

**HORIZONTAL DIRECTIONAL DRILL ANALYSIS  
WETLAND J-47 CROSSING  
PADEP SECTION 105 PERMIT NO.S:  
PA-LE-0001.0000-SR & PA-LE-0001.0000-SR-16  
(SPLP HDD No. S3-0090)**

**WETLAND J-47 CROSSING  
PADEP SECTION 105 PERMIT NO.S:  
PA-LE-0001.0000-SR & PA-LE-0001.0000-SR-16  
(SPLP HDD No. S3-0090)**

This reanalysis of the horizontal directional drill (HDD) installation of a 16-inch and 20-inch diameter pipeline crossing under Wetland J-47, has been completed in accordance with paragraphs 4 and 5 of the Stipulated Order issued under Environmental Hearing Board Docket No. 2017-009-L. This HDD is number 15 on the list of HDDs included on Exhibit 2 of the Stipulated Order.

**PIPE INFORMATION**

20-Inch: 0.456 wall thickness; X-65  
16-Inch: 0.438 wall thickness; X-70

Pipe stress allowances are an integral part of the design calculations performed for each HDD.

**ORIGINAL HORIZONTAL DIRECTIONAL DRILL DESIGN SUMMARY: 20-INCH**

- Horizontal length: 1,020 foot (ft)
- Entry/Exit angle: 10-15 degrees
- Maximum Depth of cover: 60 ft
- Pipe design radius: 2,000 ft

**ORIGINAL HORIZONTAL DIRECTIONAL DRILL DESIGN SUMMARY: 16-INCH**

- Horizontal length: 1,070 ft
- Entry/Exit angle: 10-12 degrees
- Maximum Depth of cover: 75 ft
- Pipe design radius: 1,600 ft

**GEOLOGIC AND HYDROGEOLOGIC ANALYSIS**

Based upon publications by the Pennsylvania Bureau of Topographic and Geologic Survey (BTGS, 2001 and Sevon, 2000), the site is in the Gettysburg-Newark Lowland Section of the Piedmont Physiographic Province of Pennsylvania, underlain by sedimentary rocks of the Newark Group. Local topography is characterized by rolling lowlands, shallow valleys, and isolated hills (Geyer and Wilshusen, 1982).

The HDD site geology is mapped as the Gettysburg Formation and Gettysburg Formation-Conglomerate. The Gettysburg Formation is described as red shale, red, brown and gray sandstone, and quartz and limestone conglomerate (Geyer and Wilshusen, 1982). The Gettysburg Formation-Conglomerate is described as coarse, quartz conglomerate containing rounded pebbles and cobbles in a matrix of red sand (Geyer and Wilshusen, 1982). The general structure of the Newark Group is a north-northwestward dipping homocline. Typical dip directions are north or northwest and range from 20° to 40° (Newport, 1971). Intrusive diabase has been mapped north and south of the HDD.

Karst geology is not present at this HDD location. At this HDD location the use of geophysics assessments was considered but not conducted because the results from these types of assessments provide limited useable data after 20 to 50 ft below the ground surface (bgs) varying by the nature of the geologic structure.

**WETLAND J-47 CROSSING  
PADEP SECTION 105 PERMIT NO.S:  
PA-LE-0001.0000-SR & PA-LE-0001.0000-SR-16  
(SPLP HDD No. S3-0090)**

Attachment 1 provides an extensive discussion on the geology, hydrogeology and results of the geotechnical investigation performed at this location.

## **HYDROGEOLOGY, GROUND WATER, AND WELL PRODUCTION ZONES**

Groundwater in the vicinity of the Wetland J-47 HDD moves in interconnected, secondary openings such as fractures and joints in the sedimentary bedrock aquifer system. Typically, these openings are best developed and found more frequently near the surface. At depth, these openings occur less frequently and tend to be smaller due to compressional loading (Wood, 1980).

Based upon reported data on 332 wells in the Gettysburg Formation, water-bearing zones range from 5 to 900 feet below the ground surface (bgs). Fifty percent of the 669 reported water-bearing zones were penetrated at a depth of 115 feet or less, with 90% of the water-bearing zones encountered at a depth of 288 feet bgs or less. The greatest density of water-bearing zones is from approximately 51 to 100 feet bgs. The density of water-bearing zones encountered at depths greater than 401 feet are based on five or fewer zones per 50-foot interval. Overall density of water-bearing zones in the Gettysburg Formation is 0.41 per 50-feet of well depth (Low, et. al., 2002).

Attachment 1 provides an extensive discussion on the geology, hydrogeology and results of the geotechnical investigation performed at this location.

## **INADVERTENT RETURN (IR) DISCUSSION**

HDD specialists for Sunoco Pipeline, L.P. (SPLP) reviewed the original HDD designs summarized above, and predicted that the design profiles for the 16 and 20-inch HDDs would produce an IR at or before 100 ft into the pilot profile for either pipe, where the drill crossed the first stream, and an IR to a water of the state may occur.

As presented and discussed in the Conclusion section below, the profile for both the 16 and 20-inch pipelines have been redesigned so that they are longer and deeper, and with the maximum degree of entry and exit angles allowed by the stress radius of the pipelines, to sharpen the pilot run down to horizontal depth and return exit to the land surface.

As shown on Figures 2 and 4 in Attachment 2, the weakest point in both profiles is the first stream undercrossing, occurring at Station 5+66 on the 20-inch profile, and Station 5+33 on the 16-inch profile. The revised design profiles provide for 78 ft of cover above the 20-inch pilot drill, and 91 ft of cover over the 16-inch pilot drill.

These new profile designs are based upon the fracture pressure of the overlying bedrock. As shown on the core data set forth in the attached hydrogeology report, these siltstone, sandstone and conglomeratic sandstone layers had moderate to high recovery, and varied from poor to high quality in value (RQD) indicative of good structural integrity, and low to very high strength, depending on depth in the formation. As shown on Figure 1 - Annular Pressure and Formation Pressure Capacity Curves in Attachment 3, the revised design pressures are below the bedrock fracture pressure at Drill Rod 19, so long as the return fluids and cuttings are kept below 10.5 pounds per gallon (ppg). Achieving this return fluid flow weight requires monitoring of the recycling of the return flows to ensure that cuttings are adequately removed prior to returning the recycled fluids into the drilling process. The entire HDD profile is designed to manage drilling pressures under this point in the profile.

**WETLAND J-47 CROSSING**  
**PADEP SECTION 105 PERMIT NO.S:**  
**PA-LE-0001.0000-SR & PA-LE-0001.0000-SR-16**  
**(SPLP HDD No. S3-0090)**

**ADJACENT FEATURES ANALYSIS**

The crossing of Wetland J-47 is located in rural Dauphin and Lebanon counties, approximately 3.6 miles southeast of Hershey, PA. The pipeline route follows parallel to two previously existing Sunoco pipelines.

This HDD location is within unmanaged deciduous woodlands. The HDD would cross under two streams and one wetland, none of which are designated as exceptional value. A 3.5 acre impoundment occurs approximately 385 ft north-northwest of the HDD location.

In addition to the resources listed above, based upon the data from the Pennsylvania Groundwater Information System (PaGWIS) and review of aerial photography, five domestic (private) supply wells were identified within 450 feet of the proposed HDD. Of these, three occur north of the HDD profile at distances between 180 and 530 ft. Based upon the data in PaGWIS, the well depths are 100 to 150 ft bgs, with a reported static water level of 30 bgs. Typically, a "good drilling mud program" forms a "cake wall" around the diameter of the pilot or reamer during drilling process which seals fissures within the profile geology and limits the horizontal and vertical movement of drilling fluids. Secondly, controlling the down hole mud weights and pressures should minimize the lateral movement of these materials through the geology. These wells will have to be monitored during the HDD process in accordance with PADEP requirements.

To further avoid and mitigate any adverse effects from the HDD to private water wells, and in accordance with the requirements of the Stipulated Order, SPLP will transmit a copy of this HDD analysis to all landowners having a property line within 450 ft of any direction of this HDD location. SPLP will also inform these landowners that SPLP will conduct pre-, during, and post-construction sampling of their private water wells to ensure that mitigating actions are taken, if necessary.

**ALTERNATIVES ANALYSIS**

The proposed HDD is an alternative plan of installation to a conventional open trench construction plan. Using the HDD method avoids new unavoidable direct impacts to the stream, wetlands, and associated forested woodland and riparian habitats. Alteration of the current permitted route and plans for installation would require major modifications of the state Chapter 102 and Chapter 105 permits, and authorization issued by the U.S. Army Corps of Engineers.

Both of these HDDs are 2,200 ft in horizontal length and include the crossings of two stream channels, and approximately 620 ft of an emergent and forested wetland complex.

**Open-cut and Conventional Bore Analysis**

Sunoco Pipeline, L.P. (SPLP) specifications require a minimum of 48-inches of cover over the installed pipelines. To meet these cover requirements, during construction through the stream and wetlands would require a minimum authorized open cut work space 75 ft in width to accommodate the 16 and 20-inch pipelines, allowing for each pipeline to be installed with sufficient separation for integrity management. The assessed area of impact by this open cut plan would directly affect approximately 0.09 acres of state water bottoms, 0.12 acres of emergent wetland, and 1.12 acres of forested wetland.

Due to the existing saturated ground conditions, a significant volume of produced groundwater will fill all the excavations during the open cut process. These water volumes can be pumped to a discharge filtration structure; however the current feasible filtration ability does not exceed 50 microns, therefore,



**WETLAND J-47 CROSSING  
PADEP SECTION 105 PERMIT NO.S:  
PA-LE-0001.0000-SR & PA-LE-0001.0000-SR-16  
(SPLP HDD No. S3-0090)**

cloudy water (from suspended fine clay and silt particles) will be discharged downstream regardless of all control methods employed for the entire duration of this open cut installation until completion.

The crossing distance of the emergent and forested wetlands, which are the most expansive natural features crossed by the HDDs, is beyond the technical limits of a conventional auger bore.

In sum, a combination of open-cut and conventional bores would not work as an alternative to the Wetland J-47 HDD.

### **Re-Route Analysis**

The pipeline route as currently permitted follows parallel to two existing Sunoco pipelines.

There are no existing utility corridors to the north or south that provide a practical alternative route. Any alternate route considered north or south of the existing utility corridor would require the clearing of a new "greenfield" corridor through existing woodlands and croplands, increase the number of stream crossings, and possibly encroach on additional private residences before it could rejoin the current route.

During the PADEP Chapter 105 permit process for the Mariner II East Project, SPLP created and submitted for review a project wide alternatives analysis. The baseline route provided for the pipeline construction to cross every wetland and stream on the project by open cut construction procedures. The alternatives analysis submitted to PADEP conceptually analyzed the feasibility of any alternative to trenched resource crossings (e.g., reroute, bore, HDD). The decision making processes for switching from an open cut to HDD is discussed thoroughly in the previously-submitted alternatives analysis and was an important part of the permit application package of HDD plans as currently permitted. The re-route analysis conducted for the Joanna Road HDD confirms the conclusions reached in the previously submitted alternatives analysis.

### **HORIZONTAL DIRECTIONAL DRILL REDESIGN**

Additional geologic investigations have been completed and utilized in the redesign of the planned HDDs. These redesigns adjust the HDD profile deeper to place the HDD pathway under and through bedrock having better structural integrity than a shallower profile and increase the overall length of the HDD due to pipe design requirements. A summary of the redesign factors is provided below. The original and redesigned HDD plan and profile drawings are provided in Attachment 2.

#### **REVISED HORIZONTAL DIRECTIONAL DRILL DESIGN SUMMARY: 20-INCH**

- Horizontal length: 2,200 ft
- Entry/Exit angle: 16 degrees
- Maximum Depth of cover: 119 ft
- Pipe design radius: 2,400 ft

#### **REVISED HORIZONTAL DIRECTIONAL DRILL DESIGN SUMMARY: 16-INCH**

- Horizontal length: 2,200 ft
- Entry/Exit angle: 16 degrees
- Maximum Depth of cover: 137 ft
- Pipe design radius: 1,800 ft

**WETLAND J-47 CROSSING  
PADEP SECTION 105 PERMIT NO.S:  
PA-LE-0001.0000-SR & PA-LE-0001.0000-SR-16  
(SPLP HDD No. S3-0090)**

As shown on Figure 2, the redesigned HDD profile for the 20-inch pipeline is 1,180 ft longer, with a maximum depth of cover increased by 59 ft from the permitted design. In addition, the entry/exit angles have been increased from 10-15 degrees to 16 degrees allowing for a sharper and quicker descent into more competent rock. As shown on Figure 4 the redesigned HDD profile for the 16-inch pipeline is 1,130 ft longer, with a depth of cover increased by 62 ft, and designed for a sharp and quick entry and exit from the horizontal depth.

## **CONCLUSION**

HDD specialists and geologists employed by SPLP have investigated the HDD design and subsurface geologic conditions and concluded that the original HDD design for the 16 and 20 inch pipelines, as summarized in the introduction, have an increased risk of IRs to the land surface, wetlands, and streams if implemented; therefore, the HDD for the 16-inch and 20-inch diameter pipeline have been redesigned as set forth above to maximize the potential to complete each HDD without an occurrence of an IR.

Upon the start of these HDDs, SPLP will employ the following HDD best management practices:

- SPLP will mandate annular pressure monitoring during the drilling of the pilot hole, which assists in immediate identification of pressure changes indicative of loss of return flows or over pressurization of the annulus, and allows the operator to manage the development of pressures that can induce an IR;
- SPLP inspectors will ensure that an appropriate diameter pilot tool, relative to the diameter of the drilling pipe, is used to ensure adequate "annulus spacing" around the drilling pipe exits to allow good return flows during the pilot drilling;
- SPLP will mandate short-tripping of the reaming tools to ensure an open annulus is maintained to manage the potential inducement of IRs;
- SPLP will require monitoring of the drilling fluid viscosity, such that fissures and fractures in the subsurface are sealed during the drilling process;
- SPLP will mandate monitoring of the drilling fluid cleaning, such that the return weight of the recycled drilling fluids is kept below 10.5 ppg;
- During the reaming phase, the use of Loss Control Materials may be implemented if indications of a potential IR are noted or an IR is observed, and
- If necessary, the pilot hole and reaming phases at the point of entry for the HDD may utilize casing, hammered into the substrate down to structurally better rock, to prevent vertical or lateral movement of drilling fluids at shallow depths.

**WETLAND J-47 CROSSING  
PADEP SECTION 105 PERMIT NO.S:  
PA-LE-0001.0000-SR & PA-LE-0001.0000-SR-16  
(SPLP HDD No. S3-0090)**

**ATTACHMENT 1  
GEOLOGY AND HYDROGEOLOGICAL EVALUATION REPORT**



We answer to you.

3020 Columbia Avenue, Lancaster, PA 17603 • Phone: (800) 738-8395  
E-mail: rettew@rettew.com • Website: rettew.com

Engineers

Environmental  
Consultants

Surveyors

Landscape  
Architects

Safety  
Consultants

September 22, 2017

Mr. Matthew Gordon  
Sunoco Pipeline, L.P.  
535 Fritztown Road  
Sinking Spring, PA 19608

RE: Sunoco Pipeline, L.P. Pipeline Project - Mariner East II  
Wetland J-47 Horizontal Directional Drill Location (S3-0090)  
Hydrogeological Reevaluation Report  
Conewago Township, Dauphin County and  
South Londonderry Township, Lebanon County, Pennsylvania  
RETTEW Project No. 096302011

## EXECUTIVE SUMMARY

1. The Stipulated Order dated August 8, 2017 requires a reevaluation of the Wetland J-47 Horizontal Directional Drill (HDD) location, including a geologic report.
2. HDD Wetland J-47 is underlain by sedimentary rocks of the Gettysburg Formation (Trg) and Gettysburg Formation-Conglomerate (Trgc).
3. Geologic mapping and published reports indicate typically open and moderate to steeply dipping beds, with regularly spaced bedrock joints and fractures.
4. Water-bearing zones generally occur in secondary openings along bedding planes, joints, faults and fractures. Water-bearing zones in both formations are most frequent within approximately 300 to 200 feet of the ground surface.
5. To date, no HDD operations have started for either the 16-inch or 20-inch pipeline.
6. Based on the hydro-structural characteristics of the underlying geology, and proposed bore path through shallow unconsolidated soil materials and generally shallow bedrock, the Wetland J-47 HDD is susceptible to the inadvertent return (IR) of drilling fluids during HDD operations for the planned 16-inch and 20-inch drills. The revised HDD profile and HDD best management practices during drilling operations will be used to reduce the risk of an IR.

## 1.0 INTRODUCTION

The purpose of this report is to describe the geologic and hydrogeologic setting of the Wetland J-47 (S3-0090) HDD location (the site) on the Sunoco Pipeline, L.P. (SPLP) Pennsylvania Pipeline Project - Mariner East II (PPP-ME2) Project. The site is located in Conewago Township, Dauphin County and South Londonderry Township, Lebanon County, Pennsylvania (refer to **Figure 1**). The HDD was designed to be drilled under two small streams (S-A47 and S-A48) and Wetland J-47. This reevaluation report is part of the response to the Stipulated Order dated August 8, 2017.

The HDD profile was lengthened on September 25, 2017 to provide additional protective cover beneath the streams and wetland. The HDD entry on the western side of the profile is at an elevation of approximately 525 feet above mean sea level (AMSL) for the proposed 16-inch drill and 527 feet AMSL for the proposed 20-inch drill. The exit on the eastern side of the profile is at an elevation of approximately 566 feet AMSL for the proposed 16-inch drill and 554 feet AMSL for the proposed 20-inch drill. The inclination of the entry and exit angles has been increased as a means to install the pipe through these protective soils, residual soils, and bedrock in closer proximity to the entry and exit points than the original, shorter profile.

Based on the annular pressure and formation pressure capacity curves provided by Directional Project Support (DPS) as part of the overall reevaluation submittal, the weakest point in the profile is beneath the first crossing of stream S-A47. At this location, the HDD profile is approximately 91 feet below the stream for the proposed 16-inch drill and 78 feet for the proposed 20-inch drill. Copies of the revised HDD profiles are included in **Attachment 1**.

## 2.0 GEOLOGY AND SOILS

Based upon publications by the Pennsylvania Bureau of Topographic and Geologic Survey (BTGS, 2001 and Sevon, 2000), the site is in the Gettysburg-Newark Lowland Section of the Piedmont Physiographic Province of Pennsylvania, underlain by sedimentary rocks of the Newark Group. Local topography is characterized by rolling lowlands, shallow valleys, and isolated hills (Geyer and Wilshusen, 1982).

According to the United States Department of Agriculture (USDA) Soil Surveys of Dauphin County and Lebanon County, Pennsylvania, soils within approximately 450 feet of the drill path for HDD S3-0090 consist of Basher silt loam (Bc), Brinkerton silt loam, 0 to 3 percent slopes (BrA), Brinkerton and Armagh silt loams, 0 to 3 percent slopes (BtA), Bucks silt loam, 3 to 8 percent slopes (ByB), Croton silt loam, occasionally ponded, 0 to 3 percent slopes (Cr), Lewisberry gravelly sandy loam, 3 to 8 percent slopes, moderately eroded (LrB2), Lewisberry gravelly sandy loam, 8 to 15 percent slopes, moderately eroded (LrC2), Lewisberry very stony sandy loam, 5 to 25 percent slopes (LsD), Lewisberry very stony sandy loam, 25 to 60 percent slopes (LsF), Penn channery silt loam, 3 to 8 percent slopes (PeB2), Penn channery silt loam, 8 to 15 percent slopes (PeC and PeC2), Ungers loam, 3 to 8 percent slopes (UnB), and Ungers loam, 8 to 15 percent slopes (UnC). A USDA map identifying the general area, along with the soil profile descriptions is included as **Attachment 2**.

The site geology is mapped as the Gettysburg Formation and Gettysburg Formation-Conglomerate, as shown on **Figure 2** (Berg and Dodge, 1981). The Gettysburg Formation is described as red shale, red, brown and gray sandstone, and quartz and limestone conglomerate (Geyer and Wilshusen, 1982). The Gettysburg Formation-Conglomerate is described as coarse, quartz conglomerate containing rounded pebbles and cobbles in a matrix of red sand (Geyer and Wilshusen, 1982). The general structure of the Newark Group is a north-northwestward dipping homocline. Typical dip directions are north or northwest and range from 20° to 40° (Newport, 1971). Intrusive diabase has been mapped north and south of the HDD.

The Gettysburg Formation is moderately well bedded, thin to flaggy, moderately weathered and moderately resistant to weathering. Joint and bedding plane openings provide moderate secondary porosity. Permeability is described as moderate. Weathered rock is reported to be moderately easy to

excavate whereas unweathered rock is reported to be difficult to excavate. Drilling rates are moderate to fast. Foundation stability is good when material is excavated to sound rock (Geyer and Wilshusen, 1982).

The Gettysburg Formation-Conglomerate is well bedded and thick to massive. Bedrock fracturing is described as jointed with a blocky pattern that is moderately developed and moderately abundant. The joints are regularly spaced with a moderate distance between fractures that are open and steeply dipping. The joint, bedding and fracture-plane openings provide a secondary porosity of low magnitude and low permeability. Overall, the formation is moderately resistant to weathering. These rocks reportedly provide good foundation stability (Geyer and Wilshusen, 1982).

### **3.0 HYDROGEOLOGY**

Groundwater in the vicinity of the Wetland J-47 HDD moves in interconnected, secondary openings such as fractures and joints in the sedimentary bedrock aquifer system. Typically, these openings are best developed and found more frequently near the surface. At depth, these openings occur less frequently and tend to be smaller because compressional loading results in an increase of closed openings (Wood, 1980).

Bedrock geology ultimately influences the storage, transmission, and use of groundwater. Geologic factors such as rock type, intergranular porosity, rock strata inclination, faults, joints, bedding planes, and solution channels affect groundwater movement and availability. Groundwater within the Gettysburg Formation and Gettysburg Formation-Conglomerate can occur under both unconfined (i.e., water table) and confined conditions. In general, groundwater generally occurs under unconfined conditions within the upper portion of the aquifer, and under confined or semiconfined conditions in the deeper portions of the aquifer. The groundwater flow system is described as a series of sedimentary beds with relatively high transmissivity separated by beds exhibiting lower transmissivities. This sequence of beds exhibits different hydraulic properties that collectively act as a series of alternating aquifers and confining or semi-confining units forming a leaky multi-aquifer system (LMAS). The groundwater flow direction within the Gettysburg and Gettysburg Formation-Conglomerate is controlled by hydraulic gradients and variability of hydraulic conductivity. The predominant flow direction is parallel to bedding (Wood, 1980).

Groundwater flow paths within the sedimentary rocks have both local and regional components. Locally, shallow groundwater discharges to the gaining portions of nearby streams and deeper regional groundwater flow is toward points of regional groundwater discharge such as the Susquehanna River. Groundwater divides may be different for each zone of groundwater flow, and therefore may not coincide with surface water divides. Based on our review of available reference sources, no regional water table mapping is available for the Wetland J-47 HDD or surrounding area. As a result, no water table mapping was available for review or inclusion with this HDD reevaluation report.

Based upon reported data on 332 wells in the Gettysburg Formation, water-bearing zones range from 5 to 900 feet below the ground surface (bgs). Fifty percent of the 669 reported water-bearing zones were penetrated at a depth of 115 feet or less, with 90% of the water-bearing zones encountered at a depth of 288 feet bgs or less. The greatest density of water-bearing zones is from approximately 51 to 100 feet bgs. The density of water-bearing zones encountered at depths greater than 401 feet are based on five or fewer zones per 50-foot interval. Overall density of water-bearing zones in the Gettysburg Formation is 0.41 per 50-feet of well depth (Low, et. al., 2002).

Well records reviewed within a 0.5-mile radius of the HDD location were obtained from the Pennsylvania Groundwater Information System (PaGWIS) on September 20, 2017. Records and information from 10 wells in this radius were available and are summarized below. These well locations are shown on **Figures 2 and 3**.

Well No.	Well Use	Casing Depth (feet)	Total Depth (feet)	Water Level (feet)	Yield (gpm)
86665	DOMESTIC	48	100	Not Available	12
86346	DOMESTIC	43	100	Not Available	20
637244	DOMESTIC	61	160	35	40
625206	DOMESTIC	84	140	38	50
617996	DOMESTIC	258	380	200	20
541860	DOMESTIC	99	225	26	8
491472	GEO THERMAL	60	375	Not Available	Not Available
490905	GEO THERMAL	80	375	Not Available	Not Available
415899	DOMESTIC	95	150	Not Available	20
258993	OTHER	60	100	30	40

#### 4.0 FRACTURE TRACE ANALYSIS

Fracture traces underlying, or in close proximity to, the site were evaluated using historical aerial photographs from the years 1992 through 2016 (Google Earth, 2017), the Elizabethtown and Palmyra Quadrangle Geologic Maps (Berg and Dodge, 1981), Plate 1-Part 2 in Wood (1980), and the United States Geological Survey (USGS) 7.5-Minute Topographic Quadrangle Maps. The photographs, publications and maps were reviewed to estimate lineaments or natural linear features on the ground surface. The linear features may be the surficial representation of deeper fractures, joints, faults or bedding planes within the subsurface which can transmit groundwater in the fractured bedrock aquifer at the site.

**Figures 2 and 3** show the results of the fracture trace analysis overlain on the geologic map of the site and an aerial basemap. Five fracture traces were identified within close proximity to the Wetland J-47 HDD that are likely related to the primary geologic structure. Two of the fracture traces trend approximately northwest-southeast, similar to the general structure of the regional homocline. The three perpendicular fracture traces trend approximately northeast-southwest and may represent stress-related joints.

#### 5.0 GEOTECHNICAL EVALUATION

Two geotechnical drilling evaluations were performed at the site; one was performed in 2014 and the other in 2017. Test borings were advanced by hollow-stem augers. An NQ core barrel/bit was used for rock coring. Geotechnical boring logs are included in **Attachment 1**. The locations of the borings are depicted on **Figure 2** and **Figure 3**.

The first geotechnical drilling program was performed on November 18, 2014, prior to the initiation of HDD operations. Soil Boring 01 (SB-01) was located approximately 45 feet north of the approximate mid-point of the bore path on the north side of Stream A-47 and Wetland J-47. Soil Boring 02 (SB-02) was located approximately 400 feet west of the eastern entry point and 75 feet north of the bore path. Soil Boring 03 (SB-03) was located approximately 400 feet east of the eastern entry point and 210 feet south of bore path.

Two additional borings were advanced between August 28 and September 7, 2017, prior to the initiation of HDD operations. Boring B-1 was installed near the HDD exit point on the west side of the HDD profile. Boring B-2 was installed near the HDD entry on the east side of the profile.

