conducted for the Waltonville Road HDD is consistent with the conclusions reached in the alternatives analysis previously submitted to PADEP.

HORIZONTAL DIRECTIONAL DRILL REDESIGN

After review of the original HDD designs; available geologic/geotechnical data; field reports related to IR events that occurred during installation of the 20-inch pipe, and the hydro-structural characteristics of the underlying geology, SPLP HDD specialists have redesigned this HDD. A summary of the redesign factors is provided below.

A summary of the redesign factors is provided below. The original and redesigned HDD plan and profile drawings are provided in Attachment 2.

Revised Horizontal Directional Drill Design Summary: 16-inch

Horizontal length: 4,095 ft
Entry/Exit angle: 12-16 degrees
Maximum depth of cover: 124 ft

Depths below streams and wetlands: 52-87 ft

Pipe design radius: 2,000 ft

CONCLUSION

The proposed redesign will extend the HDD approximately 125 ft, deepen the profile by 44 ft, and increases the entry/exit angles are increased to minimize the potential for IRs. The new design places the HDD deeper to allow for more cover under the aquatic resources.

Upon the start of this HDD, SPLP will employ the following HDD best management practices:

- SPLP will provide the drilling crew and company inspectors (UI, EI, PGs) the location(s) data on
 potential zones of higher risk for fluid loss and IRs, including the area related to previous IRs, and
 potential zones of fracture concentration identified by the fracture trace analysis along the drill
 path, so that monitoring can be enhanced when drilling through these locations;
- SPLP will mandate annular pressure monitoring (APM) during the drilling of the pilot hole, which
 assists in immediate identification of pressure changes indicative of loss of circulation (LOC) or
 over pressurization of the annulus, managing development pressures that can induce an IR;
- SPLP's drilling contractor will utilize the drilling and monitoring log data for the 20-inch HDD as guidance on approaching the potential zone where drilling fluids were lost during the 20-inch HDD, such that corrective action by injection of Loss Control Materials (LCMs), or grouting can be implemented if the APM or return of drilling fluids indicate a loss in the same general area of the profile, or elsewhere;
- SPLP inspectors will ensure that an appropriate diameter pilot tool, relative to the diameter of the
 drilling pipe, is used to ensure adequate "annulus spacing" around the drilling pipe exits to allow
 good return flows during the pilot drilling;
- SPLP will mandate short-tripping of the reaming tools to ensure an open annulus is maintained to manage the potential inducement of IRs;
- SPLP will implement short-tripping of the reaming tools as return flow monitoring indicates to
 ensure an open annulus is maintained to manage the potential inducement of IRs;
- SPLP will require monitoring of the drilling fluid viscosity, such that fissures and fractures in the subsurface are sealed during the drilling process;
- During all drilling phases, the use of Loss Control Materials (LCMs) will be considered if
 indications of a potential IR are noted or an IR is observed. The use of LCMs, however, is less
 effective below 70 ft of the ground surface. The AP below that depth can exceed the effective
 stabilization capability of LCMs. Accordingly, the preferred proactive corrective action needed to
 address the presence of Losses of Circulation and fractures at greater depths below ground may
 require grouting of the HDD annulus. Two types of grouting will be utilized for corrective actions

to seal the annulus. These are: 1) grouting using "neat cement"; and 2) grouting using a sand/cement mix. Neat cement grout is a slurry of Portland cement and water. The sand/cement grout mix is a slurry of mostly sand with a small percentage of Portland cement and activators that after setup results in a material having the competency of a friable sandstone or mortar. Both grouting actions require tripping out the drilling tool, and then tripping in with an open-ended drill stem to apply or inject the grout mixes. Either of these grouting actions will be implement upon the first detection of an LOC with the selection of the treatment based upon the circumstances of the LOC, being small or large in magnitude.

FEASIBILITY DETERMINATION

Based on the information reviewed by the Geotechncial Evaluation Leader, Professional Geologists, Professional Engineers, and HDD specialists, the HDD Reevaluation Team's opinion is that the proposed HDD design and implementation of the management measures contained within this re-revaluation report will minimize the risk of IRs and impacts to public and private water supplies during the construction phases of the HDD.

Pertaining to Horizontal Directional Drilling Practices and Procedures; Conventional Construction; Alternatives; and Environmental Effects

Larry J. Gremminger, CWB Geotechnical Evaluation Leader

Mariner East 2 Pipeline Project

Date

Pertaining to the practice of geology

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Director of Groundwater and Site Characterization

Geo-Environmental Services

2/17/18

Date

Pertaining to the pipeline stress and HDD geometry

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ATTACHMENT 1

GEOLOGY AND HYDROGEOLOGICAL EVALUATION REPORT

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February 13, 2019

Mr. Matthew Gordon Sunoco Pipeline, LP 535 Fritztown Road Sinking Spring, Pennsylvania 19608

> Re: Sunoco PA Pipeline Project Mariner East II. Waltonville Road HDD S3-0080, PA-DA-0056,0000-RDa-16 Hydrogeological Re-Evaluation Report for 16-inch Pipeline Derry Township, Dauphin County, Pennsylvania RETTEW Project No. 096302009

EXECUTIVE SUMMARY

- During drilling of HDD S3-0080 for installation of the 20-inch diameter pipeline, two 1. "punch out" inadvertent returns (IRs) of drilling fluids occurred during the pilot phase. Due to the occurrence of these IRs during HDD operations for the 20-inch pipeline, this hydrogeologic report was prepared to address the potential for IRs during the proposed 16-inch HDD operations.
- 2. The Waltonville Road HDD bore path is underlain by crystalline intrusive (igneous) rocks composed of Jurassic age diabase (Jd). Sedimentary rocks of the Triassic age Gettysburg Formation (Trg) are adjacent both north and south of the diabase (refer to Figure 2).
- 3. Geologic mapping and published reports indicate a moderate degree of bedrock fracturing in the Gettysburg Formation characterized by a blocky, moderately to welldeveloped pattern of open joints with low angle northwest dipping beds. Geologic mapping and published reports indicate that the younger diabase is characterized by moderately abundant, well-developed, and open joints exhibiting a blocky pattern that generally intruded along gently dipping bedding planes and fractures of older rock.
- Water-bearing zones generally occur in secondary openings along bedding planes, 4. joints, faults, and fractures. Water-bearing zones in the Gettysburg Formation are reported to be distributed within the first 5 to 900 feet of the subsurface, with the greatest density of water-bearing zones occurring within the upper 288 feet of the subsurface (half occur below 115 feet and 90% occur at depths of less than 288 feet). Waterbearing zones in the diabase generally occur in the weathered zone at the top of the bedrock; however, half of these occur within the uppermost 75 feet of the subsurface, with the greatest density of water-bearing zones occurring within the upper 350 feet of the subsurface. As a result, the storage and transmission of groundwater in the diabase is primarily dependent on the degree and extent of fracturing and joint development.
- 5. To date, HDD operations have been completed at the S3-0080 location for the 20-inch pipeline. The 20-inch product pipe pull was completed on April 10 and 11, 2018.

Office Locations: Pittsburgh, PA Morgantown, WV State College, PA Hagerstown, MD Hunt Valley, MD Mr. Matthew Gordon
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6. Based on the hydro-structural characteristics of the underlying geology and the profile of the permitted 16-inch HDD profile within shallow unconsolidated soil materials and generally shallow bedrock, the proposed 16-inch HDD is susceptible to the inadvertent return of drilling fluids during HDD operations. A redesigned 16-inch HDD profile (Attachment 2, Figure 2) and proactive Best Management Practices (BMPs) during drilling operations will be used to reduce the risk of an IR.

1.0 INTRODUCTION

The purpose of this report is to describe the hydrogeologic setting of the Waltonville Road (S3-0080) HDD location. The Waltonville Road HDD (the site) is located in Derry Township, Dauphin County, Pennsylvania. The site is located approximately 2.8 miles southeast of Hummelstown Borough and approximately 3.8 miles northeast of Middletown Borough. The HDD was designed to be drilled under wetlands, Waltonville Road and Shopes Church Road (refer to **Figure 1**). Due to the occurrence of IRs during HDD operations for the 20-inch pipeline, this hydrogeologic report was prepared to address the potential for IRs during the proposed 16-inch drilling operations.

Local relief is low to moderate and ranges in the vicinity of the site from approximately 591 feet above mean sea level (AMSL) at the western entry/exit point to 612 feet AMSL at the eastern entry/exit point (Google Earth, 2018). The site is drained by a shallow, unnamed intermittent stream and wetland situated at the eastern half of the HDD trace. The unnamed tributary flows approximately 1.7 miles to the southwest before discharging to the Middletown Reservoir. The area surrounding the HDD profile consists predominantly of a combination of agricultural, open and forested semi-rural land.

The pilot hole for the proposed 16-inch HDD entry/exit point (western end) is at a surface elevation of 591 feet AMSL and forms a slightly concave HDD profile that slopes gently upward toward the east to an elevation of 632 feet AMSL at the easternmost HDD entry/exit point. The proposed 16-inch HDD pilot hole crosses beneath Waltonville Road at a depth of approximately 80 feet below ground surface (bgs) and Shopes Church Road at 88 feet bgs. The proposed 16-inch HDD is located approximately between STATIONS 11550+63 and 11589+12 on the pipeline, for an overall approximate horizontal length of 4,095 feet and a pipe length/bore path length of 4,115 feet. The existing 20-inch and proposed 16-inch S3-0080 HDD locations are shown on **Figure 1** and the redesigned 16-inch profile is included as **Attachment 1**.

2.0 GEOLOGY AND SOILS

Ten available published and online references were reviewed to evaluate the hydrogeology and soils present in the vicinity of the proposed Waltonville Road HDD location (S3-0080). Detailed descriptions of the soils and bedrock geology underlying S3-0080 are included below.

The Pennsylvania Department of Conservation and Natural Resources (2000) reported that the S3-0080 HDD site is situated in the Gettysburg-Newark Lowland Section of the

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Piedmont Physiographic Province. The dominant topography is rolling lowlands, shallow valleys, and isolated hills with low to moderate relief. The rock type generally consists of red shale, siltstone, and sandstone with some conglomerate and diabase. The predominant geologic structure within this physiographic section consists of a half-graben having low, monoclinal, northwest-dipping beds. The surface drainage pattern is both dendritic and trellis.

According to Google Earth (2018), two geologic formations occur within a 1,500 foot radius of the site. These include the Triassic age Gettysburg Formation (Trg), and the younger Jurassic age Diabase (Jd). These geologic units are identified on the geologic mapping included as **Figure 2**.

The Gettysburg Formation located to the north and south of the site is composed of Reddish-brown shale and soft, red-brown, medium-to fine-grained sandstone; conglomeratic sandstone; minor amounts of yellowish-brown shale and sandstone; may be metamorphosed by intrusive diabase to dark-purple to black argillite; total thickness is about 16,000 feet (Geyer and Wilshusen, 1982). This formation is moderately to well-bedded with individual beds ranging from thin to flaggy with moderately developed, moderately abundant, closely spaced, naturally occurring fractures known as joints. These joints are typically blocky, open and steeply dipping. The joint and bedding plane openings collectively provide a secondary porosity of moderate magnitude and moderate permeability. Surface drainage is good. The topography is characterized by undulating hills of low relief. Natural slopes are moderately steep and stable. Drilling rates are typically moderate to fast, except in areas where the rock is adjacent to diabase intrusions making the rock harder with a slower drilling rate.

The diabase underlying the site is described as a medium- to coarse-grained, quartz-normative tholeiitic basalt; composed of labradorite and various pyroxenes; occurs as dikes, sheets, and a few small flows (DCNR, 2001). The diabase is highly resistant to weathering and commonly weathers to form large, massive, spheroidal boulders (Geyer and Wilshusen, 1982; Low, et al., 2002). Joints are well-developed, abundant, and open providing a very low secondary porosity. The overlying soil is thin. Dikes typically form narrow ridges, and larger intrusions form hills of moderate relief. Excavation and/or drilling are slow due to the density and hardness of the rock.

According to the United States Department of Agriculture Soil Survey of Dauphin County, Pennsylvania (2018), soils within approximately 600 feet of the drill path for HDD S3-0080 consist of four soil types primarily very stony silt loam with lesser amounts of silt loam, gravelly silt loam, and channery silt loam. A site map showing the spatial distribution of the various soils along with the soil profile descriptions is included as **Attachment 1**.

3.0 HYDROGEOLOGY

Bedrock geology ultimately influences the storage, transmission, and use of ground-water. Geologic factors such as rock type, intergranular porosity, rock strata inclination, faults, joints, bedding planes, and solution channels affect groundwater movement and availability.

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According to Wood (1980) and Low, et al. (2002), groundwater within the clastic rocks of the Gettysburg Formation occurs under both unconfined (i.e., water table) and confined conditions. In general, groundwater occurs under unconfined conditions within the upper portion of the aquifer and under confined or semiconfined conditions in the deeper portions of the aquifer. The groundwater flow system was conceptualized by Wood (1980) as a series of sedimentary beds with relatively high transmissivity separated by beds exhibiting lower transmissivities. This sequence of beds exhibits different hydraulic properties that collectively act as a series of alternating aquifers and confining or semi-confining units forming a leaky (i.e., hydraulically interconnected) multi-aquifer system (LMAS). Groundwater flow paths within the clastic rocks have both local and regional components. Locally, shallow groundwater discharges to the gaining portions of nearby streams and deeper regional groundwater flow is toward points of regional groundwater discharge such as the Susquehanna River. Groundwater divides may be different for each zone of groundwater flow and therefore may not coincide with surface water divides.

According to the geologic map (**Figure 2**), diabase underlies the entire site. Based on the geotechnical reports (**Attachment 2**), groundwater was encountered in the five borings at depths ranging from 6 to 17 feet bgs.

The direction of groundwater flow within the clastic rocks of the Gettysburg Formation is largely controlled by the hydraulic gradient and spatial variability of hydraulic conductivity. The groundwater flow system in the clastic rocks is highly anisotropic with the predominant flow direction parallel to the strike of the rock beds. The potential for well interference related to pumping is generally greatest for wells aligned parallel to the strike, rather than in wells drilled in the direction of bedding dip (i.e., perpendicular to the strike). The presence of diabase often acts as a barrier to flow (Becher and Root, 1981; and Wood, 1980). No groundwater modeling was performed for the area surrounding the HDD.

According to Low, et al. (2002), the depths of water-bearing zones in 322 wells completed in the Gettysburg Formation range from 5 to 900 feet bgs. Fifty percent (50%) of the 669 water-bearing zones reported were penetrated at a depth of less than 115 feet with 90% of the water-bearing zones occurring at a depth of less than 288 feet. The greatest density of water-bearing zones (0.65 per 50 feet of well depth) is from 51 to 100 feet bgs. The density of water-bearing zones encountered at depths greater than 401 feet are based on the presence of 4 or fewer water-bearing zones per 50-foot interval. The overall density of water-bearing zones in the Gettysburg Formation is 0.41 per 50-feet of well depth.

The dense, uniform, crystalline, non-granular matrix of the diabase lacks bedding planes or consistent foliation and therefore possesses very low primary porosity and hydraulic conductivity. Although abundant, joint openings within the diabase provide very low secondary porosity (low permeability) and, combined with the corresponding low hydraulic conductivity, there is minimal pore space. As a result, the storage and transmission of groundwater in the diabase are primarily dependent on the degree and extent of fracturing. Water levels in the diabase show a strong seasonal influence. A thin mantle of stiff clay that is relatively impervious to

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moisture generally overlies diabase bedrock. This results in poor drainage in low-lying areas underlain by diabase (Low, et. al, 2002). Water levels from 191 inventoried wells within this unit range from flowing at the land surface to 155 feet bgs with a median water level of 14 feet bgs. Springs are common in ravines, draws, and other depressions crossed by diabase dikes (Low, et al., 2002).

According to Low, et al. (2002), the depths of water-bearing zones from 145 wells completed in the diabase range from 4 to 583 feet bgs. Fifty percent (%) of the 249 water-bearing zones reported were penetrated at a depth of less than 75 feet with 90% of the water-bearing zones occurring at a depth of less than 226 feet. The greatest density of water-bearing zones (0.57 per 50 feet of well depth) is from 301 to 350 feet bgs. The density of water-bearing zones encountered at depths greater than 301 feet are based on the presence of 4 or fewer water-bearing zones per 50-foot interval. The overall density of water-bearing zones in the diabase is 0.41 per 50-feet of well depth.

Well records from the Pennsylvania Department of Conservation and Natural Resources (PA DCNR) Pennsylvania Groundwater Information System (PaGWIS) database were reviewed to identify domestic water supply and other wells located within a 0.5-mile radius of the proposed HDD right-of-way (ROW) boundary (PaGWIS, 2019). The search identified 62 wells within the 0.5-mile radius of the HDD. These wells consist of 35 domestic supply wells, 21 geothermal wells, 1 domestic irrigation well, and 1 well identified as "other". A map showing the well locations relative to the proposed HDD location is included as **Figure 3**. Based on the PaGWIS database (**Attachment 3**), it appears that the majority of the identified wells were completed as 6-inch-diameter open-rock wells at depths ranging from 55 to 500 feet bgs. Based solely on the PaGWIS database, the depth to bedrock ranges from 0 to 85 feet bgs, and well construction consists of 0 to 105 feet of steel casing with the open-rock portions of the wells ranging from 2 to 500 feet bgs. Reported well yields range from 0 to 80 gpm. Static water level measurements ranged from 2 to 65 feet bgs. Based on the PaGWIS database, the majority of the wells identified above were completed in the Gettysburg Formation.

In February 2019, other Sunoco subcontractors researched private water supplies within 450 feet of the Waltonville Road HDD. Six water wells were identified within the 450-foot buffer of the alignment. Well locations and limited information regarding depth to water, well yield and pump setting are shown on **Attachment 3**.

4.0 FRACTURE TRACE ANALYSIS

Fracture traces are natural linear features that are unaffected by local topographic relief and, as a result, are considered surface manifestations of concentrated high-angle bedrock fracturing. Fracture traces may be observed on aerial photographs as linear topography, straight stream segments, vegetation, or soil tonal alignments. The occurrence of fracture traces underlying, or in close proximity to, the site were mapped by Wood (1980) and McGlade and Geyer (1976). The closest fracture trace was mapped approximately 1,040 feet northwest of the HDD bore path; other fracture traces are mapped but are located at distances greater

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than 2,800 feet from the HDD trace. The local fracture traces are depicted on the Geology Map included as **Figure 2** and the Groundwater Well Location Map presented as **Figure 3**. None of the identified fracture traces crosses the proposed HDD bore path.

5.0 GEOTECHNICAL EVALUATION

Two phases of geotechnical investigation were completed at the HDD drill site. Three geotechnical borings (SB-01, SB-02 and SB-03) were completed in November 2014 during the preliminary investigation of the site and prior to initiating HDD operations. Two additional borings (B-1 and B-2) were completed in November 2017. The borings were completed to investigate soil, residual soil, and bedrock conditions using hollow-stem augers with split spoons for soil sampling and a core barrel/bit for rock coring. **Attachment 2** presents a map depicting the boring locations, boring logs, and geotechnical reports for the two studies.

SB-01 was located near the western HDD entry/exit point, SB-02 was located next to Shopes Church Road near the central portion of the HDD, and SB-03 was located near the easternmost entry/exit point. The generalized subsurface profile observed in SB-01 through SB-03 is described as follows.

- **SB-01**: Topsoil was encountered from ground surface to 1 foot bgs, and sand from 1 to 30 feet bgs. Groundwater was encountered at 8 feet bgs.
- **SB-02:** Sand from ground surface to 15 feet bgs, and sandstone from 15 to 20 feet bgs. Groundwater was encountered at 6 feet bgs.
- **SB-03:** Topsoil was encountered from ground surface to 0.5 foot bgs; sands and silts from 0.5 to 11.5 feet bgs; silt from 11.5 to 26.5 feet bgs; and sand, sandstone and gravel was encountered from 26.5 to 30 feet bgs. Groundwater was apparently encountered at 16 feet bgs.

The boring logs indicate that the soil/bedrock interface ranges from approximately 15 feet (SB-02) to 30 feet (SB-01 and SB-03) bgs. The bedrock was described in SB-02 as highly fractured and heavily weathered sandstone.

Two additional borings (B-1 and B-2) were completed during November 2017, as part of the second phase of the geotechnical investigation. B-1 was drilled near the western HHD entry/exit point, and B-2 was drilled near the eastern HDD entry/exit point. The generalized subsurface profile observed in B-1 and B-2 is described as follows.

 B-1: Clays, sands, silts and gravels were encountered from the ground surface to approximately 24 feet bgs. Alternating units of diabase and conglomeratic sandstone bedrock were encountered from 24 to the total depth of the borehole at 143 feet bgs. Groundwater was encountered at approximately 12 feet bgs. Mr. Matthew Gordon Sunoco Pipeline, LP RETTEW Project No. 096302011 Page 7 February 13, 2019 Confidential & Privileged, Subject to Attorney and Client Review

B-2: Sands and silts were encountered from the ground surface to 34 feet bgs. Alternating units of diabase and conglomeratic sandstone bedrock were encountered from 34 to the total depth of the borehole at 143 feet bgs. Groundwater was encountered at approximately 17 feet bgs.

The bedrock in both borings was described as ranging from soft to hard, and very broken to massive. Photographs of the cores obtained from B-1 and B-2 are included in **Attachment 2**.

Please note that Skelly and Loy or RETTEW did not oversee or direct the geotechnical drilling programs associated with the site, including but not limited to, the selection of boring locations, determination of location, determination of surface elevation, target depths, observations of rock cores during drilling operations, or preparation of boring logs. The geotechnical reports, boring logs, and core photographs that resulted from these programs were generated by other Sunoco Pipeline, L.P. contractors. Skelly and Loy and RETTEW relied on these reports and incorporated their data into the general geologic and hydrogeologic framework of the analysis of the proposed 16-inch S3-0080 HDD for this report.

6.0 FIELD OBSERVATIONS

Site reconnaissance activities were performed by Skelly and Loy geologists on January 11, 2018. The entire HDD trace was walked, but no obvious bedrock outcrops were noted. Local (approximately 0.9 mile from the HDD trace) exposures of the Gettysburg Formation as indicated by strike and dip symbols shown on mapping by Wood (1980) were visited. Two locations were visited near 1625 Kaylor Road, and one location was visited near 1044 Stoverdale Road. Neither location yielded bedrock outcrops where bedding planes or consistent fracture sets were observed (in part due to leaf and snow cover). Other outcrop locations were not visited because their locations were likely situated on private property. Published local structural geologic measurements (Wood, 1980) of the Gettysburg Formation indicate that the bedrock strike is generally to the northeast/southwest with bedding dip ranging from approximately 30° to 50° northwest.

Michels Directional Crossings (Michels) initiated drilling of the pilot hole for the 20-inch pipeline on June 12, 2017, from the western entry/exit point depicted on the approved HDD profile. Michels stopped the pilot hole on June 13, 2017, to install 14-inch casing into bedrock to aid in getting the pilot bit to advance through the unconsolidated material and bedrock interface along the approved bore path. Pilot hole advancement resumed on June 15 and on July 25, 2017, had reached a trajectory length of 2,903 feet when all drilling activities across the PPP-ME2 project were suspended by the Pennsylvania Department of Environmental Protection (PA DEP). Following PA DEP's re-start approval, and resumption of drilling activities on August 19, 2017, Michels advanced a "sizing" tool into the pilot hole to ensure the bore hole was still open following the suspension of drilling activities. Michels resumed pilot hole advancement on August 24 and continued until September 6, 2017, when they experienced a 20 percent loss of

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returns (LOR) at a trajectory length of 3,693.95 feet and a depth of 17.86 feet bgs. In an attempt to regain circulation, Michels tripped the pilot bit completely out of the boring and, while tripping the bit back into the boring on September 7, 2017, an IR occurred approximate 75 feet from the eastern exit point and flowed back into Wetland C26 PEM. All drilling activities were immediately stopped and Michels began to construct containment structures consisting of silt fence reinforced with sand bags around the IR and recovered the released drilling fluids. HDD activities remained suspended until the PA DEP granted re-start approval. Michels resumed pilot hole advancement on December 5th, 2017, and experienced a second IR at a trajectory length of 3,720.95 feet, approximately 128 feet from the eastern exit point. The new IR was contained, recovery operations were initiated and the pilot hole was completed.

Michels started the 30-inch ream pass on December 8, 2017, and continued until December 22, 2017, when HDD activities were suspended for the holiday break. Michels prepared to resume reaming activities on January 3, 2018; however, as the equipment was being inspected and warmed up, notification of the PADEP suspension of all work on the PPP-ME2 project was received. Following the release of the PADEP suspension, Michels resumed the 30-inch ream pass on March 2, 2018. On March 9, 2018, Michels began to trip the reamer out of the borehole to inspect the cutting cones. On March 13, the 30-inch reamer was pulled out of the borehole and two cutting cones were missing. Between March 19 and 22, 2018, Michels conducted retrieval operations to recover the two cutting cones that remained in the borehole. Michels resumed 30-inch reaming operations on March 23 after successfully recovering both cutting cones. Reaming operations continued until April 7, 2018, when the pass was completed and the 30-inch swab pass was started. Michels completed the 30-inch swab pass on April 9, 2018 and the 20-inch product line was pulled through the borehole between April 10 and 11, 2018.

