Architecture
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An Employee-Owned Company

Erosion and Sediment Control Plans Narrative

Atlantic Sunrise Project
Phase 1

Compressor Station 605
Clinton Township
Wyoming County
Pennsylvania

Prepared For:

Transcontinental Gas Pipe Line Company, LLC
2800 Post Oak Blvd
Houston, TX, 77251

Issued: August 2015
Revised: October 2016

BL Project No. 14C4909

Prepared By:

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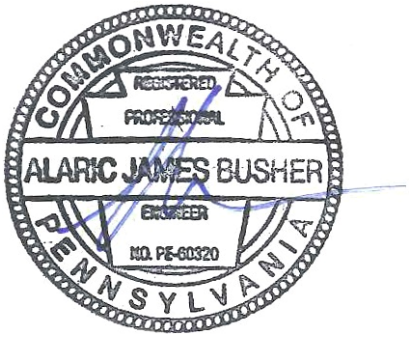

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APPENDICES

Appendix D United States Department of Agriculture (USDA) Natural Resources Conservation Service (NRCS) Custom Soil Resource Report

1.0 GENERAL INFORMATION

The following narrative was prepared as a supplement to the Transcontinental Gas Pipe Line Company, LLC's (Transco's) Environmental Construction Plan (ECP) provided in Section 4 of the Erosion and Sediment Control General Permit 2 (ESCGP-2) Notice of Intent (NOI), which was prepared for the Atlantic Sunrise Project ("Project"). This narrative is intended to describe the erosion and sediment control design for the proposed Compressor Station 605 ("Site") to be constructed as part of the Project, within Clinton Township, Wyoming County, Pennsylvania. Similar narratives were prepared, under separate cover, for facilities in other affected counties, as well as for the pipeline construction.

The facility proposed to be constructed as part of Phase 1 of the Atlantic Sunrise Project in Wyoming County is the following:

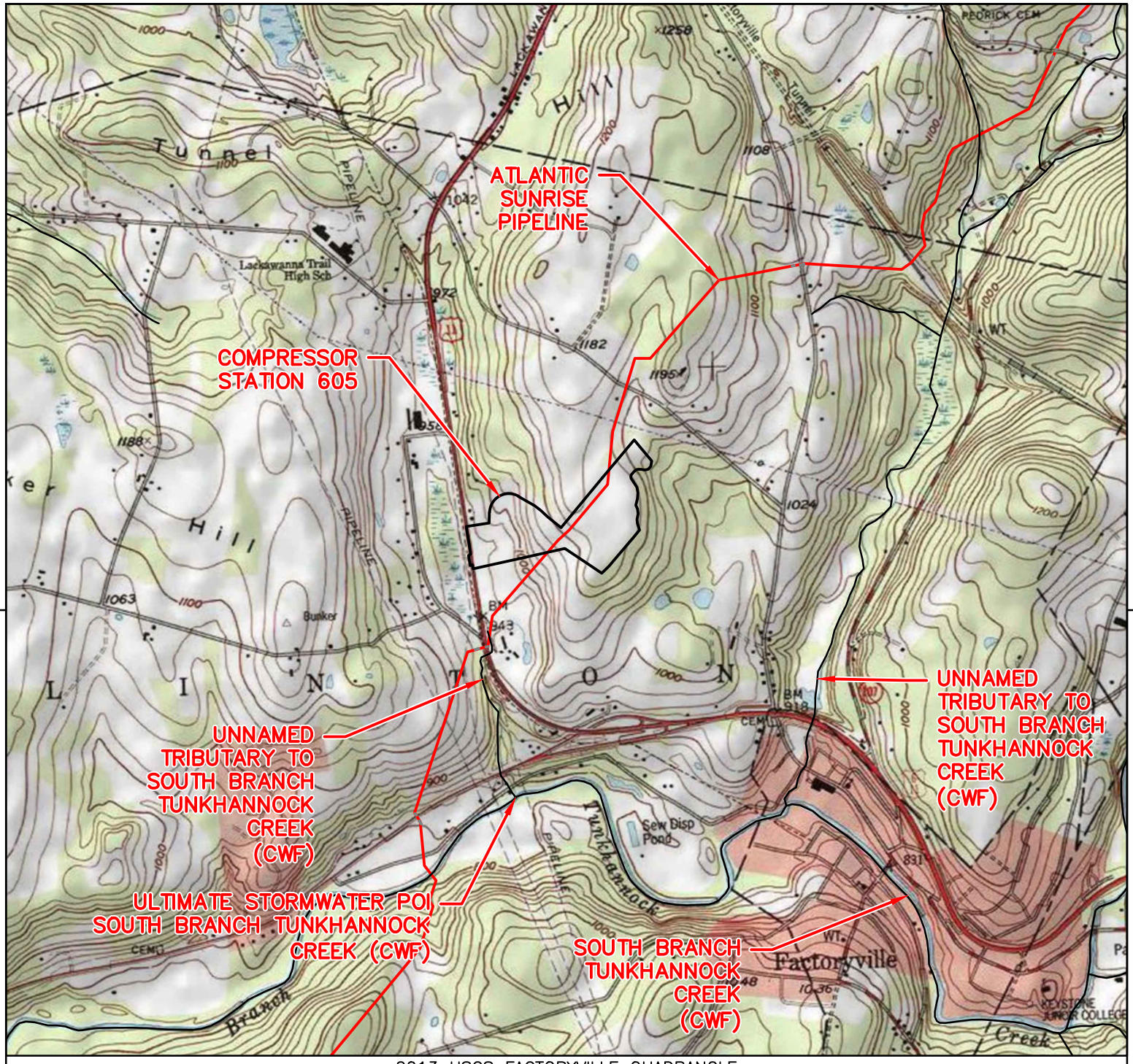
Facility Name	Facility Description	Facility Coordinates
Compressor Station 605	Compressor Station	N41°34'40.56", W75°47'48.39"