In general, the subsurface profile at the site, as observed in the borings, is described as follows:

- Soil and residual soil depths vary from west to east; 6.3 feet at B-1, 21.5 feet at SB-01, 32.5 feet at SB-02, 9.4 feet at B-2, and 30 feet at SB-03. The residual soils are described as follows:
  - **Boring B-1:** Sandy lean CLAY (CL) and poorly graded SAND with gravel (SP) (weathered sandstone);
  - **Boring SB-01:** SILT with sand (ML) and fine SAND with silt and gravel (sandstone);
  - **Boring SB-02:** Fine to medium SAND with silt and gravel (SM); Silty CLAY with sand (CL); Fine SAND with clay (SC); Silty CLAY with sand (CL); and weathered sandstone;
  - **Boring B-2:** Sandy SILT (ML) and poorly graded SAND with silt (SP-SM) (weathered sandstone); and
  - **Boring SB-03:** Silty CLAY with sand (CL); Fine to medium SAND with clay (SC); Silty CLAY with sand (CL-claystone); and weathered sandstone.
- Refusal, defined as naturally occurring rock that cannot be penetrated by standard soil sampling methods consisting of split-spoon samplers and augers, was encountered at 6.3 feet in B-1, 21.5 feet in SB-01, 32.5 feet at SB-02, 9.4 feet in B-2.
- Beneath auger refusal to the total depth of the NQ cores, bedrock was encountered and is described as follows:
  - **Boring B-1:** B-1 was completed to a total depth of 159 feet. Alternating sequences of grayish to reddish brown, conglomeratic to coarse- to fine-grained, SANDSTONE and reddish brown SILTSTONE were encountered. Two layers of CONGLOMERATE were encountered (at 40.0 to 45.6 feet and 95.3 to 96.7 feet). A total of 21 distinct strata composed of sandstone, siltstone, and conglomerate bedrock were identified, with thicknesses ranging from 1.5 feet to 34.5 feet. Rock recoveries were generally excellent (100%) in the majority of the core runs. One core run had poor core recovery (44%) from 84.0 to 87.4 feet in a highly weathered siltstone/sandstone zone. RQDs were very poor to excellent (0 to 99%), and in general the lower RQD values correlated to the siltstone layers and the higher RQD values correlate to the sandstone/conglomerate layers. Multiple soil seam and highly weathered rock were encountered in the upper 24 feet of the boring. Fractures ranging from generally horizontal to high angle were recorded in the core logs.



- **Boring B-2:** B-2 was completed to a total depth of 201 feet. Alternating sequences of grayish to reddish brown, conglomeratic and coarse- to fine-grained SANDSTONE and reddish brown SILTSTONE were encountered. Two layers of SHALE were encountered (at 84.8 to 102 feet and 153.4 to 170.8 feet). A total of 18 distinct strata of sandstone, siltstone, and shale bedrock were identified, with thicknesses ranging from 2.0 feet to 28.0 feet. Rock recoveries were generally excellent (100%) in the majority of the core runs. RQDs were poor to excellent (40 to 100%) below a depth of 20 feet. Fractures ranging from generally horizontal to high angle were recorded on the core logs.

Please note that RETTEW did not oversee or direct the geotechnical drilling program associated with the Wetland J-47 HDD, including but not limited to, the selection of boring locations and target depths, observations of rock cores during drilling operations, or preparation of boring logs. The geotechnical reports, boring logs, and core photographs that resulted from these programs were generated by other Sunoco Pipeline, L.P. contractors. RETTEW relied on these reports and incorporated their data into the general geologic and hydrogeologic framework of the analysis of the Wetland J-47 HDD in this report.

## **6.0 FIELD OBSERVATIONS**

A field investigation was performed by a RETTEW geologist on September 18, 2017, to identify rock outcrops for fracture fabric analysis, evaluation and possible ground-truthing of fracture traces identified during the desktop evaluation, and to identify potential sensitive receptors to IRs. Readily accessible bedrock outcrops were not observed. No additional sensitive receptors to IRs were identified during the site reconnaissance.

## **7.0 CONCEPTUAL HYDROGEOLOGIC MODEL AND CONCLUSION**

Based on published geologic and hydrogeologic information, and the evaluation of geotechnical borings from the site, the Wetland J-47 HDD location is underlain by sedimentary rocks of the Gettysburg Formation and Gettysburg Formation-Conglomerate. The hydrogeologic setting is dominated by groundwater flow in secondary openings along geologic features that include bedding planes, fractures, and joints. In these formations, secondary openings are more common near the surface. Well records indicate 90% of the water-bearing zones in the Gettysburg Formation are within 280 feet of the surface. Geotechnical core observations indicate that bedrock near the center of the HDD profiles is fractured.

The proposed 16-inch and 20-inch HDD profiles are relatively shallow compared to the land surface, streams S-A47 and S-A48, and Wetland J-47, and pass through both the unconsolidated overburden and fractured bedrock. The weakest point of the profile is beneath the first crossing of Stream S-A47. Based on the hydro-structural characteristics of the underlying geology described in this report and the known HDD profile through shallow soils and bedrock, the Wetland J-47 HDD site is susceptible to the inadvertent return of drilling fluids during HDD operations. The HDD profile has been lengthened to allow for deeper crossings beneath the streams and wetland. The inclination of the entry and exit angles has been increased as a means to install the pipe through these protective soils, residual soils, and bedrock in closer proximity to the entry and exit points than the original, shorter profile. From a geologic perspective, the longer and deeper profile, in conjunction with the proposed engineering controls and/or drilling best management practices will be used to reduce the risk of an IR.

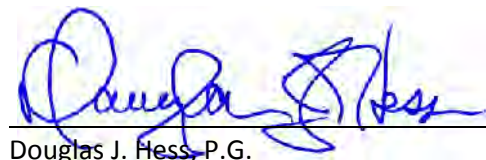
## 8.0 REFERENCES

- Berg, T. M., and C. M., Dodge, 1981, Atlas of Preliminary Geologic Quadrangle Maps of Pennsylvania, Pennsylvania Topographic and Geologic Survey, Map 61, 636 pages.
- Geyer, A. R., and P. J. Wilshusen, 1982, Engineering Characteristics of the Rocks of Pennsylvania, Pennsylvania Topographic and Geologic Survey, Environmental Geology Report 1, Second Edition, 300 pages.
- Google Earth Pro, 2017, Version 7.1.8.3036, September 20, 2017.
- Low, Dennis J., Daniel J. Hippe, and Dawna Yannacci, 2002, Geohydrology of Southeastern Pennsylvania, U.S. Geological Survey, Water-Resources Investigations Report 00-4166, 347 pages.
- Newport, T. G., 1971, Ground-water Resources of Montgomery County, Pennsylvania, Pennsylvania Topographic and Geologic Survey, Water Resources Report, W29, 83 pages.
- Pennsylvania Bureau of Topographic and Geologic Survey, Department of Conservation and Natural Resources, 2001, Bedrock Geology of PA, Edition: 1.0, Digital Map. Retrieved from internet September 18, 2017; [HTTP://www.dcnr.state.pa.us/topogeo/map1/bedmap.aspx](http://www.dcnr.state.pa.us/topogeo/map1/bedmap.aspx)DL Data: Page oexp.zip [[HTTP://www.dcnr.state.pa.us/topogeo/map1/bedmap.aspx](http://www.dcnr.state.pa.us/topogeo/map1/bedmap.aspx)].
- Pennsylvania Department of Conservation and Natural Resources, Pennsylvania Groundwater Information System (PaGWIS) database, website address: <http://www.dcnr.pa.gov/Conservation/Water/Groundwater/PAGroundwaterInformationSystem/Pages/default.aspx>, accessed September 21, 2017.
- Sevon, D., 2000, Map 13, Physiographic Provinces of Pennsylvania, Pennsylvania Bureau of Topographic and Geologic Survey, Harrisburg, Pennsylvania.
- United States Department of Agriculture, 2017, Natural Resources Conservation Service, Published Soil Surveys for Pennsylvania, Dauphin and Lebanon Counties, Pennsylvania: website address: <https://websoilsurvey.sc.egov.usda.gov/App/WebSoilSurvey.aspx> accessed September 21, 2017.
- Wood, C. R., 1980, Groundwater Resources of the Gettysburg and Hammer Creek Formations, Southeastern, Pennsylvania, Pennsylvania Geologic Survey, 4th Series, Water Resources Report 49, 87 pages.

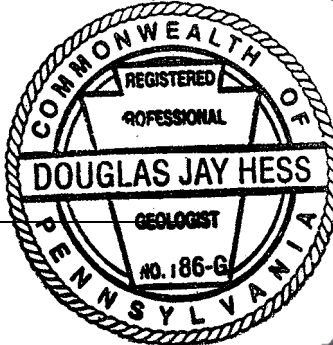
## 9.0 CERTIFICATION

The studies and evaluations presented in this report (other than Section 5) were completed under the direction of a licensed professional geologist (P.G.), and are covered under the P.G. seals that follow.

By affixing my seal to this document, I am certifying that, to my knowledge and belief, the information herein is true and correct. I further certify, that I am licensed to practice in the Commonwealth of Pennsylvania and that it is within my professional expertise to verify the correctness of the information herein.



Douglas J. Hess, P.G.  
License No. PG000186G



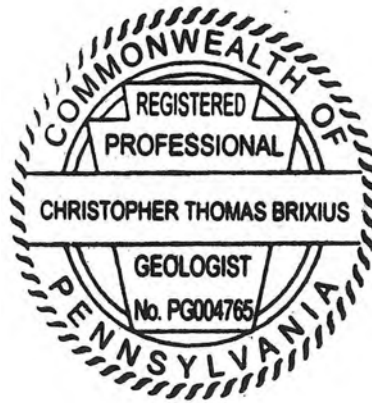


Ethan E. Prout, P.G.  
License No. PG003884





Christopher T. Brixius, P.G.  
License No. PG004765



**FIGURES**





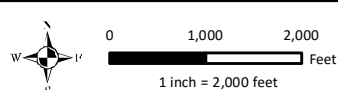
- 16" HDD Entry/Exit
- 20" HDD Entry/Exit
- 16" HDD Profile
- 20" HDD Profile

## Sunoco Pipeline, L.P.

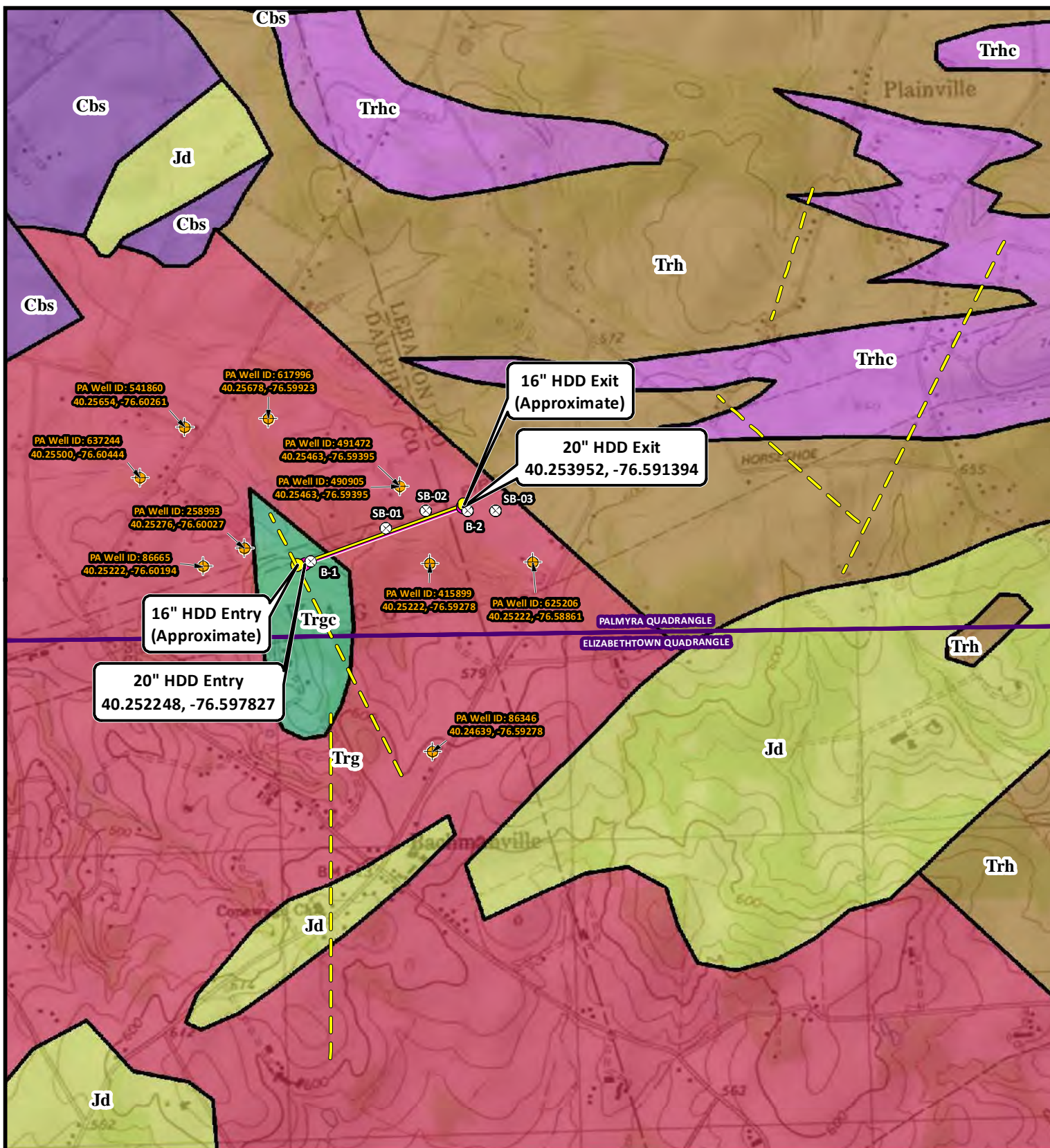
### Wetland J-47 HDD Location

#### Figure 1 - Topographic Basemap

Conewago Twp., Dauphin County, & South Londonderry Twp., Lebanon County, PA  
Project No. 096302011







- Residential Well
- Boring Location
- 16" HDD Entry/Exit
- 20" HDD Entry/Exit
- 16" HDD Profile
- 20" HDD Profile
- Inferred Fracture Trace

- Geologic Formation**
- Cbs - Buffalo Springs Formation
  - Jd - Diabase
  - Trg - Gettysburg Formation
  - Trgc - Gettysburg conglomerate
  - Trh - Hammer Creek Formation
  - Trhc - Hammer Creek conglomerate

Elizabethtown & Palmyra, PA USGS 7.5' Topographic Quadrangles

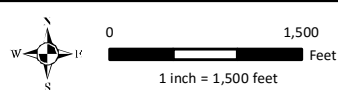
9/21/2017

## Sunoco Pipeline, L.P.

### Wetland J-47 HDD Location

#### Figure 2 - Geologic Map

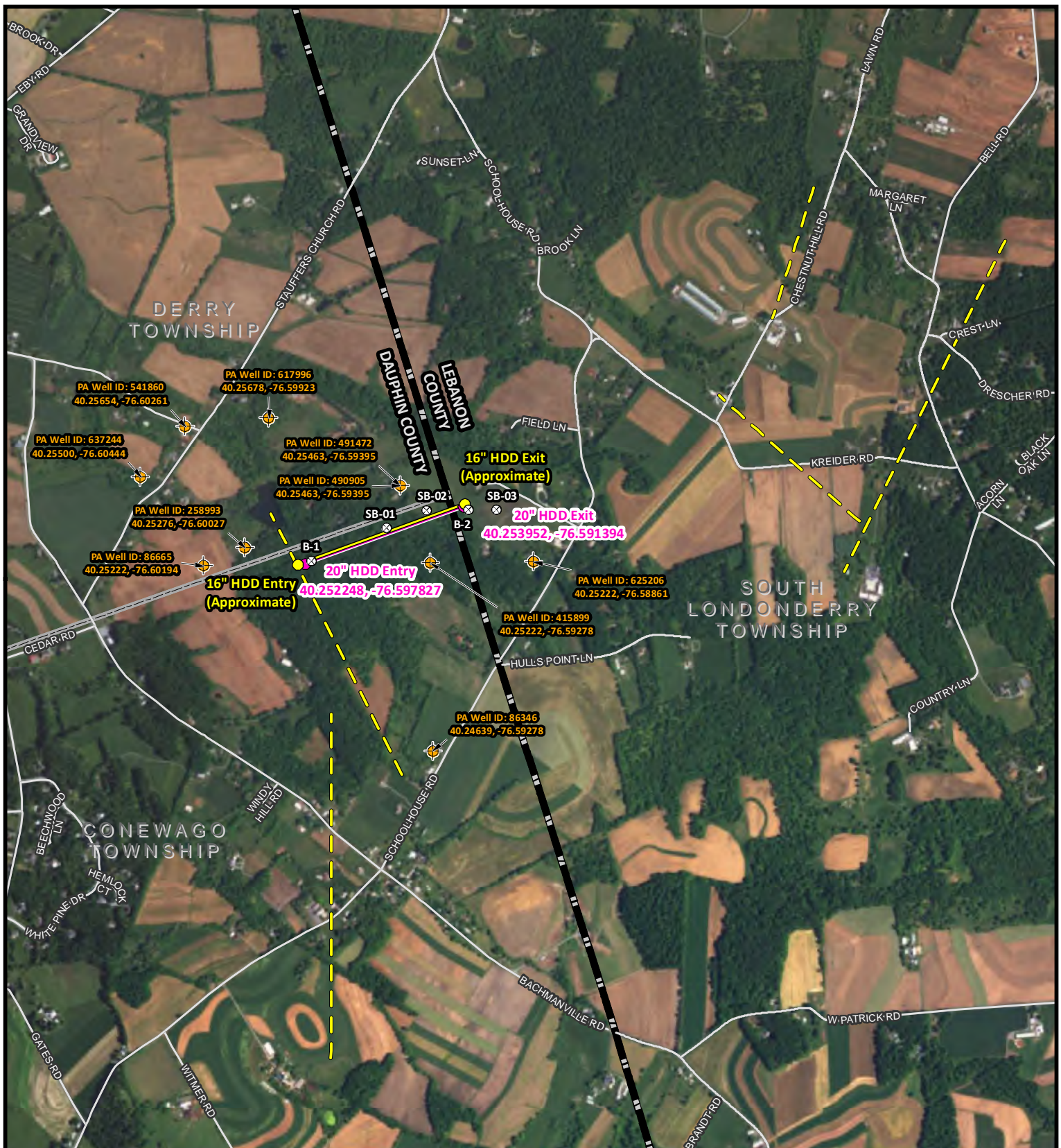
Conewago Twp., Dauphin County, & South Londonderry Twp., Lebanon County, PA  
Project No. 096302011



Service Layer Credits: Copyright: © 2013 National Geographic Society, I-cubed







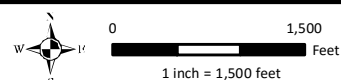
- |  |                    |  |                         |
|--|--------------------|--|-------------------------|
|  | Residential Well   |  | 20" HDD Profile         |
|  | Boring Location    |  | Inferred Fracture Trace |
|  | 16" HDD Entry/Exit |  | Road                    |
|  | 20" HDD Entry/Exit |  | Municipal Boundary      |
|  | 16" HDD Profile    |  | County Boundary         |

9/21/2017

## Sunoco Pipeline, L.P. Wetland J-47 HDD Location

### Figure 3 - Aerial Basemap

Conewago Twp., Dauphin County, & South Londonderry Twp., Lebanon County, PA  
Project No. 096302011



Source: Esri, DigitalGlobe, GeoEye, Earthstar Geographics, CNES/Airbus DS, USDA, USGS, AeroGRID, IGN, and the GIS User Community





**ATTACHMENT 1**  
**GEOTECHNICAL BORING LOGS**



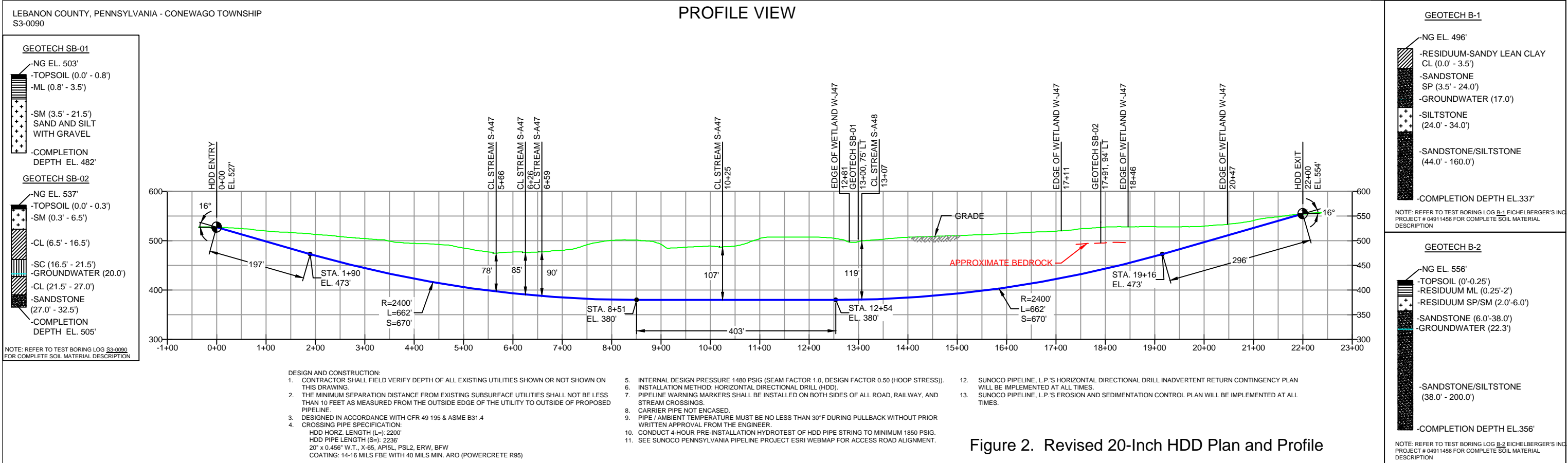
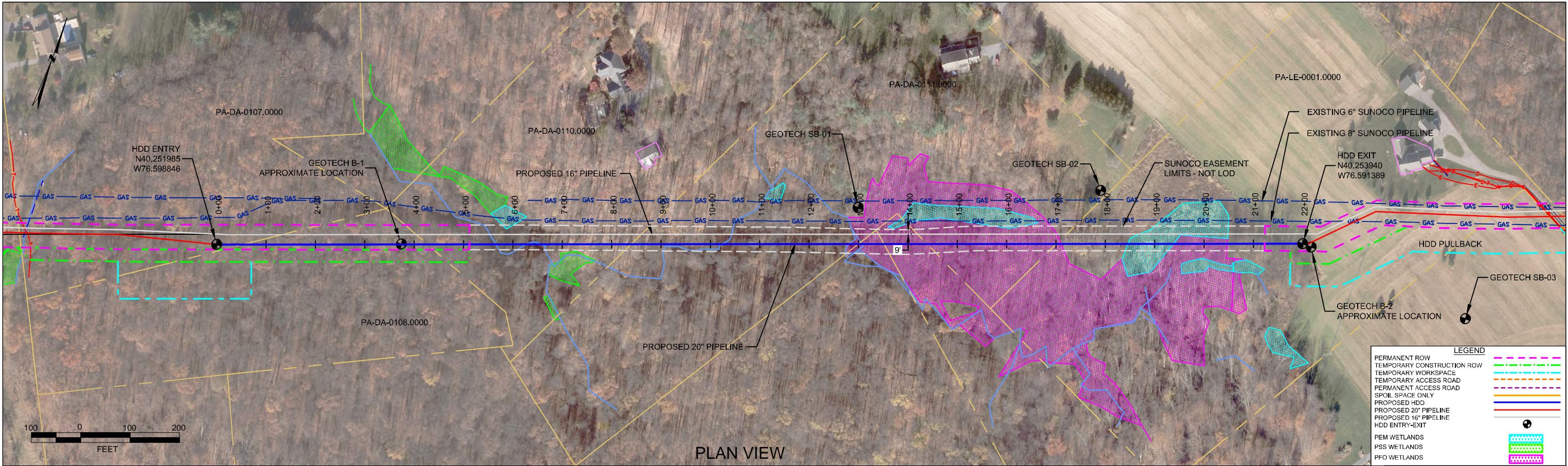


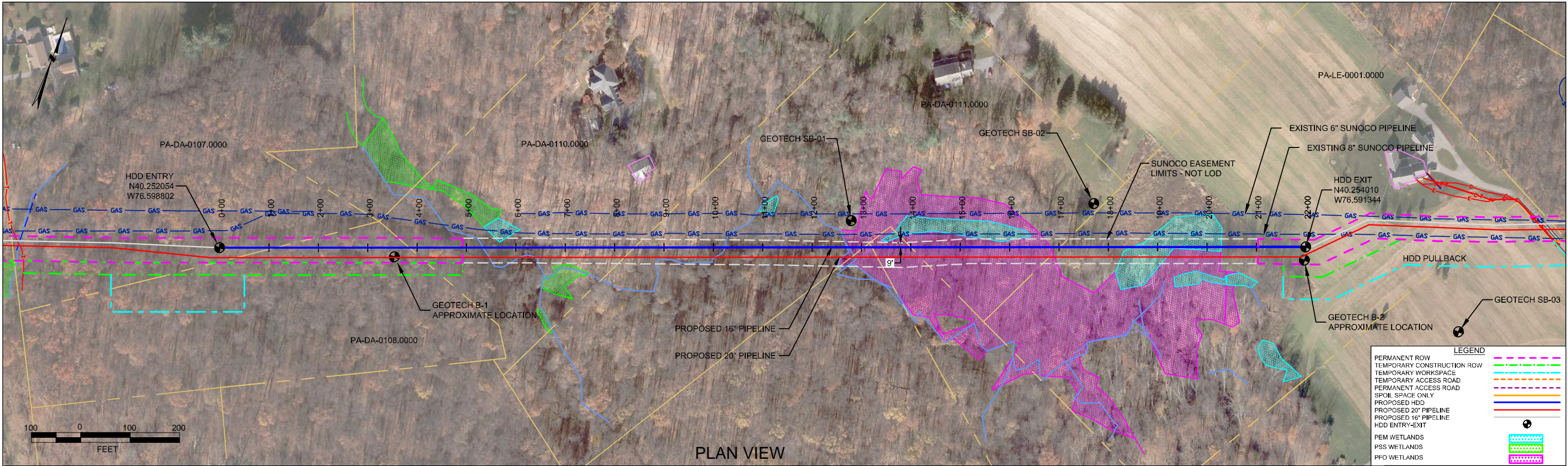


Figure 2. Revised 20-Inch HDD Plan and Profile

NOTES		REF. DRAWING			REVISIONS										<div><div>Sunoco Logistics Partners L.P.</div></div> <div><div>TETRA TECH ROONEY (303) 792-5911</div></div>		SUNOCO PIPELINE, L.P.			
1. ALL COORDINATES SHOWN ARE IN LATITUDE AND LONGITUDE. ALL MSL ELEVATIONS ARE NAD83 2. STATIONING IS BASED ON HORIZONTAL DISTANCES. 3. ROONEY ENGINEERING, INC. AND SUNOCO PIPELINE, LP ARE NOT RESPONSIBLE FOR LOCATION OF FOREIGN UTILITIES SHOWN IN PLOT PLAN OR PROFILE. THE INFORMATION SHOWN HEREON IS FURNISHED WITHOUT LIABILITY ON THE PART OF ROONEY ENGINEERING, INC. AND SUNOCO PIPELINE, LP, FOR ANY DAMAGES RESULTING FROM ERRORS OR OMISSIONS THEREIN. 4. CONTRACTOR IS RESPONSIBLE FOR LOCATING ALL UTILITIES. CONTACT ONE CALL AT 811 PRIOR TO DIGGING. 5. SUNOCO EMERGENCY HOTLINE NUMBER IS #1-800-786-7440.		ES-4.38	TO	ES-5.01	EROSION & SEDIMENT PLAN	EP3	DESIGN CHANGE - EXTENDED DRILL PER LANEY DRILLING AND CM SPREAD 5 APPROVAL				MRS	09/25/17	RMB	09/25/17			AMC	09/25/17	HORIZONTAL DIRECTIONAL DRILL WETLAND PENNSYLVANIA PIPELINE PROJECT	
		SHEET 24	TO	SHEET 1	AERIAL SITE PLAN	EP2	REVISED PER PADEP COMMENTS RECEIVED 09/06/16				DLM	09/30/16	RMB	09/30/16			AAW	09/30/16		
						EP1	REVISED PER PADEP COMMENTS				DLM	05/10/16	RMB	05/10/16			AAW	05/10/16		
					EP					MRS	03/15/16	RMB	03/15/16	AAW	03/15/16					
					C	ADDED GEOTECH INFO / DESIGN ADJUSTMENT				MRS	09/22/16	RMB	09/22/16	AAW	09/22/16					
					B	ISSUED FOR BID				DLM	07/31/15	RMB	07/31/15	AAW	07/31/15					
	DWG NO		DWG NO		DESCRIPTION	NO.	DESCRIPTION				BY	DATE	CHK	DATE	APP	DATE	SCALE: 1"=200'	DWG. NUMBER: PA-LE-0001.0000-SR		