7.0 GEOPHYSICAL SURVEY CONSIDERATIONS

No karst geology was observed during the field reconnaissance or is mapped as being present at this HDD location. Secondly, SPLP possesses a complete geologic record of the bore path from drilling the 20-inch profile. Although the Corrected Stipulated Order states that the use of geophysical surveys should be considered in karst areas, based on the lack of karst geologic features and extensively fractured bedrock observed during the 20-inch HDD, the use of geophysical surveys during the site re-evaluation was considered but was ultimately not implemented because the results of geophysical surveys would not likely provide additional information that would reduce the risk of an IR. Based on our experience working in karst geology, the lack of mapped karst geology along the HDD trace and the lack of continuous thick-bedded limestone units, the diabase and Gettysburg Formations are not deemed susceptible to the solution activity present in other more thickly bedded carbonate geologic formations in Pennsylvania. In our professional opinion, geophysical surveys would not provide additional information on the formational thickness of the interbedded sandstone and diabase along the HHD profile. Geophysical survey data would not enhance the evaluation or reduce the risk of an IR.

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8.0 CONCEPTUAL HYDROGEOLOGIC MODEL

Groundwater occurring in the watershed occupied by the Waltonville Road HDD originates as precipitation or snowmelt. The precipitation infiltrates through the overburden soils. As previously described, shallow groundwater generally occurs under unconfined conditions. Based on site-specific geotechnical data (Section 5.0) and information obtained from the PaGWIS database (Section 3.0), the groundwater table occurs within the overburden soils (approximately 6 to 17 feet bgs) proximate to the HDD path and contributes flow to local shallow groundwater discharge zones (i.e., unnamed tributary and wetlands).

The geologic formations underlying the HDD site are highly anisotropic, with the predominant groundwater flow direction parallel to bedrock strike. The transport of groundwater in the fractured bedrock is generally greatest within highly permeable fractures, and the orientation of bedding planes and fractures primarily influence the direction of groundwater flow. Some site-specific evaluations of the bedrock have been completed in the area proximate to the geotechnical core borings completed along this HDD profile. No detailed characterization or groundwater flow modeling of the bedrock aquifer was performed as part of this hydrogeologic re-evaluation.

The groundwater flow direction in the overburden soils is presumed to mimic surface topography which slopes gently to the southwest toward the unnamed tributary discharging to the Middletown Reservoir.

9.0 CONCLUSIONS

Based on published geologic and hydrogeologic information, the site is underlain by clastic sedimentary rocks (primarily sandstone and conglomeratic sandstone) of the Gettysburg Formation and dense, very fine to coarsely crystalline intrusive diabase. Groundwater movement within these rocks is primarily through a network of interconnected secondary openings (e.g., fractures, joints, and faults) that were developed by external forces following deposition of the beds and intrusion of the diabase. Geotechnical rock core observations confirm that the local bedrock ranges from fractured and broken to massive sandstone, conglomerate, and diabase comprised of well-developed thin to massive moderately steeply dipping joint and bedding planes. All of the private water supply wells identified in the vicinity of the HDD are constructed in bedrock, indicating that none of the domestic wells rely on the shallow unconsolidated overburden as a source of groundwater supply. The uppermost unconsolidated soils, weathered bedrock, and potentially the bedrock aquifer, provide groundwater discharge to the local wetlands and unnamed tributary.

The originally proposed 16-inch and 20-inch HDD profiles were relatively shallow at the entry and exit points, and passed through both the unconsolidated overburden and fractured bedrock. Based on the hydro-structural characteristics of the underlying geology described in this report and the proposed HDD profiles, the Waltonville Road HDD site is susceptible to the inadvertent return of drilling fluids during HDD operations. As a result, the HDD profile has been

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redesigned to allow for deeper crossings beneath the wetland and stream. The inclination of the entry and exit angles for the 16-inch pipeline has been increased to allow the pipe to be installed through the protective soils, residual soils, and bedrock in closer proximity to the entry and exit points than the original, shorter profile. The redesigned 16-inch HDD profile will minimize the potential for an IR. From a geologic perspective, the laterally adjusted, longer and deeper profile, in conjunction with the proposed proactive use of engineering controls and/or drilling BMPs, will reduce the risk of an IR. Drilling BMPs are described in the Horizontal Directional Drill Analysis component of the overall re-evaluation package.

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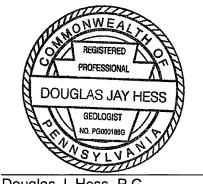
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11.0 CERTIFICATION

The studies and evaluations presented in this report (other than Section 5.0) were completed under the direction of a licensed professional geologist (P.G.) and are covered under the P.G. seal that follows.

By affixing my seal to this document, I am certifying that the information is true and correct. I further certify that I am licensed to practice in the Commonwealth of Pennsylvania and that it is within my professional expertise to verify the correctness of the information herein.



Douglas J. Hess, P.G. License No. PG-000186-G

Sincerely yours,

SKELLY and LOY, Inc.

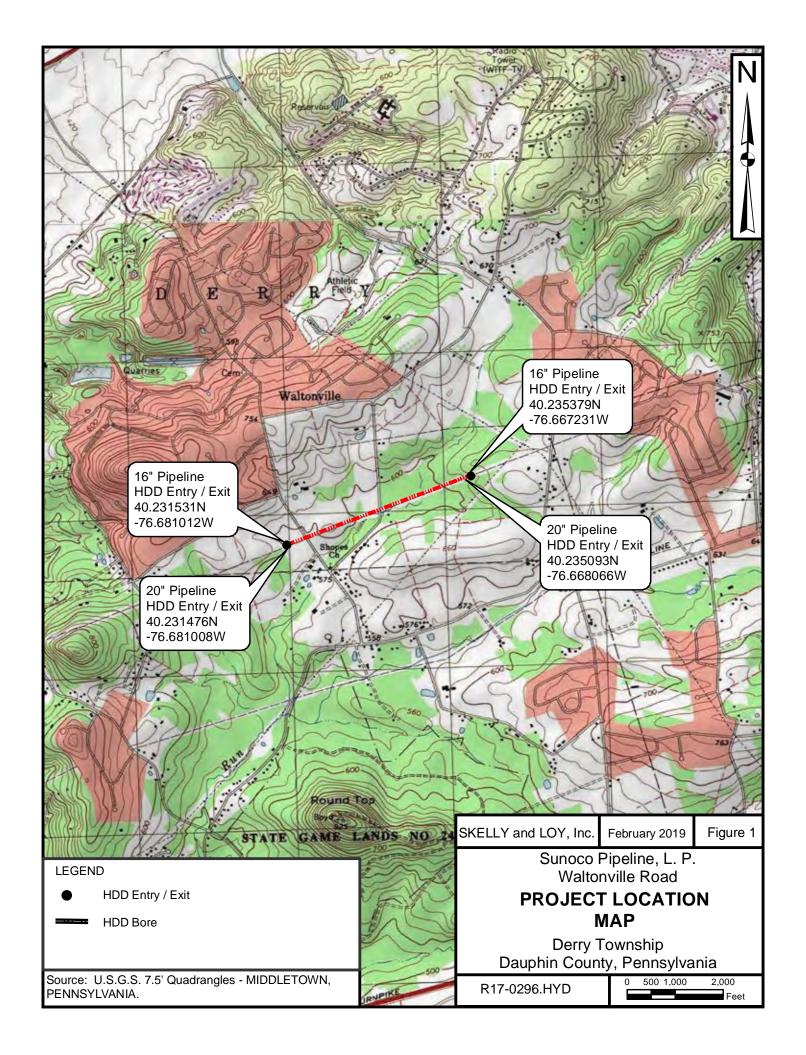
Douglas J. Hess, P.G.
Director of Groundwater
and Site Characterization
Geo-Environmental Services

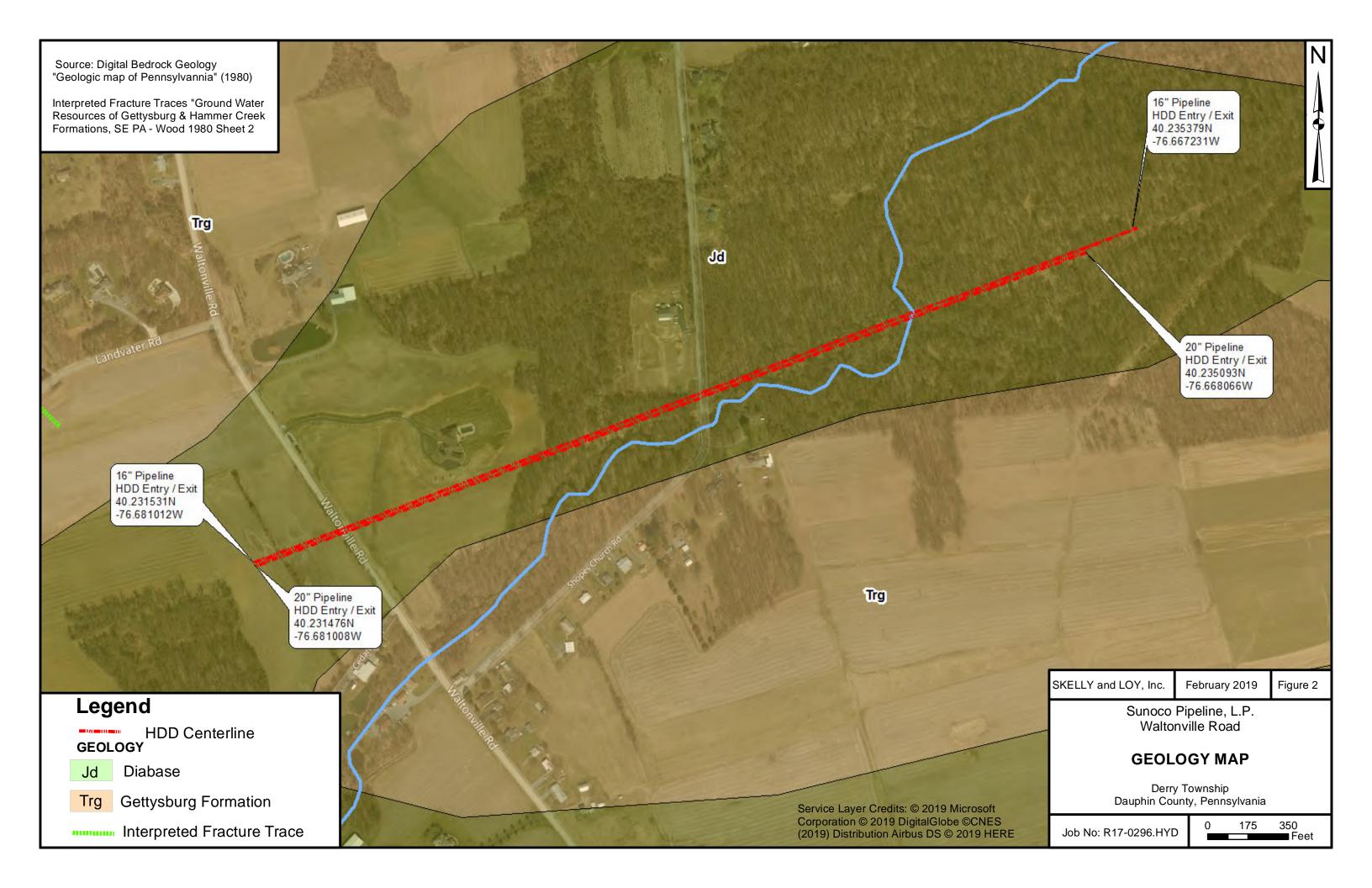
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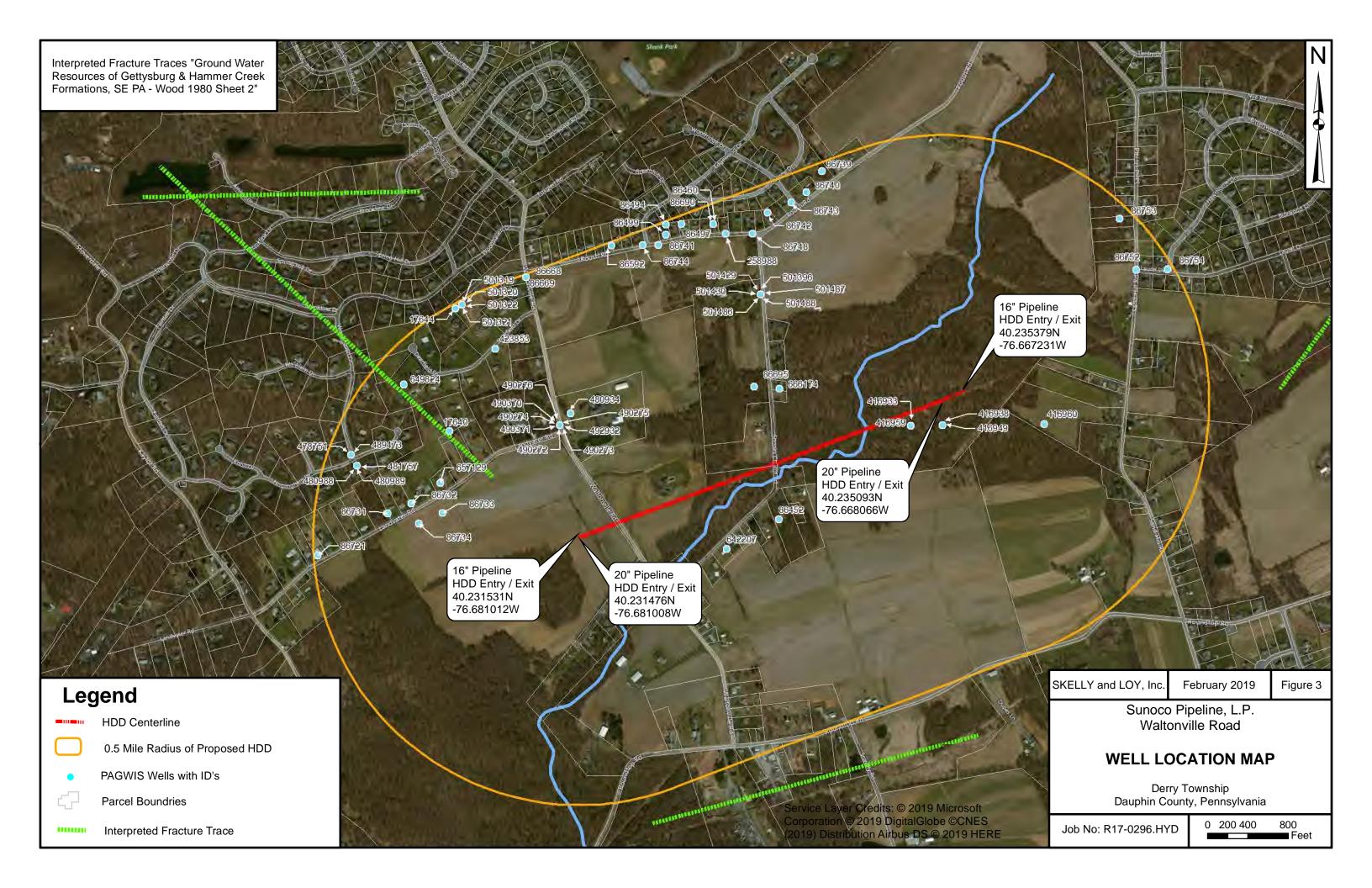
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FIGURES







ATTACHMENT 1

ATTACHMENT 1



VRCS

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Dauphin County, Pennsylvania

Waltonville Road HDD, Derry Township, Dauphin Co., PA



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2 053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

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scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

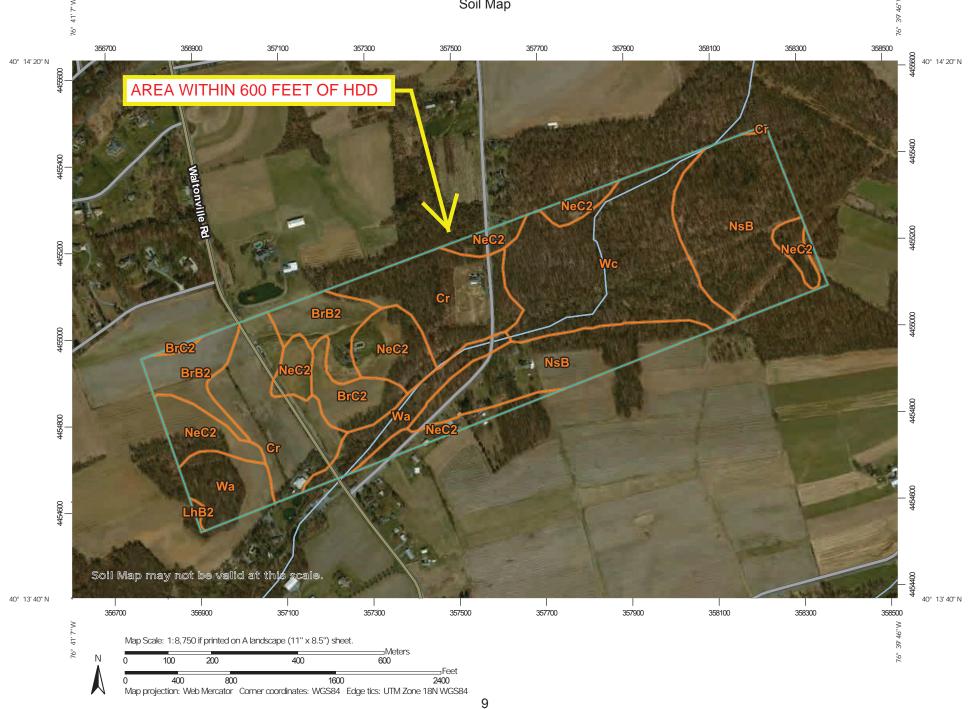
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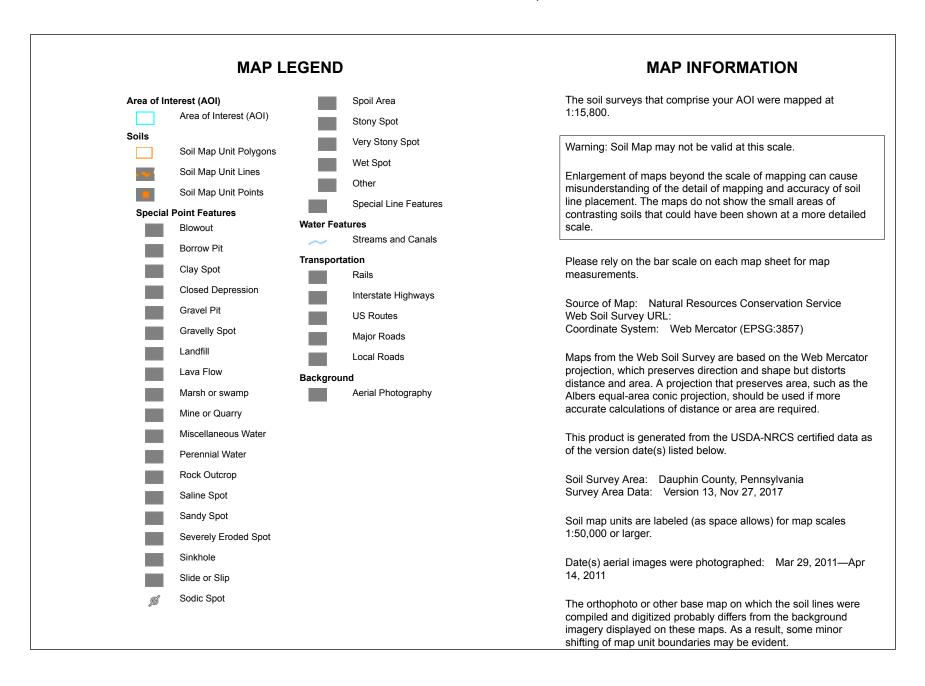
identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

Custom Soil Resource Report Soil Map





Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI	
BrB2	Brecknock channery silt loam, 3 to 8 percent slopes, moderately eroded	12.8	8.1%	
BrC2	Brecknock channery silt loam, 8 to 20 percent slopes, moderately eroded	5.9	3.7%	
Cr	Croton silt loam, occasionally ponded, 0 to 3 percent slopes	30.6	19.4%	
LhB2	Lehigh silt loam, 3 to 8 percent slopes, moderately eroded	0.3	0.2%	
NeC2	Neshaminy gravelly silt loam, 3 to 12 percent slopes, moderately eroded	23.1	14.7%	
NsB	Neshaminy very stony silt loam, 0 to 8 percent slopes	39.6	25.1%	
Wa	Watchung silt loam	13.1	8.3%	
Wc	Watchung very stony silt loam	32.2	20.4%	
Totals for Area of Interest		157.6	100.0%	

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas

are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An association is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Dauphin County, Pennsylvania

BrB2—Brecknock channery silt loam, 3 to 8 percent slopes, moderately eroded

Map Unit Setting

National map unit symbol: I4n3 Elevation: 250 to 1,000 feet

Mean annual precipitation: 40 to 48 inches Mean annual air temperature: 48 to 55 degrees F

Frost-free period: 150 to 200 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Brecknock and similar soils: 93 percent

Minor components: 7 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Brecknock

Setting

Landform: Hills, ridges

Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Interfluve, side slope

Down-slope shape: Linear, convex Across-slope shape: Convex, linear

Parent material: Residuum weathered from porcellanite and/or red metamorphosed residuum weathered from sandstone and shale

Typical profile

Ap - 0 to 10 inches: channery silt loam

Bt - 10 to 32 inches: channery silt loam

C - 32 to 41 inches: very channery silt loam

R - 41 to 51 inches: bedrock

Properties and qualities

Slope: 3 to 8 percent

Depth to restrictive feature: 40 to 60 inches to lithic bedrock

Natural drainage class: Well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to

high (0.60 to 2.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Low (about 4.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: B Hydric soil rating: No

Minor Components

Lehigh

Percent of map unit: 7 percent

Landform: Hillsides

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Side slope

Down-slope shape: Concave, linear Across-slope shape: Linear, concave

Hydric soil rating: No

BrC2—Brecknock channery silt loam, 8 to 20 percent slopes, moderately eroded

Map Unit Setting

National map unit symbol: 14n4 Elevation: 250 to 1,000 feet

Mean annual precipitation: 40 to 48 inches Mean annual air temperature: 48 to 55 degrees F

Frost-free period: 150 to 200 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Brecknock and similar soils: 91 percent

Minor components: 9 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Brecknock

Setting

Landform: Hills, ridges

Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Interfluve, side slope

Down-slope shape: Linear, convex Across-slope shape: Convex, linear

Parent material: Residuum weathered from porcellanite and/or red metamorphosed residuum weathered from sandstone and shale

Typical profile

Ap - 0 to 10 inches: channery silt loam

Bt - 10 to 32 inches: channery silt loam

C - 32 to 41 inches: very channery silt loam

R - 41 to 51 inches: bedrock

Properties and qualities

Slope: 8 to 15 percent

Depth to restrictive feature: 40 to 60 inches to lithic bedrock

Natural drainage class: Well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to

high (0.60 to 2.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Low (about 4.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: B Hydric soil rating: No

Minor Components

Lehigh

Percent of map unit: 9 percent

Landform: Hillsides

Landform position (two-dimensional): Shoulder, backslope

Landform position (three-dimensional): Side slope

Down-slope shape: Concave, linear Across-slope shape: Linear, concave

Hydric soil rating: No

Cr—Croton silt loam, occasionally ponded, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 2tkpx

Elevation: 300 to 800 feet

Mean annual precipitation: 40 to 48 inches Mean annual air temperature: 50 to 55 degrees F

Frost-free period: 160 to 190 days

Farmland classification: Not prime farmland

Map Unit Composition

Croton, occasionally ponded, and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Croton, Occasionally Ponded

Setting

Landform: Depressions

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave, linear Across-slope shape: Linear, concave

Parent material: Residuum weathered from sandstone and shale

Typical profile

Ap - 0 to 11 inches: silt loam

Btg - 11 to 19 inches: silty clay loam

Btxg - 19 to 30 inches: channery silty clay loam Cx - 30 to 44 inches: channery silt loam

R - 44 to 64 inches: bedrock

Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: 18 to 20 inches to fragipan; 40 to 60 inches to lithic

bedrock

Natural drainage class: Poorly drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: None Frequency of ponding: Occasional

Available water storage in profile: Low (about 3.5 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4w

Hydrologic Soil Group: D Hydric soil rating: Yes

Minor Components

Abbottstown, occasionally ponded

Percent of map unit: 10 percent

Landform: Depressions

Landform position (two-dimensional): Toeslope

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: No

Readington

Percent of map unit: 5 percent Landform: Depressions

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave, linear Across-slope shape: Concave, linear

Hydric soil rating: No

LhB2—Lehigh silt loam, 3 to 8 percent slopes, moderately eroded

Map Unit Setting

National map unit symbol: 14pf Elevation: 200 to 1,000 feet

Mean annual precipitation: 40 to 48 inches
Mean annual air temperature: 48 to 55 degrees F