The Compressor Station 605 will be approximately 50.68 acres in area including a 3,100 linear foot new access road, 265,400 square feet (6.09 acres) of new gravel pad, and 172,510 square feet (3.96 acres) of impervious area. The Site will utilize existing public and private roads for access to the Site during and after construction. Best Management Practices (BMPs), in accordance with the standards and specifications in the Pennsylvania Department of Environmental Protection's (PADEP's) "Erosion and Sediment Pollution Control (E&S) Program Manual," Technical Guidance No. 363-2134-008, as amended and updated (E&S Manual) will be used during all phases of construction.

Refer to the ECP (**Section 4 of the ESCGP-2 NOI**) for overall Project information.

There are no impacts to regulated wetlands associated with this proposed Site. Refer to the Wetland Delineation Report provided in **Section 5 of the ESCGP-2 NOI** for information supporting wetland mapping as shown on the Erosion and Sediment Control (E&SC) Plans (**Section 2 of the ESCGP-2 NOI**).

1.1 Topographic Features



2013 USGS FACTORYVILLE QUADRANGLE

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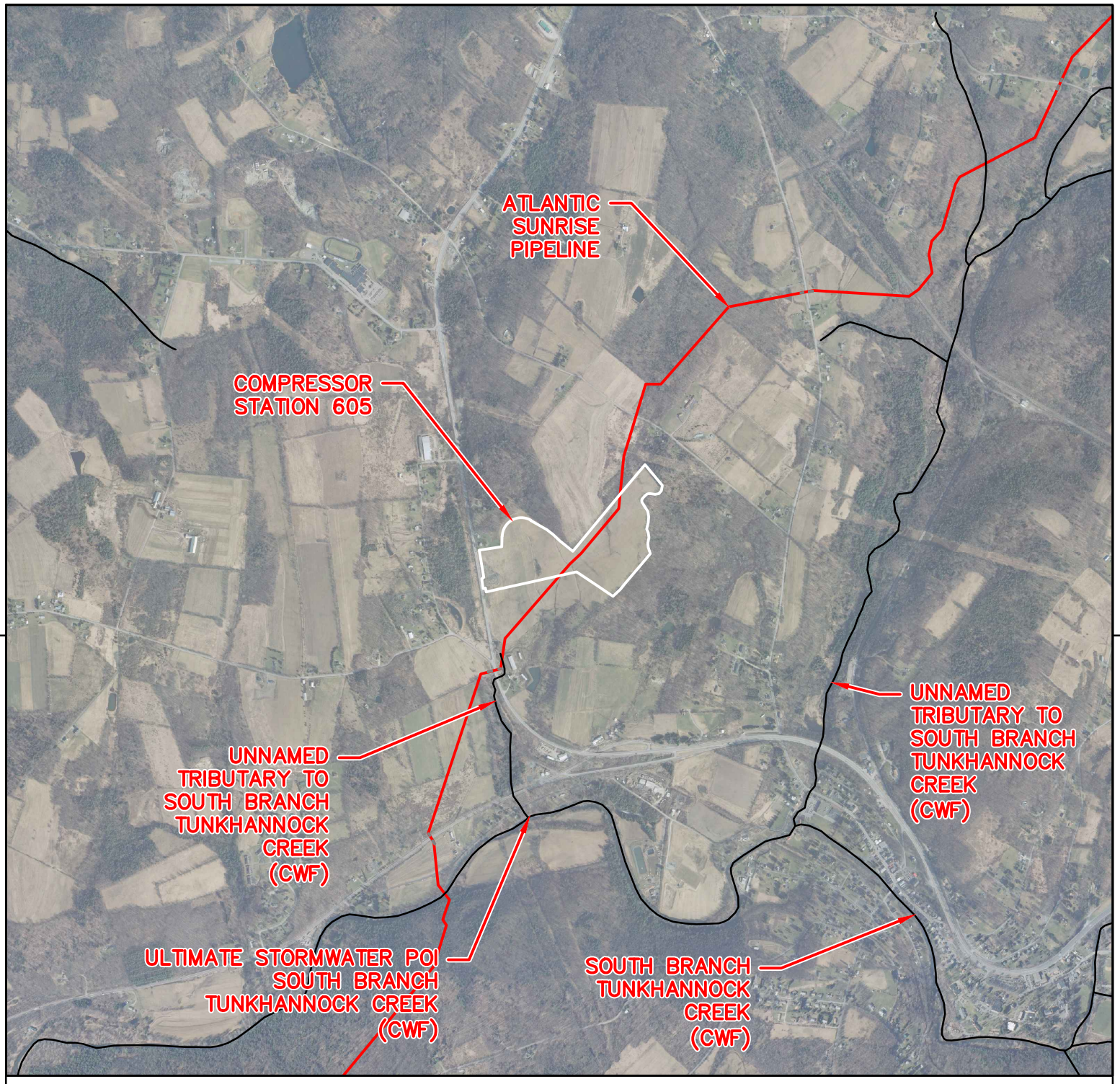
GRAPHIC SCALE
2000 1000 0 2000
SCALE IN FEET

ATLANTIC SUNRISE PROJECT
COMPRESSOR STATION 605
USGS LOCATION MAP
CLINTON TOWNSHIP
WYOMING COUNTY, PENNSYLVANIA

Williams

NO.	DATE	BY	REVISION DESCRIPTION	W.O. NO.	CHK.	APP.
0	08-28-15	BL	ISSUED FOR PADEP PERMIT SUBMITTAL	1161497	SMK	
1	12-02-15	BL	ISSUED FOR PADEP RESUBMITTAL	1161497	AJB	
2	09-01-16	BL	MOD 1 ISSUED FOR PADEP SUBMITTAL	1161481	AJB	
3	Oct. 2016	BL	PADEP TECHNICAL DEFICIENCY RESPONSE #1	1161481	AJB	

DRAWN BY: JEC	DATE: 04/03/15	ISSUED FOR BID:	SCALE: 1"=2,000'
CHECKED BY: AOE	DATE: 04/03/15	ISSUED FOR CONSTRUCTION:	
APPROVED BY: AJB	DATE: 04/03/15	DRAWING NUMBER: CS 605 LOCATION	SHEET 1 OF 1
WO: 1161497			