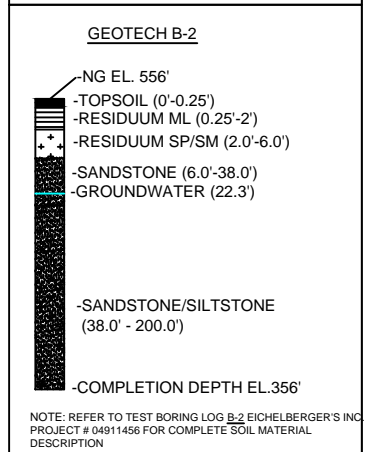
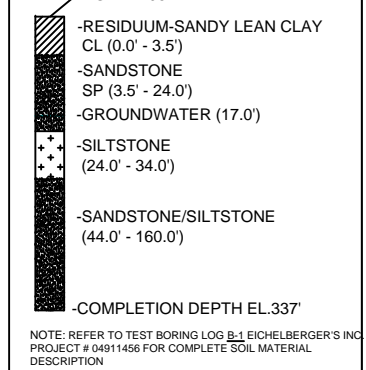
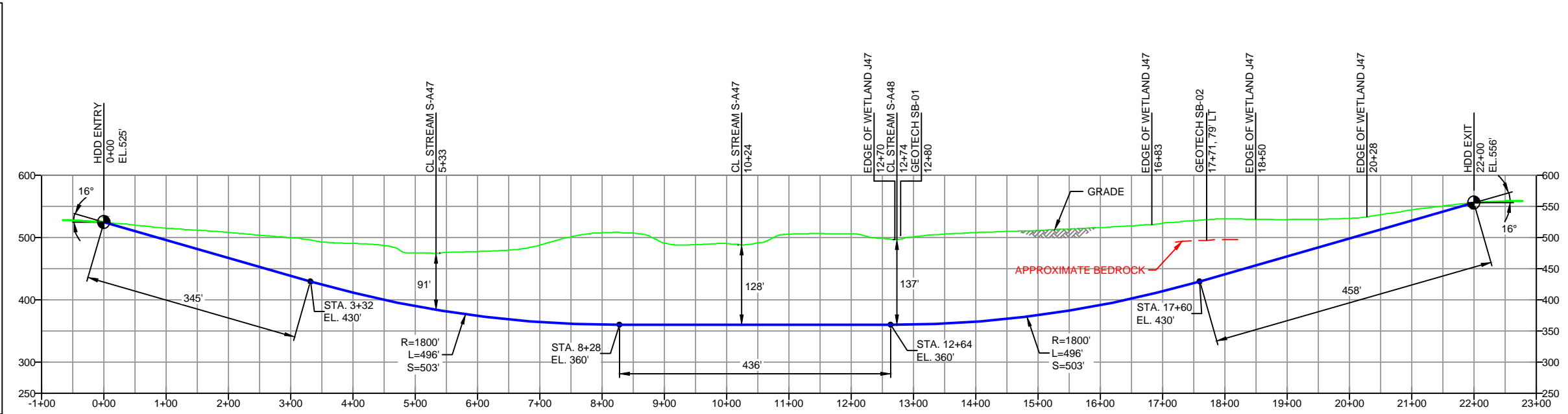
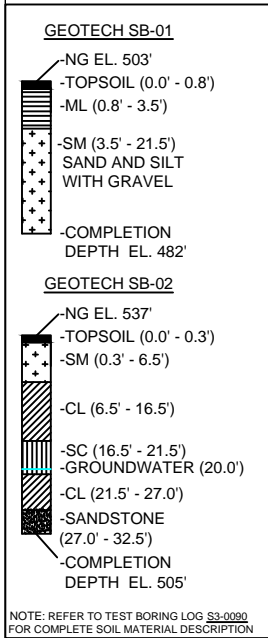




LEBANON COUNTY, PENNSYLVANIA - CONEWAGO TOWNSHIP  
S3-0090-16



PLAN VIEW

PROFILE VIEW



- DESIGN AND CONSTRUCTION:
- CONTRACTOR SHALL FIELD VERIFY DEPTH OF ALL EXISTING UTILITIES SHOWN OR NOT SHOWN ON THIS DRAWING.
  - THE MINIMUM SEPARATION DISTANCE FROM EXISTING SUBSURFACE UTILITIES SHALL NOT BE LESS THAN 10 FEET AS MEASURED FROM THE OUTSIDE EDGE OF THE UTILITY TO OUTSIDE OF PROPOSED PIPELINE.
  - DESIGNED IN ACCORDANCE WITH CFR 49 195 & ASME B31.4
  - CROSSING PIPE SPECIFICATION:  
HDD HORZ. LENGTH (L=): 2200'  
HDD PIPE LENGTH (S=): 2245'  
16" x 0.438" W.T., X-70, API 5L, PSL2, ERW, BFW  
COATING: 14-16 MILS FBE WITH 40 MILS MIN. ARO (POWERCRETE R95)
  - INTERNAL DESIGN PRESSURE 1480 PSIG (SEAM FACTOR 1.0, DESIGN FACTOR 0.50 (HOOP STRESS)).
  - INSTALLATION METHOD: HORIZONTAL DIRECTIONAL DRILL (HDD).
  - PIPELINE WARNING MARKERS SHALL BE INSTALLED ON BOTH SIDES OF ALL ROAD, RAILWAY, AND STREAM CROSSINGS.
  - CARRIER PIPE NOT ENCASED.
  - PIPE / AMBIENT TEMPERATURE MUST BE NO LESS THAN 30°F DURING PULLBACK WITHOUT PRIOR WRITTEN APPROVAL FROM THE ENGINEER.
  - CONDUCT 4-HOUR PRE-INSTALLATION HYDROTEST OF HDD PIPE STRING TO MINIMUM 1850 PSIG.
  - SEE SUNOCO PENNSYLVANIA PIPELINE PROJECT ESRI WEBMAP FOR ACCESS ROAD ALIGNMENT.
  - SUNOCO PIPELINE, L.P.'S HORIZONTAL DIRECTIONAL DRILL INADVERTENT RETURN CONTINGENCY PLAN WILL BE IMPLEMENTED AT ALL TIMES.
  - SUNOCO PIPELINE, L.P.'S EROSION AND SEDIMENTATION CONTROL PLAN WILL BE IMPLEMENTED AT ALL TIMES.

Figure 4. Revised 16-Inch Plan and Profile

<div>NOTES</div> <div>1. ALL COORDINATES SHOWN ARE IN LATITUDE AND LONGITUDE. ALL MSL ELEVATIONS ARE NAD83</div> <div>2. STATIONING IS BASED ON HORIZONTAL DISTANCES.</div> <div>3. ROONEY ENGINEERING, INC. AND SUNOCO PIPELINE, LP ARE NOT RESPONSIBLE FOR LOCATION OF FOREIGN UTILITIES SHOWN IN PLOT PLAN OR PROFILE. THE INFORMATION SHOWN HEREON IS FURNISHED WITHOUT LIABILITY ON THE PART OF ROONEY ENGINEERING, INC. AND SUNOCO PIPELINE, LP, FOR ANY DAMAGES RESULTING FROM ERRORS OR OMISSIONS THEREIN.</div> <div>4. CONTRACTOR IS RESPONSIBLE FOR LOCATING ALL UTILITIES. CONTACT ONE CALL AT 811 PRIOR TO DIGGING.</div> <div>5. SUNOCO EMERGENCY HOTLINE NUMBER IS #1-800-786-7440.</div>	REF. DRAWING				REVISIONS										<div><div>Sunoco Logistics Partners L.P.</div></div> <div><div>TETRA TECH ROONEY</div><div>(303) 792-5911</div></div>		<div>SUNOCO PIPELINE, L.P.</div> <div>HORIZONTAL DIRECTIONAL DRILL WETLAND</div> <div>PENNSYLVANIA PIPELINE PROJECT</div>				
	ES-4.38	TO	ES-5.01	EROSION & SEDIMENT PLAN	EP3	DESIGN CHANGE - EXTENDED DRILL PER LANEY DRILLING AND CM SPREAD 5 APPROVAL				MRS	09/25/17	RMB	09/25/17	AMC							09/25/17
	SHEET 24	TO	SHEET 1	AERIAL SITE PLAN	EP2	REVISED PER PADEP COMMENTS RECEIVED 09/06/16				MRS	10/07/16	RMB	10/07/16	AAW							10/07/16
					EP1	REVISED PER PADEP COMMENTS				DLM	05/17/16	RMB	05/17/16	AAW	05/17/16						
					EP					MRS	03/05/16	RMB	03/05/16	AAW	03/05/16						
					B	ADDED GEOTECH INFO				MRS	09/22/15	RMB	09/22/15	AAW	09/22/15						
					A	ISSUED FOR BID				MRS	08/31/15	RMB	08/31/15	AAW	08/31/15						
	DWG NO		DWG NO	DESCRIPTION	NO.	DESCRIPTION				BY	DATE	CHK	DATE	APP	DATE						















<b>DRILL COMPANY:</b>	Eichelberger's, Inc.
<b>DRILLER:</b> S. Taylor	<b>LOGGED BY:</b> L. Proczko
<b>DRILL RIG:</b>	Diedrich D-50
<b>DRILLING METHOD:</b>	Casing/Rock Coring
<b>SAMPLING METHOD:</b>	2-in SS1.874-in Core
<b>HAMMER TYPE:</b>	Automatic
<b>EFFICIENCY</b>	N/A
<b>REVIEWED BY:</b>	F. Hoffman

STANDARD PENETRATION TEST DATA N in blows/ft ©				Additional Remarks
<div> <div>×</div> Moisture <div>▣</div> PL </div> <div> <div>+</div> LL </div>				
<div>0</div> <div>25</div> <div>50</div>				
STRENGTH, tsf				
<div>▲</div> Qu <div>✱</div> Qp				
<div>0</div> <div>2.0</div> <div>4.0</div>				
5	<div>⊙</div>	<div>×</div> <div>▣</div> <div>+</div>		LL = 26 PL = 19
	×			>>⊙ Fines=12.2%
				26 min.
				7 min. 6 min.
				22 min.
				20 min.

The stratification lines represent approximate boundaries. The transition may be gradual.

<b>DATE STARTED:</b> 8/28/17 <b>DATE COMPLETED:</b> 8/31/17 <b>COMPLETION DEPTH:</b> 159.0 ft <b>BENCHMARK:</b> N/A <b>ELEVATION:</b> N/A <b>LATITUDE:</b> n/a° <b>LONGITUDE:</b> n/a° <b>STATION:</b> N/A <b>OFFSET:</b> N/A <b>REMARKS:</b>	<b>DRILL COMPANY:</b> Eichelberger's, Inc. <b>DRILLER:</b> S. Taylor <b>LOGGED BY:</b> L. Proczko <b>DRILL RIG:</b> Diedrich D-50 <b>DRILLING METHOD:</b> Casing/Rock Coring <b>SAMPLING METHOD:</b> 2-in SS1.874-in Core <b>HAMMER TYPE:</b> Automatic <b>EFFICIENCY:</b> N/A <b>REVIEWED BY:</b> F. Hoffman	<h2 style="margin:0;">BORING B-1</h2> <div style="display: flex; justify-content: space-between; align-items: center;"> <div style="text-align: left;"> <b>Water</b>            ▽ While Drilling            ▽ Post-Core            ▽         </div> <div style="text-align: right;">           Not Enc.            17 feet         </div> </div> <b>BORING LOCATION:</b> See Boring Location Plan
---	--	--




Elevation (feet)	Depth, (feet)	Graphic Log	Sample Type	Sample No.	Recovery (inches)	MATERIAL DESCRIPTION	USCS Classification	SPT Blows per 6-inch (SS) RQD & Recovery % (NX)	Moisture, %	STANDARD PENETRATION TEST DATA N in blows/ft  <div><div> Moisture</div><div> PL</div></div> <div><div> LL</div><div> LL</div></div> <div><div> Qu</div><div> Qp</div></div> <div><div>02550</div><div>02.04.0</div></div>				Additional Remarks
	30		R-6	48	<b>SILTSTONE</b> -Brown to red-brown, Very fine grained, Weathered to Highly Weathered, very broken to slightly broken, moderately hard		RQD=0 Rec=80%							
	35		R-7	60	<b>Conglomeratic SANDSTONE</b> -Gray-brown to dark gray-brown, Fine to very coarse grained, Weathered to Slightly Weathered, very broken to massive, hard to very hard		RQD=59 Rec=100%							17 min.
	40		R-8	60	<b>CONGLOMERATE</b> -Light gray-brown to gray-brown, Fine to very coarse grained, Weathered to Slightly Weathered, very broken to massive, hard to very hard, trace pits and vugs		RQD=70 Rec=100%						>>  Qu = 425.1 tsf 155.7 pcf 14 min.	
	45		R-9	48	<b>Conglomeratic SANDSTONE</b> -Dark gray-brown, Fine to coarse grained, Weathered to Highly Weathered, very broken to massive, very hard		RQD=26 Rec=100%						>>  Qu = 379.0 tsf 154.5 pcf 9 min.	
			R-10	12	<b>Conglomeratic SANDSTONE</b> -Gray to gray-brown, Fine to very coarse grained, Slightly Weathered, slightly broken to massive, hard to very hard		RQD=88 Rec=100%						4 min. 2 min. 2 min. 3 min. 4 min. 3 min.	
	50		R-11	60			RQD=98 Rec=100%						>>  Qu = 283.6 tsf 149.5 pcf 3 min.	
	55		R-12	60	<b>SANDSTONE</b> -Light gray to dark gray-brown, Fine to coarse grained, Slightly Weathered, very broken to massive, hard to very hard, trace pits		RQD=77 Rec=100%						>>  Qu = 441.1 tsf 149.0 pcf 3 min.	
	60												3 min. 3 min. 3 min. 3 min.	
Continued Next Page														

Continued Next Page



Professional Service Industries, Inc.  
 1707 S. Cameron Street, Suite B  
 Harrisburg, PA 17104  
 Telephone: (717) 230-8622

**PROJECT NO.:** 04911456  
**PROJECT:** Energy Transfer HDD (DPS)  
**LOCATION:** Wetland "J47" (PPP5)  
 Dauphin Co., PA  
 PA-LE-0001.0000-SR/PO#201770816-2

<b>Water</b>		While Drilling	Not Enc.
		Post-Core	17 feet
			

**BORING LOCATION:**  
See Boring Location Plan

*Continued Next Page*

Professional Service Industries, Inc.  
1707 S. Cameron Street, Suite B  
Harrisburg, PA 17104  
Telephone: (717) 230-8622

PA-LE-0001.0000-SR/PO#201770816-2

<b>DATE STARTED:</b> 8/28/17 <b>DATE COMPLETED:</b> 8/31/17 <b>COMPLETION DEPTH:</b> 159.0 ft <b>BENCHMARK:</b> N/A <b>ELEVATION:</b> N/A <b>LATITUDE:</b> n/a° <b>LONGITUDE:</b> n/a° <b>STATION:</b> N/A <b>OFFSET:</b> N/A <b>REMARKS:</b>	<b>DRILL COMPANY:</b> Eichelberger's, Inc. <b>DRILLER:</b> S. Taylor <b>LOGGED BY:</b> L. Proczko <b>DRILL RIG:</b> Diedrich D-50 <b>DRILLING METHOD:</b> Casing/Rock Coring <b>SAMPLING METHOD:</b> 2-in SS1.874-in Core <b>HAMMER TYPE:</b> Automatic <b>EFFICIENCY:</b> N/A <b>REVIEWED BY:</b> F. Hoffman	<h2 style="margin:0;">BORING B-1</h2> <div style="display: flex; justify-content: space-between; align-items: center;"> <div style="width: 30%;"> <b>Water</b>  <div style="display: flex; align-items: center;"> <div style="width: 10px; height: 10px; border: 1px solid black; margin-right: 5px;"></div> <span>While Drilling</span> </div> <div style="display: flex; align-items: center;"> <div style="width: 10px; height: 10px; border: 1px solid black; margin-right: 5px;"></div> <span>Post-Core</span> </div> </div> <div style="width: 60%; text-align: right;">           Not Enc.            17 feet         </div> </div> <b>BORING LOCATION:</b> See Boring Location Plan
---	--	--

Elevation (feet)	Depth, (feet)	Graphic Log	Sample Type	Sample No.	Recovery (inches)	MATERIAL DESCRIPTION	USCS Classification	SPT Blows per 6-inch (SS) RQD & Recovery % (NX)	Moisture, %	STANDARD PENETRATION TEST DATA N in blows/ft @				Additional Remarks
								X Moisture    PL LL						
								STRENGTH, tsf ▲ Qu                      * Qp						
	90		R-22	57		<b>Conglomeratic SANDSTONE</b> -Red-brown to gray, Fine to coarse grained, Slightly Weathered, slightly broken to massive, very hard		RQD=66 Rec=95%					9 min. 10 min. Q <sub>u</sub> = 335.9 tsf 795.3 pcf	
	95		R-23	58		<b>CONGLOMERATE</b> -Light gray-brown to dark gray-brown, Fine to very coarse grained, Weathered to Slightly Weathered, broken to slightly broken, very hard, pits and vugs Highly Weathered/Completely Weathered layer @ 96.2 feet (~ 4-1/2 inches thick)		RQD=73 Rec=97%					6 min. 5 min. 5 min. 3 min. 3 min. 8 min. 7 min.	
	100		R-24	60		<b>SILTSTONE</b> -Red-brown to dark brown, Very fine grained, Slightly Weathered, very broken to massive, moderately hard <b>SILTSTONE</b> -Red-brown to light gray-brown, Very fine grained, Weathered to Slightly Weathered, very broken to massive, moderately hard		RQD=23 Rec=100%					10 min. 6 min. 6 min.	
	105		R-25	60		<b>SANDSTONE</b> -Red-brown to dark gray-brown, Fine grained, Weathered to Highly Weathered, very broken to slightly broken, moderately hard to hard		RQD=38 Rec=100%					9 min. 9 min. 5 min. 5 min. Q <sub>u</sub> = 511.1 tsf 350.4 pcf	
	110		R-26	48		<b>SANDSTONE</b> -Brown to gray-brown, Fine to medium grained, Weathered to Highly Weathered, very broken to slightly broken, moderately hard to hard		RQD=8 Rec=100%					8 min. 8 min. 9 min. 6 min. 6 min.	
	115		R-27	12		<b>Conglomeratic SANDSTONE</b> -Light gray to dark brown, Fine to very coarse grained, Slightly Weathered, broken to massive, very hard to extremely hard Developing, soil-filled, diagonal fracture @ 115.2 feet.		RQD=58 Rec=100%					9 min. 7 min. Q <sub>u</sub> = 518.7 tsf 160.1 pcf	
			R-28	60		<b>SILTSTONE</b> -Red-brown, Very fine grained, Weathered to Slightly Weathered, very broken to massive, moderately hard		RQD=68 Rec=100%					5 min. 4 min. 5 min. 5 min.	
	120													
Continued Next Page														



Professional Service Industries, Inc.  
 1707 S. Cameron Street, Suite B  
 Harrisburg, PA 17104  
 Telephone: (717) 230-8622

**PROJECT NO.:** 04911456  
**PROJECT:** Energy Transfer HDD (DPS)  
**LOCATION:** Wetland "J47" (PPP5)  
 Dauphin Co., PA  
 PA-LE-0001.0000-SR/PO#201770816-2

**BORING LOCATION:**  
See Boring Location Plan

STANDARD PENETRATION TEST DATA N in blows/ft ©				Additional Remarks
×	Moisture	▣	PL	
		+	LL	
0	25	50		
STRENGTH, tsf				
▲	Qu	✱	Qp	
0	2.0	4.0		
			>> 9 min. 6 min. 818.5 tsf 162.4 pcf	
			6 min.	
			3 min.	
			3 min.	
			4 min.	
			3 min.	
			7 min.	
			6 min.	
			6 min.	
			5 min.	
			3 min.	
			3 min.	
			3 min.	
			3 min.	
			2 min.	
			3 min.	
			3 min.	
			3 min.	
			4 min. Q <sub>u</sub> = 801.6 tsf 157.1 pcf	
			>> 4 min.	
			4 min.	
			3 min.	
			4 min.	
			3 min.	
			3 min.	
			3 min.	
			3 min.	
			2 min.	
			3 min.	
			3 min.	

<b>DATE STARTED:</b> 8/28/17		<b>DRILL COMPANY:</b> Eichelberger's, Inc.		<b>BORING B-1</b>	
<b>DATE COMPLETED:</b> 8/31/17		<b>DRILLER:</b> S. Taylor <b>LOGGED BY:</b> L. Proczko			
<b>COMPLETION DEPTH:</b> 159.0 ft		<b>DRILL RIG:</b> Diedrich D-50		<div style="display: flex; align-items: center;"> <div style="border: 1px solid black; padding: 2px; margin-right: 5px;">Water</div> <div style="display: flex; flex-direction: column; gap: 5px;"> <div>▽ While Drilling</div> <div>▽ Post-Core</div> <div>▽</div> </div> <div style="margin-left: 20px;">             Not Enc. 17 feet           </div> </div>	
<b>BENCHMARK:</b> N/A		<b>DRILLING METHOD:</b> Casing/Rock Coring			
<b>ELEVATION:</b> N/A		<b>SAMPLING METHOD:</b> 2-in SS1.874-in Core		<b>BORING LOCATION:</b> See Boring Location Plan	
<b>LATITUDE:</b> n/a°		<b>HAMMER TYPE:</b> Automatic			
<b>LONGITUDE:</b> n/a°		<b>EFFICIENCY:</b> N/A			
<b>STATION:</b> N/A <b>OFFSET:</b> N/A		<b>REVIEWED BY:</b> F. Hoffman			
<b>REMARKS:</b>					

Elevation (feet)	Depth, (feet)	Graphic Log	Sample Type	Sample No.	Recovery (inches)	MATERIAL DESCRIPTION	USCS Classification	SPT Blows per 6-inch (SS) RQD & Recovery % (NX)	Moisture, %	STANDARD PENETRATION TEST DATA N in blows/ft @	Additional Remarks
										X Moisture    PL LL 0                    25                    50	
	150			R-36	60	<b>Conglomeratic SANDSTONE</b> -Light gray-brown to dark gray-brown to brown, Fine to very coarse grained, Slightly Weathered, very broken to massive, hard to extremely hard		RQD=86 Rec=100%		STRENGTH, tsf ▲ Qu                    * Qp 0                    2.0                    4.0	3 min. 2 min.    >>▲ Qu = 412.9 tsf 152.2 pcf 29 min.
	155			R-37	60	<b>SILTSTONE</b> -Red-brown, Very fine grained, Weathered to Highly Weathered, very broken to broken, moderately hard <b>SILTSTONE</b> -Dark red-brown, Very fine grained, Slightly Weathered, slightly broken to massive, moderately hard <b>Conglomeratic SANDSTONE</b> -Light gray to red-brown, Fine to coarse grained, Slightly Weathered, massive, hard Siltstone seam @ 156.9 feet (~ 2-1/2 inches thick) <b>SILTSTONE</b> -Dark red-brown, Very fine grained, Slightly Weathered, massive, moderately hard Test boring terminated @ 159 feet		RQD=87 Rec=100%			3 min. 4 min. 7 min. 4 min. 4 min. 5 min. 5 min.