Frost-free period: 150 to 200 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Lehigh and similar soils: 80 percent Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Lehigh

Setting

Landform: Hillsides

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Side slope

Down-slope shape: Concave, linear Across-slope shape: Linear, concave

Parent material: Residuum weathered from porcellanite

Typical profile

Ap - 0 to 7 inches: silt loam

Bt - 7 to 40 inches: channery silt loam

C - 40 to 58 inches: extremely channery silt loam

R - 58 to 62 inches: bedrock

Properties and qualities

Slope: 3 to 8 percent

Depth to restrictive feature: 40 to 60 inches to lithic bedrock

Natural drainage class: Moderately well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to

moderately high (0.06 to 0.20 in/hr)

Depth to water table: About 6 to 36 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Moderate (about 8.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2w

Hydrologic Soil Group: C/D Hydric soil rating: No

Minor Components

Brecknock

Percent of map unit: 12 percent

Landform: Hills, ridges

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Interfluve, side slope

Down-slope shape: Linear, convex Across-slope shape: Convex, linear

Hydric soil rating: No

Croton

Percent of map unit: 8 percent

Landform: Depressions

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave, linear

Across-slope shape: Linear, concave

Hydric soil rating: Yes

NeC2—Neshaminy gravelly silt loam, 3 to 12 percent slopes, moderately eroded

Map Unit Setting

National map unit symbol: 14ps Elevation: 250 to 1.600 feet

Mean annual precipitation: 36 to 50 inches
Mean annual air temperature: 46 to 57 degrees F

Frost-free period: 150 to 210 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Neshaminy and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Neshaminy

Setting

Landform: Hillslopes

Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Side slope, nose slope, interfluve

Down-slope shape: Linear, convex Across-slope shape: Convex, linear

Parent material: Residuum weathered from diabase

Typical profile

H1 - 0 to 10 inches: gravelly silt loam

H2 - 10 to 40 inches: gravelly sandy clay loam

H3 - 40 to 46 inches: bedrock

Properties and qualities

Slope: 3 to 12 percent

Depth to restrictive feature: 40 to 72 inches to lithic bedrock

Natural drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20

to 0.60 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Low (about 5.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C Hydric soil rating: No

Minor Components

Neshaminy, stony

Percent of map unit: 5 percent

Hydric soil rating: No

Brecknock

Percent of map unit: 5 percent

Landform: Hills, ridges

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Interfluve, side slope

Down-slope shape: Linear, convex Across-slope shape: Convex, linear

Hydric soil rating: No

Lehigh

Percent of map unit: 5 percent

Landform: Hills

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Side slope

Down-slope shape: Concave, linear Across-slope shape: Linear, concave

Hydric soil rating: No

NsB—Neshaminy very stony silt loam, 0 to 8 percent slopes

Map Unit Setting

National map unit symbol: 14pt Elevation: 400 to 1,600 feet

Mean annual precipitation: 36 to 50 inches Mean annual air temperature: 46 to 57 degrees F

Frost-free period: 155 to 210 days

Farmland classification: Not prime farmland

Map Unit Composition

Neshaminy and similar soils: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Neshaminy

Setting

Landform: Hillslopes

Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Interfluve, side slope, nose slope

Down-slope shape: Linear, convex Across-slope shape: Convex, linear

Parent material: Residuum weathered from diabase

Typical profile

H1 - 0 to 8 inches: channery silt loam

H2 - 8 to 49 inches: very gravelly clay loam

H3 - 49 to 53 inches: bedrock

Properties and qualities

Slope: 0 to 8 percent

Percent of area covered with surface fragments: 1.6 percent Depth to restrictive feature: 36 to 72 inches to lithic bedrock

Natural drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20

to 0.60 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Moderate (about 6.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: C Hydric soil rating: No

Wa—Watchung silt loam

Map Unit Setting

National map unit symbol: 14q9 Elevation: 200 to 2,000 feet

Mean annual precipitation: 35 to 50 inches Mean annual air temperature: 45 to 57 degrees F

Frost-free period: 140 to 220 days

Farmland classification: Not prime farmland

Map Unit Composition

Watchung, silt loam, and similar soils: 86 percent

Minor components: 14 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Watchung, Silt Loam

Setting

Landform: Depressions

Landform position (two-dimensional): Summit Landform position (three-dimensional): Interfluve

Down-slope shape: Concave Across-slope shape: Linear

Parent material: Residuum weathered from diabase

Typical profile

Ap - 0 to 9 inches: silt loam Btg1 - 9 to 18 inches: silty clay Btg2 - 18 to 25 inches: clay Btg3 - 25 to 30 inches: clay

Btg4 - 30 to 40 inches: clay C - 40 to 60 inches: loam

Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: 60 to 99 inches to lithic bedrock

Natural drainage class: Poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

high (0.00 to 0.20 in/hr)

Depth to water table: About 0 to 12 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: High (about 10.5 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4w

Hydrologic Soil Group: C/D Hydric soil rating: Yes

Minor Components

Towhee

Percent of map unit: 9 percent

Landform: Depressions

Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Side slope, head slope

Down-slope shape: Concave, linear Across-slope shape: Concave

Hydric soil rating: Yes

Codorus

Percent of map unit: 5 percent

Landform: Flood plains

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread

Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

Wc—Watchung very stony silt loam

Map Unit Setting

National map unit symbol: 14qb Elevation: 300 to 2,000 feet

Mean annual precipitation: 34 to 50 inches Mean annual air temperature: 45 to 57 degrees F

Frost-free period: 130 to 220 days

Farmland classification: Not prime farmland

Map Unit Composition

Watchung, extremely stony, and similar soils: 90 percent

Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Watchung, Extremely Stony

Setting

Landform: Drainageways, depressions

Landform position (two-dimensional): Summit Landform position (three-dimensional): Interfluve

Down-slope shape: Concave Across-slope shape: Linear

Parent material: Residuum weathered from diabase

Typical profile

A - 0 to 13 inches: silt loam

Btg - 13 to 47 inches: silty clay loam C - 47 to 65 inches: channery loam

Properties and qualities

Slope: 0 to 8 percent

Percent of area covered with surface fragments: 5.1 percent Depth to restrictive feature: 60 to 99 inches to lithic bedrock

Natural drainage class: Poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

high (0.00 to 0.20 in/hr)

Depth to water table: About 0 to 12 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: High (about 10.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: C/D Hydric soil rating: Yes

Minor Components

Mount lucas, silt loam

Percent of map unit: 10 percent Landform: Hillslopes. hillsides

Landform position (two-dimensional): Footslope, backslope, summit

Landform position (three-dimensional): Side slope Down-slope shape: Linear, concave, convex Across-slope shape: Concave, linear, convex

Hydric soil rating: No

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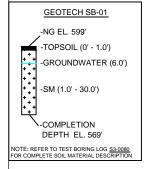
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ATTACHMENT 2





GEOTECH B-1 -NG EL. 599'

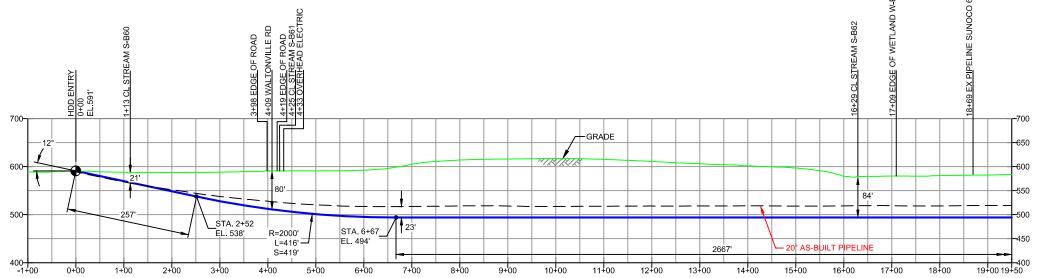
-TOPSOIL (0' - 1.0') -FILL CL (1.0' - 8.5')

-GROUNDWATER (11.8') -RESIDUUM-SILTY SAND SM (8.5' - 18.5') -RESIDUUM-SILTY SAND ML (18.5' - 24.5')

-SANDSTONE/DIABASE (24.5' - 143.0')

-BORING TERMINATED EL.456' NOTE: REFER TO TEST BORING LOG <u>B-1</u> INTERTEK PROJECT #04911517 FOR COMPLETE SOIL MATERIAL DESCRIPTION





- DESIGN AND CONSTRUCTION:

 1. CONTRACTOR SHALL FIELD VERIFY DEPTH OF ALL EXISTING UTILITIES SHOWN OR NOT SHOWN ON THIS DRAWING.

 2. THE MINIMUM SEPARATION DISTANCE FROM EXISTING SUBSURFACE UTILITIES SHALL NOT BE LESS THAN 10 FEET AS MEASURED FROM THE OUTSIDE EDGE OF THE UTILITY TO OUTSIDE OF PROPOSED PIPELINE.
- PIPELINE.
 DESIGNED IN ACCORDANCE WITH CFR 49 195 & ASME B31.4
 CROSSING PIPE SPECIFICATION:
 HDD HORZ LENGTH (L=): 4095'
 HDD PIPE LENGTH (S=): 4120'
 16" x 0.438" W.T., X-70, APIEL PSL2, ERW, BFW
 COATING: 14-16 MILS FBE WITH 40 MILS MIN. ARO (POWERCRETE R95)

- INTERNAL DESIGN PRESSURE 2100 PSIG (SEAM FACTOR 1.0, DESIGN FACTOR 0.50 (HOOP STRESS)).
 INSTALLATION METHOD: HORIZONTAL DIRECTIONAL DRILL (HDD).
 PIPELINE WARNING MARKERS SHALL BE INSTALLED ON BOTH SIDES OF ALL ROAD, RAILWAY, AND
 STREAM CROSSINGS.

 12. SUNOCO PIPELINE, L.P.'S HORIZONTAL DIRECTIONAL DRILL INADVERTENT RETURN CONTINGENCY PLAN
 WILL BE IMPLEMENTED AT ALL TIMES.
 SUNOCO PIPELINE, L.P.'S EROSION AND SEDIMENTATION CONTROL PLAN WILL BE IMPLEMENTED AT ALL
 TIMES.
- CARRIER PIPE NOT ENCASED.
- CARRIER PIPE NOT ENCASED.
 PIPE? AMBIENT TEMPERATURE MUST BE NO LESS THAN 30°F DURING PULLBACK WITHOUT PRIOR WRITTEN APPROVAL FROM THE ENGINEER.
 CONDUCT 4-HOUR PRE-INSTALLATION HYDROTEST OF HDD PIPE STRING TO MINIMUM 2625 PSIG.
 SEE SUNOCO PENNSYLVANIA PIPELINE PROJECT ESRI WEBMAP FOR ACCESS ROAD ALIGNMENT.

				(
NOTES			REF. DR	AWING		REVISIONS						
1. ALL COORDINATES SHOWN ARE IN LATITUDE AND LONGITUDE. ALL MSL ELEVATIONS ARE NAD83	ES-4.23	то	ES-4.25	EROSION & SEDIMENT PLAN	EP4	DESIGN CHANGE - INCREASED DRILL EXIT ANGLE	MRS	02/13/19	RMB	02/13/19	AMC	02/13/19
STATIONING IS BASED ON HORIZONTAL DISTANCES. ROONEY ENGINEERING, INC. AND SUNOCO PIPELINE, LP ARE NOT RESPONSIBLE FOR LOCATION	SHEET 14	то	SHEET 15	AERIAL SITE PLAN	EP3	DESIGN CHANGE - EXTENDED DRILL AND UPDATED GEOTECH INFORMATION	MRS	12/07/18	RMB	12/07/18	AMC	12/07/18
OF FOREIGN UTILITIES SHOWN IN PLOT PLAN OR PROFILE. THE INFORMATION SHOWN HEREON IS FURNISHED WITHOUT LIABILITY ON THE PART OF ROONEY ENGINEERING, INC. AND SUNOCO PIPELINE.					EP2	REVISED PER PADEP COMMENTS RECEIVED 09-06-16	MRS	10/07/16	RMB	10/07/16	AAW	10/07/16
LP, FOR ANY DAMAGES RESULTING FROM ERRORS OR OMISSIONS THEREIN.					EP1	REVISED PER PADEP COMMENTS	DLM	05/09/16	RMB	05/09/16	AAW	05/09/16
 CONTRACTOR IS RESPONSIBLE FOR LOCATING ALL UTILITIES. CONTACT ONE CALL AT 811 PRIOR TO DIGGING. 					EP		JTW	03/15/16	RMB	03/15/16	AAW	03/15/16
5. SUNOCO EMERGENCY HOTLINE NUMBER IS #1-800-786-7440.					В	ADDED GEOTECH INFO	MRS	09/22/15	RMB	09/22/15	AAW	09/22/15
	DWG NO		DWG NO	DESCRIPTION	NO.	DESCRIPTION	BY	DATE	СНК	DATE	APP	DATE



(303) 792-5911

TETRA TECH ROONEY

HORIZONTAL DIRECTIONAL DRILL
WALTONVILLE ROAD
PENNSYLVANIA PIPELINE PROJECT

SUNOCO PIPELINE, L.P.

DWG. NO: PA-DA-0056.0000-RDa-16 SCALE: 1"=200'

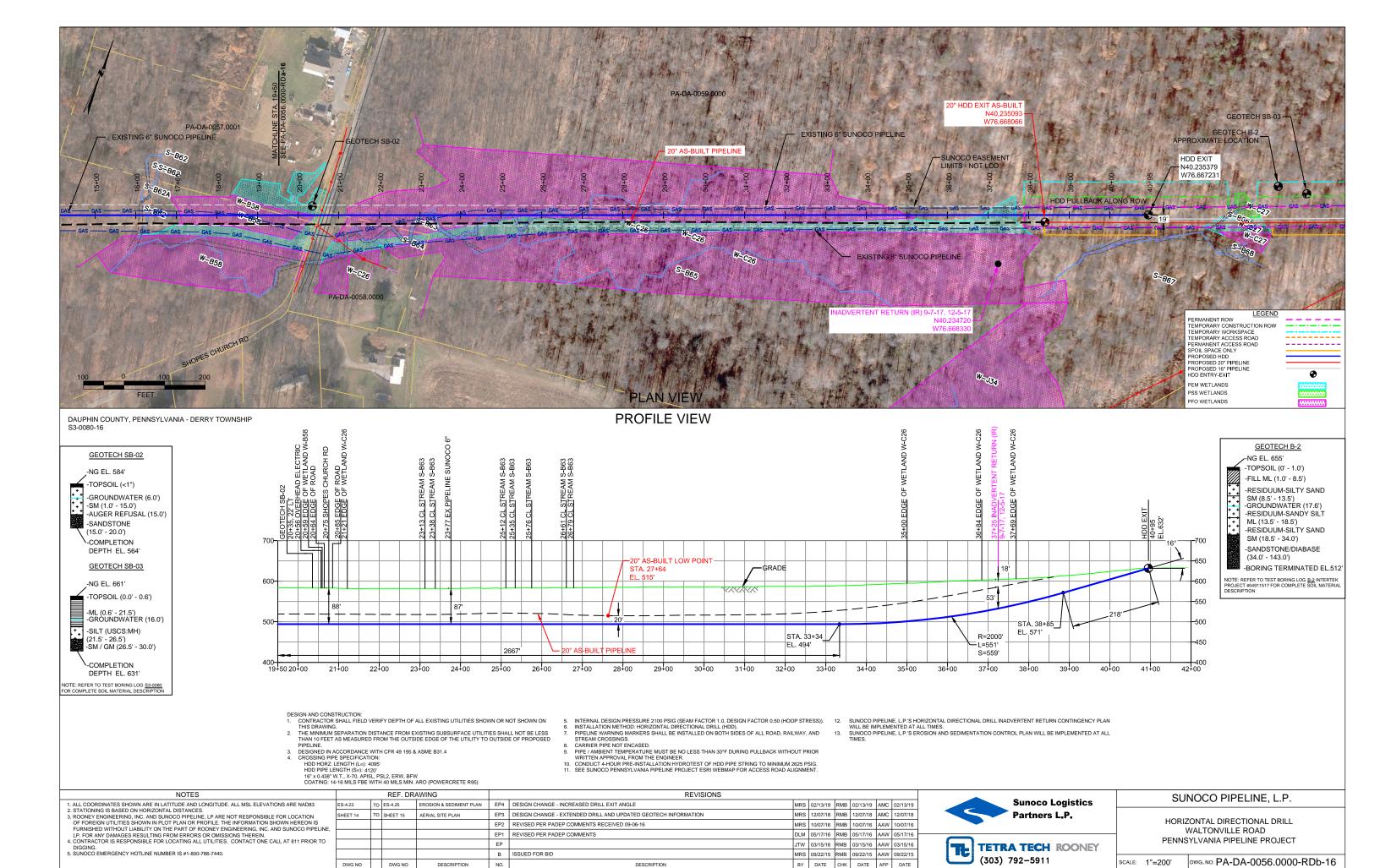


Figure 1: Site Vicinity Map

Make online reservations at www.visitPAparks.com or call toll-free 888-PA-PARKS

Visit us at http://www.dcnr.state.pa.us

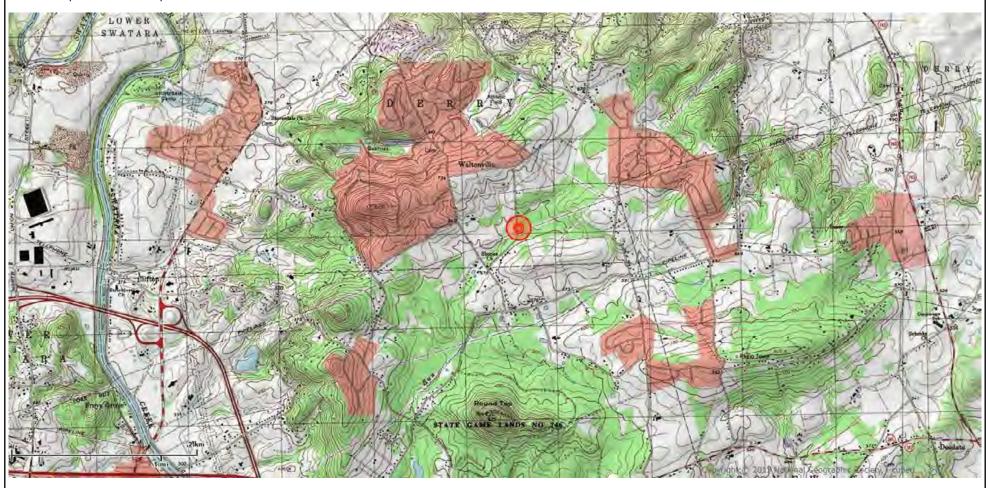


FIGURE 2A: BORING LOCATION PLAN "Waltonville Road" (PPP4)- Dauphin Co, PA

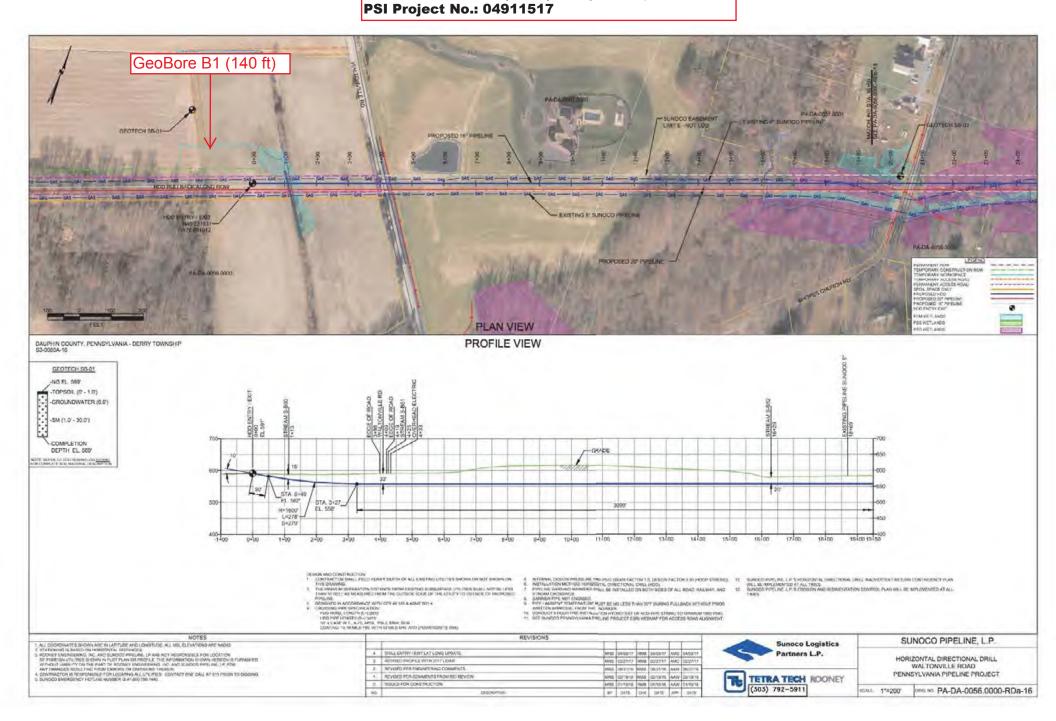


FIGURE 2B: BORING LOCATION PLAN "Waltonville Road" (PPP4)- Dauphin Co, PA

PSI Project No.: 04911517

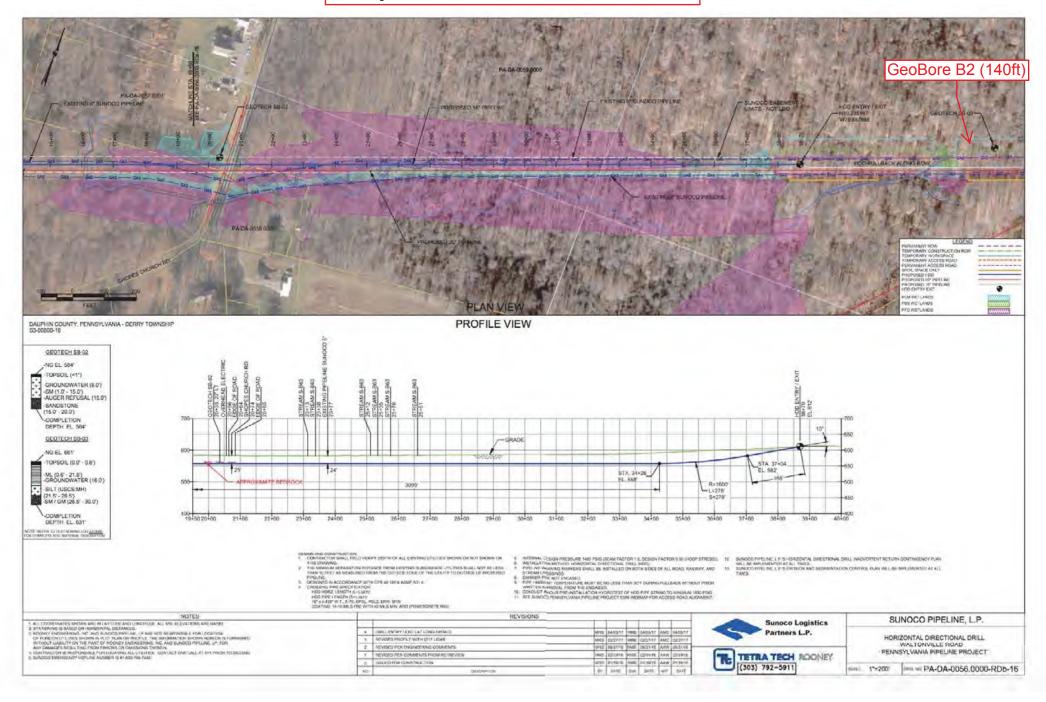
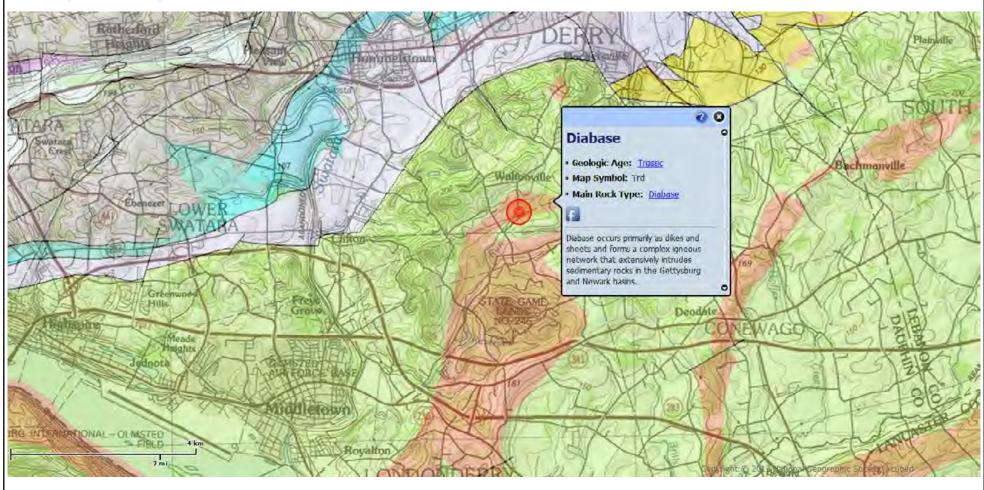