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GRAPHIC SCALE

2000 1000 0 2000

SCALE IN FEET

ATLANTIC SUNRISE PROJECT

COMPRESSOR STATION 605

AERIAL LOCATION MAP

CLINTON TOWNSHIP
WYOMING COUNTY, PENNSYLVANIA

Williams

NO.	DATE	BY	REVISION DESCRIPTION	W.O. NO.	CHK.	APP.
0	08-28-15	BL	ISSUED FOR PADEP PERMIT SUBMITTAL	1161497	SMK	
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APPROVED BY: AJB	DATE: 04/03/15	DRAWING NUMBER: CS 605 LOCATION	SHEET 1 OF 1
WO: 1161497			

1.2 Soil Characteristics

In addition to the below use limitations and resolutions, refer to Appendix D for the United States Department of Agriculture (USDA) Natural Resources Conservation Service (NRCS) Custom Soil Resource Report for the Site.

Soil Type and Use Limitations

Map Symbol	Soil Name	Slope	Cut Banks Cave	Corrosive to Concrete or Steel	Droughty	Easily Erodible	Flooding	High Water Table	Hydirc/Hydric Inclusions	Low Strength	Slow Percolation	Piping	Poor Source of Topsoil	Frost Action	Shrink-Swell	Potential Sinkhole	Ponding	Wetness
MsB	Morris very stony silt loam	0-8%	X	C/S	X	X		X	X	X	X		X	X				X
MsC	Morris channery silt loam	3-8%	X	C/S	X	X		X	X	X	X	X		X				X
MrB	Morris channery silt loam	3-8%	X	C/S	X	X		X	X	X	X	X		X				X
MrC	Morris flaggy silt loam	8-15%	X	C/S	X	X		X	X	X	X	X	X	X				X
NcB	Norwich and Chippewa soils	3-8%	X	C/S	X	X		X	X	X	X		X	X			X	X
OcC	Oquaga channery loam	8-15%	X	C	X	X			X		X			X				
OcD	Oquaga channery loam	15-25%	X	C/S	X	X			X		X			X			X	X
OfB	Oquaga flaggy loam	3-8%	X	C/S	X	X			X		X			X			X	X
WcB	Wellsboro channery loam	8-15%	X	C/S	X	X		X	X	X	X	X		X				X
WcD	Wellsboro channery loam	15-25%	X	C/S	X	X		X	X	X	X	X		X				X

Source: Appendix E, Table E-1, PADEP, *Erosion and Sediment Pollution Control (E&S) Program Manual* Technical Guidance Number 363-2134-008.

Soil Use Limitations Resolutions

Limitation	Resolution
Cut Banks Cave	Excavations will be properly supported by sheeting and shoring to prevent caves.
Corrosive to Concrete or Steel	No concrete or steel piping is proposed without appropriate coatings and protection.
Droughty	Existing suitable topsoil and soil amendments will be used during construction.
Easily Erodible	Temporary and permanent erosion control BMPs will be employed throughout the Site.
Flooding	Ensure that the Site has proper drainage.
High Water Table	A geotechnical investigation was conducted to minimize conflicts with saturated zones.
Hydric/Hydric Inclusions	A wetland investigation was completed to determine no wetlands are present in the development area.
Low Strength	A maximum of 3:1 slopes are proposed.
Slow Percolation	A field investigation of percolation rates at the infiltration areas was performed to verify the soils percolation capacity.
Piping	Watertight pipe, antiseep collars, clay cores through basin berms, and concrete endwalls will be used to minimize the danger of piping.
Poor Source of Topsoil	Existing topsoil, which has proven to be suitable, will be reused on the Site.
Frost Action	Pavement subbase will be provided to minimize frost effects.
Shrink-Swell	Stone base will be provided to prevent shrink-swell from effecting pavement.
Potential Sinkhole	Geotechnical engineer of record recommendations will be followed for any potential occurrences.
Ponding	Surface grading and drainage facilities will be provided to minimize ponding affects.
Wetness	Wet weather construction recommendations, per the geotechnical engineer's recommendations, will be employed to minimize the effects of wetness during construction, surface grading. Surface grading and drainage will be provided to minimize wetness affects after construction.