	Professional Service Industries, Inc.	<b>PROJECT NO.:</b> 04911456
	1707 S. Cameron Street, Suite B	<b>PROJECT:</b> Energy Transfer HDD (DPS)
	Harrisburg, PA 17104	<b>LOCATION:</b> Wetland "J47" (PPP5)
	Telephone: (717) 230-8622	Dauphin Co., PA
		PA-LE-0001.0000-SR/PO#201770816-2



0111456  
Spec Core B-1  
8-28-17  
6'3"-2'  
Box lot  
Wetland 347

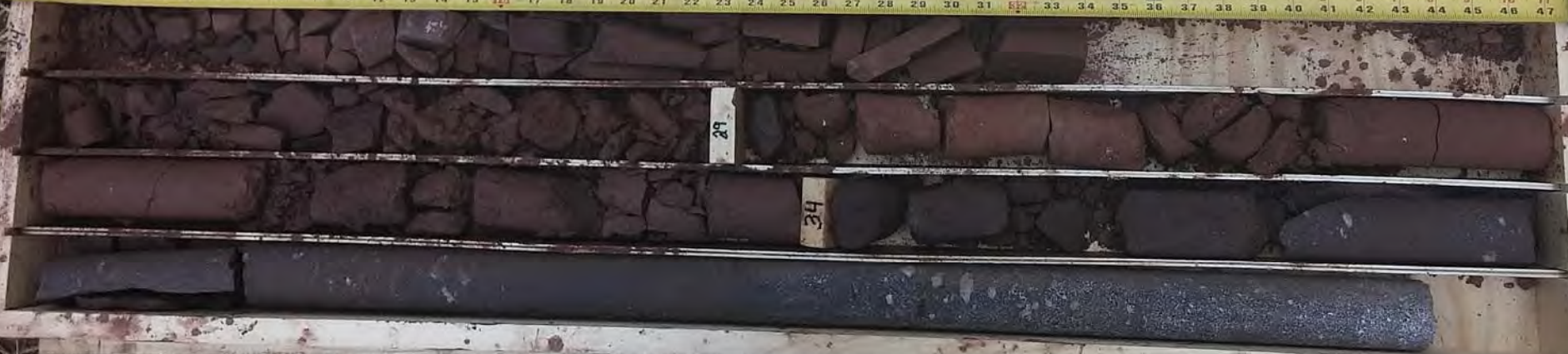
Run	Depth (ft.)	Recovery (%)	RQD (in.)
R-1	6'3"-9'	31.5	5.5
R-2	9'-16'	60	13
R-3	16'-17'	12	0.0
R-4	17'-24'	37	0.0





04911456  
Cryo Core B-1  
8-28-11  
21-37  
Box 2 of  
Wetland 347

RUN	Depth (ft.)	Rec (in.)	RAD (in.)
R5	24-29	42	0.0
R6	22-34	48	14
R7	34-59	60	40



39



04/11/1456  
Geo Boring R-1  
8:28.17  
39-52.9  
Box 3 of  
WETLAND J47

8217

RUN	Depth (ft.)	Roc (in.)	RQD (in.)
R-8	39-44	60	47
R-9	44-48	48	18
R-10	48-49	12	10.5
R-11	49-54	60	59





04/11/56  
Geo Box B-1  
829.17 / 820.17  
629.827  
Box 5 of  
Wetland J97

04/11/56  
Geo Box B-1  
829.17  
529.67.9  
Box 4 of  
Wetland J47

Run	Depth (ft)	Rec (in)	R&D (in)
R-12	54-59	60	46
R-13	59-64	60	37.5
R-14	64-69	60	37.5





PPH5  
04/11/45L  
B-1  
B-29.17  
679-67  
Box  
Wetland 547

	RUN	DPTH (ft.)	Rc (in.)	RAD (in.)
B-29.17	R-15	69-74	60	55.5
B-30.17	R-16	74-79	60	57.5
	R-17	79-81	71	8
	R-18	81-81.2	42	0
	R-19	81.2-84	34	14





PPP#5  
 04911456  
 Geo Box B-1  
 830-17  
 827-99  
 Box 6 of  
 Wetland 547

Run	Depth (ft.)	Rac (in.)	Rac (in.)
R-20	84-87.4	18	0
R-21	87.4-89	19	12.5
R-22	89-94	57	39.5
R-23	94-99	58	43.5

Water 17'





PDP#5  
04911456  
Geo Bore B-1  
8-30-17 / 8-31-17  
94-114  
Box 7 of  
Wetland J47

Run	Depth(ft)	Rec(in.)	RQD(in.)
R-24	99-104	60	14
R-25	104-109	60	22.5
R-26	109-113	48	4
R-27	113-114	12	7

8-30-17

8-31-17

99

104

113

114



PPP#5  
04911456  
B-1  
831.17  
114-128.6  
Box 8 of  
Wetland J47

RUN	Depth(ft.)	Rec(in.)	R&D(in.)
R-28	114-119	54.60	41
R-29	119-124	60.0	36.5
R-30	124-126.5	26	4
R-31	126.5-129	32	0





PPT#5  
 0491456  
 B-1  
 8.31.17  
 1286-1452  
 Box 9 of  
 Wetland J47

Run	Depth (ft.)	Rac (in.)	RQ D (in.)
R-32	129-134	50	44
R-33	134-139	41.5	8.5
R-34	139-144	60	46.5
R-35	144-149	55	35



M5.2






PPP#5  
04911456  
B-1  
8.31.17  
145.2-159  
Box 10 of 10  
Wetland J47

RUN	Depth (ft.)	REC (in.)	R&D (in.)
R-36	149-154	60	51.5
R-37	154-159	60	52

143-2  
149



04911456  
6. 8. 2. 1




<b>Water</b>		While Drilling	Not Enc.
		Post-Core	22.3 feet
			

**BORING LOCATION:**  
See Boring Location Plan

Continued Next Page

Professional Service Industries, Inc.  
1707 S. Cameron Street, Suite B  
Harrisburg, PA 17104  
Telephone: (717) 230-8622

PA-LE-0001.0000-SR/PO#201770816-2

BORING B-2			
Water		While Drilling	Not Enc.
		Post-Core	22.3 feet
			

**BORING LOCATION:**  
See Boring Location Plan

Elevation (feet)	Depth, (feet)	Graphic Log	Sample Type	Sample No.	Recovery (inches)	MATERIAL DESCRIPTION	USCS Classification	SPT Blows per 6-inch (SS) RQD & Recovery % (NX)	Moisture, %  STRENGTH, tsf ▲ Qu * Qp	Additional Remarks
									TEST DATA N in blows/ft © X Moisture PL LL 0 25 50 0 2.0 4.0	
30		[Pattern]	R-4	96		<b>SANDSTONE</b> -Brown to gray-brown, Fine grained, Weathered to Slightly Weathered, very broken to massive, hard		RQD=49 Rec=100%		3 min. 3 min. 3 min. 3 min. 3 min. 3 min. 3 min.
35		[Pattern]								3 min. 3 min. 3 min. 3 min.
40		[Pattern]	R-5	84		<b>SANDSTONE</b> -Brown to gray-brown, Fine grained, Highly Weathered, very broken to broken, moderately hard, multiple soil seams and layers <b>SILTSTONE</b> -Red-brown to red-gray-brown, Very fine grained, Slightly Weathered, broken to massive, moderately hard		RQD=89 Rec=100%	>> ▲ Q = 43.6 tsf 168.8 pcf	3 min. 3 min. 3 min. 3 min. 3 min. 4 min. 3 min.
45		[Pattern]				Broken/very broken layer @ 44.7 feet (~ 3-1/2 inches thick)				3 min.
50		[Pattern]	R-6	120		<b>SILTSTONE</b> -Brown to red-brown to red-gray-brown, Very fine grained, Slightly Weathered, slightly broken to massive, moderately hard		RQD=75 Rec=100%	>> ▲ Q = 417.3 tsf 167.6 pcf	4 min. 4 min. 4 min. 4 min.
55		[Pattern]				<b>SANDSTONE</b> -Light gray-brown to red-gray-brown to dark brown, Fine to medium grained, Slightly Weathered, very broken to massive, moderately hard to very hard Nearly vertical fracture from 54.4 to 54.8 feet. Weathered/Highly Weathered seam @ 54.8 (~ 2-1/2 inches thick)			>> ▲ Q = 603.0 tsf 161.1 pcf	4 min. 4 min. 4 min. 4 min.
60		[Pattern]	R-7	70				RQD=72 Rec=97%		4 min. 4 min. 4 min.

Continued Next Page






BORING B-2			
Water	▽	While Drilling	Not Enc.
	▼	Post-Core	22.3 feet
	▽		

**BORING LOCATION:**  
See Boring Location Plan

Elevation (feet)	Depth, (feet)	Graphic Log	Sample Type	Sample No.	Recovery (inches)	MATERIAL DESCRIPTION	USCS Classification	SPT Blows per 6-inch (SS) RQD & Recovery % (NX)	Moisture, %	STANDARD PENETRATION TEST DATA N in blows/ft ©  X Moisture    ■ PL + LL  STRENGTH, tsf ▲ Qu       * Qp	Additional Remarks
									0          25          50	0          2.0          4.0	
60						<b>SANDSTONE</b> -Gray-brown to dark gray-brown, Fine grained, Weathered to Slightly Weathered, very broken to massive, very hard to extremely hard					4 min. ▶ 63.7 tsf 164.7 pcf 4 min.
				R-8	76	<b>SILTSTONE</b> -Red-brown to dark red-brown, Very fine grained, Weathered to Slightly Weathered, broken to massive, moderately hard					4 min.
65						<b>SILTSTONE</b> -Dark gray-brown, Very fine grained, Highly Weathered, very broken to broken, moderately hard		RQD=49 Rec=84%			4 min.
						<b>SILTSTONE</b> -Red-brown to red-gray-brown, Very fine grained, Slightly Weathered, broken to massive, moderately hard					4 min.
						<b>SILTSTONE</b> -Red-gray-brown, Very fine grained, Highly Weathered, very broken to slightly broken, moderately hard					4 min. 3 min. 3 min.
70				R-9	78	<b>SILTSTONE</b> -Red-brown to red-gray-brown, Very fine grained, Slightly Weathered, broken to massive, moderately hard		RQD=97 Rec=100%			3 min. ▶ 411.2 tsf 167.7 pcf 3 min.
											3 min.
75											3 min.
											4 min.
											4 min.
						<b>SILTSTONE/SANDSTONE</b> -Red-brown to dark gray-brown, Very fine to fine grained, Weathered, broken to slightly broken, moderately hard to very hard					4 min.
80				R-10	120	<b>SANDSTONE</b> -Gray-brown to dark gray-brown, Fine to medium grained, Weathered to Slightly Weathered, hard to very hard, trace calcite stringers Broken layer @ 80.1 feet (~ 5-1/4 inches thick) Weathered seam @ 82.5 feet (~ 1-1/2 inches thick)		RQD=62 Rec=100%			▶ 836.8 tsf 167.7 pcf 4 min.
											4 min.
											4 min.
85						Broken layer @ 83.3 feet (~ 4-1/2 inches thick)					▶ 106.1 tsf 163.5 pcf 4 min.
				R-11	60	<b>SHALE</b> -Red-brown, Very fine grained, Slightly Weathered, very broken to massive, moderately hard		RQD=88 Rec=100%			4 min.
											4 min.
90											









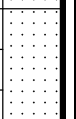




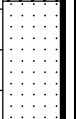


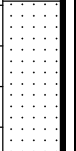


Continued Next Page

BORING B-2			
Water		While Drilling	Not Enc.
		Post-Core	22.3 feet
			

**BORING LOCATION:**  
See Boring Location Plan

[illegible]

<b>DATE STARTED:</b> 9/5/17		<b>DRILL COMPANY:</b> Eichelberger's, Inc.		<b>BORING B-2</b>	
<b>DATE COMPLETED:</b> 9/7/17		<b>DRILLER:</b> T. Growden <b>LOGGED BY:</b> C. Lehman			
<b>COMPLETION DEPTH:</b> 201.0 ft		<b>DRILL RIG:</b> Diedrich D-50		<div style="display: flex; justify-content: space-between;"> <div style="width: 30%;"> <b>Water</b>  <div style="display: flex; align-items: center;"> <div style="width: 10px; height: 10px; border: 1px solid black; margin-right: 5px;"></div> While Drilling </div> <div style="width: 10px; height: 10px; border: 1px solid black; margin-right: 5px;"></div> Post-Core </div> <div style="width: 30%;"> Not Enc. 22.3 feet </div> </div>	
<b>BENCHMARK:</b> N/A		<b>DRILLING METHOD:</b> Casing/Rock Coring			
<b>ELEVATION:</b> N/A		<b>SAMPLING METHOD:</b> 2-in SS1.874-in Core		<b>BORING LOCATION:</b> See Boring Location Plan	
<b>LATITUDE:</b> n/a°		<b>HAMMER TYPE:</b> Automatic			
<b>LONGITUDE:</b> n/a°		<b>EFFICIENCY:</b> N/A			
<b>STATION:</b> N/A		<b>OFFSET:</b> N/A			
<b>REMARKS:</b>		<b>REVIEWED BY:</b> F. Hoffman			




Elevation (feet)	Depth, (feet)	Graphic Log	Sample Type	Sample No.	Recovery (inches)	MATERIAL DESCRIPTION	USCS Classification	SPT Blows per 6-inch (SS) RQD & Recovery % (NX)	Moisture, %	STANDARD PENETRATION TEST DATA N in blows/ft  PL  LL				Additional Remarks
										0                      25                      50				
										STRENGTH, tsf  Qu  Qp				
									0                      2.0                      4.0					
	120		R-15	85		<b>SILTSTONE</b> -Red-brown to dark red-gray-brown, Very fine grained, Highly Weathered, very broken to slightly broken, moderately hard		RQD=53 Rec=71%						4 min. 4 min. 4 min. 3 min.
						<b>SILTSTONE</b> -Red-gray-brown, Very fine grained, Slightly Weathered, broken to massive, moderately hard							>>  Qu = 496.4 tsf 166.0 pcf 4 min.	
	125					<b>SANDSTONE</b> -Gray to red-brown, Fine grained, Slightly Weathered, slightly broken to massive, moderately hard to extremely hard, trace calcite stringers							4 min.	
			R-16	60		<b>Conglomeratic SANDSTONE</b> -Gray to red-gray-brown, Fine to very coarse grained, Slightly Weathered, broken to massive, hard to extremely hard, trace calcite		RQD=50 Rec=100%					4 min. 4 min. 4 min. 4 min.	
	130					<b>Conglomeratic SANDSTONE</b> -Gray-brown to dark red-brown, Fine to coarse grained, Weathered to Slightly Weathered, very broken to massive, moderately hard to very hard, trace pits							4 min. 4 min. 4 min.	
			R-17	120		<b>SANDSTONE</b> -Red-brown to dark brown, Fine to very coarse grained, Slightly Weathered, broken to massive, moderately hard to hard, trace calcite stringers		RQD=75 Rec=100%					>>  Qu = 409.5 tsf 160.4 pcf 4 min.	
	135					<b>SILTSTONE</b> -Brown to red-brown, Very fine grained, Slightly Weathered, slightly broken to massive, moderately hard							4 min. 4 min.	
			R-18	120		Broken/very broken layer @ 144 feet (~ 10-1/2 inches thick) <b>SANDSTONE</b> -Light gray-brown to dark red-brown, Fine to medium grained, Slightly Weathered, broken to massive, moderately hard to very hard, trace calcite stringers		RQD=78 Rec=100%					>>  Qu = 789.7 tsf 160.4 pcf 4 min.	
	140												4 min. 4 min.	
													>>  Qu = 380.6 tsf 165.6 pcf 4 min.	
	145												4 min. 4 min. 4 min. 4 min.	
	150					Broken layer @ 149.5 feet (~ 6-1/2 inches								

Continued Next Page

Qu

Qp

	Professional Service Industries, Inc. 1707 S. Cameron Street, Suite B Harrisburg, PA 17104 Telephone: (717) 230-8622		<b>PROJECT NO.:</b> 04911456 <b>PROJECT:</b> Energy Transfer HDD (DPS) <b>LOCATION:</b> Wetland "J47" (PPP5) Dauphin Co., PA
			PA-LE-0001.0000-SR/PO#201770816-2




BORING B-2			
Water		While Drilling	Not Enc.
		Post-Core	22.3 feet
			

**BORING LOCATION:**  
See Boring Location Plan

Elevation (feet)	Depth, (feet)	Graphic Log	Sample Type	Sample No.	Recovery (inches)	MATERIAL DESCRIPTION	USCS Classification	SPT Blows per 6-inch (SS) RQD & Recovery % (NX)	Moisture, %  STRENGTH, tsf ▲ Qu * Qp	Additional Remarks
									TEST DATA N in blows/ft © X Moisture □ PL 0 25 50 + LL 0 2.0 4.0	
150						thick) <b>SANDSTONE</b> -Light gray-brown to dark red-brown, Fine to medium grained, Slightly Weathered, broken to massive, moderately hard to very hard, trace calcite stringers				4 min. 4 min. >>> ▲ Q <sub>u</sub> = 383.3 tsf 163.9 pcf
			R-19	115		<b>SHALE</b> -Red-brown to dark red-brown, Very fine grained, Weathered to Slightly Weathered, very broken to massive, moderately hard		RQD=59 Rec=96%		4 min. 4 min. 4 min. 4 min. 4 min. 4 min. 4 min.
						Weathered/Highly Weathered seam @ 157.1 feet (~ 2-3/4 inches thick) Highly Weathered layer @ 158.3 feet (~ 5 inches thick)				4 min. 4 min. 4 min. 4 min. 4 min.
			R-20	58		<b>SHALE</b> -Dark red-brown to dark red-gray-brown, Very fine grained, Slightly Weathered, very broken to massive, moderately hard Weathered layer @ 160 feet (~ 4-1/2 inches thick)		RQD=60 Rec=96%		4 min. 4 min. 4 min. 4 min. 4 min.
										4 min. 4 min. >>> ▲ Q <sub>u</sub> = 410.3 tsf 165.6 pcf
										4 min. 4 min. >>> ▲ Q <sub>u</sub> = 284.8 tsf 168.5 pcf
			R-21	120		Weathered/Highly Weathered layer @ 168.4 feet (~ 11 inches thick)		RQD=54 Rec=100%		4 min. 4 min. 4 min. 4 min.
						<b>SANDSTONE</b> -Light gray-brown to dark red-brown, Fine grained, Slightly Weathered, very broken to massive, hard to very hard				4 min. 4 min. >>> ▲ Q <sub>u</sub> = 846.0 tsf 171.0 pcf
						Broken/very broken layer @ 174.7 feet (~ 4 inches thick)				4 min. 4 min. 4 min. 4 min.
			R-22	60		Broken/very broken layer @ 178.1 feet (~ 8 inches thick)		RQD=42 Rec=100%		4 min. 4 min. 4 min. 4 min.
180										

Continued Next Page



<b>Water</b>		While Drilling	Not Enc.
		Post-Core	22.3 feet
			

**BORING LOCATION:**  
See Boring Location Plan

STANDARD PENETRATION TEST DATA				Additional Remarks
N in blows/ft. ©				
✕ Moisture	☐ PL			
0	25	+	LL	
0			50	
STRENGTH, tsf				
▲ Qu	✱			
0	2.0	4.0		

Professional Service Industries, Inc.  
1707 S. Cameron Street, Suite B  
Harrisburg, PA 17104  
Telephone: (717) 230-8622

PA-LE-0001.0000-SR/PO#201770816-2

0491-1456  
PPDS

Wetland J47

B-2

9/5/17

Box 1 of 1

Run	Depth	Rec	Rqd
R-1	94-130	2.0	0.0
R-2	13.0-20.0	6.3	1.9
R-3	20.0-30.0	9.2	5.4

TOP





0491-1456  
PPP5  
Wetland J47  
B-2  
9/5/17  
Box 2 of -

Rain	Depth	Rer.	ROD
R-3 (cont)	20.0-30.0	9.2	5.4
R-4	30.0-38.0	8.0	3.9
R-5	38.0-45.0	25	6.2

TCP



0491-1456  
 PPPS  
 Wetland J47  
 B-2  
 Box 3 of -  
 915117

Run	Depth	Rc.	RQD
R-5(cont)	38.0-45.0	75	6.2
R-6	45.0-55.0	100	75



TOP



550





0491-1456  
PPPS  
Wetland J47  
B-2  
Box 1 of 1  
9/6/17

Run	Depth	Rec.	RSD
R-7	55.0-61.0	5.8	4.3
R-8	61.0-68.5	6.3	3.7
R-9	68.5-75.0	6.5	6.3

TOP

SSD

61.0

55.0





0491-1456  
PPPS  
Wetland 547  
B-2  
Box 5 of —  
9/6/17

Run	Depth	Per	RM
R-10	750-850	10.0	6.2
\$			

T4P



D491-1456  
PPP5  
Wetland J47  
B-2  
Box 6 of  
916/17

Run	Depth	Re.	ROD
R-11	85.0-90.0	50	4.4
R-12	90.0-100.0	10.0	9.5

Top

90.0

100.0



0491-1456  
PPDS  
Wetland J47  
B-2  
Box 7 of \_  
9/6/17

Run	Depth	Rec.	Run
R-13	100.0 - 105.0	5.0	2.7
R-14	105.0 - 115.0	10.0	5.5

Top

100.0

105.0

115.0





0191-1456

PPPS

Wetland J47

B-2

Box 8 of

9/6/17

Run	Depth	Re.	Rod
R-15	115.0-125.0	7.1	5.3
R-16	125.0-130.0	5.0	2.5
R-17	130.0-140.0	10.0	7.5

TOP

130.0

135.0

0491-1456

PPF5

Wetland J47

B-2

Box 9 of 10

9/7/17

Run	Depth	Rec	ROD
R-7A (cont)	130.0-140.0	8.0	7.5
R-18	140.0-150.0	10.0	7.8

Top

140.0

140.0





D491-1456  
PPPS  
We Hard J47  
B-2  
Box 10 of -  
9/87/17

Run	Depth	R <sub>h</sub>	RQD
R-18(cont)	140.0-150.0	10.0	7.8
R-19	150.0-160.0	9.6	5.9
R-20	160.0-165.0	4.8	3.0

Top





0491-1456  
PPP5  
Wetland J47  
B-2  
Box 11 of  
9/7/17

Run	Depth	Rc	RSD
R-20 (cont)	160.0 - 165.0	4.8	3.0
R-21	165.0 - 175.0	10.0	5.4
R-22	175.0 - 180.0	5.0	2.1

Top



0491-1456

PPP5

Wetland J47

B-2

Box 12 of -

9/2/17

Run	Depth	Res.	R90
R-22 (cont)	175.0-180.0	5.0	2.1
R-23	180.0-190.0	9.8	6.9
R-24	190.0-195.0	5.0	5.0

190.0

180.0



0491-1456  
PPPS  
Wetland J47  
B-2  
Box 13 of 13  
9/7/17

Rim	Depth	Rec.	RSD
R-24 (cm)	190.0-195.0	5.0	5.0
R-25	195.0-200.0	5.0	9.3
	EOB		

TOP

195.0

200.0

210.0





## GENERAL NOTES

### SAMPLE IDENTIFICATION

The Unified Soil Classification System (USCS), AASHTO 1988 and ASTM designations D2487 and D-2488 are used to identify the encountered materials unless otherwise noted. Coarse-grained soils are defined as having more than 50% of their dry weight retained on a #200 sieve (0.075mm); they are described as: boulders, cobbles, gravel or sand. Fine-grained soils have less than 50% of their dry weight retained on a #200 sieve; they are defined as silts or clay depending on their Atterberg Limit attributes. Major constituents may be added as modifiers and minor constituents may be added according to the relative proportions based on grain size.

### DRILLING AND SAMPLING SYMBOLS

SFA: Solid Flight Auger - typically 4" diameter flights, except where noted.	☒ SS: Split-Spoon - 1 3/8" I.D., 2" O.D., except where noted.
HSA: Hollow Stem Auger - typically 3 1/4" or 4 1/4" I.D. openings, except where noted.	■ ST: Shelby Tube - 3" O.D., except where noted.
M.R.: Mud Rotary - Uses a rotary head with Bentonite or Polymer Slurry	▮ RC: Rock Core
R.C.: Diamond Bit Core Sampler	↓ TC: Texas Cone
H.A.: Hand Auger	☞ BS: Bulk Sample
P.A.: Power Auger - Handheld motorized auger	☒ PM: Pressuremeter
	CPT-U: Cone Penetrometer Testing with Pore-Pressure Readings

### SOIL PROPERTY SYMBOLS

N: Standard "N" penetration: Blows per foot of a 140 pound hammer falling 30 inches on a 2-inch O.D. Split-Spoon.
N <sub>60</sub> : A "N" penetration value corrected to an equivalent 60% hammer energy transfer efficiency (ETR)
Q <sub>u</sub> : Unconfined compressive strength, TSF
Q <sub>p</sub> : Pocket penetrometer value, unconfined compressive strength, TSF
w%: Moisture/water content, %
LL: Liquid Limit, %
PL: Plastic Limit, %
PI: Plasticity Index = (LL-PL), %
DD: Dry unit weight, pcf
▼, ▽, ▾ Apparent groundwater level at time noted

### RELATIVE DENSITY OF COARSE-GRAINED SOILS    ANGULARITY OF COARSE-GRAINED PARTICLES

Relative Density	N - Blows/foot
Very Loose	0 - 4
Loose	4 - 10
Medium Dense	10 - 30
Dense	30 - 50
Very Dense	50 - 80
Extremely Dense	80+

Description	Criteria
Angular:	Particles have sharp edges and relatively plane sides with unpolished surfaces
Subangular:	Particles are similar to angular description, but have rounded edges
Subrounded:	Particles have nearly plane sides, but have well-rounded corners and edges
Rounded:	Particles have smoothly curved sides and no edges

### GRAIN-SIZE TERMINOLOGY

Component	Size Range
Boulders:	Over 300 mm (>12 in.)
Cobbles:	75 mm to 300 mm (3 in. to 12 in.)
Coarse-Grained Gravel:	19 mm to 75 mm (¾ in. to 3 in.)
Fine-Grained Gravel:	4.75 mm to 19 mm (No.4 to ¾ in.)
Coarse-Grained Sand:	2 mm to 4.75 mm (No.10 to No.4)
Medium-Grained Sand:	0.42 mm to 2 mm (No.40 to No.10)
Fine-Grained Sand:	0.075 mm to 0.42 mm (No. 200 to No.40)
Silt:	0.005 mm to 0.075 mm
Clay:	<0.005 mm

### PARTICLE SHAPE

Description	Criteria
Flat:	Particles with width/thickness ratio > 3
Elongated:	Particles with length/width ratio > 3
Flat & Elongated:	Particles meet criteria for both flat and elongated

### RELATIVE PROPORTIONS OF FINES

Descriptive Term	% Dry Weight
Trace:	< 5%
With:	5% to 12%
Modifier:	>12%

## GENERAL NOTES

(Continued)

### CONSISTENCY OF FINE-GRAINED SOILS

<u>Q<sub>u</sub> - TSF</u>	<u>N - Blows/foot</u>	<u>Consistency</u>
0 - 0.25	0 - 2	Very Soft
0.25 - 0.50	2 - 4	Soft
0.50 - 1.00	4 - 8	Firm (Medium Stiff)
1.00 - 2.00	8 - 15	Stiff
2.00 - 4.00	15 - 30	Very Stiff
4.00 - 8.00	30 - 50	Hard
8.00+	50+	Very Hard

### MOISTURE CONDITION DESCRIPTION

<u>Description</u>	<u>Criteria</u>
Dry:	Absence of moisture, dusty, dry to the touch
Moist:	Damp but no visible water
Wet:	Visible free water, usually soil is below water table

### RELATIVE PROPORTIONS OF SAND AND GRAVEL

<u>Descriptive Term</u>	<u>% Dry Weight</u>
Trace:	< 15%
With:	15% to 30%
Modifier:	>30%

### STRUCTURE DESCRIPTION

<u>Description</u>	<u>Criteria</u>	<u>Description</u>	<u>Criteria</u>
Stratified:	Alternating layers of varying material or color with layers at least ¼-inch (6 mm) thick	Blocky:	Cohesive soil that can be broken down into small angular lumps which resist further breakdown
Laminated:	Alternating layers of varying material or color with layers less than ¼-inch (6 mm) thick	Lensed:	Inclusion of small pockets of different soils
Fissured:	Breaks along definite planes of fracture with little resistance to fracturing	Layer:	Inclusion greater than 3 inches thick (75 mm)
Slickensided:	Fracture planes appear polished or glossy, sometimes striated	Seam:	Inclusion 1/8-inch to 3 inches (3 to 75 mm) thick extending through the sample
		Parting:	Inclusion less than 1/8-inch (3 mm) thick

### SCALE OF RELATIVE ROCK HARDNESS

<u>Q<sub>u</sub> - TSF</u>	<u>Consistency</u>
2.5 - 10	Extremely Soft
10 - 50	Very Soft
50 - 250	Soft
250 - 525	Medium Hard
525 - 1,050	Moderately Hard
1,050 - 2,600	Hard
>2,600	Very Hard

### ROCK BEDDING THICKNESSES

<u>Description</u>	<u>Criteria</u>
Very Thick Bedded	Greater than 3-foot (>1.0 m)
Thick Bedded	1-foot to 3-foot (0.3 m to 1.0 m)
Medium Bedded	4-inch to 1-foot (0.1 m to 0.3 m)
Thin Bedded	1¼-inch to 4-inch (30 mm to 100 mm)
Very Thin Bedded	½-inch to 1¼-inch (10 mm to 30 mm)
Thickly Laminated	1/8-inch to ½-inch (3 mm to 10 mm)
Thinly Laminated	1/8-inch or less "paper thin" (<3 mm)

### ROCK VOIDS

<u>Voids</u>	<u>Void Diameter</u>
Pit	<6 mm (<0.25 in)
Vug	6 mm to 50 mm (0.25 in to 2 in)
Cavity	50 mm to 600 mm (2 in to 24 in)
Cave	>600 mm (>24 in)

### GRAIN-SIZED TERMINOLOGY

(Typically Sedimentary Rock)	
<u>Component</u>	<u>Size Range</u>
Very Coarse Grained	>4.76 mm
Coarse Grained	2.0 mm - 4.76 mm
Medium Grained	0.42 mm - 2.0 mm
Fine Grained	0.075 mm - 0.42 mm
Very Fine Grained	<0.075 mm

### ROCK QUALITY DESCRIPTION

<u>Rock Mass Description</u>	<u>RQD Value</u>
Excellent	90 -100
Good	75 - 90
Fair	50 - 75
Poor	25 -50
Very Poor	Less than 25

### DEGREE OF WEATHERING

Slightly Weathered:	Rock generally fresh, joints stained and discoloration extends into rock up to 25 mm (1 in), open joints may contain clay, core rings under hammer impact.
Weathered:	Rock mass is decomposed 50% or less, significant portions of the rock show discoloration and weathering effects, cores cannot be broken by hand or scraped by knife.
Highly Weathered:	Rock mass is more than 50% decomposed, complete discoloration of rock fabric, core may be extremely broken and gives clunk sound when struck by hammer, may be shaved with a knife.