Figure 3: Site Geology Map

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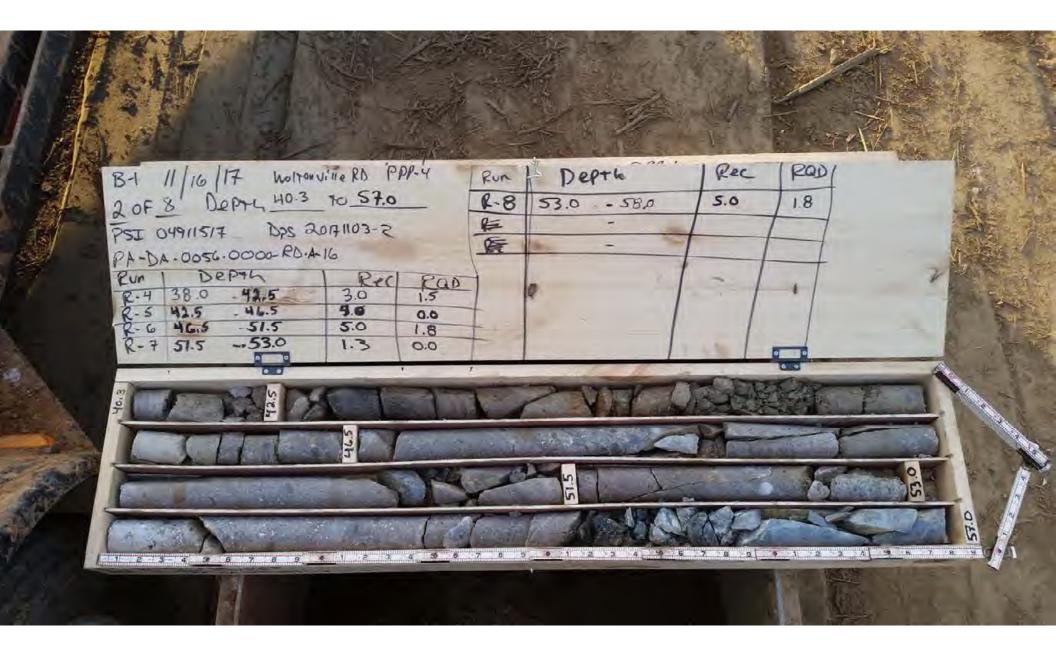
	E STA COM		_		1	<u>1/16/17</u> 11/17/17		l Drilling V: K Gibne		BORING B-1						
	IPLET!			_		143.0 ft	_ DRILLER: B. Deininger DRILL RIG: Ve	ersadrill			<u>y</u>	₽ \\ \[\sqrt{\sq}}}}}}}}\sqit{\sqrt{\sqrt{\sqrt{\sqrt{\sqrt{\sqrt{\sqrt{\sqrt{\sqrt{\sqrt{\sqrt{\sqrt{\sqrt{\sq}}}}}}}\sqrt{\sqrt{\sq}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}	Pre-Core		6.7 feet	
	HMAF			-		N/A	DRILLING METHOD:			ck Coring		Water Ā Ā			11.8 feet	
	/ATIO	-				N/A	SAMPLING METHOD:			000-in Core	_	≽ ∡				
						′a°	HAMMER TYPE:		utoma			BORING	LOCATION:			
LÔNG	TUDE:	E: _			r	n/a°	EFFICIENCY		N/A			See Bori	ng Location F	Plan		
STAT	_		N/A		OFF	SET: N/A	REVIEWED BY:	F.	Hoffm	nan	_					
REMA	ARKS:		_			1				_						
Elevation (feet)	O Depth, (feet)	Graphic Log	Sample Type	Sample No.	Recovery (inches)	МАТІ	ERIAL DESCRIPTION	I	USCS Classification	SPT Blows per 6-inch (SS) RQD & Recovery % (NX)	Moisture, %	× M	25 TRENGTH, tsf		Additional Remarks	
		71/2	$\mathbb{N}^{\mathbb{N}}$			Approximately	1 foot topsoil									
	 			S-1	20		red-brown, Lean CLAY, trac	ce		WOH-1-2-5 N=3	28		* ×			
	- 5 - - 5 - 			S-2	11 5	Grades to San from 5 to 7 fee	dy Lean CLAY with Gravel t.		CL	6-18-16-39 N=34	32			•	LL = 44 PL = 25 Fines=60.4%	
	 - 10 - 			S-3	22	RESIDUUM-Lo wet	ose, Light gray, Silty SAND,	,	SM	2-2-4-6 N=6	25		*		Fines=29.4%	
	 - 15 - 			S-4	20	RESIDUUM-Me Silty SAND, me	edium Dense, Gray-brown, pist/wet		SM	7-15-13-22 N=28	17		×			
	_ 20 _			S-5	24	RESIDUUM-Ve Sandy SILT, m	ery Stiff, Dark gray-brown, oist/wet		ML	11-14-13-15 N=27	28		•		Fines=63.1%	
	_ 25			R-1	35	24.5 feet Conglomeratic light gray-brow Weathered, ve bedded, thin to interbeds of fin Sandstone, sh	· ·	5		RQD=29 Rec=83%				>>4	Q _u = 647.0 tsf ¶55.9 pcf	
int Total Qua		-7.3	k	L	ps	1707 S. Ca Harrisburg	Continued Next Page al Service Industries, ameron Street, Suite E , PA 17104 :: (717) 230-8622			PR	CAT	CT NO.: CT: ION:	Energy Tra Waltonvi Daur	lle Road hin Co.		
The st	atifica	tion li	nes	repr	esent (approximate boun	daries. The transition may	be grac	lual.					S	heet 1 of 5	

DATE STARTED: 11/16/17 DATE COMPLETED: 11/17/17							DRILLER: B. Deininger LOGGED BY: K. Gibney					BORING B-1					
		ON D				143.0 ft	DRILL RIG:	Versadr			<u>y</u>	er	$\overline{\Delta}$	Pre-Core		6.7 feet	
BENC						N/A	DRILLING METHOD	:н	SA/Ro	ck Coring		Water	Ţ	Post-Core		11.8 feet	
ELEV	'ATIO	N:				I/A	SAMPLING METHO			000-in Core		-	Ā				
LATIT	UDE:	_—				a°	HAMMER TYPE:		Automa	atic				LOCATION:			
STAT			I/A		OFFS	n/a° BET: N/A	_ EFFICIENCY REVIEWED BY:		N/A . Hoffm			366	DUIII	ig Location	riali		
REMA	_		N/A		OFFS	DEI. N/A	_ KEVIEWED DI		. HOIIII	Idii	_						
Elevation (feet)	ith, (feet)	Graphic Log	Sample Type	Sample No.	Recovery (inches)	MATE	TERIAL DESCRIPTION			SPT Blows per 6-inch (SS) RQD & Recovery % (NX)	Moisture, %		N	ARD PENETR TEST DATA I in blows/ft © isture		Additional Remarks	
Eleva	S Depth,	Gra	San	Sar	Recov				USCS Classification	SPT Blow RQD & R	Mo	0	ST • Qu	FRENGTH, tsf			
	- 30 - 			R-2	56	light gray-brown Weathered, very bedded, thin to r	SANDSTONE-Light gra , Weathered to Highly broken to massive, cr nedium bedding, with	oss		RQD=46 Rec=94%					>>.	Q _u = 647.0 tsf 154.1 pcf	
						Sandstone, shal	grained and large grain low to sheer, narrowly discontinuities, narrowings	to								1 min.	
	- 35 - 			R-3	60					RQD=32 Rec=100%						1 min. 1 min.	
	 - 40 - 			R-4	36	gray-brown, We. Weathered, sligl bedded, thin to r interbeds of fine Sandstone, shal	SANDSTONE-Light athered to Slightly ntly broken to massive, medium bedding, with grained and large grain low to sheer, narrowly discontinuities, narrow	ned to		RQD=33 Rec=67%					>>,	2nffr284.8 tsf 152.6 pcf 2 min. 1 min.	
	 - 45 -			R-5	48	large joint openi Weathered/very 4-1/4 inches thic Highly Weathere from 40.5 to 42.	ngs broken layer @ 39 fee k) ed/Completely Weather	t (~ red		RQD=0 Rec=100%						2 min. 2 min. 2 min. 2 min.	
	 - 50 _			R-6	60	inches thick) Weathered/High	en layer @ 48.1 feet (~			RQD=36 Rec=100%					>>	1 min. 1 min. 2 min. Q _u = 528.8 tsf	
	 			R-7	16	feet (~ 11 inches Weathered layer thick)	r @ 52.5 feet (~ 6 inche	es		RQD=0 Rec=87%					>>,	Q _u = 647.0 tsf 253 i9.pcf	
	_ 55 _ 60			R-8	60	feet (~ 9 inches DIABASE-Light Weathered to Hi to massive, indis very hard, shallo	ed/very broken layer @ thick) brown to dark gray, ighly Weathered, very b stinct bedding/flow boul w to sheer, narrowly to discontinuities, tight to	oroken ndary,		RQD=36 Rec=100%					>>_	2 min. 2 min. 2 min. 2 min. 2 min1235.0 tsf 167.3 pcf 2 min.	
		, .	_				Continued Next Page										
int Total Qual			k		08	1707 S. Ca Harrisburg,	al Service Industrie meron Street, Suit PA 17104 (717) 230-8622			PR	CAT	ECT I ECT: FION: PA-D	_		ille Roa		

TE COMPLE OMPLETION NCHMARK:	_		11/17/17	DitiEEE to B. Bollinger		DRILLER: B. Deininger LOGGED BY: K. Gibney					BORING B-1						
			143.0 ft	sadrill GT		<u>, </u>	<u>7</u>	Z Pre-	Core		6.7 fee						
			N/A	DRILLING METHOD:		ock Coring		<u> </u>	Z Post	-Core		11.8 fee					
EVATION:			I/A	SAMPLING METHOD:		.000-in Core			-								
TITUDE: —			a°	HAMMER TYPE:	Auton	natic			G LOCA								
TITUDE: — NGITUDE:			/a°	EFFICIENCY	N/A		_	See Bo	ring Loc	ation Pla	an						
ATION: MARKS:	N/A	OFFS	ET: N/A	REVIEWED BY:	F. Hoff	man	_										
Depth, (feet)	Sample Type	Recovery (inches)	MATE	RIAL DESCRIPTION	S Classification	SPT Blows per 6-inch (SS) RQD & Recovery % (NX)	Moisture, %		NDARD PE TEST N in blow Moisture	DATA ws/ft ⊚ ☑ F		Additional Remarks					
60 - 877		Reco			SOSN	SPT BIO RQD &		0	STRENGTH, tsf Qu		Qp 4.0						
	R-	9	61.3 feet. DIABASE -Light to Weathered to High to massive, indisevery hard, shallow medium spaced	broken layer from 58.7 to brown to dark gray, ghly Weathered, very broke tinct bedding/flow boundary w to sheer, narrowly to discontinuities, tight to wide	/,							2 min.					
- 65 -	R-	10 60	feet. DIABASE-Light b Weathered to Sli broken to massiv boundary, very h	ren layer from 61.4 to 64.8 brown to dark gray, ghtly Weathered, very /e, indistinct bedding/flow ard, shallow to sheer, um spaced discontinuities,		RQD=26 Rec=100%						2 min. 2 min. 2 min. 2 min.					
- 70 - 70 	R-	11 60	tight to wide joint			RQD=46 Rec=100%					:	Q. = 844.1 tsf 849.7 pcf 2 min. 2 min. 1 min. 1 min.					
75 -	R-	12 60	feet.	en layer from 75.7 to 77.1		RQD=0 Rec=100%						2 min. 2 min.					
80	R-	13 60	dark brown, Wea Weathered, very hard, cross bedd with interbeds of grained Sandstor to medium space large joint openir Weathered layer thick)	thered to Slightly broken to massive, very ed, thin to medium bedding fine grained and large ne, shallow to sheer, narrov ed discontinuities, narrow to gs @ 79.2 feet (~ 6-1/4 inche en layer @ 80.8 feet (~ 19-	wly o	RQD=30 Rec=100%					>>	2 min. Q _u = 492.2 tsf 255 i.6 pcf 2 min. 2 min.					
85	_	14 60	Conglomeratic S red-gray-brown to Weathered, very hard, cross bedd with interbeds of grained Sandsto	candstone-Light gray to be dark gray-brown, Slightly broken to massive, very ed, thin to medium bedding fine grained and large ne, shallow to sheer, narrowed discontinuities, narrow to gs	wly	RQD=40 Rec=100%					>> \(\)	2 min. 2 min. 1 min. 2 min. 3 min. 3 min. 443.5 tsf					
				Continued Next Page													
				I Service Industries, I		PR	OJI	ECT NC).:	n	49115	17					
terto	ale	no	1707 S. Cai	meron Street, Suite B		PR	OJE	ECT:	Ener			DD (DPS)					
/3/ [/	-K	25	Harrisburg,	PA 17104 (717) 230-8622				TION:		altonville Dauphi							

DATE STARTED: 11/16/17							DRILL COMPANY: Allied Well Drilling					BORING B-1							
DATE CO						11/17/17	DRILLER: B. Deininger LOGGED BY: K. Gibney DRILL RIG: Versadrill GT8 Track					<u>.</u>		-Core	-	6.7 feet			
						143.0 ft N/A	DRILL RIG: VI				_	te		st-Core		11.8 feet			
BENCHN ELEVAT	TION	N. –			N	I/A	SAMPLING METHOD:			ck Coring 000-in Core	_		$ar{ar{f X}}$			11.0 1000			
						a°	HAMMER TYPE:						NG LOCA	ATION:					
LATITUI LONGIT	UDE:	:				/a°	EFFICIENCY N/A						oring Lo	cation F	Plan				
STATION		N	/A		OFFS	ET:N/A	REVIEWED BY:	F. H	offn	nan									
REMARK	(S :_	I	_							T ^		T							
Elevation (feet)	Jepin, (reet)	Graphic Log	Sample Type	Sample No.	Recovery (inches)	MATE	RIAL DESCRIPTION	N	USCS Classification	SPT Blows per 6-inch (SS) RQD & Recovery % (NX)	Moisture, %		N in blo	DATA		Additional Remarks			
9			0)		Rec				sn —	SPT B RQD		0	Qu	GTH, tsf #	Qp 4.0				
- - -	- - - - - -			R-15	60	red-gray-brown to Weathered, very hard, cross bedd with interbeds of grained Sandstor	ANDSTONE-Light gray to be dark gray-brown, Slightl broken to massive, very ed, thin to medium bedding fine grained and large ne, shallow to sheer, narrow and discontinuities, narrow and discontinuities, narrow	ng,		RQD=50 Rec=100%						2 min. 2 min. 2 min. 2 min. 2 min. 2 min2 min.			
-	-			R-16	60					RQD=66 Rec=100%					>>4	2 min. 2 min. 2 min. 2 min. Q. = 623.3 tsf 151.8 pcf 1 min.			
-	05-			R-17	60	Slightly Weather indistinct bedding shallow to sheer, discontinuities, ti	o dark gray, Weathered to ed, very broken to massiv y/flow boundary, very hard narrowly to medium spac ght to wide joint openings 103 feet (~ 2-1/2 inches th	ve, d, ced		RQD=72 Rec=100%					>>,	1 min. a min 83.7 tsf 265.8 pcf 2 min. 2 min.			
- - -				R-18	60	Broken layer @ 1 thick)	106.5 feet (~ 4-1/2 inches	:		RQD=44 Rec=100%						2 min. 1 min. 1 min. 2 min.			
_11′ _ _ _	10_			R-19	56	Weathered/broke	en layer @ 112.3 feet (~ ck)			RQD=18 Rec=94%					>>,	1 min. 2 min. Q = 181.2 tsf f60.6 pcf 1 min.			
1	15			R-20	60	·	@ 114 feet (~ 3 inches the	,		RQD=56 Rec=100%						2 min. 2 min. 2 min. 2 min.			
	20_					, -	117.4 feet (~ 4 inches thic	ck)							>>,	2 min. 1 min. Q _u = 551.3 tsf			
							Service Industries,	Inc.		PF	ROJE	CT N	0.:	1	04044	517			
inte Total Quality.			K	[i	05	1707 S. Car Harrisburg,	meron Street, Suite I			PF	ROJE	CT: ION:	Ene V	Valtonvi Daup	lle Roa	517 IDD (DPS) d (PPP4) , PA DPS PO#2017 110 3			

















DATE STARTED:		DRILL COMPANY:	Allied Well		BORING B-2							
DATE COMPLETED:	11/15/17	DRILL PIC: Vo			a ∑		16.9 feet					
COMPLETION DEPTH BENCHMARK:		DRILL RIG: Ve	rsadrill GT8 Casing/Ro		Water ⊼ A 		17.6 feet					
ELEVATION:	N/A	SAMPLING METHOD:		100-in Core								
	n/a°	HAMMER TYPE:				LOCATION:						
LATITUDE:	n/a°	EFFICIENCY	N/A		See Borii	ng Location Plan						
STATION: N/A	OFFSET:N/A	REVIEWED BY:	F. Hoffm	an			_					
REMARKS:				- T	1							
Elevation (feet) Depth, (feet) Graphic Log Sample Type Sample No.	Recovery (inches)	RIAL DESCRIPTION	USCS Classification	SPT Blows per 6-inch (SS) RQD & Recovery % (NX) Moisture. %	MC × MC	DARD PENETRATION TEST DATA N in blows/ft pisture PL 25 LL 5 TRENGTH, tsf	Additional Remarks					
0 - 3/2 3/1	Approximately 1	foot topsoil	<u> </u>	SPT	Q							
	4 64	ed-brown, SILT with Sand,		7-5-7-6 N=12		××						
5	2 24 Trace organics f	rom 5 to 7 feet.	ML	8-8-8-8 N=16	5		LL = 49 PL = 33					
- 10 -	Gravel, wet	se, Brown, Silty SAND with	SM	2-3-5-7 N=8		×	Fines=12.0%					
	SILT, moist	, Yellow-brown, Sandy	ML	4-7-6-7 N=13) >>;	Non-Plastic Fines=54.7%					
		se, Brown to /n, Silty SAND, moist		2-4-3-7 N=7		×						
25	6 22		SM	3-5-56 48 N=10	3 0	×	Fines=30.5%					
_ 30 _ 10 10	Silty SAND, mois	Continued Next Page	SM				-					
intertek /	1707 S. Car Harrisburg,	l Service Industries, I meron Street, Suite B PA 17104 (717) 230-8622		PROJ PROJ LOCA	TION:	04911 Energy Transfer F Waltonville Roa Dauphin Co 056.0000-Rda+b-16	IDD (DPS)					

DATE STARTED: 11/14/17 DATE COMPLETED: 11/15/17						DRILLER: B. Deininger LOGGED BY: K. Gibney					BORING B-2						
OMPLETIC			_		143.0 ft		rsadrill GT8			P Z		-Core		16.9 fee			
NCHMAR	_				N/A	DRILLING METHOD:		Rock Coring	_	Water Z		t-Core		17.6 fee			
LEVATION	1:				I/A a°	SAMPLING METHOD:						TION					
ATITUDE: ONGITUDE					<u>a </u>	HAMMER TYPE: EFFICIENCY	Auton N/A	iatic	_	BORING See Bo			Plan				
ATION:		/A		OFFS		REVIEWED BY:		man									
MARKS:				-				T -	_					1			
Depth, (feet)	Graphic Log	Sample Type	Sample No.	Recovery (inches)	MATE	RIAL DESCRIPTION	USCS Classification	SPT Blows per 6-inch (SS) RQD & Recovery % (NX)	Moisture, %	× 1	TEST N in blo Moisture STRENG	25 GTH, tsf		Nomano			
30			S-7	23	RESIDUUM-Medi Silty SAND, mois	um Dense, Gray-brown, it	SM	5-5-7-30 N=12	31	(9	×					
- 35 -			R-1	12	Casing refusal @ DIABASE-Light g Highly Weathered broken	234.0 feet ray-brown to light gray, d, very broken to slightly		RQD=0 Rec=25%									
- 40 - 			R-2	26				RQD=0 Rec=44%									
- 45 - 			R-3	42				RQD=0 Rec=70%									
_ 50 _			R-4	24				RQD=0 Rec=40%									
_ 55 _			R-5	60	Weathered to Slip broken to massiv flow bending, pre bending, mineral laminated to med	ray-brown to dark gray, ghtly Weathered, very e, very hard, laminated to gmatic in areas, flow veining, shallow to steep, lium spaced discontinuitie dip, random fractures, tighings	s,	RQD=26 Rec=100%						Q _u = 766.0 tsf 169.1 pcf 2 min.			
60 _	$\rangle\!\rangle\!\rangle\!\rangle$													1			
						Continued Next Page I Service Industries,	Inc										
					1707 S Car	neron Street, Suite E				ECT NO.			049115				
ter	6	4		osi	Harrisburg,	PA 17104	-			ECT:				DD (DPS)			
ality. Assur		•			Telephone:	(717) 230-8622		LC	JCΑ	ΓΙΟN:	VV	Daup	ne Road hin Co.	d (PPP4) , PA			

ATE STAI ATE COMI					1/14/1 <i>7</i> 11/15/17	DRILL COMPANY: DRILLER: B. Deininger	BORING B-2								
COMPLETION DEPTH 143.0 ft										Z 6	Z Pre-	Core		16.9 fee	
NCHMAR	_			ı	N/A	DRILLING METHOD:		Rock Coring		ğ Ţ	Pos	t-Core		17.6 fee	
EVATIO	N:				I/A	SAMPLING METHOD:		2.000-in Core		BORING LOCATION:					
TITUDE: NGITUDI	<u>_</u>			n/a	a° /a°	_ HAMMER TYPE: EFFICIENCY	Autoi N/A	matic		See Bo					
ATION:		I/A		OFFS		REVIEWED BY:	F. Hof				9				
MARKS:															
Depth, (feet)	Graphic Log	Sample Type	Sample No.	Recovery (inches)	MATE	ERIAL DESCRIPTION	USCS Classification	SPT Blows per 6-inch (SS) RQD & Recovery % (NX)	Moisture, %	× 1	TEST N in blo Moisture 2 STRENG	ws/ft	PL LL 50	Additional Remarks	
	X// <i>X</i>		П.С							0	2	.0	4.0	2 min.	
- 65			R-6 R-7 R-8	60	red-gray-brown broken to mass steep, laminate discontinuities, wide joint openi	SANDSTONE-Light to brown, Slightly Weather ive, very hard, shallow to d to medium spaced shallow to shear dip, tight to ngs		RQD=28 Rec=98% RQD=46 Rec=100% RQD=66 Rec=100% RQD=48 Rec=100%					>> 	2 min. 2 min. 2 min. 2 min. 2 min. 2 min. 2 prim1118.7 tsf 158.2 pcf 2 min.	
_ 80 _			R-10	60	Highly Weather	ed layer from 78.8 to 80 fee	et.	RQD=28						2 min. 1 min. Q _u = 459.5 tsf 257in. pcf	
_ 85 _			R-11	60	Weathered to S broken to mass flow bending, pi bending, minera laminated to me shallow to shea to wide joint ope	gray to gray-brown, lightly Weathered, very ive, very hard, laminated to regmatic in areas, flow al veining, shallow to steep, edium spaced discontinuitie r dip, random fractures, tighenings 84.6 feet (~ 10 inches thick	es, nt	Rec=100% RQD=16 Rec=100%						2 min.	
_ 90 _						Continued Next Page									
	m				Profession	al Service Industries, ameron Street, Suite E				ECT NO			49115		
ter		K		osi	Harrisburg	, PA 17104 : (717) 230-8622				ECT: TION:		rgy Tran: 'altonville Dauph		DD (DPS) (PPP4) PA	