1.3 Earth Disturbance Activity

Proposed Improvements and Land Use

The proposed Compressor Station 605 will be constructed in Clinton Township, Wyoming County, Pennsylvania. Compressor Station 605 will involve the construction of a natural gas compressor station. The earthmoving activity will involve the stripping and stockpiling of top soil, Site grading, Site excavation, placement of fill, trenching and backfill, construction of buildings and equipment with gravel pad/parking lot, construction of an asphalt access drive, construction of a stormwater management system, finish grading, and stabilization of disturbed surfaces stormwater management system, finish grading, and stabilization of disturbed surfaces. Approximately 172,510 square feet (3.96 acres) of additional impervious area and 265,400 square feet (6.09 acres) of additional gravel surface will result on-site. Areas outside the Site limit of disturbance (LOD) may be used for staging of equipment and materials, but no earth disturbance will occur in these areas.

Present/Past Land Use

This section identifies the land requirements for construction and operation of the proposed CPL North, CPL South, and Associated Facilities. Table 1.3.1 summarizes the land requirements for the proposed Compressor Station 605 associated with the CPL North and CPL South mainlines.

The characterization of land use within the proposed CPL North, CPL South, and Associated Facilities project areas is based on interpretation of aerial photographs taken in the spring of 2014 and information gathered from field surveys conducted during 2014 and 2015. Transco classified land uses within the proposed CPL North, CPL South, and Associated Facilities project areas into the following eight broad types:

- Agricultural Land – land associated with active cultivation of row and field crops; areas of grasses planted for livestock grazing or for the production of hay crops; orchards; and specialty crops, including vineyards, Christmas trees, and fruits and vegetables.

- Upland Forest/Woodland – includes upland deciduous forest, evergreen forest, and mixed (deciduous and evergreen) forest, but does not include forested wetlands.

- Industrial/Commercial Land – land used for mines or quarries and associated processing plants; manufacturing or other industrial facilities; and land developed

for commercial or retail uses, including malls, strip plazas, business parks, and medical facilities.

- Transportation Land – land used for transportation purposes, including interstate highways; state, county, and local highways and roads; and railroad lines.
- Residential Land – residential areas, including yards of individual residences.
- Open Land – non-forested and undeveloped land not classified for another use, including land maintained as utility ROWs for overhead and underground electric transmission, natural gas transmission, and oil transmission facilities.
- Wetlands – includes wetlands covered with emergent, scrub-shrub, and forested vegetation.
- Open Water – include rivers, streams, creeks, canals, and other linear waterbodies, as well as lakes, ponds, and other non-flowing waterbodies.

New MLVs will be wholly located within the permanent ROWs for the proposed CPL North and CPL South mainlines. Construction will primarily occur within the proposed CPL North and CPL South construction ROWs.

Table 1.3.1
Land Requirements for the New Aboveground Facilities[a]

Facility	Milepost	County	Agricultural Land (acres)		Upland Forest / Woodland (acres)		Open Land (acres)		Total (acres)	
			Cons	Op	Cons	Op	Cons	Op	Cons	Op
New Compressor Station 605	CPL North 44.9	Wyoming	45.0	36.0	5.1	3.2	0.0	0.0	50.1	39.2
Compressor Station 605 Subtotal			**45.0**	**36.0**	**5.1**	**3.2**	**0.0**	**0.0**	**50.1**	**39.2**

Notes:
[a] Land use acreages for construction and operation are provided for reference only. Acreages provided were calculated by using kmz files and prepared as part of the June 8, 2015 FERC Supplement. Refer to plans and ESCGP-2 NOI for actual site conditions.