#### Degree of Brokenness

<u>Characteristic</u>	<u>Description</u>
Less than 1 inch	Very Broken
1 inch to 3 inches	Broken
3 inches to 6 inches	Slightly Broken
Greater than 6 inches	Massive



# SOIL CLASSIFICATION CHART

NOTE: DUAL SYMBOLS ARE USED TO INDICATE BORDERLINE SOIL CLASSIFICATIONS

MAJOR DIVISIONS			SYMBOLS		TYPICAL DESCRIPTIONS
			GRAPH	LETTER	
COARSE GRAINED SOILS	GRAVEL AND GRAVELLY SOILS	CLEAN GRAVELS		GW	WELL-GRADED GRAVELS, GRAVEL - SAND MIXTURES, LITTLE OR NO FINES
		(LITTLE OR NO FINES)		GP	POORLY-GRADED GRAVELS, GRAVEL - SAND MIXTURES, LITTLE OR NO FINES
		GRAVELS WITH FINES		GM	SILTY GRAVELS, GRAVEL - SAND - SILT MIXTURES
		(APPRECIABLE AMOUNT OF FINES)		GC	CLAYEY GRAVELS, GRAVEL - SAND - CLAY MIXTURES
	SAND AND SANDY SOILS	CLEAN SANDS		SW	WELL-GRADED SANDS, GRAVELLY SANDS, LITTLE OR NO FINES
		(LITTLE OR NO FINES)		SP	POORLY-GRADED SANDS, GRAVELLY SAND, LITTLE OR NO FINES
		SANDS WITH FINES		SM	SILTY SANDS, SAND - SILT MIXTURES
		(APPRECIABLE AMOUNT OF FINES)		SC	CLAYEY SANDS, SAND - CLAY MIXTURES
FINE GRAINED SOILS	SILTS AND CLAYS	LIQUID LIMIT LESS THAN 50		ML	INORGANIC SILTS AND VERY FINE SANDS, ROCK FLOUR, SILTY OR CLAYEY FINE SANDS OR CLAYEY SILTS WITH SLIGHT PLASTICITY
				CL	INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS
				OL	ORGANIC SILTS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY
	SILTS AND CLAYS	LIQUID LIMIT GREATER THAN 50		MH	INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS FINE SAND OR SILTY SOILS
				CH	INORGANIC CLAYS OF HIGH PLASTICITY
				OH	ORGANIC CLAYS OF MEDIUM TO HIGH PLASTICITY, ORGANIC SILTS
			HIGHLY ORGANIC SOILS		

**Table 4-3** Hardness and unconfined compressive strength of rock materials

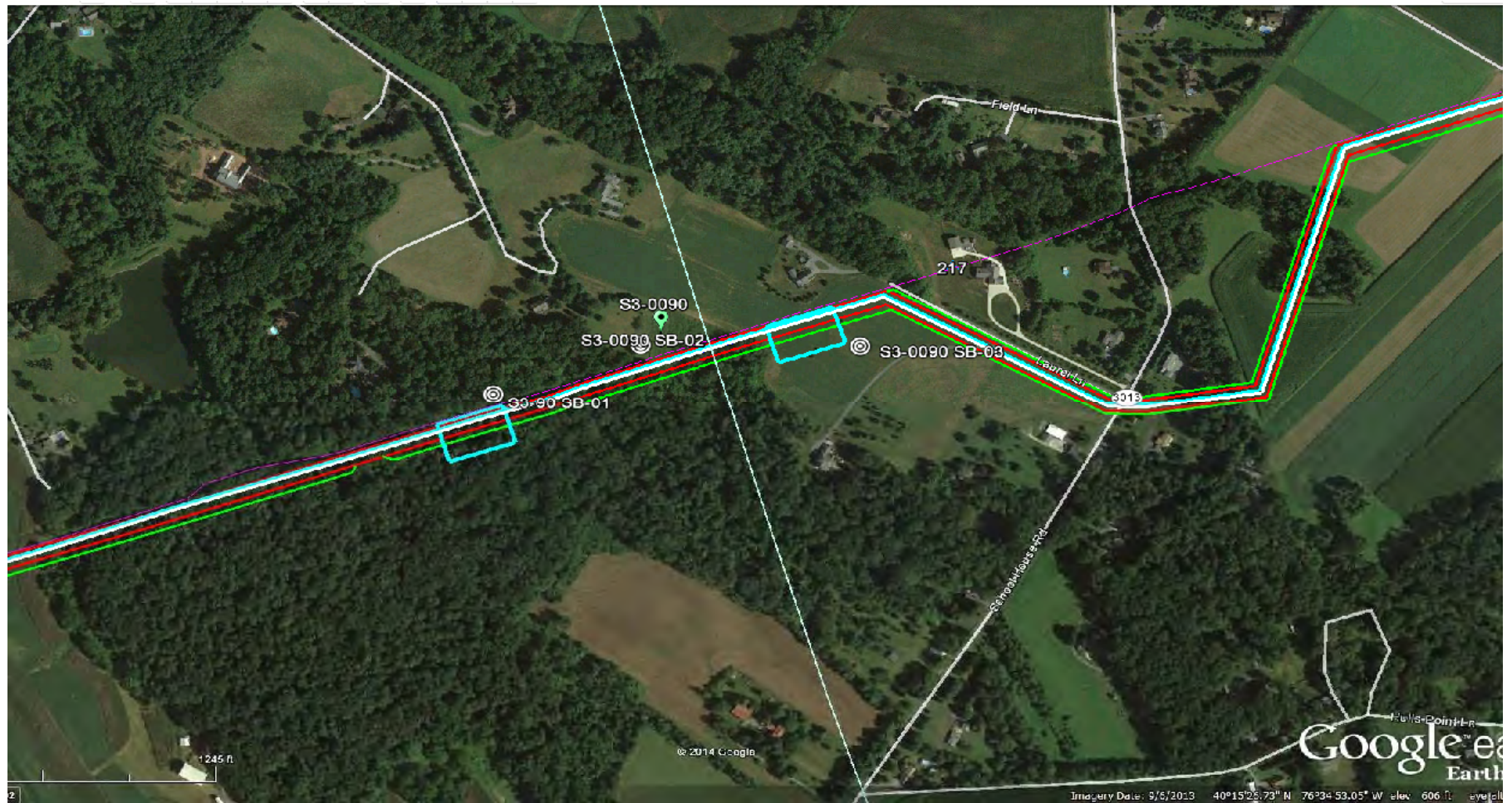
Hardness category	Typical range in unconfined compressive strength (MPa)	Strength value selected (MPa)	Field test on sample	Field test on outcrop
Soil*	< 0.60		Use USCS classifications	
Very soft rock or hard, soil-like material	0.60–1.25		Scratched with fingernail. Slight indentation by light blow of point of geologic pick. Requires power tools for excavation. Peels with pocket knife.	
Soft rock	1.25–5.0		Permits denting by moderate pressure of the fingers. Handheld specimen crumbles under firm blows with point of geologic pick.	Easily deformable with finger pressure.
Moderately soft rock	5.0–12.5		Shallow indentations (1–3 mm) by firm blows with point of geologic pick. Peels with difficulty with pocket knife. Resists denting by the fingers, but can be abraded and pierced to a shallow depth by a pencil point. Crumbles by rubbing with fingers.	Crumbles by rubbing with fingers.
Moderately hard rock	12.5–50		Cannot be scraped or peeled with pocket knife. Intact handheld specimen breaks with single blow of geologic hammer. Can be distinctly scratched with 20d common steel nail. Resists a pencil point, but can be scratched and cut with a knife blade.	Unfractured outcrop crumbles under light hammer blows.
Hard rock	50–100		Handheld specimen requires more than one hammer blow to break it. Can be faintly scratched with 20d common steel nail. Resistant to abrasion or cutting by a knife blade, but can be easily dented or broken by light blows of a hammer.	Outcrop withstands a few firm blows before breaking.
Very hard rock	100–250		Specimen breaks only by repeated, heavy blows with geologic hammer. Cannot be scratched with 20d common steel nail.	Outcrop withstands a few heavy ringing hammer blows but will yield large fragments.
Extremely hard rock	> 250		Specimen can only be chipped, not broken by repeated, heavy blows of geologic hammer.	Outcrop resists heavy ringing hammer blows and yields, with difficulty, only dust and small fragments.

Method used to determine consistency or hardness (check one):

Field assessment: \_\_\_\_\_ Uniaxial lab test: \_\_\_\_\_ Other: \_\_\_\_\_ Rebound hammer (ASTM D5873): \_\_\_\_\_

\* See NEH631.03 for consistency and density of soil materials. For very stiff soil, SPT N values = 15 to 30. For very soft rock or hard, soil-like material, SPT N values exceed 30 blows per foot.





**LEGEND:**

- ⊙ Geotechnical Soil Boring (SB) Locations

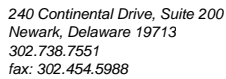


**TETRA TECH**

**GEOTECHNICAL BORING LOCATIONS**

HDD S3-0090

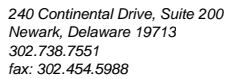
LEBANON COUNTY, SOUTH LONDONDERRY TOWNSHIP &  
DAUGHIN COUNTY, CONEWAGO TOWNSHIP, PA  
SUNOCO PENNSYLVANIA PIPELINE PROJECT



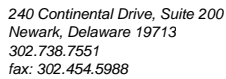
Project Name:	SUNOCO PENNSYLVANIA PIPELINE PROJECT			Project No.: 103IP3406
Project Location:	95 LAUREL LANE, PALMYRA, PA			Page 1 of 1
HDD No.:	S3-0090	Dates(s) Drilled: 11-18-14	Inspector:	E. WATT
Boring No.:	SB-01	Drilling Method: SPT - ASTM D1586	Driller:	S. HOFFER
Drilling Contractor:	HAD DRILLING	Groundwater Depth (ft): NOT ENCOUNTERED	Total Depth (ft):	21.5
Boring Location Coordinates:	40° 15' 11.995" N		76° 35' 40.296" W	

Notes/Comments:	
<u>Pocket Pentrometer Testing</u>	DR: DECOMPOSED ROCK
<p>Strata (USCS) Designations are approximated based on visual review, except where indicated in Description of Materials.</p> <p>* Number of blows of 140 lb. Hammer dropped 30 in. required to drive 2 in. split-spoon sampler in 6 in. increments.  N: Number of blows to drive spoon from 6" to 18" interval.</p>	





N: Number of blows to drive spoon from 6" to 18" interval.



N: Number of blows to drive spoon from 6" to 18" interval.



**GEOTECHNICAL LABORATORY TESTING SUMMARY**  
**SUNOCO PENNSYLVANIA PIPELINE PROJECT**  
**HDD S3-0090**

HDD No.	Test Boring No.	Sample No.	Depth of Sample (ft.)		Water Content, % (ASTM D2216)	Percent Silts/Clays, % (ASTM D1140)	Atterburg Limits (ASTM D4318)			USCS Classif. (ASTM D2487)
			From	To			Liquid Limit, %	Plastic Limit, %	Plasticity Index, %	
S3-0090	SB-01	1	3.0	5.0	6.4	41.2	-	-	-	-
		2	8.0	8.7	3.6	39.2	-	-	-	-
		4	18.0	19.2	5.7	39.8	-	-	-	-
		5	20.0	20.3	6.3	41.9	-	-	-	-
	SB-02	1	3.0	5.0	9.2	21.9	-	-	-	-
		2	8.0	10.0	10.4	80.8	30	19	11	CL
		3	13.0	15.0	12.5	75.1	-	-	-	-
		4	18.0	20.0	14.2	16.3	-	-	-	-
		5	23.0	24.4	10.5	90.7	-	-	-	-
		6	28.0	28.5	5.7	21.4	-	-	-	-
	SB-03	1	3.0	5.0	14.2	99.2	32	19	13	CL
		2	8.0	10.0	9.2	21.1	-	-	-	-
		4	18.0	20.0	13.7	38.8	-	-	-	-
		5	23.0	24.4	9.6	75.3	-	-	-	-

Notes:

- 1) Sample depths based on feet below grade at time of exploration.

**REGIONAL GEOLOGY SUMMARY**  
**SUNOCO PENNSYLVANIA PIPELINE PROJECT**  
**HDD S3-0090**

HDD No.	NAME	BORING NO.	REGIONAL GEOLOGY DESCRIPTION	GENERAL TOPOGRAPHIC SETTING	BEDROCK FORMATION	GENERAL ROCK TYPE	APPROX MAX FM THICKNESS (FT)	DEPTH TO ROCK (Ft bgs) based on nearby well drilling logs	NOTES / COMMENTS
S3-0090	Wetland J47	SB-01	<b>Gettysburg Fm</b> - reddish-brown to maroon silty mudstone and shale and soft, red-brown, medium- to fine-grained sandstone, with minor amounts of yellowish-brown shale and sandstone and thin beds of impure limestone.	Gently sloping lowland to forested wetlands	Gettysburg Fm	Silty mudstone-shale-sandstone w/ some impure limestone		12-22	
		SB-02							
		SB-03							

Note : Source of well log data - <http://www.dcnr.state.pa.us/topogeo/groundwater/pagwis/records/index.htm>. All other sources as referenced in comments section.

# FIELD DESCRIPTION AND LOGGING SYSTEM FOR SOIL EXPLORATION

## GRANULAR SOILS

(Sand, Gravel & Combinations)

<u>Density</u>	<u>N (blows)*</u>
Very Loose	5 or less
Loose	6 to 10
Medium Dense	11 to 30
Dense	31 to 50
Very Dense	51 or more

### Relative Proportions

<u>Description Term</u>	<u>Percent</u>
Trace	1 - 10
Little	11 - 20
Some	21 - 35
And	36 - 50

### Particle Size Identification

Boulders	8 in. diameter or more
Cobbles	3 to 8 in. diameter
Gravel	Coarse (C) 3 in. to ¾ in. sieve Fine (F) ¾ in. to No. 4 sieve
Sand	Coarse (C) No. 4 to No. 10 sieve (4.75mm-2.00mm) Medium (M) No. 10 to No. 40 sieve (2.00mm – 0.425mm) Fine (F) No. 40 to No. 200 sieve (0.425 – 0.074mm)
Silt/Clay	Less Than a No. 200 sieve (<0.074mm)

## COHESIVE SOILS

(Silt, Clay & Combinations)

<u>Consistency</u>	<u>N (blows)*</u>
Very Soft	3 or less
Soft	4 to 5
Medium Stiff	6 to 10
Stiff	11 to 15
Very Stiff	16 to 30
Hard	31 or more

### Plasticity

<u>Degree of Plasticity</u>	<u>Plasticity Index</u>
None to Slight	0 - 4
Slight	5 - 7
Medium	8- 22
High to Very High	> 22

## ROCK

(Rock Cores)

<u>Rock Quality Designation (RQD), %</u>	<u>Rock Quality Description</u>
0-25	Very Poor
25-50	Poor
50-75	Fair
75-90	Good
90-100	Excellent

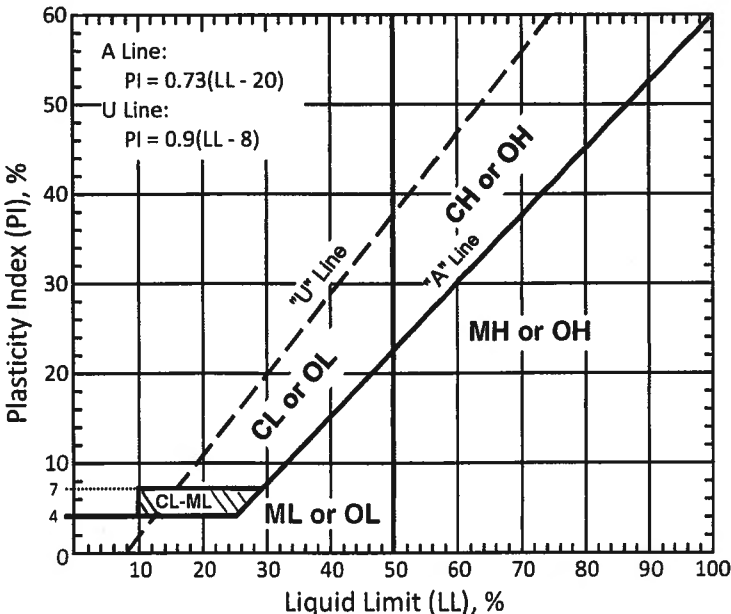
**\*N - Standard Penetration Resistance.** Driving a 2.0" O.D., 1-3/8" I.D. sampler a distance of 18 inches into undisturbed soil with a 140 pound hammer free falling a distance of 30.0 inches. The number of hammer blows to drive the sampler through each 6 inch interval is recorded; the number of blows required to drive the sampler through the final 12 inch interval is termed the Standard Penetration Resistance (SPR) N-value. For example, blow counts of 6/8/9 (through three 6-inch intervals) results in an SPR N-value of 17 (8+9).

**Groundwater** observations were made at the times indicated. Groundwater elevations fluctuate throughout a given year, depending on actual field porosity and variations in seasonal and annual precipitation.



# UNIFIED SOIL CLASSIFICATION SYSTEM [Casagrande (1948)]

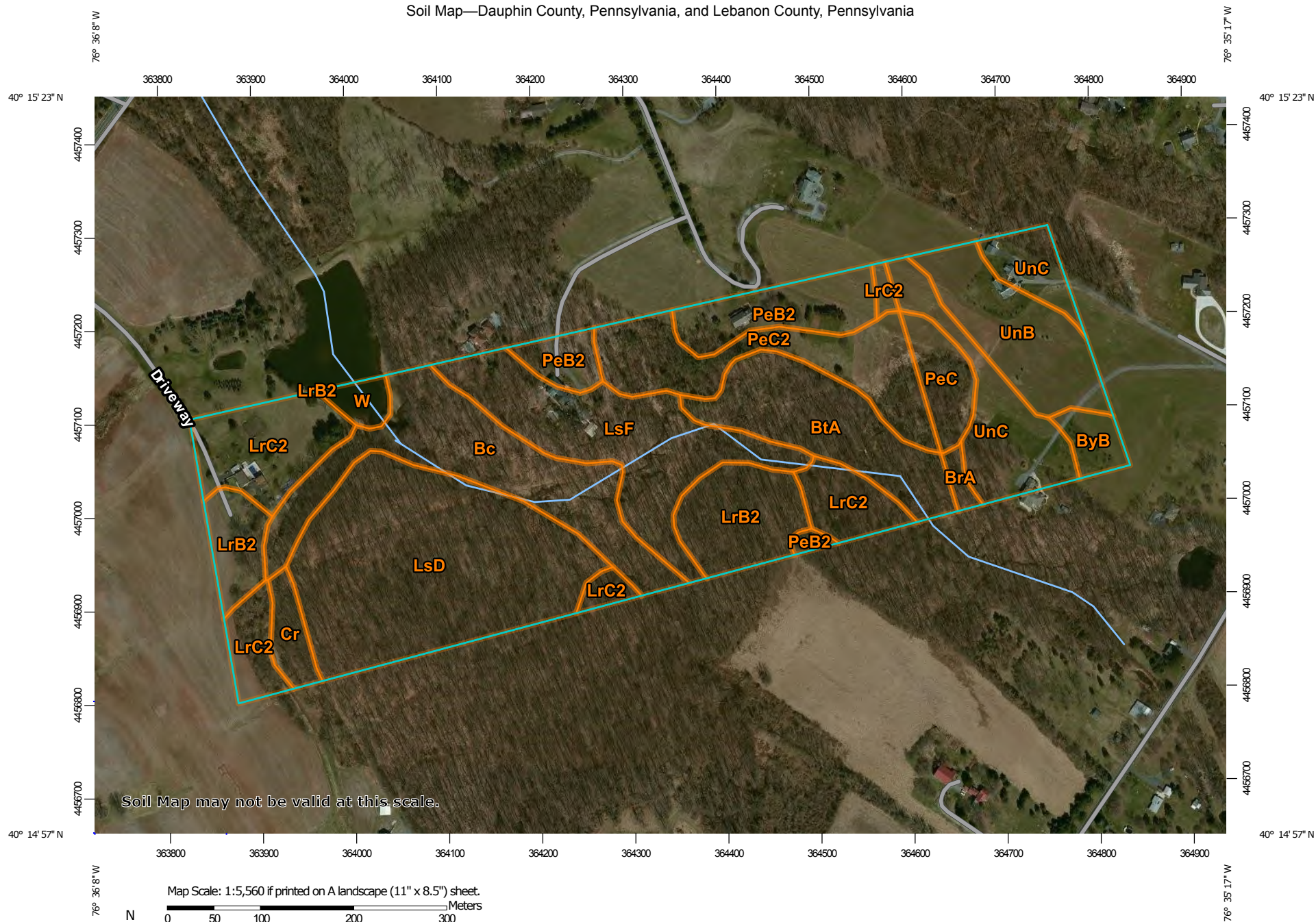
Major Divisions			Group Symbols	Typical Descriptions	Laboratory Classifications			
Coarse Grained Soils (More than half of material is larger than No. 200 sieve)	Gravels  More than half of coarse fraction is larger than No. 4 sieve size	Clean gravel (Little or no fines)	GW	Well-graded gravels, gravel-sand mixtures, little or no fines	Determine Percentage of sand and gravel from grain size curve. Depending on Percentage of fines (fraction smaller than No. 200 sieve), coarse-grained soils are classified as follows:  Less than 5 percent GW, GP, SW, SP More than 12 percent GM, GC, SM, SC 5 to 12 percent Borderline cases requiring dual symbols <sup>(1)</sup>	$C_u = \frac{D_{60}}{D_{10}}$ greater than 4: $C_c = \frac{(D_{30})^2}{D_{10} \times D_{60}}$ between 1 and 3		
			GP	Poorly graded gravels, gravel-sand mixtures, little or no fines		Not meeting $C_u$ or $C_c$ requirements for GW		
		Gravel with fines (Appreciable amount of fines)	GM	Silty gravels, gravel-sand-silt mixtures		Atterberg limits below A Line or $I_p$ less than 4	Limits plotting in hatched zone with $I_p$ between 4 and 7 are borderline cases requiring use of dual symbols	
			GC	Clayey gravels, gravel-sand-clay mixtures		Atterberg limits above A line with $I_p$ greater than 7		
	Sands  More than half of coarse fraction is smaller than No. 4 Sieve)	Clean sands (Little or no fines)	SW	Well graded sands, gravelly sands, little or no fines		$C_u = \frac{D_{60}}{D_{10}}$ greater than 6: $C_c = \frac{(D_{30})^2}{D_{10} \times D_{60}}$ between 1 and 3		
			SP	Poorly graded sands, gravelly sands, little or no fines		Not meeting $C_u$ or $C_c$ requirements for SW		
		Sands with fines (Appreciable amount of fines)	SM	Silty sands, sand-silt mixtures		Atterberg limits below A Line or $I_p$ less than 4	Limits Plotting in hatched zone with $I_p$ between 4 and 7 are borderline cases requiring use of dual symbols	
			SC	Clayey sands, sand-clay mixtures		Atterberg limits above A line with $I_p$ greater than 7		

Major Divisions		Group Symbols	Typical Descriptions	<div>For soils plotting nearly on A line use dual symbols i.e., <math>I_p = 29.5</math>, <math>w_L = 60</math> gives CH-MH. When <math>w_L</math> is near 50 use CL-CH or ML-MH. Take near as <math>\pm 2</math> percent.</div> <div></div>
Fine-grained soils (More than half of material is smaller than No. 200 sieve)	Sils and clays (Liquid limit less than 50)	ML	Inorganic silts and very fine sands, rock flour, silty or clayey fine sands, or clayey silts with slight plasticity	
		CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays	
		OL	Organic silts and organic silty clays of low plasticity	
	Sils and Clays (Liquid limit greater than 50)	MH	Inorganic silts, micaceous or diatomaceous fine sandy or silty soils, elastic silts	
		CH	Inorganic clays of high plasticity, fat clays	
		OH	Organic clays of medium to high plasticity, organic silts	
	Highly organic soils	Pt	Peat and other highly organic soils	

(1) Borderline classifications, used for soils possessing characteristics of two groups, are designated by combinations of group symbols. For example: GW-GC. well-graded gravel-sand mixture with clay binder.

**ATTACHMENT 2**  
**SOIL RESOURCES MAP AND PROFILE DESCRIPTIONS**

# Soil Map—Dauphin County, Pennsylvania, and Lebanon County, Pennsylvania



Soil Map may not be valid at this scale.