DATE STARTED: 11/14/17			DRILL COMPANY: Allied Well Drilling BORII				ORIN	IG	B-2						
DATE						11/15/17	DRILLER: B. Deininger L			<u>y</u>					
						143.0 ft	· -	sadrill GT8		-	Ē	_	Core t-Core		16.9 feet
BENCH	IMAR	K: _				N/A	DRILLING METHOD:		ock Coring	_		▼ Pos	t-Core		17.6 feet
ELEVA	ATION	N:			N n/a	/A	SAMPLING METHOD:		000-in Core	_			TION		
LATITU LONGI	JDE:					a ⁻ /a°	HAMMER TYPE: EFFICIENCY	Autom N/A	iatic			NG LOCA Soring Loc		lan	
STATIC			/A		OFFS		REVIEWED BY:	F. Hoffr	man	_ `	J00 L	oring Loc			
REMAR	_	IN	/A		OFFS	N/A		1 . 1 10111	IIaII						
	Depth, (feet)	Graphic Log	Sample Type	Sample No.	Recovery (inches)	MATE	RIAL DESCRIPTION	USCS Classification	SPT Blows per 6-inch (SS) RQD & Recovery % (NX)	Moisture, %		N in blo Moisture	DATA ws/ft © a b c c c c c c c c c c c c		Additional Remarks
	90 -				ă.		20.05 1/ 5: 1 11:1	٥	SPT		0			Qp 4.0	
- - -	_		R	·12	60	Conglomeratic S brown, Slightly W massive, very ha intrusions, shallo medium spaced shear dip, tight to	89.6 feet (~ 5 inches thick) SANDSTONE-Gray-brown to Veathered, very broken to ard, occasional Diabase by to steep, laminated to discontinuities, shallow to by wide joint openings en layer @ 92.3 feet (~ 4-1/2)		RQD=30 Rec=100%					>>4	2 min. 2 min. 2 min. 2 min. 2 min. 6 min. 159.2 pcf 2 min.
-	95 -		R	1-13	60	,	n from 95.2 to 97.7 feet.		RQD=36 Rec=100%						2 min. 2 min.
-	- - -					Broken layer @ 9	97.6 feet (~ 5 inches thick)								2 min. 2 min. 2 min.
-	100 <u> </u>		R	k-14	60	Highly Weathere	d/very broken layer @ 102		RQD=58 Rec=100%						2 min. Q.,,≣,1417.7 tsf 160.1 pcf 2 min.
	_ _ 105_					feet (~ 11-3/4 inc	ches thick) d layer @ 104.8 feet (~ 9								2 min. 2 min. 2 min.
-	- - -		R	R-15	54	inches thick)	d layer @ 106.5 feet (~ 2-1	/4	RQD=42 Rec=90%						2 min. 2 min. 2 min.
- - -	- 110_ - -		R	k-16	60				RQD=20 Rec=100%						amin'185.2 tsf 256.4 pcf 2 min. 2 min. 2 min.
- - - -	- 115_ - -		R	!-17	60				RQD=82 Rec=100%					>>_	2 min. 2 min. 2 min. 2 min. 62.4 pcf 2 min. 2 min. 2 min.
-	- 120_						Continued Next Page al Service Industries, li	nc.	PR	OJE	CT N	O.:			1 min.
into Total Quality			k	[i)Si	1707 S. Cai Harrisburg,	meron Street, Suite B		PR	CAT	CT:	Ene	rgy Trar		DD (DPS) 1 (PPP4) 1 PA

	E STAI		_			1/14/17		_	L COMPA				l Drilling				BC	RII	NG	B-2
	COM					11/15/		_					': K. Gibne	<u>y</u>	_	∇				
	PLETI		EPT	н _) ft	_	L RIG:		sadrill G			_	Water	_	Pre-C			16.9 feet
	HMAF					N/A		_	LING ME				ck Coring	_	S	_	Post-	-Core		17.6 feet
	/ATIOI	N:				I/A		_	PLING ME	_			000-in Core	_	\vdash	Ā				
	UDE:	_			n/			_	MER TYP	E:	Auto		atic	_				TION:	llon	
	SITUDI					/a°		-	CIENCY		N/A				See I	Boring	LOC	ation P	rian	
STAT	_	N	I/A		OFFS	ET:	N/A	REVI	EWED BY	:	F. Ho	offm	ian	_						
REMA	ARKS:																			
Elevation (feet)	Depth, (feet)	Graphic Log	Sample Type	Sample No.	Recovery (inches)		MATE	RIAL	DESCR	RIPTION		USCS CIASSIIICALION	SPT Blows per 6-inch (SS) RQD & Recovery % (NX)	Moisture, %	× 0	T N i Mois	EST [in blow ture	vs/ft © TH, tsf **	PL LL 50 Qp	- Remarks
	-120-					Cond	olomeratic :	SANDS	TONE-Gra	av-brown to			DOD 00		0		2.0)	4.0	
	- 120- 125- 		- - - -	R-18 R-19 R-20	60 60 60	brow mass intrus medi shea	glomeratic in, Slightly was ive, very his isons, shalld ium spaced ir dip, tight the days ase intrusionals in the same interest in the same intrusionals in the same interest in the same intrusionals in the same intrusionals in the same intrusionals in the same interest	Weather ard, occow to strong discomo o wide	red, very t easional D eep, lamir tinuities, s joint open	oroken to iabase nated to shallow to ings			RQD=62 Rec=100% RQD=92 Rec=100% RQD=88 Rec=100% RQD=72 Rec=98%						>>,	2 min.
126		L					rofessiona 707 S. Ca	al Ser meroi	vice Indi	ustries, Ir	nc.				ECT N		Ener		04911!	
int	er	æ	Κ	Li	15	J Ha	arrisburg,								ΓΙΟN:					
Total Qua						Τe	elephone	(717) 230-86	622			LC	, OM	. IOIV.		000		hin Co.	d (PPP4) ., PA

















SAMPLE IDENTIFICATION

The Unified Soil Classification System (USCS), AASHTO 1988 and ASTM designations D2487 and D-2488 are used to identify the encountered materials unless otherwise noted. Coarse-grained soils are defined as having more than 50% of their dry weight retained on a #200 sieve (0.075mm); they are described as: boulders, cobbles, gravel or sand. Fine-grained soils have less than 50% of their dry weight retained on a #200 sieve; they are defined as silts or clay depending on their Atterberg Limit attributes. Major constituents may be added as modifiers and minor constituents may be added according to the relative proportions based on grain size.

DRILLING AND SAMPLING SYMBOLS

SFA: Solid Flight Auger - typically 4" diameter

flights, except where noted.

HSA: Hollow Stem Auger - typically 31/4" or 41/4 I.D.

openings, except where noted.

M.R.: Mud Rotary - Uses a rotary head with

Bentonite or Polymer Slurry

R.C.: Diamond Bit Core Sampler

H.A.: Hand Auger

P.A.: Power Auger - Handheld motorized auger

SS: Split-Spoon - 1 3/8" I.D., 2" O.D., except where noted.

ST: Shelby Tube - 3" O.D., except where noted.

RC: Rock Core

TC: Texas Cone BS: Bulk Sample

PM: Pressuremeter

CPT-U: Cone Penetrometer Testing with Pore-Pressure Readings

SOIL PROPERTY SYMBOLS

N: Standard "N" penetration: Blows per foot of a 140 pound hammer falling 30 inches on a 2-inch O.D. Split-Spoon.

N₆₀: A "N" penetration value corrected to an equivalent 60% hammer energy transfer efficiency (ETR)

Qu: Unconfined compressive strength, TSF

Q_o: Pocket penetrometer value, unconfined compressive strength, TSF

w%: Moisture/water content, %

LL: Liquid Limit, %

PL: Plastic Limit, %

PI: Plasticity Index = (LL-PL),%

DD: Dry unit weight, pcf

▼,▽,▼ Apparent groundwater level at time noted

RELATIVE DENSITY OF COARSE-GRAINED SOILS ANGULARITY OF COARSE-GRAINED PARTICLES

Relative Density	N - Blows/foot	<u>Description</u>	<u>Criteria</u>
Very Loose Loose	0 - 4 4 - 10	-	Particles have sharp edges and relatively plane sides with unpolished surfaces
Medium Dense	10 - 30	Subangular:	Particles are similar to angular description, but have rounded edges
Dense Very Dense	30 - 50 50 - 80	Subrounded:	Particles have nearly plane sides, but have well-rounded corners and edges
Extremely Dense	80+	Rounded:	Particles have smoothly curved sides and no edges

GRAIN-SIZE TERMINOLOGY

PARTICLE SHAPE

Component	Size Range	<u>Description</u>	Criteria
Boulders:	Over 300 mm (>12 in.)	Flat:	Particles with width/thickness ratio > 3
Cobbles:	75 mm to 300 mm (3 in. to 12 in.)	Elongated:	Particles with length/width ratio > 3
Coarse-Grained Gravel:	19 mm to 75 mm (¾ in. to 3 in.)	Flat & Elongated:	Particles meet criteria for both flat and
Fine-Grained Gravel:	4.75 mm to 19 mm (No.4 to 3/4 in.)		elongated
Coarse-Grained Sand:	2 mm to 4.75 mm (No.10 to No.4)		

Medium-Grained Sand: 0.42 mm to 2 mm (No.40 to No.10) Fine-Grained Sand: 0.075 mm to 0.42 mm (No. 200 to No.40)

Silt: 0.005 mm to 0.075 mm

Clay: <0.005 mm

RELATIVE PROPORTIONS OF FINES

Descriptive Term % Dry Weight

Trace: < 5% With: 5% to 12% Modifier: >12%

Page 1 of 2



GENERAL NOTES

CONSISTENCY OF FINE-GRAINED SOILS

MOISTURE CONDITION DESCRIPTION Description Criteria

Q _U - TSF	N - Blows/foot	Consistency
0 - 0.25	0 - 2	Very Soft
0.25 - 0.50	2 - 4	Soft
0.50 - 1.00	4 - 8	Firm (Medium Stiff)
1.00 - 2.00	8 - 15	Stiff
2.00 - 4.00	15 - 30	Very Stiff
4.00 - 8.00	30 - 50	Hard
8.00+	50+	Very Hard

Dry: Absence of moisture, dusty, dry to the touch Moist: Damp but no visible water Wet: Visible free water, usually soil is below water table

RELATIVE PROPORTIONS OF SAND AND GRAVEL Descriptive Term % Dry Weight

Trace: < 15% With: 15% to 30% Modifier: >30%

STRUCTURE DESCRIPTION

Description	Criteria	Description	<u>Criteria</u>
Stratified:	Alternating layers of varying material or color with	Blocky:	Cohesive soil that can be broken down into small
	layers at least 1/4-inch (6 mm) thick		angular lumps which resist further breakdown
Laminated:	Alternating layers of varying material or color with	Lensed:	Inclusion of small pockets of different soils
	layers less than 1/4-inch (6 mm) thick	Layer:	Inclusion greater than 3 inches thick (75 mm)
Fissured:	Breaks along definite planes of fracture with little	Seam:	Inclusion 1/8-inch to 3 inches (3 to 75 mm) thick
	resistance to fracturing		extending through the sample
Slickensided:	Fracture planes appear polished or glossy, sometimes striated	Parting:	Inclusion less than 1/8-inch (3 mm) thick

SCALE OF RELATIVE ROCK HARDNESS

ROCK BEDDING THICKNESSES

GRAIN-SIZED TERMINOLOGY

Q _U - TSF	Consistency	Description	Criteria
-	Fortuna and a Conft	Very Thick Bedded	Greater than 3-foot (>1.0 m)
2.5 - 10	Extremely Soft	Thick Bedded	1-foot to 3-foot (0.3 m to 1.0 m)
10 - 50	Very Soft	Medium Bedded	4-inch to 1-foot (0.1 m to 0.3 m)
50 - 250	Soft	Thin Bedded	11/4-inch to 4-inch (30 mm to 100 mm)
250 - 525	Medium Hard	Very Thin Bedded	1/2-inch to 11/4-inch (10 mm to 30 mm)
525 - 1,050	Moderately Hard	Thickly Laminated	1/8-inch to ½-inch (3 mm to 10 mm)
1,050 - 2,600 >2 600	Hard Very Hard	Thinly Laminated	1/8-inch or less "paper thin" (<3 mm)

ROCK VOIDS

Voids	Void Diameter	(Typically Sedi	
	<6 mm (<0.25 in)	Component	Size Range
	6 mm to 50 mm (0.25 in to 2 in	Very Coarse Grained	>4.76 mm
0	50 mm to 600 mm (2 in to 24 in	Coargo Grained	2.0 mm - 4.76 mm
•	>600 mm (>24 in)	Medium Grained	0.42 mm - 2.0 mm
Cave	2000 Hilli (224 III)	Fine Grained	0.075 mm - 0.42 mm
		Very Fine Grained	<0.075 mm

ROCK QUALITY DESCRIPTION

Cha

1 inch to 3 inches

3 inches to 6 inches

Greater than 6 inches

DEGREE OF WEATHERING

Rock Mass Description	RQD Value	Slightly Weathered:	Rock generally fresh, joints stained and discoloration
Excellent	90 -100		extends into rock up to 25 mm (1 in), open joints may
Good	75 - 90		contain clay, core rings under hammer impact.
Fair	50 - 75		
Poor	25 -50	Weathered:	Rock mass is decomposed 50% or less, significant
Very Poor	Less than 25		portions of the rock show discoloration and weathering effects, cores cannot be broken by hand or scraped by knife.
gree of Brokeness			
haracteristic	Description	Highly Weathered:	Rock mass is more than 50% decomposed, complete
ess than 1 inch	Very Broken	0 ,	

discoloration of rock fabric, core may be extremely broken and gives clunk sound when struck by Slightly Broken

hammer, may be shaved with a knife.

Page 2 of 2

SOIL CLASSIFICATION CHART

NOTE: DUAL SYMBOLS ARE USED TO INDICATE BORDERLINE SOIL CLASSIFICATIONS

R.A.		ONE	SYMI	BOLS	TYPICAL	
	AJOR DIVISI		GRAPH	LETTER	DESCRIPTIONS	
	GRAVEL AND	CLEAN GRAVELS		GW	WELL-GRADED GRAVELS, GRAVEL - SAND MIXTURES, LITTLE OR NO FINES	
	GRAVELLY SOILS	(LITTLE OR NO FINES)		GP	POORLY-GRADED GRAVELS, GRAVEL - SAND MIXTURES, LITTLE OR NO FINES	
COARSE GRAINED SOILS	MORE THAN 50% OF COARSE	GRAVELS WITH FINES		GM	SILTY GRAVELS, GRAVEL - SAND - SILT MIXTURES	
	FRACTION RETAINED ON NO. 4 SIEVE	(APPRECIABLE AMOUNT OF FINES)		GC	CLAYEY GRAVELS, GRAVEL - SAND - CLAY MIXTURES	
MORE THAN 50% OF MATERIAL IS	SAND AND	CLEAN SANDS		SW	WELL-GRADED SANDS, GRAVELLY SANDS, LITTLE OR NO FINES	
LARGER THAN NO. 200 SIEVE SIZE	SANDY SOILS	(LITTLE OR NO FINES)		SP	POORLY-GRADED SANDS, GRAVELLY SAND, LITTLE OR NO FINES	
	MORE THAN 50% OF COARSE	SANDS WITH FINES		SM	SILTY SANDS, SAND - SILT MIXTURES	
	FRACTION PASSING ON NO. 4 SIEVE	(APPRECIABLE AMOUNT OF FINES)		sc	CLAYEY SANDS, SAND - CLAY MIXTURES	
				ML	INORGANIC SILTS AND VERY FINE SANDS, ROCK FLOUR, SILTY OR CLAYEY FINE SANDS OR CLAYEY SILTS WITH SLIGHT PLASTICITY	
FINE GRAINED SOILS	SILTS AND CLAYS	LIQUID LIMIT LESS THAN 50		CL	INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS	
COILO				OL	ORGANIC SILTS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY	
MORE THAN 50% OF MATERIAL IS SMALLER THAN NO. 200 SIEVE				МН	INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS FINE SAND OR SILTY SOILS	
SIZE	SILTS AND CLAYS	LIQUID LIMIT GREATER THAN 50		СН	INORGANIC CLAYS OF HIGH PLASTICITY	
				ОН	ORGANIC CLAYS OF MEDIUM TO HIGH PLASTICITY, ORGANIC SILTS	
HI	GHLY ORGANIC S	SOILS	77 77 77 77 7 77 77 77 77 77 77 77 77	PT	PEAT, HUMUS, SWAMP SOILS WITH HIGH ORGANIC CONTENTS	



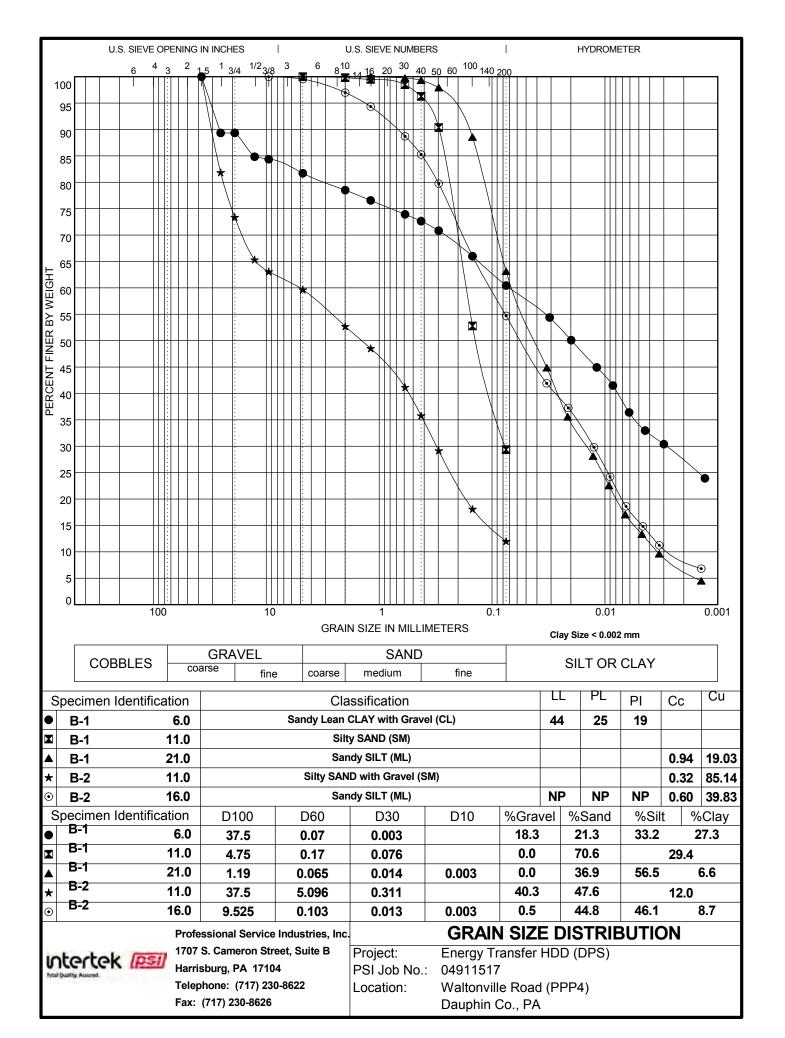
Chapter 4	Engineering Classification of Rock	Part 631
	Materials	National Engineering Handbook

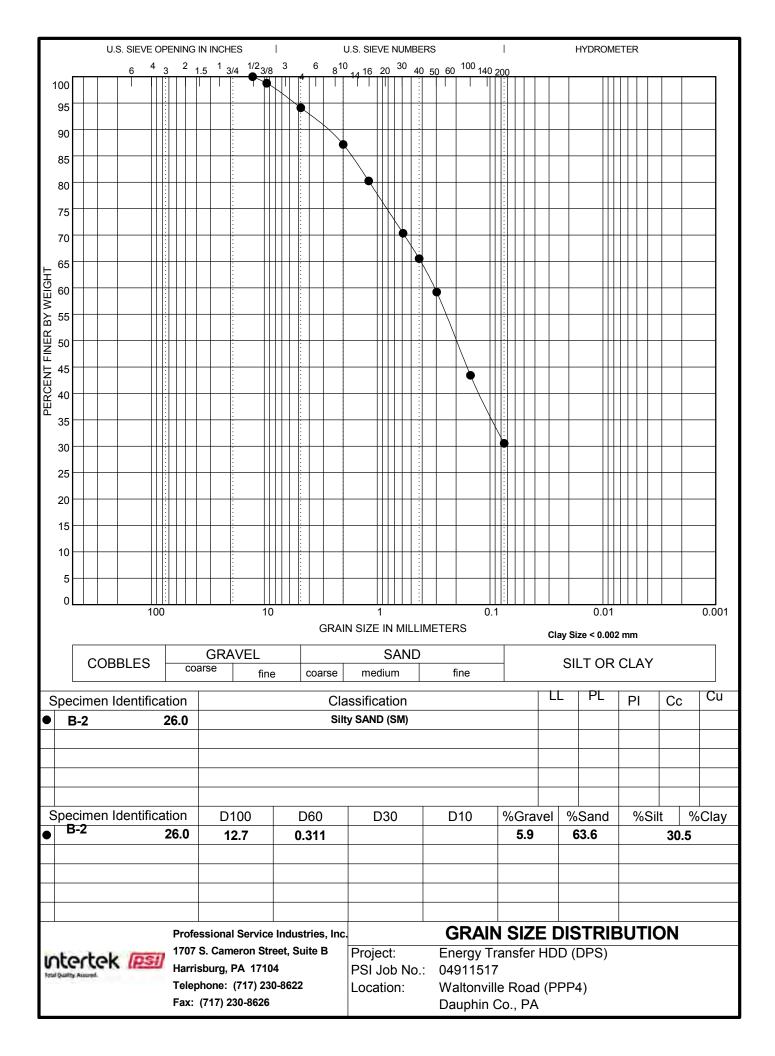
Table 4–3 Hardness and unconfined compressive strength of rock materials

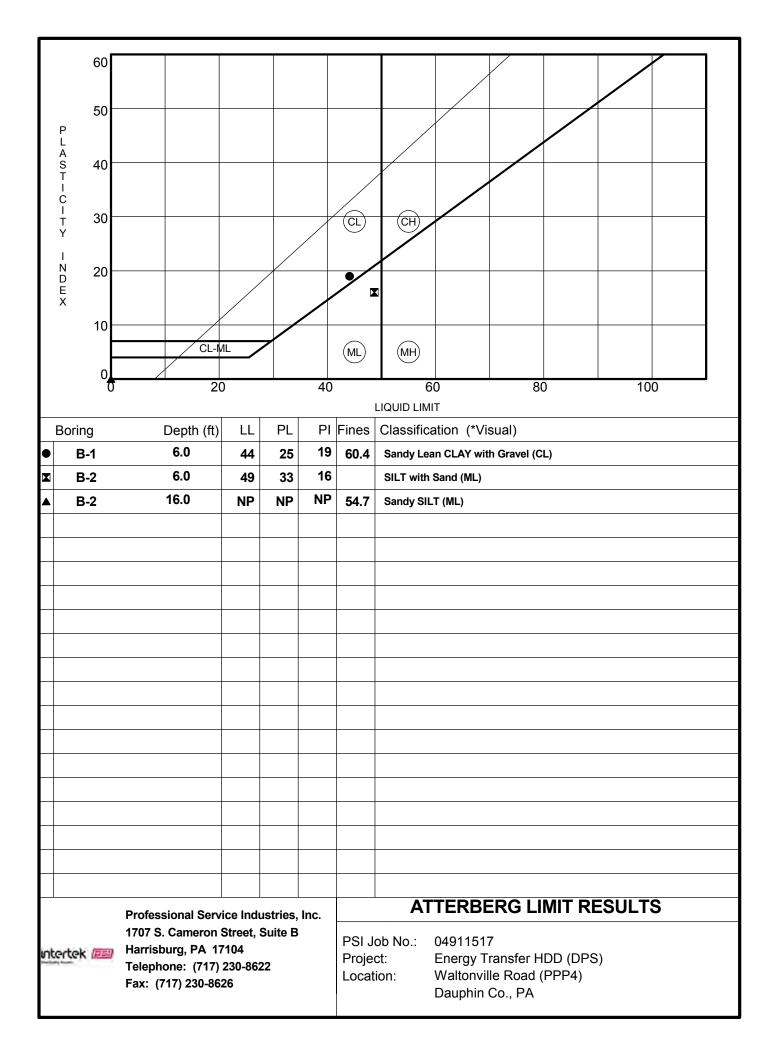
Hardness category	Typical range in unconfined compressive strength (MPa)	Strength value selected (MPa)	Field test on sample	Field test on outcrop
Soil*	< 0.60		Use USCS classification	s
Very soft rock or hard, soil- like material	0.60-1.25		Scratched with fingernail. Slight indentation by light blow of point of geologic pick. Requires power tools for excavation. Peels with pocket knife.	
Soft rock	1.25–5.0		Permits denting by moderate pressure of the fingers. Handheld specimen crumbles under firm blows with point of geologic pick.	
Moderately soft rock	5.0–12.5		Shallow indentations (1–3 mm) by firm blows with point of geologic pick. Peels with difficulty with pocket knife. Resists denting by the fingers, but can be abraded and pierced to a shallow depth by a pencil point. Crumbles by rubbing with fingers.	Crumbles by rubbing with fingers.
Moderately hard rock	12.5–50		Cannot be scraped or peeled with pocket knife. Intact handheld specimen breaks with single blow of geologic hammer. Can be distinctly scratched with 20d common steel nail. Resists a pencil point, but can be scratched and cut with a knife blade.	Unfractured outcrop crumbles under light hammer blows.
Hard rock	50–100		Handheld specimen requires more than one hammer blow to break it. Can be faintly scratched with 20d common steel nail. Resistant to abrasion or cutting by a knife blade, but can be easily dented or broken by light blows of a hammer.	Outcrop withstands a few firm blows before breaking.
Very hard rock	100–250		Specimen breaks only by repeated, heavy blows with geologic hammer. Cannot be scratched with 20d common steel nail.	Outcrop withstands a few heavy ringing hammer blows but will yield large frag- ments.
Extremely hard rock	> 250		Specimen can only be chipped, not broken by repeated, heavy blows of geologic hammer.	Outcrop resists heavy ringing hammer blows and yields, with difficulty, only dust and small fragments.