Key:
Cons = Construction
L = Leidy Line system milepost
Op = Operation

1.4 Project Site Runoff

Runoff rate calculations have been performed for the Site and its upstream watershed area.

Runoff Rate Summary Table

STORM EVENT	POINT OF INTEREST A			POINT OF INTEREST B			POINT OF INTEREST C		
	PRE (CFS)	POST (CFS)	REDUCTION (CFS)	PRE (CFS)	POST (CFS)	REDUCTION (CFS)	PRE (CFS)	POST (CFS)	REDUCTION (CFS)
1-yr	22.95	20.73	2.22	25.77	25.57	0.20	79.40	77.71	1.69
2-yr	35.73	32.75	2.98	40.04	39.67	0.37	123.66	121.03	2.63
5-yr	55.79	51.43	4.36	62.23	61.54	0.69	192.98	188.88	4.10
10-yr	72.72	67.87	4.85	80.90	79.85	1.05	252.17	246.80	5.37
25-yr	98.04	93.83	4.21	108.36	106.38	1.98	340.76	333.51	7.25
50-yr	119.71	114.92	4.79	131.35	128.12	3.23	417.04	408.16	8.88
100-yr	143.36	139.06	4.30	156.60	152.21	4.39	500.28	489.64	10.64

*****See the Post Construction Stormwater Management (PCSM/SR) Narrative for additional rate and volume calculations, as provided in Appendix A, of the PCSM/SR Narrative.

1.5 Surface Water Classification

The E&SC drawings in **Section 2 of the ESCGP-2 NOI** depict the locations of the streams and wetlands in and near the LOD for the Site. The Site area surface water runoff drains to South Branch Tunkhannock Creek, which is not a High Quality (HQ) or Exceptional Value (EV) stream. The receiving waters are designated as Cold Water Fishery (CWF) under PA Code 25 Chapter 93. The Site's watershed is not listed as impaired in the PADEP Integrated List.

1.6 BMP Description Narrative

E&SC BMPs, consistent with the PADEP E&S Manual are planned to be used at the Site before, during, and after earth disturbance activities. Perimeter and onsite E&SC BMPs will be installed prior to any disturbance of areas tributary to the E&SC BMPs. Installation and maintenance guidelines, as well as E&SC BMP locations are as shown

on the E&SC Plans and Detail Sheets (**Section 2 of the ESCGP-2 NOI**). The E&SC BMPs that will be used on Compressor Station 605 include the following:

Temporary E&SC BMPs

- Rock Construction Entrances: A Rock Construction Entrance (RCE) is a method of stabilizing a temporary construction entrance to the Site from a paved roadway by placement of AASHTO #1 Stone. RCEs will be placed at all entrances to the Project area.

- Sediment Basins: Sediment basins will be used for drainage areas greater than 5.0 acres. Upon Site stabilization, the basins shall be removed along with any unsuitable material, and the area restored or converted to final grades.

- Temporary Vegetated Channels: Vegetated Channels may be temporary or permanent. Channels may be designed to convey clean water around disturbed areas or may be designed to convey sediment-laden water to sediment removal BMPs. Upon Site stabilization, temporary channels shall be removed along with any unsuitable material, and the area restored or converted to final grades. Permanent channels will remain in place and be part of the final Post Construction Stormwater Management (PCSM) design.

- Rock Filter Outlets: Rock Filter Outlets (RFOs) may be used to control runoff; they may also be used below construction work while flow is being diverted past the work area. RFOs may be used to control sediment either during construction or during temporary disturbance. RFOs should be constructed according to the specifications shown in the Standard Detail Sheets. RFOs should be inspected weekly and needed repairs should be initiated within 72 hours after inspection. Anchored compost layer shall be used on upslope face in HQ and EV watersheds.

- Pumped Water Filter Bag: Sediment laden water that collects during excavation is required to be pumped from the excavation and shall be treated in a sediment pumped water filter bag. The Contractor and Environmental Inspector will dictate the location and placement of the bag. The Contractor and Environmental Inspector must meet PADEP requirements and the manufacturer's recommendations for use.