**Natural Resources  
Conservation Service**

Web Soil Survey  
National Cooperative Soil Survey

9/21/2017  
Page 1 of 4





## MAP LEGEND

### Area of Interest (AOI)

 Area of Interest (AOI)




















### Soils







 Soil Map Unit Polygons

 Soil Map Unit Lines


 Soil Map Unit Points

### Special Point Features






 Blowout  
 Borrow Pit  
 Clay Spot  
 Closed Depression  
 Gravel Pit  
 Gravelly Spot  
 Landfill  
 Lava Flow  
 Marsh or swamp  
 Mine or Quarry  
 Miscellaneous Water  
 Perennial Water  
 Rock Outcrop  
 Saline Spot  
 Sandy Spot  
 Severely Eroded Spot  
 Sinkhole  
 Slide or Slip  
 Sodic Spot

 Spoil Area  
 Stony Spot  
 Very Stony Spot  
 Wet Spot  
 Other  
 Special Line Features


### Water Features

 Streams and Canals

### Transportation

 Rails  
 Interstate Highways  
 US Routes  
 Major Roads  
 Local Roads

### Background

 Aerial Photography

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at scales ranging from 1:15,800 to 1:20,000.

**Warning:** Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
 Web Soil Survey URL:  
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Dauphin County, Pennsylvania  
 Survey Area Data: Version 10, Sep 19, 2016

Soil Survey Area: Lebanon County, Pennsylvania  
 Survey Area Data: Version 11, Sep 19, 2016

Your area of interest (AOI) includes more than one soil survey area. These survey areas may have been mapped at different scales, with a different land use in mind, at different times, or at different levels of detail. This may result in map unit symbols, soil properties, and interpretations that do not completely agree across soil survey area boundaries.

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Mar 29, 2011—Apr 14, 2011

## MAP LEGEND

## MAP INFORMATION

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Map Unit Legend

Dauphin County, Pennsylvania (PA043)			
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
Bc	Basher silt loam	7.5	10.9%
BtA	Brinkerton and Armagh silt loams, 0 to 3 percent slopes	5.4	7.7%
Cr	Croton silt loam, occasionally ponded, 0 to 3 percent slopes	1.1	1.5%
LrB2	Lewisberry gravelly sandy loam, 3 to 8 percent slopes, moderately eroded	4.9	7.1%
LrC2	Lewisberry gravelly sandy loam, 8 to 15 percent slopes, moderately eroded	7.3	10.5%
LsD	Lewisberry very stony sandy loam, 5 to 25 percent slopes	13.2	18.9%
LsF	Lewisberry very stony sandy loam, 25 to 60 percent slopes	7.4	10.7%
PeB2	Penn channery silt loam, 3 to 8 percent slopes	4.1	5.9%
PeC2	Penn channery silt loam, 8 to 15 percent slopes	5.4	7.7%
W	Water	0.7	1.0%
<b>Subtotals for Soil Survey Area</b>		<b>56.9</b>	<b>81.9%</b>
<b>Totals for Area of Interest</b>		<b>69.5</b>	<b>100.0%</b>

Lebanon County, Pennsylvania (PA075)			
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
BrA	Brinkerton silt loam, 0 to 3 percent slopes	0.4	0.5%
ByB	Bucks silt loam, 3 to 8 percent slopes	1.0	1.4%
PeC	Penn channery silt loam, 8 to 15 percent slopes	1.7	2.4%
UnB	Ungers loam, 3 to 8 percent slopes	4.4	6.4%
UnC	Ungers loam, 8 to 15 percent slopes	5.2	7.5%
<b>Subtotals for Soil Survey Area</b>		<b>12.6</b>	<b>18.1%</b>
<b>Totals for Area of Interest</b>		<b>69.5</b>	<b>100.0%</b>

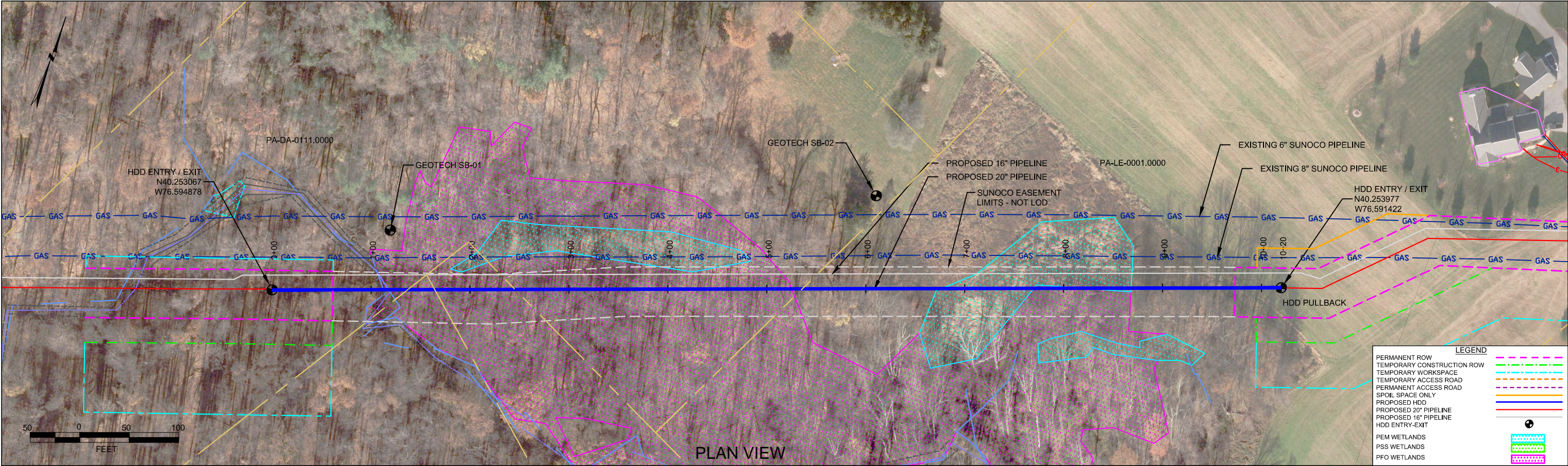


**WETLAND J-47 CROSSING  
PADEP SECTION 105 PERMIT NO.S:  
PA-LE-0001.0000-SR & PA-LE-0001.0000-SR-16  
(SPLP HDD No. S3-0090)**

**ATTACHMENT 2**

**ORIGINAL AND REVISED HORIZONTAL DIRECTIONAL DRILL PLAN AND PROFILES**

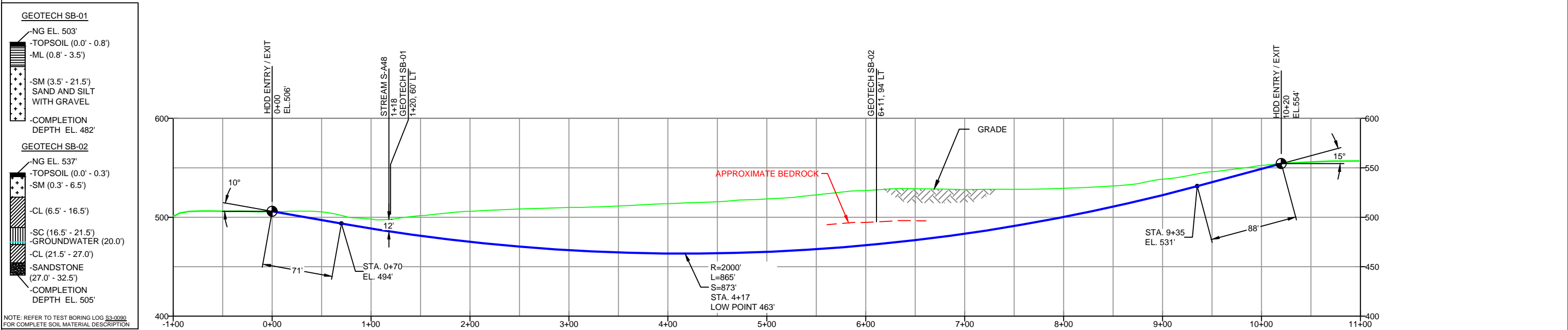




LEBANON COUNTY, PENNSYLVANIA - CONEWAGO TOWNSHIP  
S3-0090

PLAN VIEW

PROFILE VIEW



- DESIGN AND CONSTRUCTION:
- CONTRACTOR SHALL FIELD VERIFY DEPTH OF ALL EXISTING UTILITIES SHOWN OR NOT SHOWN ON THIS DRAWING.
  - THE MINIMUM SEPARATION DISTANCE FROM EXISTING SUBSURFACE UTILITIES SHALL NOT BE LESS THAN 10 FEET AS MEASURED FROM THE OUTSIDE EDGE OF THE UTILITY TO OUTSIDE OF PROPOSED PIPELINE.
  - DESIGNED IN ACCORDANCE WITH CFR 49 195 & ASME B31.4
  - CROSSING PIPE SPECIFICATION:  
HDD HORZ. LENGTH (L=): 1020'  
HDD PIPE LENGTH (S=): 1032'  
20" x 0.456" W.T., X-65, API 5L, PSL2, ERW, BFW  
COATING: 14-16 MILS FBE WITH 40 MILS MIN. ARO (POWERCRETE R95)
  - INTERNAL DESIGN PRESSURE 1480 PSIG (SEAM FACTOR 1.0, DESIGN FACTOR 0.50 (HOOP STRESS)).
  - INSTALLATION METHOD: HORIZONTAL DIRECTIONAL DRILL (HDD).
  - PIPELINE WARNING MARKERS SHALL BE INSTALLED ON BOTH SIDES OF ALL ROAD, RAILWAY, AND STREAM CROSSINGS.
  - CARRIER PIPE NOT ENCASED.
  - PIPE / AMBIENT TEMPERATURE MUST BE NO LESS THAN 30°F DURING PULLBACK WITHOUT PRIOR WRITTEN APPROVAL FROM THE ENGINEER.
  - CONDUCT 4-HOUR PRE-INSTALLATION HYDROTEST OF HDD PIPE STRING TO MINIMUM 1850 PSIG.
  - SEE SUNOCO PENNSYLVANIA PIPELINE PROJECT ESRI WEBMAP FOR ACCESS ROAD ALIGNMENT.
  - SUNOCO PIPELINE, L.P.'S HORIZONTAL DIRECTIONAL DRILL INADVERTENT RETURN CONTINGENCY PLAN WILL BE IMPLEMENTED AT ALL TIMES.
  - SUNOCO PIPELINE, L.P.'S EROSION AND SEDIMENTATION CONTROL PLAN WILL BE IMPLEMENTED AT ALL TIMES.



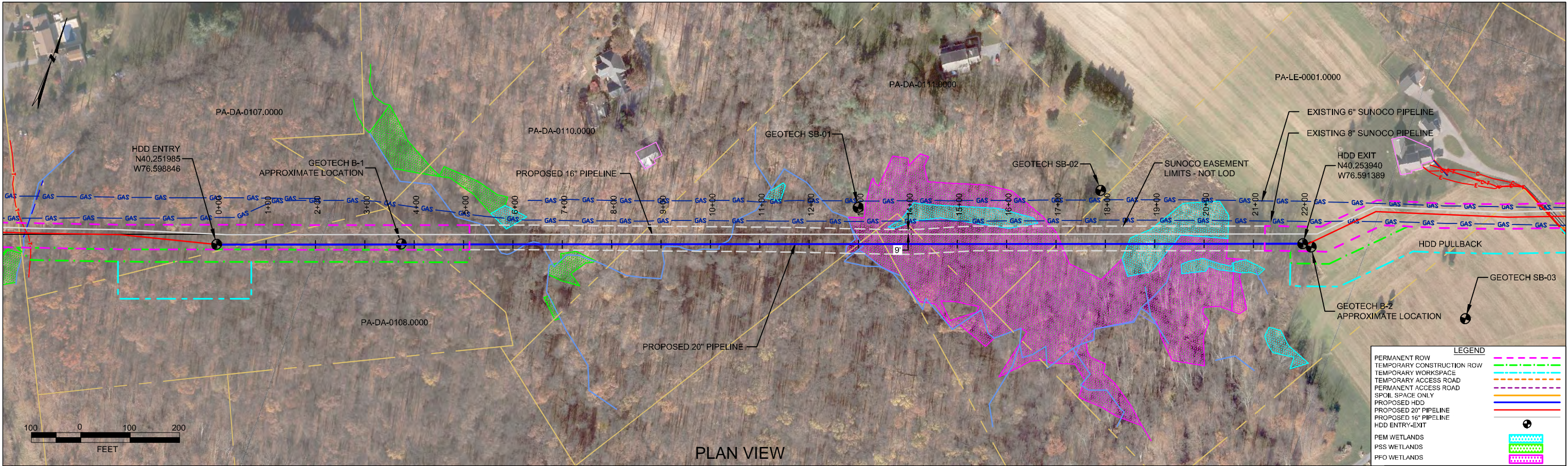
NOTES				REVISIONS						 <b>Sunoco Logistics Partners L.P.</b>		 <b>TETRA TECH ROONEY</b> (303) 792-5911		SUNOCO PIPELINE, L.P.  HORIZONTAL DIRECTIONAL DRILL WETLAND PENNSYLVANIA PIPELINE PROJECT	
1. ALL COORDINATES SHOWN ARE IN LATITUDE AND LONGITUDE. ALL MSL ELEVATIONS ARE NAD83															
2. STATIONING IS BASED ON HORIZONTAL DISTANCES															
3. ROONEY ENGINEERING, INC. AND SUNOCO PIPELINE, L.P. ARE NOT RESPONSIBLE FOR LOCATION OF FOREIGN UTILITIES SHOWN IN PLOT PLAN OR PROFILE. THE INFORMATION SHOWN HEREON IS FURNISHED WITHOUT LIABILITY ON THE PART OF ROONEY ENGINEERING, INC. AND SUNOCO PIPELINE, L.P. FOR ANY DAMAGES RESULTING FROM ERRORS OR OMISSIONS THEREIN.															
4. CONTRACTOR IS RESPONSIBLE FOR LOCATING ALL UTILITIES. CONTACT ONE CALL AT 811 PRIOR TO DIGGING.				2	REVISED PER ENGINEERING COMMENTS	MRS	08/19/16	RMB	08/19/16	AAW	08/19/16				
5. SUNOCO EMERGENCY HOTLINE NUMBER IS #1-800-786-7440.				1	REVISED PER COMMENTS FROM REI REVIEW	MRS	02/26/16	RMB	02/26/16	AAW	02/26/16				
				0	ISSUED FOR CONSTRUCTION	MRS	01/21/16	RMB	01/21/16	AAW	01/21/16				
				NO.	DESCRIPTION	BY	DATE	CHK	DATE	APP	DATE				

Figure 1. Original 20-Inch HDD Plan and Profile





PLAN VIEW

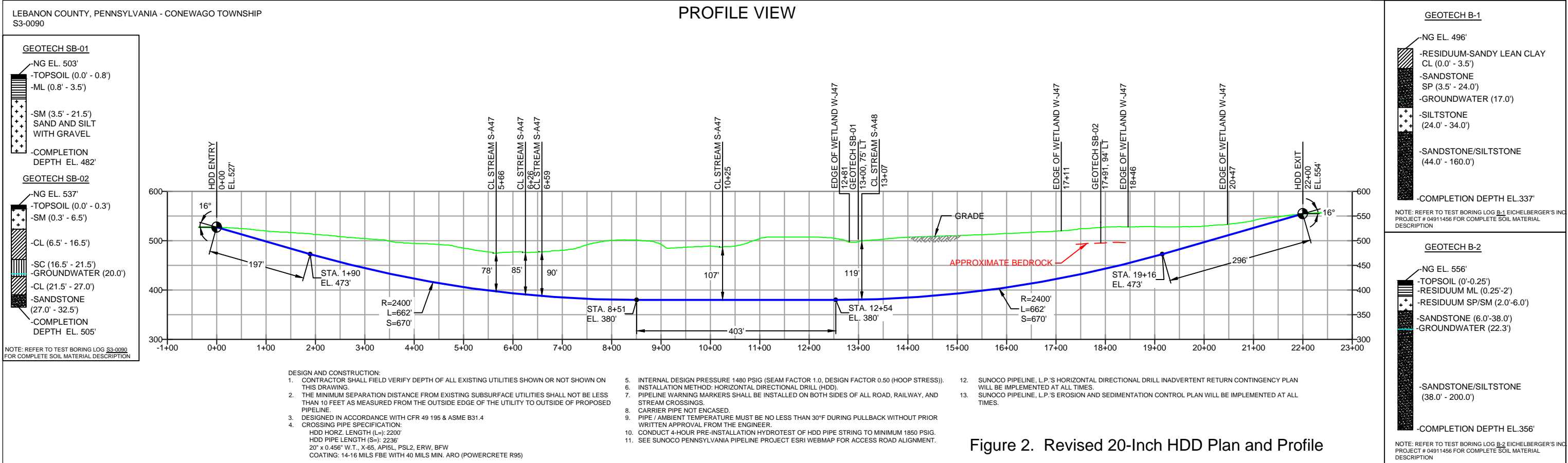


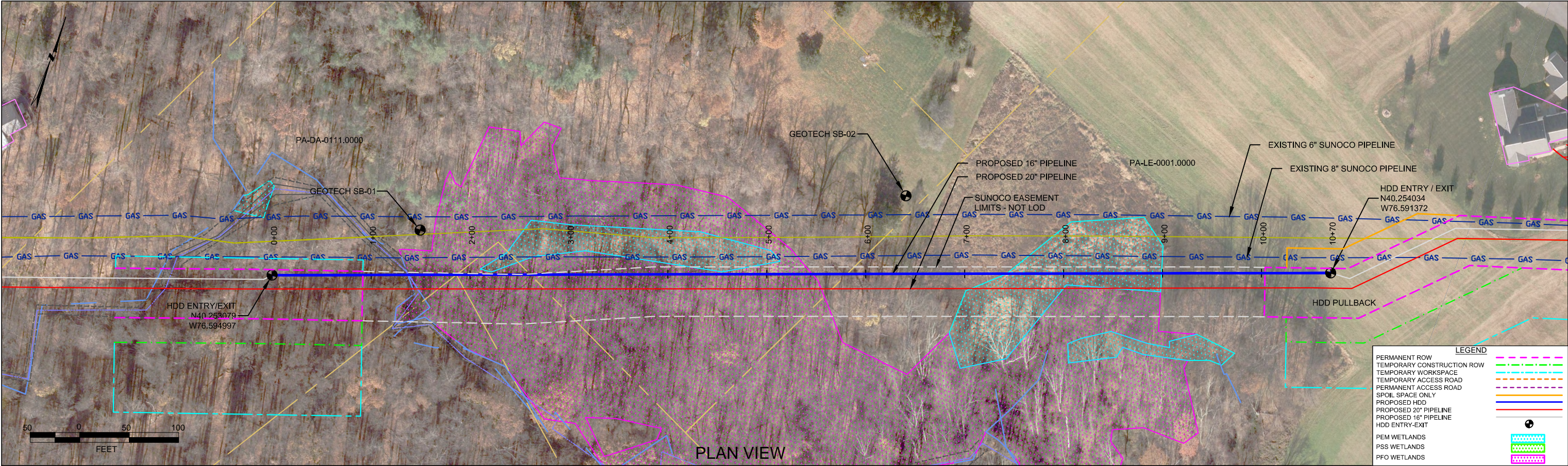


Figure 2. Revised 20-Inch HDD Plan and Profile

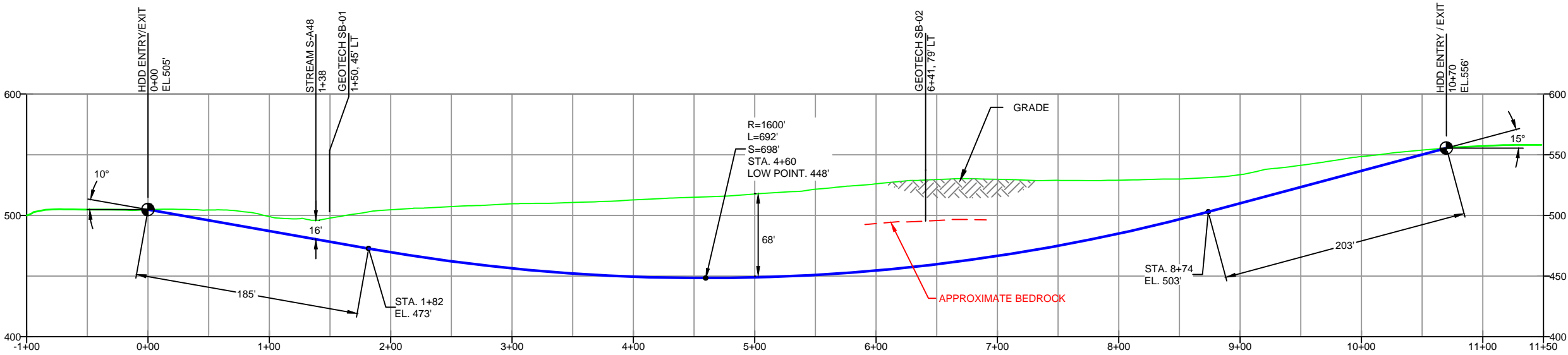
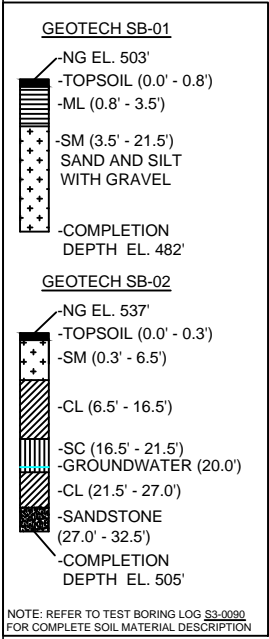
NOTES	REF. DRAWING				REVISIONS												<div><div>Sunoco Logistics Partners L.P.</div></div> <div><div>TETRA TECH ROONEY (303) 792-5911</div></div>		SUNOCO PIPELINE, L.P.			
1. ALL COORDINATES SHOWN ARE IN LATITUDE AND LONGITUDE. ALL MSL ELEVATIONS ARE NAD83 2. STATIONING IS BASED ON HORIZONTAL DISTANCES. 3. ROONEY ENGINEERING, INC. AND SUNOCO PIPELINE, LP ARE NOT RESPONSIBLE FOR LOCATION OF FOREIGN UTILITIES SHOWN IN PLOT PLAN OR PROFILE. THE INFORMATION SHOWN HEREON IS FURNISHED WITHOUT LIABILITY ON THE PART OF ROONEY ENGINEERING, INC. AND SUNOCO PIPELINE, LP, FOR ANY DAMAGES RESULTING FROM ERRORS OR OMISSIONS THEREIN. 4. CONTRACTOR IS RESPONSIBLE FOR LOCATING ALL UTILITIES. CONTACT ONE CALL AT 811 PRIOR TO DIGGING. 5. SUNOCO EMERGENCY HOTLINE NUMBER IS #1-800-786-7440.	ES-4.38	TO	ES-5.01	EROSION & SEDIMENT PLAN	EP3	DESIGN CHANGE - EXTENDED DRILL PER LANEY DRILLING AND CM SPREAD 5 APPROVAL						MRS	09/25/17	RMB	09/25/17	AMC			09/25/17	HORIZONTAL DIRECTIONAL DRILL WETLAND PENNSYLVANIA PIPELINE PROJECT	SCALE: 1"=200'	DWG. NUMBER: PA-LE-0001.0000-SR
	SHEET 24	TO	SHEET 1	AERIAL SITE PLAN	EP2	REVISED PER PADEP COMMENTS RECEIVED 09/06/16						DLM	09/30/16	RMB	09/30/16	AAW			09/30/16			
					EP1	REVISED PER PADEP COMMENTS						DLM	05/10/16	RMB	05/10/16	AAW			05/10/16			
					EP							MRS	03/15/16	RMB	03/15/16	AAW	03/15/16					
					C	ADDED GEOTECH INFO / DESIGN ADJUSTMENT						MRS	09/22/16	RMB	09/22/16	AAW	09/22/16					
					B	ISSUED FOR BID						DLM	07/31/15	RMB	07/31/15	AAW	07/31/15					
	DWG NO		DWG NO	DESCRIPTION	NO.	DESCRIPTION						BY	DATE	CHK	DATE	APP	DATE					







LEBANON COUNTY, PENNSYLVANIA - CONEWAGO TOWNSHIP  
S3-0090-16

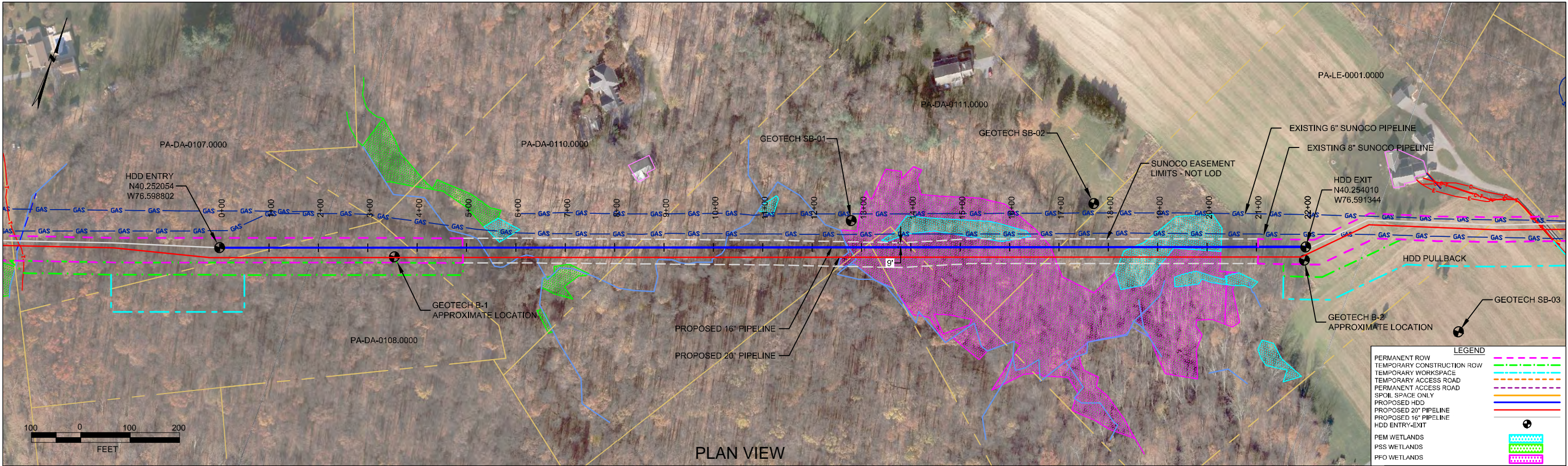
PROFILE VIEW



- DESIGN AND CONSTRUCTION:
- CONTRACTOR SHALL FIELD VERIFY DEPTH OF ALL EXISTING UTILITIES SHOWN OR NOT SHOWN ON THIS DRAWING.
  - THE MINIMUM SEPARATION DISTANCE FROM EXISTING SUBSURFACE UTILITIES SHALL NOT BE LESS THAN 10 FEET AS MEASURED FROM THE OUTSIDE EDGE OF THE UTILITY TO OUTSIDE OF PROPOSED PIPELINE.
  - DESIGNED IN ACCORDANCE WITH CFR 49 195 & ASME B31.4
  - CROSSING PIPE SPECIFICATION:  
HDD HORZ. LENGTH (L=): 1070'  
HDD PIPE LENGTH (S=): 1083'  
16" x 0.438" W.T., X-70, API5L, PSL2, ERW, BFW  
COATING: 14-16 MILS FBE WITH 40 MILS MIN. ARO (POWERCRETE R95)
  - INTERNAL DESIGN PRESSURE 1480 PSIG (SEAM FACTOR 1.0, DESIGN FACTOR 0.50 (HOOP STRESS)).
  - INSTALLATION METHOD: HORIZONTAL DIRECTIONAL DRILL (HDD).
  - PIPELINE WARNING MARKERS SHALL BE INSTALLED ON BOTH SIDES OF ALL ROAD, RAILWAY, AND STREAM CROSSINGS.
  - CARRIER PIPE NOT ENCASED.
  - PIPE / AMBIENT TEMPERATURE MUST BE NO LESS THAN 30°F DURING PULLBACK WITHOUT PRIOR WRITTEN APPROVAL FROM THE ENGINEER.
  - CONDUCT 4-HOUR PRE-INSTALLATION HYDROTEST OF HDD PIPE STRING TO MINIMUM 1850 PSIG.
  - SEE SUNOCO PENNSYLVANIA PIPELINE PROJECT ESRI WEBMAP FOR ACCESS ROAD ALIGNMENT.
  - SUNOCO PIPELINE, L.P.'S HORIZONTAL DIRECTIONAL DRILL INADVERTENT RETURN CONTINGENCY PLAN WILL BE IMPLEMENTED AT ALL TIMES.
  - SUNOCO PIPELINE, L.P.'S EROSION AND SEDIMENTATION CONTROL PLAN WILL BE IMPLEMENTED AT ALL TIMES.