Method used to determine consistency or hardness (check or	ne).	

Field assessment: ____ Uniaxial lab test: ____ Other: ____ Rebound hammer (ASTM D5873): ____ * See NEH631.03 for consistency and density of soil materials. For very stiff soil, SPT N values = 15 to 30. For very soft rock or hard, soil-like material, SPT N values exceed 30 blows per foot.







			Lc	abura	lory	Sullii	mary	SHEE	けし	Sheet	t 1 of 1
Borehole	Approx. Depth	Liquid Limit	Plastic Limit	Plasticity Index	Qu (tsf)	%<#200 Sieve	Est. Specific Gravity	Water Content (%)	Dry Density (pcf)	Satur- ation (%)	Void Ratio
B-1	1							28	<u> </u>	<u> </u>	
B-1	6	44	25	19		60.4%		32			
B-1	11					29.4%		25			
B-1	16							17			
B-1	21					63.1%		28			
B-1	28				646.98				<u> </u>		
B-1	32				647.03						
B-1	38				284.81						
B-1	49.9				528.80						
B-1	53.6				647.03						
B-1	57.1				1235.03				1	1	
B-1	68.7				844.06				1	1	
B-1	78.5				492.15	1					
B-1	88.4				943.47				1		
B-1	98.8				623.26				<u>'</u>		
B-1	102.3				683.70	ĺ					
B-1	111.8				181.21				1		
B-1	119.4				551.27				1		
B-1	126.3				935.26				1		
B-1	133.5				319.85				<u>'</u>		
B-2	1					ĺ		21			
B-2	6	49	33	16				35	1		
B-2	11					12.0%		34	1		
B-2	16	0	0	0		54.7%		56	1		
B-2	21							30	1		
B-2	26					30.5%		48			
B-2	31							31			
B-2	55.6				766.01	1			1		
B-2	64.1				1118.69				1		
B-2	68.1				890.90				1		
B-2	75.1				329.21	ĺ					
B-2	80.4				459.50				1		
B-2	93.2				804.37				<u> </u>		
B-2	100.9			†	1417.73	1			<u>'</u>	,	
B-2	109.3				185.15				1		
B-2	115				572.07	1			<u>'</u>	,	
B-2	121.8				315.22				<u>'</u>		
B-2	129.8				799.05						
B-2	140.4				916.49				<u> </u>	<u> </u>	

Lahoratory Summary Sheet



Professional Service Industries 1707 S. Cameron Street, Suite B

Harrisburg, PA 17104 Telephone: (717) 230-8622 Fax: (717) 230-8626

Summary of Laboratory Results PSI Job No.: 04911517

Energy Transfer HDD (DPS) Waltonville Road (PPP4) Dauphin Co., PA Project: Location:

PA-DA-0056.0000-Rda+b-16/DPS PO#20171103-2



LEGEND:

© Geotechnical Soil Boring (SB) Locations



GEOTECHNICAL BORING LOCATIONS
HDD S3-0080
DAUPHIN COUNTY, DERRY TOWNSHIP, PA
SUNOCO PENNSYLVANIA PIPELINE PROJECT



TETRA TECH

240 Continental Drive, Suite 200 Newark, Delaware 19713 302.738.7551 fax: 302.454.5988

TEST BORING LOG

Project Name:	SUNOCO PENNSYLVANIA PII	PELINE PROJECT		Project No.: 103IP3406
Project Location:	WALTONVILLE ROAD, HUMM	Page 1 of 1		
HDD No.:	S3-0080	Dates(s) Drilled: 11-11-14	Inspector:	E. WATT
Boring No.:	SB-01	Drilling Method: SPT - ASTM D1586	Driller:	S. HOFFER
Drilling Contractor:	HAD DRILLING	Groundwater Depth (ft): 6.0	Total Depth (ft):	30.0
Boring Location Coording	nates:	40° 13' 55.015" N	76° 40' 54.952" W	/

Doming	Location	n Oooran					10 10 00.010 17					
Sample	Sample	Depth (ft)	Strata D	Depth (ft)	Recov.	Strata	Description of Materials	6" 1	ncrem	ent Blo	we *	N
No.	From	То	From	То	Re.	(USCS)	Description of Materials	0 11	loreni	ciit Dio		
			0.0	1.0			TOPSOIL (12")					
1	3.0	5.0	1.0		16		BROWN TO ORANGE BROWN MEDIUM TO COARSE SAND WITH	2	8	10	11	18
							SOME SILT AND A LITTLE FINE TO COARSE GRAVEL.					
2	8.0	10.0			20		GRAY FINE TO MEIDUM SAND WITH SOME SILT.	2	6	6	6	12
3	13.0	15.0			24		GRAY FINE SAND WITH SOME SILT, TRACE FINE GRAVEL.	1	3	6	12	9
						014						
4	18.0	20.0			8	SM	GRAY FINE TO MEDIUM SAND WITH SOME SILT, AND WITH SOME	3	14	15	15	29
							FINE TO COARSE GRAVEL.					
5	23.0	25.0			22		GRAY AND BROWN FINE TO MEDIUM SAND WITH A LITTLE SILT, AND	6	22	19	50	41
							A LITTLE FINE GRAVEL.					
6	28.0	29.2			10		BROWN TO ORANGE BROWN MEDIUM TO COARSE SAND WITH A	2	15	50/2"		>65
				30.0			LITTLE SILT.					
								†				
								<u> </u>				
							WET ON SPOON AT 6'.	<u> </u>				
							WATER LEVEL THROUGH AUGERS AT 8'.	<u> </u>				
							CAVED AT 21', WATER LEVEL ON CAVE AT 5'.	<u> </u>				
								<u> </u>				
								<u> </u>				
								<u> </u>				
								+				
								+				
								+				
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												<u> </u>

Notes/Comments:

Pocket Pentrometer Testing

DR: DECOMPOSED ROCK

Strata (USCS) Designations are approximated based on visual review, except where indicated in Description of Materials.

* Number of blows of 140 lb. Hammer dropped 30 in. required to drive 2 in. split-spoon sampler in 6 in. increments.

N: Number of blows to drive spoon from 6" to 18" interval.



TETRA TECH

240 Continental Drive, Suite 200 Newark, Delaware 19713 302.738.7551 fax: 302.454.5988

TEST BORING LOG

Project Name:	SUNOCO PENNSYLVANIA PI	PELINE PROJECT		Project No.: 103IP3406					
Project Location:	SHOPS CHURCH ROAD, HUN	HOPS CHURCH ROAD, HUMMELSTOWN, PA							
HDD No.:	S3-0080	Dates(s) Drilled: 11-11-14	Inspector:	E. WATT					
Boring No.:	SB-02	Drilling Method: SPT - ASTM D1586	Driller:	S. HOFFER					
Drilling Contractor:	HAD DRILLING	Groundwater Depth (ft): 6.0	Total Depth (ft):	20.0					
Boring Location Coordin	nates:	40° 14' 0.606" N	76° 40' 27.087" V	<i>I</i>					

Donnig	Lucation	ii Coordii	iales.				40 14 0.000 N					
Sample	Sample	Depth (ft)	Strata D	Depth (ft)	Recov.	Strata	Description of Materials	6" 1	ncreme	ent Ric	WC *	N
No.	From	То	From	То	Re.	(USCS)	Description of Materials	U 11	iciciii	ciit Dic	ws	.,
			0.0	0.0			TOPSOIL (<1")					
1	3.0	5.0	0.0		18		BROWN, YELLOWISH BROWN TO ORANGE BROWN FINE TO COARSE	1	6	11	11	17
							SAND WITH A LITTLE SILT, AND LITTLE F-C GRAVEL.					
2	8.0	9.9			24	=	SAME, WITH PIECES OF UNWEATHERED SANDSTONE.	2	9	26	50/5"	35
							AUGER REFUSAL AT 12', OFF-SET 10' SOUTH, AND CONTINUOULSY					
						SM	AUGERED TO 10'.					
	40.0	40.0					DD WEATHERED TO A VEH OWIGH PROWN TO CRAY FINE TO	8	20	47	F0/0"	40
3	10.0	12.0					DR WEATHERED TO A YELLOWISH BROWN TO GRAY FINE TO		29	17	50/6"	46
							COARSE SAND AND SILT, WITH SOME F-C UNWEATHERED SANDSTON					
				15.0			GRAVEL.					
							AUGERS STICKING UP TOO HIGH TO ROCK CORE. OFF-SET BORING					
							AND CONTINUOUSLY AUGERED TO REFUSAL AT 15"					
							DOCK CODING					
DUNA	45.0	20.0	45.0	20.0	0.4		ROCK CORING	TOD: 4	100/ 00	D: 00/ I	DOD: 00/	
RUN 1	15.0	20.0	15.0	20.0	24		HIGHLY FRACTURED AND HEAVILY WEATHERED GRAY SAND STONE.	TCR: 4	0%, SC	R: 0%, I	RQD: 0%)
							COULD NOT PERFORM AN ADDITIONAL ROCK CORE RUN. BORING					
							CAVED DUE TO HEAVILY FRACTURED/WEATHERED ROCK.					
							WET ON SPOON AT 10'					
							WATER LEVEL THROUGH AUGERS AT 6'.					
							CAVED AT 4', WATER AT SURFACE.					
									<u> </u>			
·												
	ı	1	1	1	1	i	1	ı	1	1	1	

Notes/Comments:

Pocket Pentrometer Testing

DR: DECOMPOSED ROCK

Strata (USCS) Designations are approximated based on visual review, except where indicated in Description of Materials.

^{*} Number of blows of 140 lb. Hammer dropped 30 in. required to drive 2 in. split-spoon sampler in 6 in. increments. N: Number of blows to drive spoon from 6" to 18" interval.



TETRA TECH

240 Continental Drive, Suite 200 Newark, Delaware 19713 302.738.7551 fax: 302.454.5988

TEST BORING LOG

Project N	lame:	SUNOCO PENN	SYLV	ANIA PI	PELINE PROJECT		Project No.: 103IP3406				
Project L	ocation:	SAND HILL ROA	D, NU	MMELS	Page 1 of 1						
HDD No.	:	S3-0080			Dates(s) Drilled: 11-12-14	Inspector:	E. WA	ТТ			
Boring No	0.:	SB-03			Drilling Method: SPT - ASTM D1586	Driller:	S. HO	FER			
Drilling C	ontractor:	HAD DRILLING			Groundwater Depth (ft): 16.0	Total Depth (ft):	30.0				
Boring Location Coordinates:					40° 14' 9.164" N	76° 39' 57.534" V	76° 39' 57.534" W				
	Sample Depth (ft)	Strata Denth (ft)	>	Strata							

Sample	Sample	Depth (ft)	Strata D	Depth (ft)	٥٥. (د	Strata Description of Materials 6" Increment Bl		nt Dia	*	N.		
No.	From	То	From	То	Recov. (in)	(USCS)	Description of iviaterials	0 11	icieme	ant plo	ws	N
			0.0	0.6			TOPSOIL (7")					
1	3.0	5.0	0.6		17		BROWN SILT AND FINE SAND WITH A TRACE FINE	2	7	8	9	15
				6.5			GRAEL.					
2	8.0	10.0	6.5		24		ORANGE BROWN CLAYEY SILT AND FINE SAND, TRACE FINE	4	9	7	12	16
				11.5		N 41	GRAVEL (USCS: ML).					
3	13.0	15.0	11.5		24	ML	ORANGE BROWN TO REDDISH BROWN CLAYEY SILT WITH A LITTLE		2	4	5	6
							FINE SAND, TRACE FINE GRAVEL.					
4	18.0	20.0			24		ORANGE BROWN TO REDDISH BROWN CLAYEY SILT AND FINE		1	7	22	8
				21.5			SAND, TRACE FINE GRAVEL.					
5	23.0	25.0	21.5		15		MOTTLED (GRAY, YELLOWISH BRWN,BLACK) CLAYEY SILT WITH		12	3	11	15
-				26.5		MH	SOME FINE SAND, TRACE FINE GRAVEL. (USCS: MH)					
6	28.0	30.0	26.5		13	SM/	VARI-COLORED FINE TO COARSE SAND AND FINE TO COARSE		21	34	43	55
				30.0		GM	SANDSTONE GRAVEL.					
							SOME GRINDING AT 9'.					
							WET ON SPOON AT 16'.					
							WATER LEVEL NOT DETECTED THORUGH AUGERS.					
							CAVED AT 26', WATER LEVEL ON CAVE AT 20'.					
-												

Notes/Comments:

Pocket Pentrometer Testing

S1: > 4 TSF S4: 1.25 TSF

S2: 3 TSF S3: 1.5 TSF DR: DECOMPOSED ROCK

Strata (USCS) Designations are approximated based on visual review, except where indicated in Description of Materials.

* Number of blows of 140 lb. Hammer dropped 30 in. required to drive 2 in. split-spoon sampler in 6 in. increments.

N: Number of blows to drive spoon from 6" to 18" interval.

GEOTECHNICAL LABORATORY TESTING SUMMARY SUNOCO PENNSYLVANIA PIPELINE PROJECT HDD \$3-0080

	Test					Percent	Atterburg	Limits (AS	TM D4318)	USCS
HDD	Boring	Sample	Depth of S	Sample (ft.)	Content, %	Silts/Clays, %	Liquid	Plastic	Plasticity	Classif.
No.	No.	No.	From To		(ASTM D2216)	(ASTM D1140)	Limit, %	Limit, %	Index, %	(ASTM D2487)
	2		8.0	10.0	19.1	30.4	-	-	-	-
	SB-01	3	13.0	15.0	17.5	27.2	-	-	-	-
	36-01	5	23.0	25.0	16.3	21.0	-	-	-	-
		6	28.0	29.2	16.7	16.2	-	-	-	-
	SB-02	1	3.0	5.0	13.8	18.9	-	-	-	-
S3-0080		2	8.0	9.9	9.6	14.5	-	-	-	-
33-0000		3	10.0	12.0	29.8	46.2	-	-	-	-
		1	3.0	5.0	15.1	55.7	-	-	-	-
		2	8.0	10.0	39.4	54.0	49	34	15	ML
	SB-03	3	13.0	15.0	50.0	81.0	-	-	-	-
		4	18.0	20.0	49.5	66.3	-	-	-	-
		5	23.0	25.0	45.5	73.7	53	38	15	MH

Notes:

1) Sample depths based on feet below grade at time of exploration.

REGIONAL GEOLOGY SUMMARY SUNOCO PENNSYLVANIA PIPELINE PROJECT HDD S3-0080

HDD No.	NAME	BORING NO.	REGIONAL GEOLOGY DESCRIPTION	GENERAL TOPOGRAPHIC SETTING	BEDROCK FORMATION	GENERAL ROCK TYPE	APPROX MAX FM THICKNESS (FT)	DEPTH TO ROCK (Ft bgs) based on nearby well drilling logs	NOTES / COMMENTS
\$3-0080	Wetland C26 - Shopes Church Rd.	SB-02	Diabase - occurs primarily as dikes and sheets and forms a complex igneous network that extensively intrudes sedimentary rocks in the Gettysburg and Newark basins.	Moderately sloping rolling hills	Diabase	Ophitic texture, an important variety of basalt texture where pyroxene (or occasionally olivine) forms larger crystals and typically contains numerous crystals of plagioclase (right).	N/A	10-62	Diabase - Medium- to coarse-grained, quartz-normative tholeiite; composed of labradorite and various pyroxenes; occurs as dikes, sheets, and a few small flows. Includes the dark-gray York Haven Diabase (high titanium oxide) and the slightly younger Rossville Diabase (low titanium oxide). In chilled margins, the Rossville is distinguished from the York Haven by its lighter gray color and distinctive, sparse, centimeter-sized calcic-plagioclase phenocrysts.

<u>Note</u>: Source of well log data - http://www.dcnr.state.pa.us/topogeo/groundwater/pagwis/records/index.htm. All other sources as referenced in comments section.

ROCK CORE DESCRIPTION SUMMARY SUNOCO PENNSYLVANIA PIPELINE PROJECT HDD \$3-0080

			Core De	epth (ft)				Dept	h (ft)			Bedding		
Location	Boring No.	Core Run	From	То	TCR (%)	SCR (%)	RQD (%)	From	То	Weathering	Classification	Thickness (ft)	Color	Discontinuity Data
S3-0080	SB-2	1	15	20	40	0	0	15	20	Heavily	Sandstone	Massive	ı (¬rav	Heavily fractured, ranging from 0° to 90°

FIELD DESCRIPTION AND LOGGING SYSTEM FOR SOIL EXPLORATION

GRANULAR SOILS

(Sand, Gravel & Combinations)

<u>Density</u>	N (blows)*	Particle S	ize Identifica	tion				
Very Loose	5 or less	Boulders	8 in. diame					
Loose	6 to 10							
Medium Dense	11 to 30	Cobbles	3 to 8 in. diameter					
Dense	31to 50	Gravel	Coarse (C)	3 in. to ¾ in. sieve				
Very Dense	51 or more		Fine (F)	¾ in. to No. 4 sieve				
very bense	31 01 111010	Sand	Coarse (C)	No. 4 to No. 10 sieve				
				(4.75mm-2.00mm)				
Relative Proporti	ons		Medium	No. 10 to No. 40 sieve				
Description Term	<u>Percent</u>		(M)	(2.00mm – 0.425mm)				
Trace	1 - 10		Fine (F)	No. 40 to No. 200 sieve				
Little	11 - 20			(0.425 – 0.074mm)				
Some	21 - 35	Silt/Clay	Less Than a	No. 200 sieve (<0.074mm)				
And	36 - 50	Site, cia,						

COHESIVE SOILS

(Silt, Clay & Combinations)

Consistency	N (blows)*	Plasticity	
Very Soft	3 or less	<u>Degree of Plasticity</u>	Plasticity Index
Soft	4 to 5	None to Slight	0 - 4
Medium Stiff	6 to 10	Slight	5 - 7
Stiff	11 to 15	Medium	8- 22
Very Stiff	16 to 30	High to Very High	> 22
Hard	31 or more	, ,	

ROCK (Rock Cores)

Rock	Rock
Quality Designation	Quality <u>Descripti</u>
(RQD), %	<u>on</u>
0-25	Very Poor
25-50	Poor
50-75	Fair
75-90	Good
90-100	Excellent

*N - Standard Penetration Resistance. Driving a 2.0" O.D., 1-3/8" I.D. sampler a distance of 18 inches into undisturbed soil with a 140 pound hammer free falling a distance of 30.0 inches. The number of hammer blows to drive the sampler through each 6 inch interval is recorded; the number of blows required to drive the sampler through the final 12 inch interval is termed the Standard Penetration Resistance (SPR) N-value. For example, blow counts of 6/8/9 (through three 6-inch intervals) results in an SPR N-value of 17 (8+9).

Groundwater observations were made at the times indicated. Groundwater elevations fluctuate throughout a given year, depending on actual field porosity and variations in seasonal and annual precipitation.

UNIFIED SOIL CLASSIFICATION SYSTEM [Casagrande (1948)]

Major Divisions			Group Symbols	Typical Descriptions	Laboratory Classifications												
	n is larger	Clean gravel (Little or no fines)	GW	Well-graded gravels, gravel- sand mixtures, little or no fines		nbols ⁽¹⁾	$C_{u=\frac{D_{60}}{D_{10}}}$ greater than 4: $C_{c=\frac{(D_{30})2}{D_{10} \times D_{60}}}$ between 1 and 3										
No. 200 sieve)	Gravels More than half of coarse fraction is larger than No. 4 sieve size	Clean (Little or	GP	Poorly graded gravels, gravel- sand mixtures, little or no fines	d gravel from grain size curve. station smaller than No. 200 sieve), classified as follows: GW, GP, SW, SP GM. GC, SM, SC	ng dualsyr	Not meeting C _u or C _c requirem	ents for GW									
	Gra n half of co than No. 4	Gravel with fines (Appreciable amount of fines)	GM	Silty gravels, gravel-sand-silt mixtures	grain size of the No. 2 sllows:	1, SC ases requir	Atterberg limits below A Line or I p less than 4	Limits plotting in hatched zone with I p between 4 and 7 are									
Grained Soils al is larger than No	More tha	Gravel v (Appre amount	GC	Clayey gravels, gravel-sand-clay mixtures	gravel from tion smaller assified as fr w, GP, SW	ordenline ca	Atterberg limits above A line with I p greater than 7	borderline cases requiring use of dual symbols									
Coarse Graine f material is la	maller than	sands to fines)	sw	Well graded sands, gravely sands, little or no fines	of sand and of fines (fraced soils are claps of percent Gercent Gercen		$C_{u=\frac{D_{60}}{D_{10}}}$ greater than 6 $C_{c=}=\frac{(D_{30})2}{D_{10}\times D_{60}}$ between 1 and 3										
Coarse Grained Soils (More than half of material is larger than No. 200 sieve)	Sands (More than half of coarse fraction is smaller than No. 4 Sieve)	Clean sands {Little or no fines}	SP	Poorly graded sands, gravelly sands, little or no fines	Determine Percentage of sand and gravel from grain size curve. Depending on Percentage of fines (fraction smaller than No. 200 sieve), coarse-grained soils are classified as follows: Less than 5 percent GW, GP, SW, SP More than 12 percent GM. GC, SM, SC	5 to 12	Not meeting C_u or C_σ requirements for SW										
W)	half of coa	ı fines able fines)	SM	Silty sands, sand- silt mixtures	Determing		Atterberg limits below A Line or I p less than 4	Limits Plotting in hatched									
	(More than	Sands with fines (Appreciable amount of fines)	sc	Clayey sands, sand-clay mixtures			Atterberg limits above A line with I p greater than 7	zone with I p between 4 and 7 are borderline cases requiring use of dual symbols									
Major	Divisions	Group Symbols	Typica	Descriptions	For soils plotting r When w _L is near	early o	on A line use dual symbols i.e., lp : a CL-CH or ML-MH. Take near as :	= 29.5, w _L =60 gives CH-MH. ± 2 percent.									
	ys han 50)	ML	sands, rock fl	s and very fine our, silty or clayey r clayey silts with y		புப Line:											
200 sieve)	Silts and clays d limit less than 50)	CL	plasticity, gra	ys of low to medium velly clays , sandy ays, lean clays	50 — U	Line:	0.73(LL - 20) 0.9(LL - 8)	Or I									
ls r than No.	Sits (Liquid li	OL	Organic silts clays of low	and organic silty plasticity	% (L) %			, or other lands of the lands o									
Fine-grained soils (More than half of material is smaller than No. 200 sieve)	iquid ilmit 150)	мн	Inorganic silts diatomaceous soils, elastic s	s, micaceous or s fine sandy or silty silts	Plasticity Index (PI), %	:	13 y 1 y 3	MH or OH									
Fir half of mat	Silts and Clays (Liquid limit greater than 50)	СН	Inorganic clay	ys of high plasticity,	Plas		Cr. or										
(More than	Silts ar	ОН	Organic clays plasticity, org	s of medium to high anic silts	7	10	ML or OL 20 30 40 50 60	70 80 90 100									
	Peat and other highly organic solls				Liquid Limit (LL)												

⁽¹⁾ Borderline classifications, used for soils possessing characteristics of two groups, are designated by combinations of group symbols. For example: GW-GC. well-graded gravel-sand mixture with clay binder.

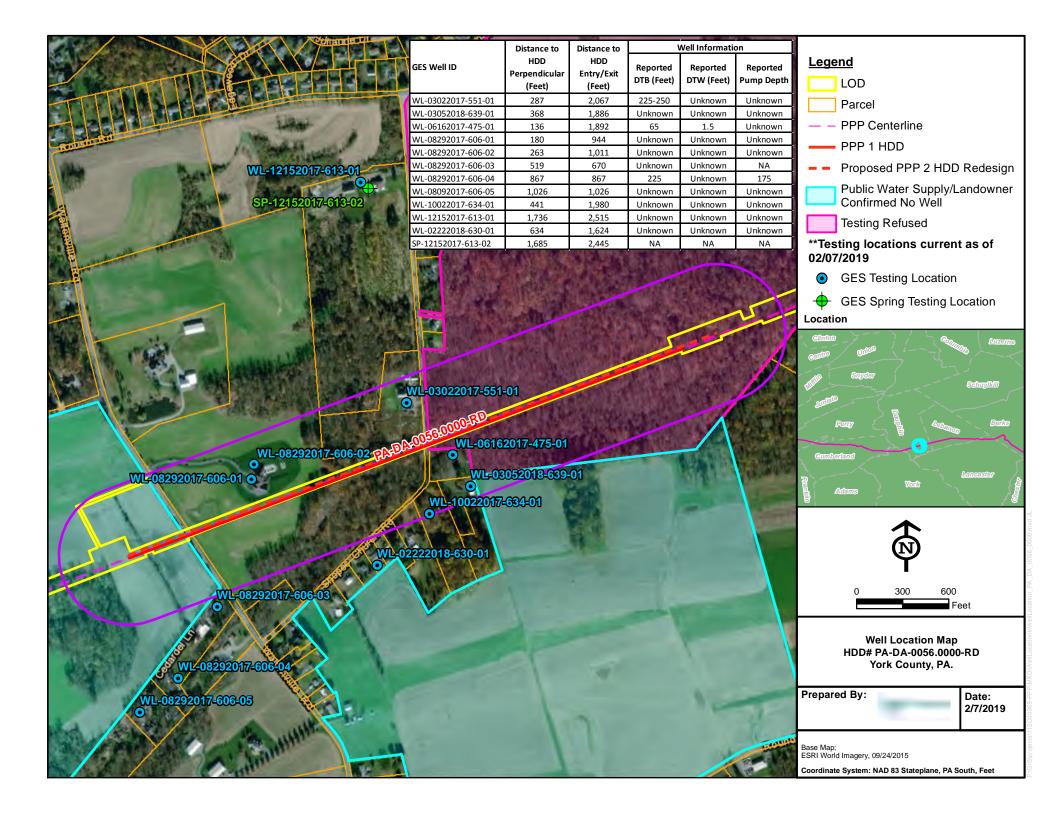
ATTACHMENT 3

ATTACHMENT 3 WELLS WITHIN 0.5 MILES OF PROPOSED 16" HDD TRACE - SUNOCO WALTONVILLE ROAD FROM PAGWIS DATABASE 2-12-19

FID	PAWeIIID	County	Municipali	QuadName	WellAddres	WellZip	DataDrilla	TypeOfActi	LatitudeDD	LongitudeD	Driller	OriginalOw		
		•	•		WellAddleS	Cod	DateDille			· ·		=		
0	86721		DERRY TWP.	MIDDLETOWN	4000 Now '	47000	0000 00 17	NEW WELL	40.23111	-76.69028	ETNOYER WELL DRILLING	SHULER GARY		
1	478751 489473		DERRY TWP. DERRY TWP.		1629 Nottingham Drive 1629 Nottingham Drive		2009-06-17 2009-06-17	OTHER OTHER	40.23383 40.23383	-76.68906 -76.68906	MYERS BROS DRILLING CONTRACTORS INC MYERS BROS DRILLING CONTRACTORS INC	Lutz Lutz		
3	480988		DERRY TWP.		1630 Nottingham Drive	17030	2010-08-02	NEW WELL	40.23354	-76.68886	MYERS BROS DRILLING CONTRACTORS INC	Button		
4	480989		DERRY TWP.		1630 Nottingham Drive		2010-08-02	NEW WELL	40.23354	-76.68886	MYERS BROS DRILLING CONTRACTORS INC	Button		
5	481757		DERRY TWP.		1630 Nottingham Drive		2010-08-02	NEW WELL	40.23354	-76.68886	MYERS BROS DRILLING CONTRACTORS INC	Button		
6	86731		DERRY TWP.	MIDDLETOWN				NEW WELL	40.23222	-76.68778	MYERS BROS DRILLING CONTRACTORS INC	WHITTLE STEVE		
7	649824	DAUPHIN	DERRY TWP.		Deerfield Dr Hummlestown	17036	2017-05-10	NEW WELL	40.23573	-76.68715	MYERS BROS DRILLING CONTRACTORS INC	Bellezza		
8	86732	DAUPHIN	DERRY TWP.	MIDDLETOWN				NEW WELL	40.2325	-76.68694	MYERS BROS DRILLING CONTRACTORS INC	DEMMEL BILL		
9	86734	DAUPHIN		MIDDLETOWN				NEW WELL	40.23194	-76.68667	MYERS BROS DRILLING CONTRACTORS INC	NYE HAROLD E		
10	657129		DERRY TWP.	MIDDLETOWN	1625 Landvater Rd. Hummelstown	17036	1994-12-02	NEW WELL	40.23305	-76.68589	MYERS BROS DRILLING CONTRACTORS INC	Kiessling		
11	86733		DERRY TWP.	MIDDLETOWN			1070 10 00	NEW WELL	40.23222	-76.68583	MYERS BROS DRILLING CONTRACTORS INC	VICKROY RICHARD		
12	17640		DERRY TWP.	MIDDLETOWN			1972-10-06		40.23444	-76.68556	HARRISBURG'S KOHL BROS INC	LINEBAUGH L L		
13	17644		DERRY TWP.	MIDDLETOWN	1108 Waltonville Road	17036	1973-03-27	NEW WELL	40.23778 40.23788	-76.68528 -76.68505	ETNOYER WELL DRILLING SENSENIG & WEAVER WELL DRILLING	LIM HANG		
15	501319 501320		DERRY TWP. DERRY TWP.		1108 Waltonville Road		2012-08-16	NEW WELL	40.23788	-76.68505	SENSENIG & WEAVER WELL DRILLING SENSENIG & WEAVER WELL DRILLING	Sheppard and Son Builders Sheppard and Son Builders		
16	501320		DERRY TWP.		1108 Waltonville Road		2012-08-16	NEW WELL	40.23788	-76.68505	SENSENIG & WEAVER WELL DRILLING	Sheppard and Son Builders		
17	501321		DERRY TWP.		1108 Waltonville Road		2012-08-16	NEW WELL	40.23788	-76.68505	SENSENIG & WEAVER WELL DRILLING	Sheppard and Son Builders		
18	423853		DERRY TWP.		1441 DEERFIELD DRIVE	11000	2008-05-21	NEW WELL	40.23667	-76.68389	MYERS BROS DRILLING CONTRACTORS INC	MCCURDY		
19	86668		DERRY TWP.	MIDDLETOWN	= == = =			NEW WELL	40.23861	-76.68278	HARRISBURG'S KOHL BROS INC	PROJECT BLDRS		
20	86669		DERRY TWP.	MIDDLETOWN				NEW WELL	40.23861	-76.68278	HARRISBURG'S KOHL BROS INC	PROJECT BLDRS		
21	490370	DAUPHIN	DERRY TWP.		1301 Waltonville Road Hummelstown PA		2010-02-19	OTHER	40.23457	-76.68163	MYERS BROS DRILLING CONTRACTORS INC	Custer Homes		
22	490371	DAUPHIN	DERRY TWP.		1301 Waltonville Road Hummelstown PA		2010-02-19	OTHER	40.23457	-76.68163	MYERS BROS DRILLING CONTRACTORS INC	Custer Homes		
23	490275		DERRY TWP.		1301 Waltonville Road Hummelstown PA		2010-02-19	OTHER	40.23457	-76.68163	MYERS BROS DRILLING CONTRACTORS INC	Custer Homes		
24	490276	DAUPHIN			1301 Waltonville Road Hummelstown PA		2010-02-18	OTHER	40.23457	-76.68163	MYERS BROS DRILLING CONTRACTORS INC	Custer Homes		
25	490274		DERRY TWP.		1301 Waltonville Road Hummelstown PA		2010-02-18	OTHER	40.23457	-76.68163	MYERS BROS DRILLING CONTRACTORS INC	Custer Homes		
26	490272		DERRY TWP.		1301 Waltonville Road Hummelstown PA		2010-02-17	OTHER	40.23457	-76.68163	MYERS BROS DRILLING CONTRACTORS INC	Custer Homes		
27	490273		DERRY TWP.		1301 Waltonville Road Hummelstown PA		2010-02-17	OTHER	40.23457	-76.68163	MYERS BROS DRILLING CONTRACTORS INC	Custer Homes		
28	492932		DERRY TWP.		1301 Waltonville Road		2010-02-05 2010-07-21	NEW WELL	40.23457 40.23489	-76.68163	MYERS BROS DRILLING CONTRACTORS INC MYERS BROS DRILLING CONTRACTORS INC	Custer Homes		
30	480934 86592		DERRY TWP. DERRY TWP.	MIDDLETOWN	1301 Waltonville Road		2010-07-21	NEW WELL	40.23489	-76.68125 -76.67972	JOHN THRAN	Custer Homes BERTOLDI A		
31	86744		DERRY TWP.	MIDDLETOWN				NEW WELL	40.23944	-76.67861	MYERS BROS DRILLING CONTRACTORS INC	SMITH GERRY		
32	86741		DERRY TWP.	MIDDLETOWN				NEW WELL	40.23944	-76.67806	MYERS BROS DRILLING CONTRACTORS INC	PEFFLEY S		
33	86494		DERRY TWP.	MIDDLETOWN			1980-12-12	NEW WELL	40.24	-76.67778	MYERS BROS DRILLING CONTRACTORS INC	RIDGELAND CORP		
34	86499		DERRY TWP.	MIDDLETOWN			1983-09-29	NEW WELL	40.23972	-76.67778	MYERS BROS DRILLING CONTRACTORS INC	RIDGELAND CORP		
35	86497	DAUPHIN	DERRY TWP.	MIDDLETOWN			1979-08-16	NEW WELL	40.24	-76.67722	MYERS BROS DRILLING CONTRACTORS INC	GROVE D		
36	86460	DAUPHIN	DERRY TWP.	MIDDLETOWN			1981-11-01	NEW WELL	40.24	-76.67611	EICHELBERGERS INC.	LORD P		
37	86690		DERRY TWP.	MIDDLETOWN				NEW WELL	40.24	-76.67611	EICHELBERGERS INC.	EBERSOLE RALPH		
38	642207		DERRY TWP.	MIDDLETOWN	1425 Shopes Church Road	17036	2016-05-31	NEW WELL	40.23115	-76.67577	EICHELBERGERS INC.	Homesale Settlement Services		
39	258988		DERRY TWP.	MIDDLETOWN	Rousch Road		1995-03-27	NEW WELL	40.23972	-76.67566		Hogg		
40	86695	DAUPHIN		MIDDLETOWN				NEW WELL	40.23556	-76.67472	HARRISBURG'S KOHL BROS INC	BONAWITZ GLADYS		
41	86748	DAUPHIN		MIDDLETOWN	4050 Charas Church Dand	47000	2042 00 02	NEW WELL	40.23972	-76.67472	MYERS BROS DRILLING CONTRACTORS INC	WINFRED HOMES		
42	501396 501429		DERRY TWP.		1250 Shopes Church Road		2012-08-23 2012-08-22	NEW WELL	40.23806 40.23806	-76.67445 76.67445	SENSENIG & WEAVER WELL DRILLING	Zimmerman		
43	501429		DERRY TWP. DERRY TWP.		1250 Shopes Church Road 1250 Shopes Church Road		2012-08-22	NEW WELL	40.23806	-76.67445 -76.67445	SENSENIG & WEAVER WELL DRILLING SENSENIG & WEAVER WELL DRILLING	Zimmerman Zimmerman		
45	501486		DERRY TWP.		1250 Shopes Church Road		2012-08-22	NEW WELL	40.23806	-76.67445	SENSENIG & WEAVER WELL DRILLING SENSENIG & WEAVER WELL DRILLING	Zimmerman		
46	501487		DERRY TWP.		1250 Shopes Church Road		2012-08-22	NEW WELL	40.23806	-76.67445	SENSENIG & WEAVER WELL DRILLING	Zimmerman		
47	501488		DERRY TWP.		1250 Shopes Church Road		2012-08-22	NEW WELL	40.23806	-76.67445	SENSENIG & WEAVER WELL DRILLING	Zimmerman		
48	86742		DERRY TWP.	MIDDLETOWN	·			NEW WELL	40.24028	-76.67417	MYERS BROS DRILLING CONTRACTORS INC	MATTHEWS JIM		
49	86452	DAUPHIN	DERRY TWP.	MIDDLETOWN			1980-10-01	NEW WELL	40.23194	-76.67389	EICHELBERGERS INC.	SHISSLER J		
50	666174	DAUPHIN	DERRY TWP.		1335 SHOPE'S CHURCH ROAD		2005-06-02	NEW WELL	40.2355	-76.67383	MYERS BROS DRILLING CONTRACTORS INC	MCLAIN & amp; SON CONTR		
51	86743		DERRY TWP.	MIDDLETOWN				NEW WELL	40.24056	-76.67333	MYERS BROS DRILLING CONTRACTORS INC	DICKERSON LEE		
52	86740		DERRY TWP.	MIDDLETOWN				NEW WELL	40.24083	-76.67278	JOHN THRAN	MOWRER D		
53	86739		DERRY TWP.	MIDDLETOWN				NEW WELL	40.24139	-76.67222	MYERS BROS DRILLING CONTRACTORS INC	TOMKO P		
54	416933		DERRY TWP.		2149 SANDHILL ROAD		2006-06-01	NEW WELL	40.23444	-76.66917	MYERS BROS DRILLING CONTRACTORS INC	CULLARI		
55	416959		DERRY TWP.		2149 SANDHILL ROAD		2006-05-31	NEW WELL	40.23444	-76.66917	MYERS BROS DRILLING CONTRACTORS INC	CULLARI		
56	416938		DERRY TWP.		2149 SANDHILL ROAD		2006-05-31	NEW WELL	40.23444	-76.66806	MYERS BROS DRILLING CONTRACTORS INC	CULLARI		
57	416949		DERRY TWP.		2149 SANDHILL ROAD		2006-05-26	NEW WELL	40.23444	-76.66806	MYERS BROS DRILLING CONTRACTORS INC	CULLARI		
58	416960		DERRY TWP.	MIDDLETOWY	2149 SANDHILL ROAD		2006-05-30	NEW WELL	40.23444	-76.66444	MYERS BROS DRILLING CONTRACTORS INC	CULLARI CHANK JERRY		
59 60	86753 86752		DERRY TWP. DERRY TWP.	MIDDLETOWN				NEW WELL	40.24 40.23861	-76.66167 -76.66111	ETNOYER WELL DRILLING MYERS BROS DRILLING CONTRACTORS INC	SHANK JERRY LUTRELL INC R W		
61	86754		DERRY TWP.	MIDDLETOWN				NEW WELL	40.23861	-76.66	MYERS BROS DRILLING CONTRACTORS INC	LUTRELL INC R W		
01	00704	PAOFIIN	DEIXIXI TWP.	INIDDEE LONN				IALAA AAETT	40.2300 I	-70.00	MILEVO DIVOS DIVIETINO CONTRACTORS INC	LOTINELL INC IX W		

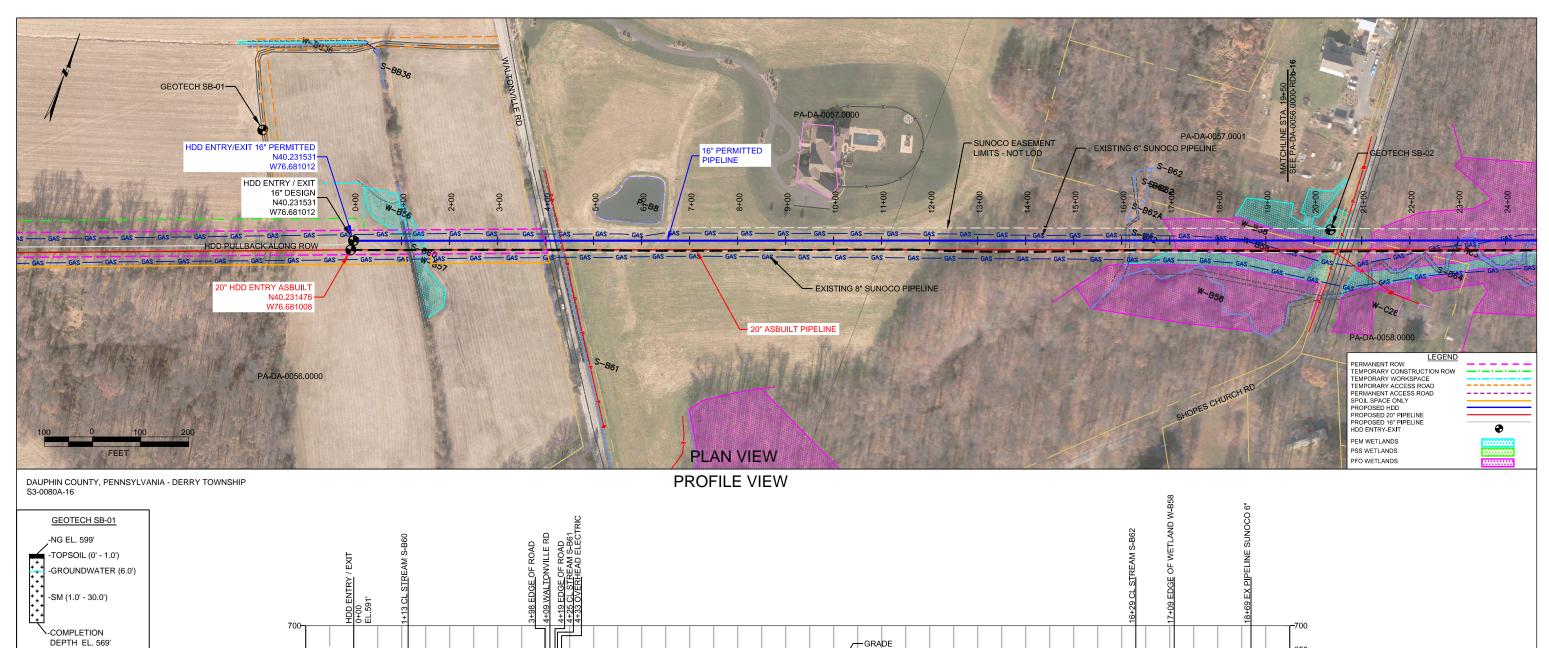
ATTACHMENT 3 WELLS WITHIN 0.5 MILES OF PROPOSED 16" HDD TRACE - SUNOCO WALTONVILLE ROAD FROM PAGWIS DATABASE 2-12-19

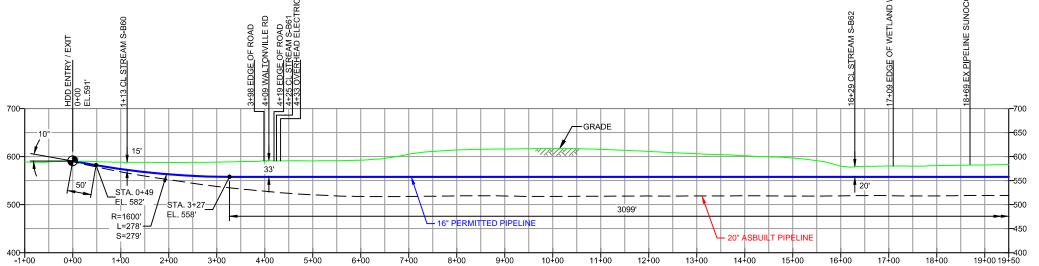
									PAGWIS							
FID	PAWeIIID	WellUse	WaterUse	Well Depth	TopOf Casin	Bottom OfCa	Casing Diam	Depth ToBed	Bedrock Not	Well Yield	Static Wate	Water Level	Length OfTe	YieldMeasu	FormationN	Remark
0	86721	WITHDRAWAL	DOMESTIC	107	0	43	6	34	False	15	55			UNKNOWN	GETTYSBURG FORMATION	
1	478751	GEOTHERMAL	UNUSED	450	0	40	6	15	False	30				VOLUMETRIC WATCH & BUCKET		
2	489473	GEOTHERMAL	UNUSED	450	0	40	6	15	False	30				VOLUMETRIC WATCH & BUCKET		
3	480988	GEOTHERMAL	UNUSED	300	0	0	0	18	False	5				VOLUMETRIC WATCH & BUCKET		
4	480989	GEOTHERMAL	UNUSED	300	0	0	0	18	False	15				VOLUMETRIC WATCH & BUCKET		
5	481757	GEOTHERMAL	UNUSED	300	0	0	0	20	False	3				VOLUMETRIC WATCH & BUCKET		
6	86731	WITHDRAWAL	DOMESTIC	200	0	76	6	68	False	12					GETTYSBURG FORMATION	
7	649824	WITHDRAWAL	DOMESTIC	400	0	105	6	10	False	4				VOLUMETRIC WATCH & BUCKET		
8	86732	WITHDRAWAL	DOMESTIC	275	0	72	6	62	False	5					GETTYSBURG FORMATION	
9	86734	WITHDRAWAL	DOMESTIC	100	0	61	6	46	False	30					GETTYSBURG FORMATION	
10	657129	WITHDRAWAL	DOMESTIC	500	0	0	0	57	False	1			90			
11	86733	WITHDRAWAL	DOMESTIC	250	0	77	6	65	False	20					GETTYSBURG FORMATION	
12	17640	WITHDRAWAL	DOMESTIC	160	0	50	6	0	False	20	50	160	1		GETTYSBURG FORMATION	
13	17644	WITHDRAWAL	DOMESTIC	74	0	36	6	0	False	14	35	74	1		GETTYSBURG FORMATION	
14	501319	CLOSED-LOOP GEOTHERMAL	GEOTHERMAL	300	0	40	6	39	False	0						
15	501320	CLOSED-LOOP GEOTHERMAL	GEOTHERMAL	300	0	40	6	39	False	0						
16	501321	CLOSED-LOOP GEOTHERMAL	GEOTHERMAL	300	0	40	6	39	False	0						
17	501322	CLOSED-LOOP GEOTHERMAL	GEOTHERMAL	300	0	40	6	39	False	0						
18	423853	WITHDRAWAL	DOMESTIC	500	0	84	9	30	False	10				VOLUMETRIC WATCH & BUCKET		
19	86668	WITHDRAWAL	DOMESTIC	120	0	47	6	40	False	15	50		1	UNKNOWN	GETTYSBURG FORMATION	
20	86669	WITHDRAWAL	DOMESTIC	100	0	62	6	55	False	15	45		1	UNKNOWN	GETTYSBURG FORMATION	
21	490370	GEOTHERMAL	UNUSED	225	0	20	6	18	False	40				VOLUMETRIC WATCH & BUCKET		
22	490371	GEOTHERMAL	UNUSED	225	0	20	6	18	False	40				VOLUMETRIC WATCH & BUCKET		
23	490275	GEOTHERMAL	UNUSED	225	0	20	6	18	False	40				VOLUMETRIC WATCH & BUCKET		
24	490276	GEOTHERMAL	UNUSED	225	0	20	6	18	False	40				VOLUMETRIC WATCH & BUCKET		
25	490274	GEOTHERMAL	UNUSED	225	0	20	6	18	False	10				VOLUMETRIC WATCH & BUCKET		
26	490272	GEOTHERMAL	UNUSED	225	0	20	6	18	False	10				VOLUMETRIC WATCH & BUCKET		
27	490273	GEOTHERMAL	UNUSED	225	0	20	6	18	False	40				VOLUMETRIC WATCH & BUCKET		
28	492932	WITHDRAWAL	DOMESTIC	300	0	84	6	10	False	15				VOLUMETRIC WATCH & BUCKET		
29	480934	WITHDRAWAL	IRRIGATION	250	0	60	6	45	False	80				VOLUMETRIC WATCH & BUCKET		
30	86592	WITHDRAWAL	DOMESTIC	200	0	45	6	50	False	5				UNKNOWN	GETTYSBURG FORMATION	
31	86744	WITHDRAWAL	DOMESTIC	125	0	61	6	43	False	20					GETTYSBURG FORMATION	
32	86741	WITHDRAWAL	DOMESTIC	175	0	68	6	58	False	12				UNKNOWN	GETTYSBURG FORMATION	
33	86494	WITHDRAWAL	DOMESTIC	100	0	74	6	7	False	60				VOLUMETRIC WATCH & BUCKET	GETTYSBURG FORMATION	
34	86499	WITHDRAWAL	DOMESTIC	150	0	94	6	79	False	45				VOLUMETRIC WATCH & BUCKET	GETTYSBURG FORMATION	
35	86497	WITHDRAWAL	DOMESTIC	150	0	82	6	64	False	60				VOLUMETRIC WATCH & BUCKET	GETTYSBURG FORMATION	
36	86460	WITHDRAWAL	DOMESTIC	175	0	2	6	0	False	8	65	165	0.5	VOLUMETRIC WATCH & BUCKET	HEIDLERSBURG MEM OF GETTY	REDRILL
37	86690	WITHDRAWAL	DOMESTIC	143	0	90	6	85	False	10				UNKNOWN	GETTYSBURG FORMATION	
38	642207	WITHDRAWAL	DOMESTIC	150	0	78	6	62	False	50	20		30	VOLUMETRIC WATCH & BUCKET		
39	258988		OTHER	120	0	62	6	34	False	12	25	100		VOLUMETRIC WATCH & BUCKET		
40	86695	WITHDRAWAL	DOMESTIC	58	0	25	6	25	False	40	2		1	UNKNOWN	GETTYSBURG FORMATION	
41	86748	WITHDRAWAL	DOMESTIC	225	0	61	6	47	False	7					GETTYSBURG FORMATION	
42	501396	WITHDRAWAL	DOMESTIC	180	0	42	6	36	False	60				VOLUMETRIC WATCH & BUCKET		
43	501429	CLOSED-LOOP GEOTHERMAL	GEOTHERMAL	300	0	16	6	14	False	0						
44	501430	CLOSED-LOOP GEOTHERMAL	GEOTHERMAL	300	0	16	6	14	False	0						
45	501486	CLOSED-LOOP GEOTHERMAL	GEOTHERMAL	300	0	21	6	14	False	0						
46	501487	CLOSED-LOOP GEOTHERMAL	GEOTHERMAL	225	0	16	6	14	False	0						
47	501488	CLOSED-LOOP GEOTHERMAL	GEOTHERMAL	225	0	16	6	14	False	0						
48	86742	WITHDRAWAL	DOMESTIC	150	0	82	6	71	False	25					GETTYSBURG FORMATION	
49	86452	WITHDRAWAL	DOMESTIC	450	0	26	6	21	False	1				VOLUMETRIC WATCH & BUCKET	DIABASE DIKES AND SILLS	ROCK TYPE= HORNFELS
50	666174	WITHDRAWAL	DOMESTIC	100	0	20	6	14	False	80				VOLUMETRIC WATCH & BUCKET		
51	86743	WITHDRAWAL	DOMESTIC	125	0	61	6	47	False	30					GETTYSBURG FORMATION	
52	86740	WITHDRAWAL	DOMESTIC	175	0	60	6	0	False	10				UNKNOWN	GETTYSBURG FORMATION	
53	86739	WITHDRAWAL	DOMESTIC	250	0	82	6	70	False	10				UNKNOWN	GETTYSBURG FORMATION	
54	416933		GEOTHERMAL	275	0	41	6	24	False	10				VOLUMETRIC WATCH & BUCKET		
55	416959		GEOTHERMAL	275	0	41	6	19	False	40				VOLUMETRIC WATCH & BUCKET		
56	416938		GEOTHERMAL	275	0	41	6	25	False	10				VOLUMETRIC WATCH & BUCKET		
57	416949		GEOTHERMAL	275	0	41	6	55	False	40				VOLUMETRIC WATCH & BUCKET		
58	416960		DOMESTIC	300	0	80	6	19	False	10				VOLUMETRIC WATCH & BUCKET		
59	86753	WITHDRAWAL	DOMESTIC	55	0	44	6	0	False	28	23		1	UNKNOWN	GETTYSBURG FORMATION	
60	86752	WITHDRAWAL	DOMESTIC	175	0	61	6	50	False	15					GETTYSBURG FORMATION	
61	86754	WITHDRAWAL	DOMESTIC	150	0	61	6	51	False	30					GETTYSBURG FORMATION	



HORIZONTAL DIRECTIONAL DRILL ANALYSIS WALTONVLLE ROAD CROSSING PADEP SECTION 105 PERMIT NO.: E22-617 PA-DA-0056.0000-RD (SPLP HDD No. S3-0080-16)

ATTACHMENT 2 HORIZONTAL DIRECTIONAL DRILL PLAN AND PROFILES





NOTE: REFER TO TEST BORING LOG <u>\$3-0080</u> FOR COMPLETE SOIL MATERIAL DESCRIPTION

- DESIGN AND CONSTRUCTION:

 1. CONTRACTOR SHALL FIELD VERIFY DEPTH OF ALL EXISTING UTILITIES SHOWN OR NOT SHOWN ON THIS DRAWNING.

 2. THE MINIMUM SEPARATION DISTANCE FROM EXISTING SUBSURFACE UTILITIES SHALL NOT BE LESS THAN 10 FEET AS MEASURED FROM THE OUTSIDE EDGE OF THE UTILITY TO OUTSIDE OF PROPOSED CONTRACT.
- PIPELINE.