NOTES										REVISIONS										<div><div>Sunoco Logistics Partners L.P.</div></div> <div><div>TETRA TECH ROONEY (303) 792-5911</div></div>		SUNOCO PIPELINE, L.P.																																																																																															
1. ALL COORDINATES SHOWN ARE IN LATITUDE AND LONGITUDE. ALL MSL ELEVATIONS ARE NAD83 2. STATIONING IS BASED ON HORIZONTAL DISTANCES. 3. ROONEY ENGINEERING, INC. AND SUNOCO PIPELINE, LP ARE NOT RESPONSIBLE FOR LOCATION OF FOREIGN UTILITIES SHOWN IN PLOT PLAN OR PROFILE. THE INFORMATION SHOWN HEREON IS FURNISHED WITHOUT LIABILITY ON THE PART OF ROONEY ENGINEERING, INC. AND SUNOCO PIPELINE, LP, FOR ANY DAMAGES RESULTING FROM ERRORS OR OMISSIONS THEREIN. 4. CONTRACTOR IS RESPONSIBLE FOR LOCATING ALL UTILITIES. CONTACT ONE CALL AT 811 PRIOR TO DIGGING. 5. SUNOCO EMERGENCY HOTLINE NUMBER IS #1-800-786-7440.										<table><tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td>2</td><td>REVISED PER ENGINEERING COMMENTS</td><td>MRS</td><td>08/19/16</td><td>RMB</td><td>08/19/16</td><td>AAW</td><td>08/19/16</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td>1</td><td>REVISED PER COMMENTS FROM REI REVIEW</td><td>MRS</td><td>02/26/16</td><td>RMB</td><td>02/26/16</td><td>AAW</td><td>02/26/16</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td>0</td><td>ISSUED FOR CONSTRUCTION</td><td>MRS</td><td>01/21/16</td><td>RMB</td><td>01/21/16</td><td>AAW</td><td>01/21/16</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td>NO.</td><td colspan="2">DESCRIPTION</td><td>BY</td><td>DATE</td><td>CHK</td><td>DATE</td><td>APP</td><td>DATE</td><td colspan="6"></td><td colspan="2"></td></tr></table>																																										2	REVISED PER ENGINEERING COMMENTS	MRS	08/19/16	RMB	08/19/16	AAW	08/19/16								1	REVISED PER COMMENTS FROM REI REVIEW	MRS	02/26/16	RMB	02/26/16	AAW	02/26/16								0	ISSUED FOR CONSTRUCTION	MRS	01/21/16	RMB	01/21/16	AAW	01/21/16								NO.	DESCRIPTION		BY	DATE	CHK	DATE	APP	DATE									HORIZONTAL DIRECTIONAL DRILL WETLAND PENNSYLVANIA PIPELINE PROJECT			
2	REVISED PER ENGINEERING COMMENTS	MRS	08/19/16	RMB	08/19/16	AAW	08/19/16																																																																																																														
1	REVISED PER COMMENTS FROM REI REVIEW	MRS	02/26/16	RMB	02/26/16	AAW	02/26/16																																																																																																														
0	ISSUED FOR CONSTRUCTION	MRS	01/21/16	RMB	01/21/16	AAW	01/21/16																																																																																																														
NO.	DESCRIPTION		BY	DATE	CHK	DATE	APP	DATE																																																																																																													
														SCALE: 1"=100'		DWG. NO: PA-LE-0001.0000-SR-16																																																																																																					

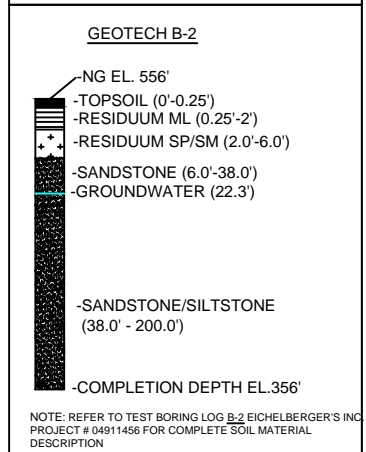
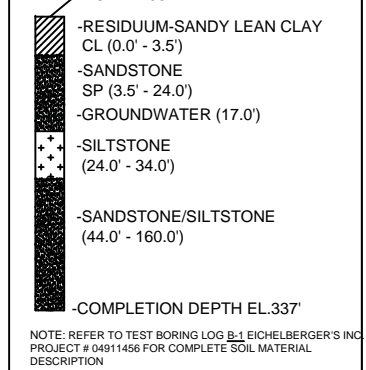
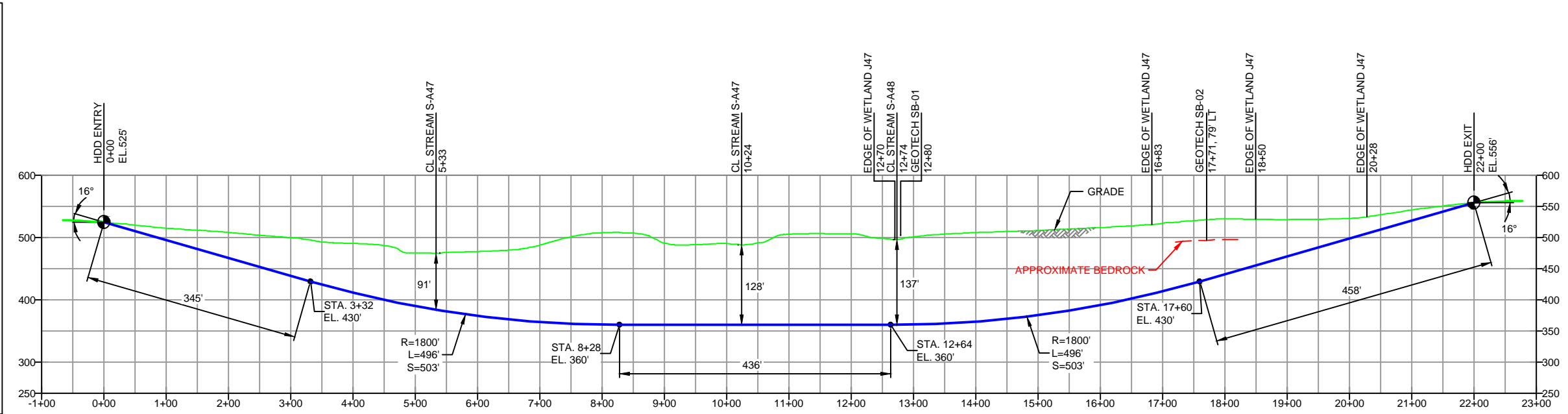
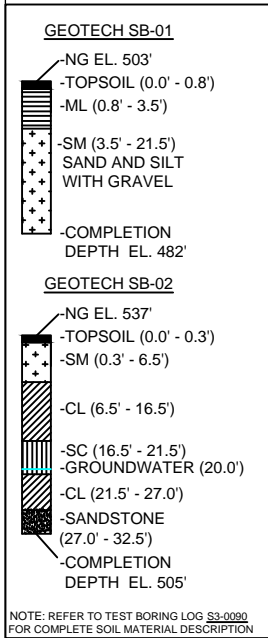




LEBANON COUNTY, PENNSYLVANIA - CONEWAGO TOWNSHIP  
S3-0090-16


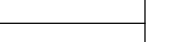
PLAN VIEW

PROFILE VIEW



- DESIGN AND CONSTRUCTION:
- CONTRACTOR SHALL FIELD VERIFY DEPTH OF ALL EXISTING UTILITIES SHOWN OR NOT SHOWN ON THIS DRAWING.
  - THE MINIMUM SEPARATION DISTANCE FROM EXISTING SUBSURFACE UTILITIES SHALL NOT BE LESS THAN 10 FEET AS MEASURED FROM THE OUTSIDE EDGE OF THE UTILITY TO OUTSIDE OF PROPOSED PIPELINE.
  - DESIGNED IN ACCORDANCE WITH CFR 49 195 & ASME B31.4
  - CROSSING PIPE SPECIFICATION:
    - HDD HORZ. LENGTH (L=): 2200'
    - HDD PIPE LENGTH (S=): 2245'
    - 16" x 0.438" W.T., X-70, API 5L, PSL2, ERW, BFW
    - COATING: 14-16 MILS FBE WITH 40 MILS MIN. ARO (POWERCRETE R95)
  - INTERNAL DESIGN PRESSURE 1480 PSIG (SEAM FACTOR 1.0, DESIGN FACTOR 0.50 (HOOP STRESS)).
  - INSTALLATION METHOD: HORIZONTAL DIRECTIONAL DRILL (HDD).
  - PIPELINE WARNING MARKERS SHALL BE INSTALLED ON BOTH SIDES OF ALL ROAD, RAILWAY, AND STREAM CROSSINGS.
  - CARRIER PIPE NOT ENCASED.
  - PIPE / AMBIENT TEMPERATURE MUST BE NO LESS THAN 30°F DURING PULLBACK WITHOUT PRIOR WRITTEN APPROVAL FROM THE ENGINEER.
  - CONDUCT 4-HOUR PRE-INSTALLATION HYDROTEST OF HDD PIPE STRING TO MINIMUM 1850 PSIG.
  - SEE SUNOCO PENNSYLVANIA PIPELINE PROJECT ESRI WEBMAP FOR ACCESS ROAD ALIGNMENT.
  - SUNOCO PIPELINE, L.P.'S HORIZONTAL DIRECTIONAL DRILL INADVERTENT RETURN CONTINGENCY PLAN WILL BE IMPLEMENTED AT ALL TIMES.
  - SUNOCO PIPELINE, L.P.'S EROSION AND SEDIMENTATION CONTROL PLAN WILL BE IMPLEMENTED AT ALL TIMES.

Figure 4. Revised 16-Inch Plan and Profile

<div>NOTES</div> <div>1. ALL COORDINATES SHOWN ARE IN LATITUDE AND LONGITUDE. ALL MSL ELEVATIONS ARE NAD83</div> <div>2. STATIONING IS BASED ON HORIZONTAL DISTANCES.</div> <div>3. ROONEY ENGINEERING, INC. AND SUNOCO PIPELINE, LP ARE NOT RESPONSIBLE FOR LOCATION OF FOREIGN UTILITIES SHOWN IN PLOT PLAN OR PROFILE. THE INFORMATION SHOWN HEREON IS FURNISHED WITHOUT LIABILITY ON THE PART OF ROONEY ENGINEERING, INC. AND SUNOCO PIPELINE, LP, FOR ANY DAMAGES RESULTING FROM ERRORS OR OMISSIONS THEREIN.</div> <div>4. CONTRACTOR IS RESPONSIBLE FOR LOCATING ALL UTILITIES. CONTACT ONE CALL AT 811 PRIOR TO DIGGING.</div> <div>5. SUNOCO EMERGENCY HOTLINE NUMBER IS #1-800-786-7440.</div>	REF. DRAWING				REVISIONS								<div><div>Sunoco Logistics Partners L.P.</div></div> <div><div>TETRA TECH ROONEY</div><div>(303) 792-5911</div></div>		<div>SUNOCO PIPELINE, L.P.</div> <div>HORIZONTAL DIRECTIONAL DRILL WETLAND</div> <div>PENNSYLVANIA PIPELINE PROJECT</div>		
	ES-4.38	TO	ES-5.01	EROSION & SEDIMENT PLAN	EP3	DESIGN CHANGE - EXTENDED DRILL PER LANEY DRILLING AND CM SPREAD 5 APPROVAL		MRS	09/25/17	RMB	09/25/17	AMC					09/25/17
	SHEET 24	TO	SHEET 1	AERIAL SITE PLAN	EP2	REVISED PER PADEP COMMENTS RECEIVED 09/06/16		MRS	10/07/16	RMB	10/07/16	AAW					10/07/16
					EP1	REVISED PER PADEP COMMENTS		DLM	05/17/16	RMB	05/17/16	AAW					05/17/16
					EP			MRS	03/05/16	RMB	03/05/16	AAW	03/05/16				
					B	ADDED GEOTECH INFO		MRS	09/22/15	RMB	09/22/15	AAW	09/22/15				
					A	ISSUED FOR BID		MRS	08/31/15	RMB	08/31/15	AAW	08/31/15				
		DWG NO		DWG NO	DESCRIPTION	NO.	DESCRIPTION		BY	DATE	CHK	DATE	APP	DATE			



**WETLAND J-47 CROSSING  
PADEP SECTION 105 PERMIT NO.S:  
PA-LE-0001.0000-SR & PA-LE-0001.0000-SR-16  
(SPLP HDD No. S3-0090)**

**ATTACHMENT 3**

**ANNULAR PRESSURE AND FRACTURE PRESSURE CALCULATIONS**





## HORIZONTAL DIRECTIONAL CONCEPTUAL DRILL DESIGN

**PROJECT:** Sunoco Pipeline, L.P.  
Mariner East Pipeline  
Lebanon County, Pennsylvania

**CROSSING:** WETLAND J47 - West to East R1  
20-INCH STEEL PIPE

**ISSUE:** APC/FPC DESIGN

### Contents:

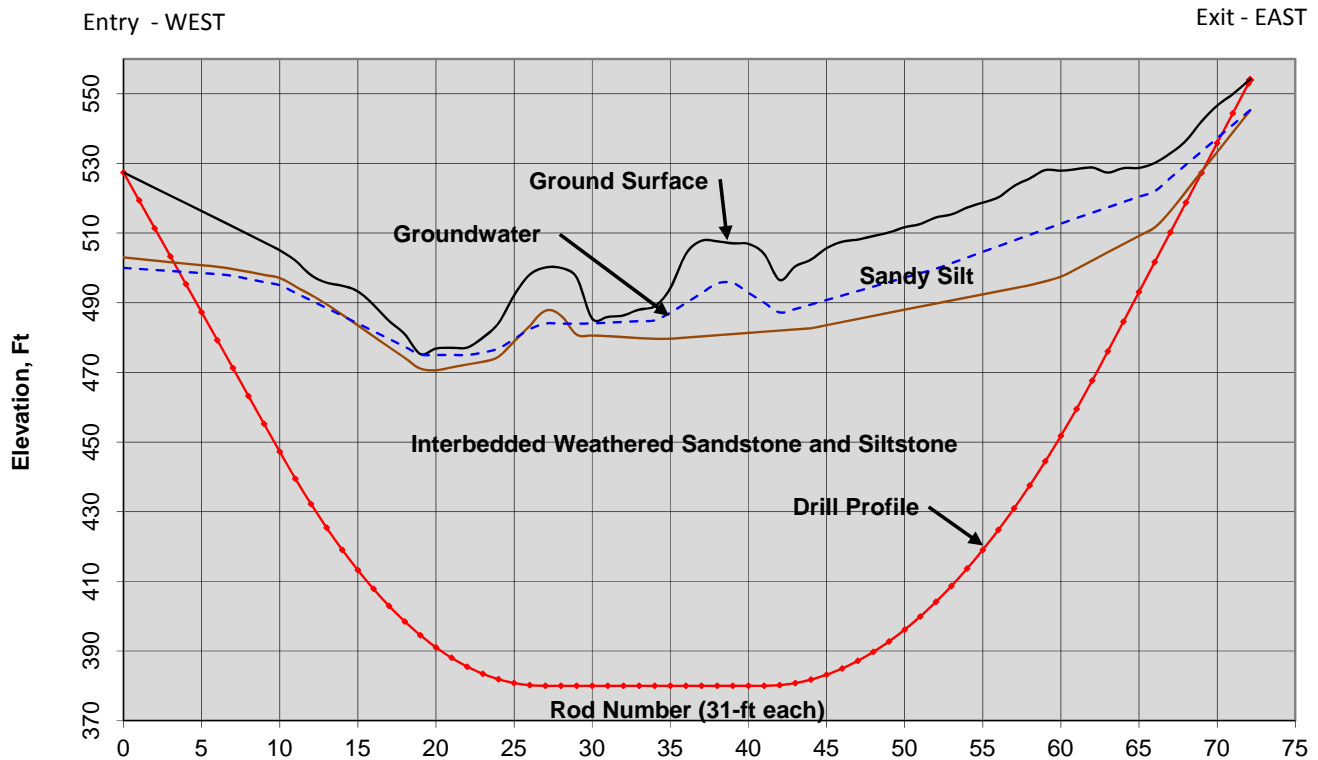
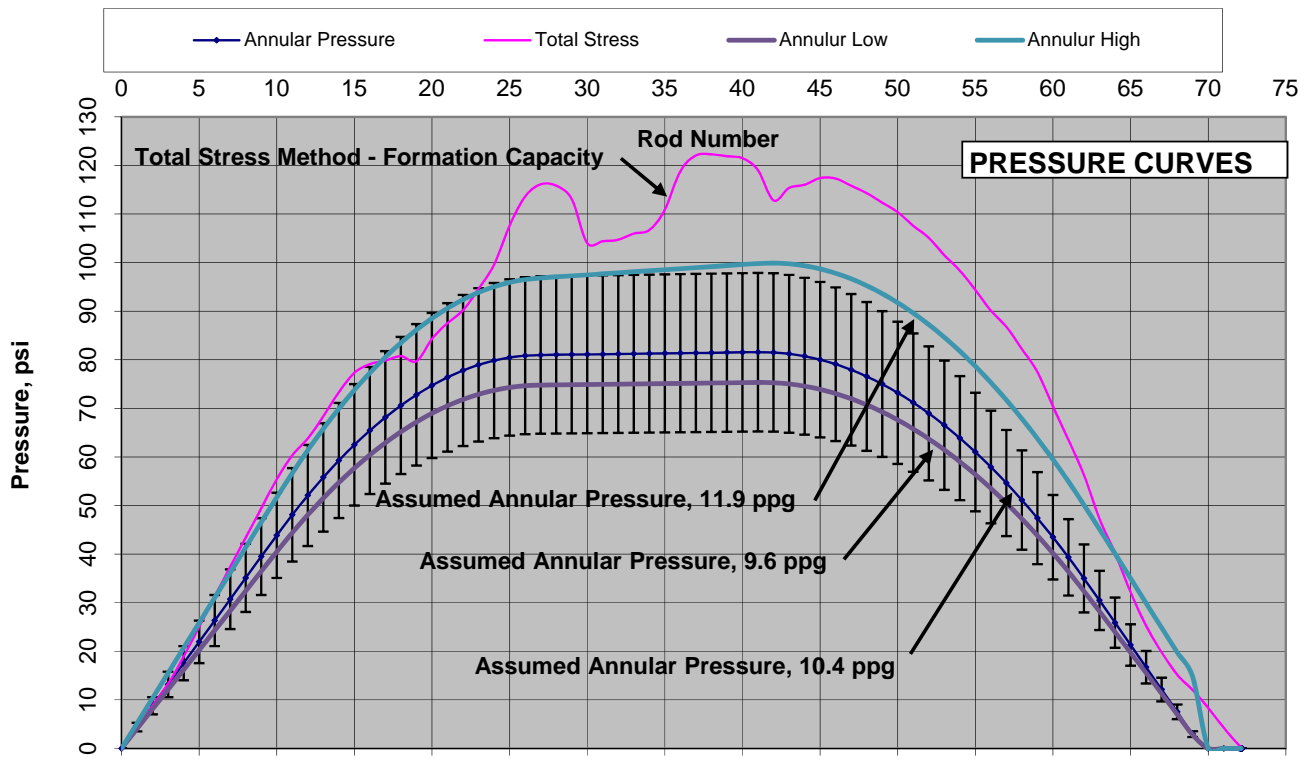
	Figure 1 - Annular Pressure and Formation Pressure Capacity Curves
	Table 1 - Design Summary, Assumptions, Conditions
	Table 2 - Design Drill Path Calculation
	Table 3 - Estimated Annular Pressure Curve Example Calculation
	Table 4 - Estimated Formation Pressure Curve Example Calculation

**Prepared For:** Sunoco Logistics Partners L.P.  
525 Fritztown Road  
Sinking Spring, PA 19608  
855-430-4491

**Prepared By:** Directional Project Support  
33311 Lois Lane, Suite A  
Magnolia, Texas 77354  
281.259.7819 (O) 617.510.8090 (C)  
B. Dorwart

**Project No:** 0  
**Print Date:** 22-Sep-2017

Revision	ID	DESCRIPTION	BY
9/21/2017	0	APC/FPC Design	BCD
9/22/2017	1	Moved entry 300 feet back, chg angle & radius	bcd



**Notes:**

1. Geology is interpreted from project data

2. APC pressure basis:

12.31 in	Pilot Hole Diameter
78.0 pcf	Assumed Fluid Weight
300 gal/min	Assumed Pump Rate
6.63 in	Drill Rod Diameter

3. Rod length: 31 Ft per rod

4. The error bars are at 20% for APC curve

ISSUED FOR: APC/FPC DESIGN



Directional Project Support  
33311 Lois Lane, Suite A  
Magnolia, Texas 77354

Sunoco Pipeline, L.P.  
Mariner East Pipeline  
Lebanon County, Pennsylvania

**ANNULAR PRESSURE AND FORMATION  
PRESSURE CURVES  
WETLAND J47 - West to East R1**

Revision 1

**FIGURE 1**



# PATH DESIGN CALCULATIONS

Entry Station	0+00.00	FT
Exit Station	21+99.25	FT
<b>Entry and Exit Design Coordinates &amp; Elevations (Ft) (Note 2)</b>		
East	North	Elevation
Entry 2289803.5501	336743.7681	527.40 ft
Horizontal Curve PI 2290837.9745	337116.7845	
Exit 2291872.3990	337489.8010	554.00 ft
Depth to Mudline 42.40 ft	Clearance Depth =	105.00 ft
Measured Plan Length at ties =	2199.2501 ft	
Coordinate Length =	2199.2501 ft	
<b>OK-HORIZONTAL CURVE</b>		
Water Surface Elev. 485.30 ft		
Mudline Elev. 485.00 ft		
Lowest centerline Elev. 380.00 ft		

## SUMMARY HORIZONTAL CURVE CALCULATIONS

	Start			End				Length	Radius	Angle
	Station	Easting	Northing	Station	Easting	Northing	Azimuth			
Tangent	0+00.00	2289803.5501	336743.7681	10+99.63	2290837.9745	337116.7845	E 019.82945 N	1099.63		
Curve	10+99.63	2290837.9745	337116.7845	10+99.63	2290837.9745	337116.7845	E 019.82945 N	0.00	0.00	0.000 deg.
Tangent	10+99.63	2290837.9745	337116.7845	21+99.25	2291872.3990	337489.8010	E 019.82945 N	1099.63		

## HORIZONTAL PLAN CALCULATIONS (FT)

Entry Tangent Segment	Horizontal Curve Segment	Exit Tangent Segment	Check Delta 0.0000 OK CALC  Exit Station 21+99.25 OK STA
Plan Length, ft. 1099.63	Input Radius, ft. 0.00	Plan Length, ft. 1099.63	
Entry Azimuth, deg. <sup>5</sup> E 019.82945 N	Curve, deg. 0.000 deg.	Exit Azimuth, deg. <sup>5</sup> E 019.82945 N	
Entry Azimuth, rad. <sup>5</sup> 0.34609	Curve, rad. 0.00000	Exit Azimuth, rad. <sup>5</sup> 0.34609	
<b>Calculate PCH</b>	<b>Calculate PTH</b>	<b>Calculate Exit</b>	
PCH Easting 2290837.9745	Chord Length, ft. 0.00	Easting 2291872.3990	
PCH Northing 337116.7845	Arc Length, ft. 0.00	Northing 337489.8010	
	Chord Azimuth, deg. 19.8295		
	PI Easting = 2291452.2366		
	PI Northing = 337338.2892		
	PTH Easting = 2290837.9745		
	PTH Northing = 337116.7845		
Cum Plan Length 1099.63	Cum Plan Length 1099.63	Cum Plan Length 2199.250096	

## Pull Geometry

Pipe Entry	EXIT		Enter the pipe entry location into the hole: Entry/Exit			Path Length	Curve Radius
	Elevations		Vertical Angle, (-) = Clockwise				
Segment	Start	End	Start	End	Δ Angle		
Entry Tangent	554.00 ft	472.97 ft	16.00 deg	16.00 deg	0.00 deg	293.97 ft	0.00 ft
Entry Curve	472.97 ft	380.00 ft	16.00 deg	0.00 deg	-16.00 deg	670.21 ft	2400.00 ft
Bottom Tangent	380.00 ft	380.00 ft	0.00 deg	0.00 deg	0.00 deg	441.73 ft	0.00 ft
Exit Curve	380.00 ft	448.15 ft	0.00 deg	-15.00 deg	-15.00 deg	523.60 ft	2000.00 ft
Exit Tangent	448.15 ft	527.40 ft	-15.00 deg	-15.00 deg	0.00 deg	306.20 ft	0.00 ft
Total Check =						2235.71 ft	OK

## Compound Curve Assessment

	Vert. Plan	Horiz. Plan	
Entry	813.41	1099.63	No, Horiz > Entry V(Tan+Curve)
Exit	944.11	1099.63	No, Horiz > Entry V(Tan+Curve)

## VERTICLE PATH DESIGN CALCULATIONS (FT)

Entry Tangent Segment 1	Entry Vert. Curve Segment 2	Middle Tangent Segment 3	Exit Vert. Curve Segment 4	Exit Tangent Segment 5
Entry Angle -15.000 deg.	Vertical Radius 2000.00	Rod Length 441.73270	Radius 2400.00	Exit Elevation 554.00
Entry Angle, rad. -0.2618 rad	Vert. Curve, deg. 15.000 deg.	Inclined Bottom Tan NO	Design Exit Angle 16.000 deg.	
Rod/Path Length 306.20	Vert. Curve, rad. 0.2618 rad		Vert. Curve, rad. 0.2793 rad	
<b>Calculate Vertical PCV</b>	<b>Calculate Vertical PTV</b>	<b>Calculate Vertical PCV</b>	<b>Calculate Vertical PTV</b>	<b>Calculate Exit</b>
Plan Length 295.77	Plan Length 517.64	Plan Length 441.7326957	Vert. Curve, deg. 16.000 deg.	Plan Length 282.58
Path Length 306.20	Arc Path Length 523.60	Path Length 441.73	Vert. Curve, rad. 0.27925268	Path Length 293.97
Tangent Depth -79.25	Curve Vert Depth -68.15	End Elevation 380.00	Plan Length 661.53	Elevation 554.00
End Elevation 448.15	End Elevation 380.00	Rise/drop 0.00	Path Arc Length 670.21	Rise/drop 81.03
	Lowest Elevation 380.00		Lowest Elevation 380.00	
	End Vert Angle 0.000 deg.	End Vert Angle 0.000 deg.	Elevation 472.97	
	End Vert Angle, rad 0.0000 rad	End Vert Angle, rad 0.0000 rad	Curve Vert Depth 92.97	
<b>Prop. Plan Length 2199.250096</b>				

## SUMMARY VERTICLE CURVE CALCULATIONS

Start Station 0+00.00	Start Station 2+95.77	Start Station 8+13.41	Start Station 12+55.14	Start Station 19+16.67
PVC Station 2+95.77	PTV Station 8+13.41	PCV Station 12+55.14	PTV Station 19+16.67	Exit Station 21+99.250
Cum Plan Length 295.77	Cum Plan Length 813.41	Cum Plan Length 1255.14 ft	Cum Plan Length 1916.67	Cum Plan Length 2199.250096
Cum Path Length 306.20	Cum Path Length 829.80	Cum Path Length 1271.54 ft	Cum Path Length 1941.74	Cum Path Length 2235.708991
Cum Depth -79.25	Cum Depth -147.40	Cum Depth -147.40 ft	Cum Depth -54.43	Cum Depth 26.60

## Summary of Drill Calculations

Entry to Exit Elevation Change =	26.60 ft
Minimum Design Elevation =	380.00 ft
Invert Depth below exit =	174.00 ft
Invert Depth below entry =	147.40 ft
Path Length =	2,235.71 ft
Plan Length =	2,199.25 ft
Minimum Plan Length (No Tangent) =	1,757.52 ft
Entry Angle =	-15.00 deg
Exit Angle =	16.00 deg
Compound Curve at Entry =	NO
Compound Curve at Exit =	NO

## Stationing Check

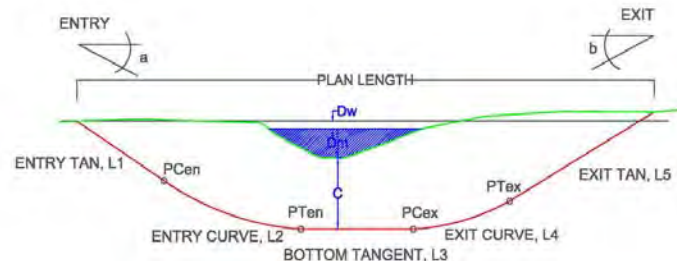
OK STATIONING

## Plan Length Check

OK CALCULATION

## NOTES:

- Sign convention for angles - positive (+) angles are counterclockwise.  
Due East is defined as 0 degrees.
- Coordinates are in feet and reference NAD 83 Pennsylvania South State Plane
- Elevations are in feet and reference NAVD 88.
- All calculation locations represent the center of the drill hole.