 DESIGNED IN ACCORDANCE WITH CFR 49 195 & ASME B31.4

 CROSSING PIPE SPECIFICATION:
 HDD HORZ. LENGTH (L=): 3870'
 HDD PIPE LENGTH (S=): 3875'
 16" X 0.438" W.T., X-70, APISL, PSL2, ERW, BFW
 COATING: 14-16 MILS FBE WITH 40 MILS MIN. ARO (POWERCE

- STREAM CROSSINGS.

 8. CARRIER PIPE NOT ENCASED.

 9. PIPE / AMBIENT TEMPERATURE MUST BE NO LESS THAN 30°F DURING PULLBACK WITHOUT PRIOR WRITTEN APPROVAL FROM THE ENGINEER.

 10. CONDUCT 4-HOUR PRE-INSTALLATION HYDROTEST OF HDD PIPE STRING TO MINIMUM 1850 PSIG.

 11. SEE SUNOCO PENNSYLVANIA PIPELINE PROJECT ESRI WEBMAP FOR ACCESS ROAD ALIGNMENT.
- INTERNAL DESIGN PRESSURE 1480 PSIG (SEAM FACTOR 1.0, DESIGN FACTOR 0.50 (HOOP STRESS)).
 INSTALLATION METHOD: HORIZONTAL DIRECTIONAL DRILL (HDD).
 PIPELINE WARNING MARKERS SHALL BE INSTALLED ON BOTH SIDES OF ALL ROAD, RAILWAY, AND
 STREAM CROSSINGS.

 12. SUNOCO PIPELINE, L.P.'S HORIZONTAL DIRECTIONAL DRILL INADVERTENT RETURN CONTINGENCY PLAN WILL BE IMPLEMENTED AT ALL TIMES.
 SUNOCO PIPELINE, L.P.'S EROSION AND SEDIMENTATION CONTROL PLAN WILL BE IMPLEMENTED AT ALL TIMES.
 SUNOCO PIPELINE, L.P.'S EROSION AND SEDIMENTATION CONTROL PLAN WILL BE IMPLEMENTED AT ALL TIMES.

Figure 1A. Permitted 16-Inch HDD Plan and Profile with 20-Inch IR Data

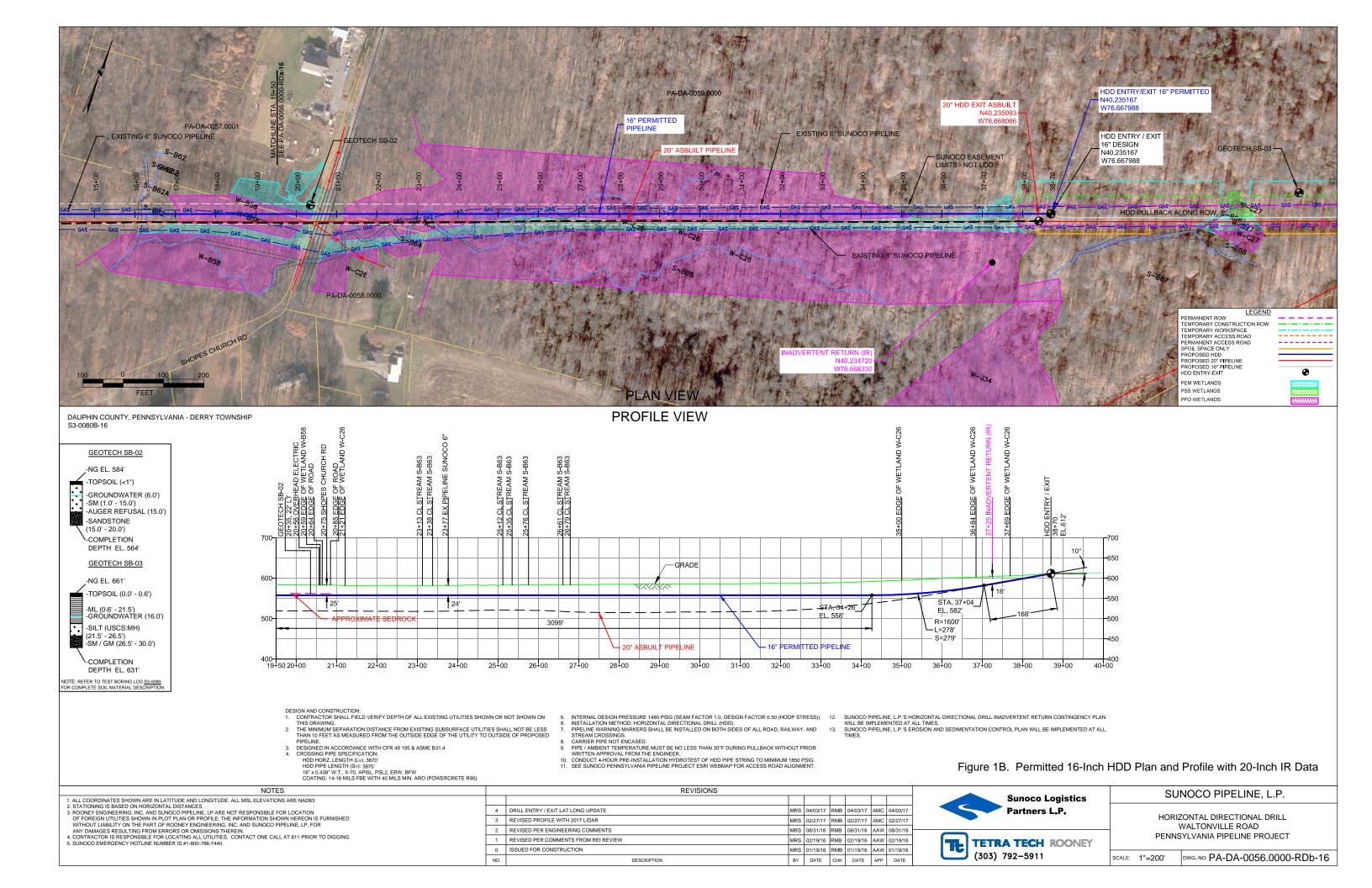
COATING: 14-16 MILS FBE WITH 40 MILS MIN. ARO (POWERCRETE R95)								
NOTES		REVISIONS						
1. ALL COORDINATES SHOWN ARE IN LATITUDE AND LONGITUDE. ALL MSL ELEVATIONS ARE NAD83								
Stationing is based on Horizontal distances. Rooney engineering, inc. and sungoco pipeline, ip are not responsible for location of foreign utilities shown in Plot Plan or Profile. The information shown hereon is furnished without labelilty on the part of rooney engineering. Inc. and sungoco pipeline. Ip- for	4	DRILL ENTRY / EXIT LAT LONG UPDATE	MRS	04/03/17	RMB	04/03/17	AMC	04/03/17
	3	REVISED PROFILE WITH 2017 LIDAR	MRS	02/27/17	RMB	02/27/17	AMC	02/27/17
ANY DAMAGES RESULTING FROM ERRORS OR OMISSIONS THEREIN.		REVISED PER ENGINEERING COMMENTS	MRS	08/31/16	RMB	08/31/16	AAW (08/31/16
4. CONTRACTOR IS RESPONSIBLE FOR LOCATING ALL UTILITIES. CONTACT ONE CALL AT 811 PRIOR TO DIGGING. 5. SUNOCO EMERGENCY HOTLINE NUMBER IS #1-80-0786-7440.	1	REVISED PER COMMENTS FROM REI REVIEW	MRS	02/19/16	RMB	02/19/16	AAW	C 04/03/17 C 02/27/17 W 08/31/16 W 02/19/16 W 01/19/16
C. GOLGGE ZIIIZ. GOLGE TO INCLUIZ TO INCLUI ZI GOLGE TO INCLUI ZI GOLG	0	ISSUED FOR CONSTRUCTION	MRS	01/19/16	RMB	01/19/16	AAW (01/19/16
	NO	DESCRIPTION	DV	DATE	OLIK	DATE	400	02/27/17 08/31/16 02/19/16 01/19/16

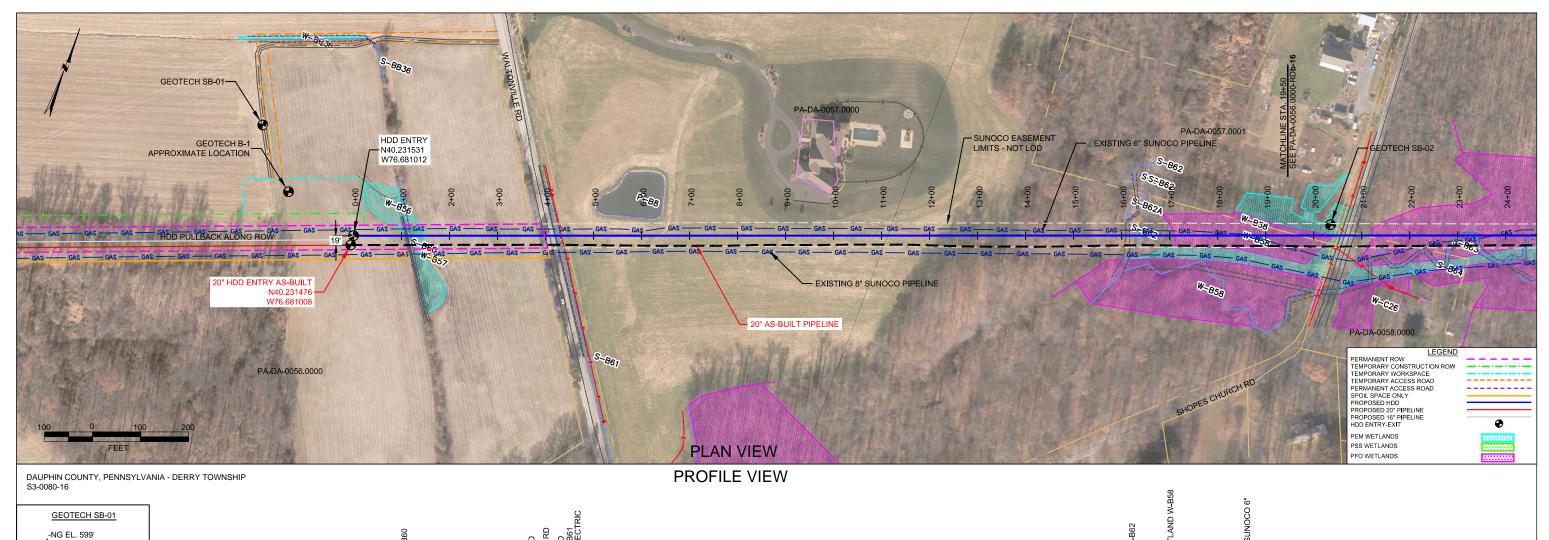


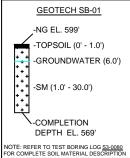
HORIZONTAL DIRECTIONAL DRILL WALTONVILLE ROAD PENNSYLVANIA PIPELINE PROJECT

SUNOCO PIPELINE, L.P.

DWG. NO: PA-DA-0056.0000-RDa-16 SCALE: 1"=200'

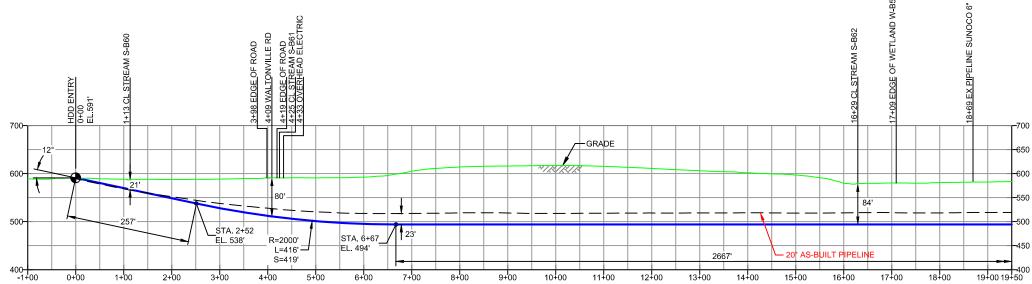






GEOTECH B-1 -NG EL. 599' -TOPSOIL (0' - 1.0') -FILL CL (1.0' - 8.5') -GROUNDWATER (11.8') -RESIDUUM-SILTY SAND SM (8.5' - 18.5') -RESIDUUM-SILTY SAND ML (18.5' - 24.5') -SANDSTONE/DIABASE (24.5' - 143.0') -BORING TERMINATED EL.456

NOTE: REFER TO TEST BORING LOG <u>B-1</u> INTERTEK PROJECT #04911517 FOR COMPLETE SOIL MATERIA DESCRIPTION



- DESIGN AND CONSTRUCTION:

 1. CONTRACTOR SHALL FIELD VERIFY DEPTH OF ALL EXISTING UTILITIES SHOWN OR NOT SHOWN ON THIS DRAWNING.

 2. THE MINIMUM SEPARATION DISTANCE FROM EXISTING SUBSURFACE UTILITIES SHALL NOT BE LESS THAN 10 FEET AS MEASURED FROM THE OUTSIDE EDGE OF THE UTILITY TO OUTSIDE OF PROPOSED CONTRACT. PIPELINE.
- PIPELINE.
 DESIGNED IN ACCORDANCE WITH CFR 49 195 & ASME B31.4
 CROSSING PIPE SPECIFICATION:
 HDD HORZ. LENGTH (L=): 4095'
 HDD PIPE LENGTH (S=): 4120'
 16" x 0.438" W.T., X-70, APISL, PSL2, ERW, BFW
 COATING: 41-16 MILS FBE WITH 40 MILS MIN. ARO (POWERCRETE R95)
- INTERNAL DESIGN PRESSURE 2100 PSIG (SEAM FACTOR 1.0, DESIGN FACTOR 0.50 (HOOP STRESS)). INSTALLATION METHOD: HORIZONTAL DIRECTIONAL DRILL (HDD), PIPELINE WARNING MARKERS SHALL BE INSTALLED ON BOTH SIDES OF ALL ROAD, RAILWAY, AND STREAM CROSSINGS.

 12. SUNOCO PIPELINE, L.P.'S HORIZONTAL DIRECTIONAL DRILL INADVERTENT RETURN CONTINGENCY PLAN WILL BE IMPLEMENTED AT ALL TIMES. SUNOCO PIPELINE, L.P.'S EROSION AND SEDIMENTATION CONTROL PLAN WILL BE IMPLEMENTED AT ALL TIMES. SUNOCO PIPELINE, L.P.'S EROSION AND SEDIMENTATION CONTROL PLAN WILL BE IMPLEMENTED AT ALL TIMES.
- STREAM CROSSINGS.

 2. CARRIER PIPE NOT ENCASED.

 9. PIPE / AMBIENT TEMPERATURE MUST BE NO LESS THAN 30°F DURING PULLBACK WITHOUT PRIOR WRITTEN APPROVAL FROM THE ENGINEER.

 10. CONDUCT 4-HOUR PRE-INSTALLATION HYDROTEST OF HDD PIPE STRING TO MINIMUM 2625 PSIG.

 11. SEE SUNOCO PENNSYLVANIA PIPELINE PROJECT ESRI WEBMAP FOR ACCESS ROAD ALIGNMENT.

Figure 2A. Revised 16-Inch HDD Plan and Profile

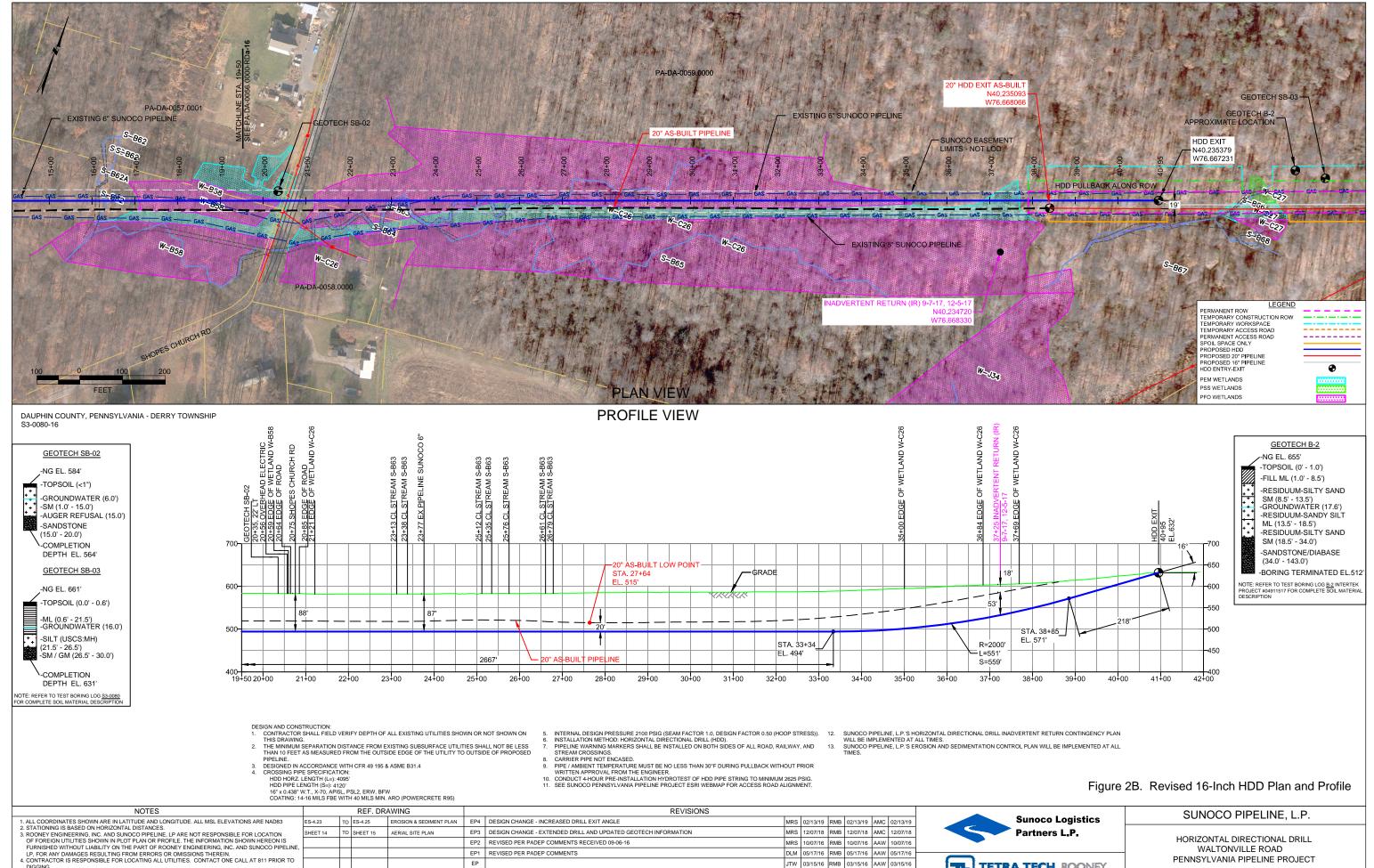
COATING. I	4-10 MILS FBL	vviiii	1 40 IVIILO IVIIIV.	ARO (FOWERCRETE R95)											
NOTES		REF. DRAWING				REVISIONS									
ALL COORDINATES SHOWN ARE IN LATITUDE AND LONGITUDE. ALL MSL ELEVATIONS ARE NAD83 ACTA FIGURE OF PACES OF LAND STANDING.	ES-4.23	то	ES-4.25	EROSION & SEDIMENT PLAN	EP4	DESIGN CHANGE - INCREASED DRILL EXIT ANGLE	MRS	02/13/19	RMB	02/13/19	AMC	02/13/19			
STATIONING IS BASED ON HORIZONTAL DISTANCES. ROONEY ENGINEERING, INC. AND SUNOCO PIPELINE, LP ARE NOT RESPONSIBLE FOR LOCATION	SHEET 14	то	SHEET 15	AERIAL SITE PLAN	EP3	DESIGN CHANGE - EXTENDED DRILL AND UPDATED GEOTECH INFORMATION	MRS	12/07/18	RMB	12/07/18	AMC	12/07/18			
OF FOREIGN UTILITIES SHOWN IN PLOT PLAN OR PROFILE. THE INFORMATION SHOWN HEREON IS FURNISHED WITHOUT LIABILITY ON THE PART OF ROONEY ENGINEERING. INC. AND SUNOCO PIPELINE.					EP2	REVISED PER PADEP COMMENTS RECEIVED 09-06-16	MRS	10/07/16	RMB	10/07/16	AAW	10/07/16			
LP, FOR ANY DAMAGES RESULTING FROM ERRORS OR OMISSIONS THEREIN.					EP1	REVISED PER PADEP COMMENTS	DLM	05/09/16	RMB	05/09/16	AAW	05/09/16			
4. CONTRACTOR IS RESPONSIBLE FOR LOCATING ALL UTILITIES. CONTACT ONE CALL AT 811 PRIOR TO DIGGING.					EP		JTW	03/15/16	RMB	03/15/16	AAW	03/15/16			
5. SUNOCO EMERGENCY HOTLINE NUMBER IS #1-800-786-7440.					В	ADDED GEOTECH INFO	MRS	09/22/15	RMB	09/22/15	AAW	09/22/15			
	DWG NO		DWG NO	DESCRIPTION	NO.	DESCRIPTION	BY	DATE	CHK	DATE	APP	DATE			



SUNOCO PIPELINE, L.P. HORIZONTAL DIRECTIONAL DRILL

WALTONVILLE ROAD PENNSYLVANIA PIPELINE PROJECT TETRA TECH ROONEY (303) 792-5911

DWG. NO: PA-DA-0056.0000-RDa-16 SCALE: 1"=200'



JTW 03/15/16 RMB 03/15/16 AAW 03/15/16

MRS 09/22/15 RMB 09/22/15 AAW 09/22/15

BY DATE CHK DATE APP

EP

NO.

DESCRIPTION

DWG NO

B ISSUED FOR BID

DESCRIPTION

DIGGING.

5. SUNOCO EMERGENCY HOTLINE NUMBER IS #1-800-786-7440.

WALTONVILLE ROAD PENNSYLVANIA PIPELINE PROJECT TETRA TECH ROONEY (303) 792-5911 DWG. NO: PA-DA-0056.0000-RDb-16

SCALE: 1"=200'