Indicates inputs  
Indicates status on internal design checks  
ISSUE: APC/FPC DESIGN



Directional Project Support  
33311 Lois Lane, Suite A  
Magnolia, Texas 77354

Sunoco Pipeline, L.P.  
Mariner East Pipeline  
Lebanon County, Pennsylvania

TABLE 2  
DESIGN DRILL PATH CALCULATION  
WETLAND J47 - West to East R1  
20-INCH STEEL PIPE

Revision 1

1/0/1900

**TABLE 3**  
**ESTIMATED ANNULAR PRESSURE CURVE (APC) EXAMPLE CALCULATION**  
 Sunoco Pipeline, L.P.  
 Mariner East Pipeline  
 Lebanon County, Pennsylvania



**WETLAND J47 - West to East R1**  
**20-INCH STEEL PIPE**  
**INPUT**

**1. Drill path data**

	Measured Distance	Elevations	Angles	Lengths	Angle Change
Drill Entry	0.000 ft	527.4	-15	Entry to PC	306.205 ft
PC	306.205 ft			PC to PT	523.599 ft
PT	829.804 ft			Invert Tangent	441.733 ft
PC	1271.536 ft			PC to PT	670.206 ft
PT	1941.743 ft			PT to Exit	293.966 ft
Drill Exit	<b>2235.709 ft</b>	554.00 ft	16		<b>2235.709 ft</b>
					<b>Length Ck OK</b>

**2. Drill Fluid Hydraulic Assumptions**

	Assumed	Low	High
Density, $\gamma_f$ =	78	72	89
Dynamic annulus pressure $P_d$ =	0.0014 psi/ft	0.0013 psi/ft	0.0068 psi/ft
Drill fluid viscosity, $\mu_p$ =	2 cp	6 cp	13 cp
Yield point of drill fluid, $Y_P$ =	41	19	5

**3. Drill Data Assumptions**

Assumed Drill Size:	<b>DD660</b>
Avg Rod length =	31.0 feet
Diameter of hole, $D_h$ =	12.31125
Drill Rod Tube Diameter, $D_r$ =	6.625 in
Drilling Pump rate, gpm =	300 gal/min

Max Rig Pump =	<b>1200 gpm</b>
Number of drill rods =	<b>72</b>
Estimated annular pilot uphole drill fluid velocity, $V_{ha}$ =	<b>68.29 ft/min</b>

**4. Calculate Annular Pressure, P**

**Method A - (API RP) 13D**

$$P_A = [\gamma_f (Y_{\text{entry}} - Y)/144] + (P_d)(MD)$$

**Method B - HDD Good Practices Cavity Expansion Annular Pressure**

$$P_B = [\gamma_f * (Y_{\text{entry}} - Y)/144] + MD * [\mu_p * (V_{ha}/60)/(1000 * (D_h - D_r)^2) + Y_P/[200 * (D_h - D_r)]]$$

Start Station	0+00.00	1						
Drill Path			Assumed Return Density		Low Return Density		High Return Density	
			Density, $\gamma_{fE}$ = 78		Density, $\gamma_{fL}$ = 72		Density, $\gamma_{fH}$ = 89	
Rod Measured Distance MD	Station X	Elevation Y	Annular Fluid Pressure $P_A$	Annular Fluid Pressure $P_B$	Annular Fluid Pressure $P_A$	Annular Fluid Pressure $P_B$	Annular Fluid Pressure $P_A$	Annular Fluid Pressure $P_B$
ft	ft	ft	psi	psi	psi	psi	psi	psi
0.00	0+00.00	527.40	0.00	0.00	0.00	0.00	0.00	0.00
31.00	0+29.94	519.38	4.39	5.47	4.05	4.54	5.17	5.11
62.00	0+59.89	511.35	8.78	10.93	8.10	9.07	10.34	10.22
93.00	0+89.83	503.33	13.16	16.40	12.15	13.61	15.51	15.33
124.00	1+19.77	495.31	17.55	21.86	16.21	18.14	20.68	20.44
155.00	1+49.72	487.28	21.94	27.33	20.26	22.68	25.86	25.55
186.00	1+79.66	479.26	26.33	32.79	24.31	27.21	31.03	30.66
217.00	2+09.61	471.24	30.72	38.26	28.36	31.75	36.20	35.77
248.00	2+39.55	463.21	35.10	43.73	32.41	36.29	41.37	40.88
279.00	2+69.49	455.19	39.49	49.19	36.46	40.82	46.54	45.98
310.00	2+99.44	447.19	43.86	54.64	40.50	45.34	51.69	51.08
341.00	3+29.46	439.46	48.09	59.95	44.41	49.74	56.69	56.01
372.00	3+59.60	432.19	52.07	65.01	48.08	53.89	61.39	60.65
403.00	3+89.85	425.39	55.80	69.81	51.52	57.82	65.81	65.00
434.00	4+20.19	419.06	59.27	74.36	54.73	61.51	69.93	69.07



Drill Path			Assumed Return Density		Low Return Density		High Return Density	
			Density, $\gamma_{FE} = 78$		Density, $\gamma_{FL} = 72$		Density, $\gamma_{FH} = 89$	
Rod Measured Distance MD	Station X	Elevation Y	Annular Fluid Pressure $P_A$	Annular Fluid Pressure $P_B$	Annular Fluid Pressure $P_A$	Annular Fluid Pressure $P_B$	Annular Fluid Pressure $P_A$	Annular Fluid Pressure $P_B$
ft	ft	ft	psi	psi	psi	psi	psi	psi
465.00	4+50.63	413.20	62.48	78.65	57.70	64.96	73.76	72.84
496.00	4+81.16	407.82	65.44	82.69	60.43	68.18	77.31	76.32
527.00	5+11.77	402.90	68.15	86.47	62.92	71.16	80.56	79.50
558.00	5+42.45	398.47	70.59	90.00	65.18	73.90	83.51	82.40
589.00	5+73.20	394.50	72.78	93.26	67.20	76.41	86.17	85.00
620.00	6+04.00	391.02	74.71	96.27	68.99	78.67	88.54	87.30
651.00	6+34.85	388.01	76.38	99.02	70.53	80.70	90.61	89.31
682.00	6+65.75	385.48	77.79	101.51	71.83	82.49	92.38	91.02
713.00	6+96.68	383.43	78.94	103.74	72.90	84.04	93.86	92.44
744.00	7+27.64	381.86	79.84	105.71	73.72	85.35	95.04	93.56
775.00	7+58.62	380.78	80.47	107.42	74.31	86.42	95.93	94.38
806.00	7+89.62	380.17	80.84	108.87	74.65	87.24	96.52	94.91
837.00	8+20.62	379.98	80.98	110.09	74.78	87.86	96.85	95.18
868.00	8+51.62	379.98	81.02	111.21	74.82	88.39	97.06	95.33
899.00	8+82.62	379.98	81.07	112.33	74.86	88.91	97.27	95.48
930.00	9+13.62	379.98	81.11	113.45	74.90	89.43	97.48	95.63
961.00	9+44.62	379.98	81.15	114.57	74.94	89.96	97.69	95.78
992.00	9+75.62	379.98	81.19	115.69	74.98	90.48	97.91	95.93
1023.00	10+06.62	379.98	81.23	116.80	75.02	91.01	98.12	96.08
1054.00	10+37.62	379.98	81.27	117.92	75.06	91.53	98.33	96.23
1085.00	10+68.62	379.98	81.32	119.04	75.10	92.05	98.54	96.38
1116.00	10+99.62	379.98	81.36	120.16	75.14	92.58	98.76	96.53
1147.00	11+30.62	379.98	81.40	121.28	75.18	93.10	98.97	96.68
1178.00	11+61.62	379.98	81.44	122.40	75.22	93.63	99.18	96.83
1209.00	11+92.62	379.98	81.48	123.52	75.26	94.15	99.39	96.98
1240.00	12+23.62	379.98	81.53	124.64	75.30	94.67	99.61	97.13
1271.00	12+54.62	379.98	81.57	125.76	75.34	95.20	99.82	97.28
1302.00	12+85.62	380.18	81.50	126.78	75.28	95.62	99.91	97.31
1333.00	13+16.61	380.77	81.22	127.57	75.02	95.85	99.75	97.09
1364.00	13+47.59	381.77	80.73	128.16	74.57	95.88	99.35	96.63
1395.00	13+78.56	383.16	80.01	128.52	73.91	95.71	98.70	95.92
1426.00	14+09.51	384.95	79.08	128.67	73.05	95.33	97.81	94.96
1457.00	14+40.43	387.15	77.94	128.60	72.00	94.76	96.66	93.76
1488.00	14+71.33	389.74	76.57	128.32	70.74	93.99	95.27	92.30
1519.00	15+02.18	392.73	75.00	127.82	69.28	93.02	93.64	90.61
1550.00	15+32.99	396.12	73.20	127.10	67.63	91.85	91.75	88.66
1581.00	15+63.76	399.91	71.19	126.17	65.77	90.48	89.62	86.47
1612.00	15+94.48	404.09	68.97	125.02	63.72	88.91	87.25	84.04
1643.00	16+25.14	408.67	66.53	123.66	61.47	87.14	84.63	81.35
1674.00	16+55.74	413.65	63.87	122.08	59.02	85.18	81.77	78.43
1705.00	16+86.27	419.02	61.01	120.29	56.38	83.02	78.66	75.26
1736.00	17+16.73	424.79	57.93	118.29	53.53	80.66	75.31	71.85
1767.00	17+47.11	430.95	54.63	116.07	50.49	78.10	71.72	68.19
1798.00	17+77.41	437.50	51.13	113.65	47.26	75.35	67.88	64.29
1829.00	18+07.62	444.44	47.41	111.01	43.83	72.41	63.80	60.15
1860.00	18+37.74	451.77	43.48	108.15	40.20	69.26	59.48	55.77
1891.00	18+67.77	459.49	39.34	105.09	36.38	65.93	54.93	51.15
1922.00	18+97.69	467.59	34.99	101.82	32.37	62.40	50.13	46.29
1953.00	19+27.52	476.02	30.47	98.38	28.20	58.71	45.13	41.24
1984.00	19+57.32	484.56	25.88	94.87	23.96	54.96	40.07	36.11
2015.00	19+87.12	493.11	21.30	91.36	19.73	51.22	35.00	30.98
2046.00	20+16.92	501.65	16.71	87.85	15.50	47.47	29.93	25.85
2077.00	20+46.72	510.19	12.12	84.35	11.27	43.72	24.86	20.72
2108.00	20+76.52	518.74	7.54	80.84	7.03	39.97	19.79	15.59
2139.00	21+06.32	527.28	2.95	77.33	2.80	36.22	14.72	10.45
2170.00	21+36.12	535.83	0.00	0.00	0.00	0.00	0.00	0.00
2201.00	21+65.91	544.37	0.00	0.00	0.00	0.00	0.00	0.00
2232.00	21+95.71	552.92	0.00	0.00	0.00	0.00	0.00	0.00

Drill Path			Assumed Return Density		Low Return Density		High Return Density	
			Density, $\gamma_{FE} = 78$		Density, $\gamma_{FL} = 72$		Density, $\gamma_{FH} = 89$	
Rod Measured Distance MD	Station X	Elevation Y	Annular Fluid Pressure $P_A$	Annular Fluid Pressure $P_B$	Annular Fluid Pressure $P_A$	Annular Fluid Pressure $P_B$	Annular Fluid Pressure $P_A$	Annular Fluid Pressure $P_B$
ft	ft	ft	psi	psi	psi	psi	psi	psi
2235.71	21+99.28	553.94	0.00	0.00	0.00	0.00	0.00	0.00

**TABLE 4**  
**ESTIMATED FORMATION PRESSURE CURVE (FPC) EXAMPLE CALCULATION**  
 Sunoco Pipeline, L.P.  
 Mariner East Pipeline  
 Lebanon County, Pennsylvania



**WETLAND J47 - West to East R1**  
**20-INCH STEEL PIPE**  
**INPUT**

**1. Drill path data from vertical path calculations**

	Measured Distance	Elevations	Angles	Lengths	Angle Change
Entry	0.000 ft	527.4	-15	Entry to PC	306.205 ft
PC	306.205 ft			PC to PT	523.599 ft -0.029 deg/ft
PT	829.804 ft		0	Invert Tangent	441.733 ft
PC	1271.536 ft			PC to PT	670.206 ft 0.024 deg/ft
PT	1941.743 ft			PT to Exit	293.966 ft
Exit	<b>2235.709 ft</b>	554.00 ft	16	<b>2235.709 ft Length Ck</b>	<b>OK</b>

**2. Drill Fluid Hydraulic Data for Estimated Drill Fluid**

Dynamic annulus pressure =	0.00135 psi/LF
Uphole Drill Fluid Density =	78 10.4 lb/gal
Drill fluid viscosity, cp =	2 cp
Up hole drill fluid velocity, ft/sec =	68.29 ft/sec
Pump rate, gpm =	300 gal/min
Diameter of hole D <sub>H</sub> , in =	12.31125
Diameter of Drill Rod D <sub>R</sub> , in =	6.625
Yield point of drill fluid, lb/100 ft <sup>2</sup> =	41.00 Lb/100FT <sup>2</sup>

<b>Radius</b>
R <sub>H</sub> = 6.156 in
R <sub>R</sub> = 3.313 in

**3. Soil Profile Data**

Technical approach to generate data as no testing available

Material Layer	Dry Density γ (pcf)	Moisture Content %	Insitu Saturated Density (pcf)	Effective UW (pcf)	Phi, Φ	Undrained Cohesion c, psf	Poisson Ratio μ	Slow Shear Modulus, psf G	OCR Cohesive (Use 0 if non- cohesive)	Model Material Layer Description	Cohesive
1	110	15.0%	126.5	47.60 pcf	32	500	0.3	7,727	1	Sandy Silt	Y
2	130	10.0%	143	67.60 pcf	55	0.01	0.3	121,763	1	Sandstone	N
3								0			
4								0			
5								0			
6								0			
7								0			
8								0			
9								0			
10								0			
Water	62.4			62.40 pcf							

Dynamic Shear Velocity,  $V_s = 61.4 \cdot N_{60}^{1/2}$  Based on Seed and Idris approximation

Dynamic Shear Modulus,  $G_{max} = (\gamma'/g) \cdot V_s^2$

Extended Strain Shear Modulus G is typically between 5% and 20% of  $G_{max}$

g = acceleration of gravity = 32.2 ft/s<sup>2</sup>

Select Reduction Factor, RF = 10% Ref 1

165.36

**4 Select Controlling Location and list properties (Based on inspection of Figure 1 plot**

Joint = 9 Away Distance from Entry = 269.49 ft Depth of Cover = 52.13 ft

Layers	Surface 1-2	Surface 2-3	Surface 3-4	Surface 4-5	Surface 5-6	Surface 6-7	Surface 7-8	Surface 8-9	Surface 9-10	TOTAL
Soil Type in Layer =	1	2	2							
Dry Density in Layer, γ <sub>d</sub> =	110.00 pcf	130.00 pcf	130.00 pcf							
Insitu Density in Layer, γ <sub>s</sub> =	126.50 pcf	143.00 pcf	143.00 pcf							
Effective Weight in Layer, γ' <sub>e</sub> =	47.60 pcf	67.60 pcf	67.60 pcf							
Total Layer Thickness over drill, h <sub>s</sub> =	9.35 ft	42.78 ft	0.00 ft							52.13 ft
Saturated Thickness over drill, h <sub>sat</sub> =	0.00 ft	40.73 ft	0.00 ft	0.00 ft	0.00 ft	0.00 ft	0.00 ft	0.00 ft	0.00 ft	40.73 ft
Dry Thickness over drill, h <sub>dry</sub> =	9.35 ft	2.06 ft	0.00 ft	0.00 ft	0.00 ft	0.00 ft	0.00 ft	0.00 ft	0.00 ft	11.40 ft
Contribution Effective Stress, σ' =	1,028.17 psf	3,549.81 psf	0.00 psf							
Contribution Total Stress, σ = h <sub>s</sub> · γ <sub>s</sub>	1,028.17 psf	6,091.09 psf	0.00 psf							
Shear Modulus, G =	7,727 psf	121,763 psf	121,763 psf							
Height of Water above Soil Surface, h <sub>w</sub> =										0.00 ft
Total soil and water height above drill path, H <sub>T</sub> =										52.13 ft
Total water height above drill path, H <sub>w</sub> =										40.73 ft

**Properties At Drill Depth for Selected Joint**

R<sub>H</sub> = 0.51 ft Radius of drill hole  
 R<sub>max</sub> = h<sub>s</sub>/FS<sub>D</sub> = 34.75 ft Maximum allowable radius of plastic zone = Height of soil above Drill Path (h<sub>s</sub>) divided by Delft & Queens Equation FS<sub>D</sub>



	2	Soil Layer At Drill Depth
$G_w =$	121,763 psf	Large Strain Shear Modulus at drill depth
$S_u = c = q_u/2$	0 psf	Cohesive material: cohesion $c$ = unconfined compressive strength ( $q_u$ ) divided by 2
$\phi =$	55 deg	Granular Soil: Angle of internal friction of layer at drill path depth
$H_w =$	40.73 ft	Total water height above drill path
$FS_D =$	1.5	Factor of Safety for Delft & Queens Equation soil type: Use 1.5 for Sand and 2 for Clay at Drill Depth - Apply to $R_{max}$ and $P_{max}$
$\mu =$	0.3	Poisson ration of layer at drill path depth
OCR =	1	Over Consolidation Ratio
$K_o =$	0.429	Coefficient of lateral earth pressure at rest. For OCR = 1 use relation $K_o = \mu/(1 - \mu)$ ; For OCR >1 use $K_o = (K_{onormally\ consolidated}) * OCR^{1/2}$
$\sigma_o =$	7,119 psf	Total Stress at drill depth, $\sigma = \gamma_d(\text{above water}) * h_{dry} + \gamma_s(\text{saturated}) * h_{sat}$
$u =$	2,541 psf	Water pressure at drill depth, $u = \gamma_w * H_w$
$\sigma' =$	4,578 psf	Effective Stress at drill depth, $\sigma' = \sigma - u$

#### 5. Method A - Total Stress Method (Conservative)

Calculate Allowable Controlling Formation Pressure Capacity

$$P_{max} = \sigma_o = \Sigma (h_s * \gamma_s) + h_w * \gamma_w$$

$P_{maxA} =$	7,119 psf	49.44 psi
	49.44 psi	Check Calculation

#### 6. Method B - Total Stress Method + Local Formation Strength

Calculate Allowable Controlling Formation Pressure Capacity

$$P_{max} = \Sigma (h_s * \gamma_s) + h_w * \gamma_w + S$$

$P_{maxB} =$	13,657 psf	94.84 psi
	94.84 psi	Check Calculation

Based on Mohr-Coulomb

$$\text{Strength} = c + \sigma' * \tan(\phi)$$

6,538 psf	45.40 psi
-----------	-----------

#### 7. Method C - Delft Equation for cavity expansion (Assumes drained properties)

$$P_{max} = \mu + [p'_i + c * \cot \phi] * \{ [R_o/R_{pmax}]^2 + [(\sigma'_o * \sin \phi + c * \cos \phi) / G] \}^{-\sin \phi / (1 + \sin \phi)} - c * \cot(\phi)$$

$$\sin(\phi) = 0.819152$$

$$\cos(\phi) = 0.5735764$$

$$\cot(\phi) = 0.7002075$$

$$\mu = 0.3$$

$$\sigma'_o = 4,578 \text{ psf}$$

$$p'_i = 8,328 \text{ psf}$$

$$\text{Initial Pore Pressure, } \mu = \gamma_w * H_w$$

$$\text{Effective Stress, } \sigma'_o = \Sigma [ \gamma_d * h_d + \gamma' * h_s ]$$

$$p'_i = \sigma'_o(1 + \sin(\phi)) + c * \cos(\phi)$$

$$A = 8328.058502$$

$$B = 0.000217874$$

$$C = 0.030798182$$

$$D = -0.450293337$$

$$E = 0.007002075$$

$$\sigma' = 4,577.98$$

$$A = p'_i + c * \cot \phi$$

$$B = [R_o/R_{pmax}]^2$$

$$C = (\sigma'_o * \sin \phi + c * \cos \phi) / G$$

$$D = -\sin \phi / (1 + \sin \phi)$$

$$E = c * \cot \phi$$

$$\sigma' = 4,577.98$$

Checks
8328.058502
0.000217872
0.030798182
-0.450293337
0.007002075

$$P_{max} = 42,331 \text{ psf}$$

$$293.97 \text{ psi}$$

$$P_{max} = \mu + A * (B + C)^U - E$$

$$P_{allC} = 28,221 \text{ psf}$$

$$195.98 \text{ psi}$$

$$P_{all} = P_{max} / FS$$

$$42,331 \text{ psf}$$

$$\text{Check Calculation}$$

#### 8. Method D - Queens Equation (Cohesive Soils Only) better for softer clay soils

(Assumes undrained properties)

$$K_o < 1 \quad P_i = S_u + (1/2) * (3K_o - 1) * \sigma'_o - S_u * \ln[(R_o/R_{pmax})^2 + (S_u/G)]$$

$$K_o > 1 \quad P_i = S_u + (1/2) * (3 - K_o) * \sigma'_o - S_u * \ln[(R_o/R_{pmax})^2 + S_u/G]$$

To Determine if hydraulic fracturing or blowout occurs

(<2Su) indicates hydraulic fracturing; (>2Su) indicates blowout

$$K_o < 1 \quad F_1(K_o, \sigma'_o, S_u) = (3 * K_o - 1) * \sigma'_o$$

$$K_o > 1 \quad F_1(K_o, \sigma'_o, S_u) = (3 - K_o) * \sigma'_o$$

$$K_o = 0.429$$

$$P_i = 1,017 \text{ psf}$$

$$7.06 \text{ psi}$$

$$7.06 \text{ psi}$$

$$\text{Check Calculation}$$

$$F_1 = \text{Expect Blowout}$$

#### 9. SUMMARY and Assessment of Estimated Drilling Annular Pressure and Formation Capacity

(See Annular Pressure Calculations for joint by joint calculations)

##### Method A - (API RP) 13D

##### Method B - HDD Good Practices Cavity Expansion Annular Pressure

$$P_{annularA} = 39.49 \text{ psi}$$

$$P_A = [\gamma_f (Y_{entry} - Y)/144] + (P_d)(MD)$$

$$P_{annularB} = 49.19 \text{ psi}$$

$$P_B = [\gamma_f * (Y_{entry} - Y)/144] + MD * [u_p * V_{ha}/(1000 * (D_h - D_r)^2)] + YP/[200 * (D_h - D_r)]$$

$$\text{Method A} \quad 49.44 \text{ psi}$$

$$FS = 1$$

$$\text{Total Stress}$$

$$\text{Method B} \quad 94.84 \text{ psi}$$

$$FS = 1$$

$$\text{Total Stress + Strength}$$

$$\text{Method C} \quad 195.98 \text{ psi}$$

$$\text{At } FS_D = 1.5$$

$$\text{Delft Equation}$$

$$\text{Method D} \quad 7.06 \text{ psi}$$

$$\text{At } FS_D = 1.5$$

$$\text{Queens Equation}$$

##### Comparative Factor of Safety against Drill Fluid Loss at Critical Joint

$$\text{Critical Joint} = 9$$

$$\text{Depth of Cover} = 52.1 \text{ ft}$$

Confining Pressure Calculation Method	Method A	Method B	Method C	Method D
Method (X)/ $P_{annularA}$	1.25	2.40	4.96	0.18
Method (X)/ $P_{annularB}$	1.01	1.93	3.98	0.14

Acceptable if Factor of Safety >=1.0