- Compost Filter Sock: Compost Filter Sock (CFS) is a sediment barrier consisting of a mesh sock and coarse compost. CFS will be placed to control runoff and collect sedementation. CFS is Antidegradation Best Available Combination of Technologies (ABACT) for HQ and EV watersheds.

- Orange Construction Fence: Orange construction fence shall be installed at the limits of all streams, wetlands, stormwater management facilities, and public roads to be protected from construction vehicle access. Upon Site stabilization or conversion of stormwater management facilities to permanent conditions, the fences shall be removed.

- Erosion Control Blanket: Erosion Control Blanket (ECB) is a soil covering made from straw, coir, excelsior, or synthetic material used to minimize the potential for erosion of an exposed soil until a suitable vegetative cover can be established. It will be placed in the Project area within 50 feet of streams and wetlands, as well as in the Site area where a slope greater than 3:1 exists (unless located in an agricultural area).

- Hydraulically Applied Erosion Control Blanket: A Hydraulically Applied ECB is Bonded Fiber Matrix (BFM) that can be used in place of ECBs where necessary. For slopes up to 3H:1V, the BFM will be applied at a rate of 3,000 pounds per acre. Slopes steeper than 3H:1V will need to be applied at a rate of 4,000 pounds per acre. In any case, manufacturer's recommendations should be followed.

- Temporary Vegetative Stabilization: Upon temporary cessation of an earth disturbance activity or any stage or phase of an activity where cessation of earth disturbance activities will exceed four days, the Site shall be immediately seeded, mulched, or otherwise protected from accelerated erosion.

Permanent E&SC BMPs

- Infiltration Basins: Depending on Site soils conditions, infiltration basins or extended detention basins may be proposed. Basins will promote suspended solid removal, as well as nutrient pollutant removal. Upon Site stabilization, the basin areas will be prepared and converted to final grades and be part of the permanent PCSM design.

- Permanent Vegetated Channels: Vegetated Channels may be temporary or permanent. Channels may be designed to convey clean water around disturbed areas or may be designed to convey sediment-laden water to sediment removal

BMPs. Upon Site stabilization, temporary channels shall be removed along with any unsuitable material, and the area restored or converted to final grades. Permanent channels will remain in place and be part of the final PCSM design.

- Rock Filters: Rock Filters will be installed as shown on the Plan Drawings and according to the Standard Detail Sheets. Rock Filters help dissipate energy from the concentrated flow in roadside ditches and channels to prevent erosion of the channel and at the outlet. Rock Filters may be used in HQ watersheds if a 6" layer of compost is layered on the upgradient side.

- Riprap Aprons / Outlet Protection: Outlet Protection shall be installed as shown on Plan Drawings and according to the Standard Detail Sheets. Outlet Protection will help dissipate energy from flow concentrated through culverts.

- Permanent Vegetative Stabilization: Upon reaching final grades, and upon cessation of earth disturbance activities, disturbed areas will receive topsoil, seed, and mulch to establish permanent vegetative stabilization.

1.7 BMP Installation Sequence Narrative

Refer to the E&SC Plans (as provided in **Section 2 of the ESCGP-2 NOI**) for the location of the proposed work and the associated E&SC BMPs. Necessary parts for proper and complete execution of work pertaining to this sequence, whether specifically mentioned or not, are to be performed by the Contractor. It is not intended that the drawings and this E&SC narrative show every detailed piece of material or equipment. The Contractor shall comply with all requirements listed in this Section 1.7. The Contractor may be required to alter controls based on effectiveness of controls or differing conditions encountered in the field.

1. At least 7 days prior to starting any earth disturbance activities, including clearing and grubbing, the owner and/or operator shall invite all contractors, Environmental Inspectors, the landowner, appropriate municipal officials, the E&S plan preparer, the PCSM plan preparer, the licensed professional responsible for oversight of critical stages of implementation of the PCSM plan, and a representative from the local conservation district to an on-site preconstruction meeting.

2. At least 3 days prior to starting any earth disturbance activities, or expanding into an area previously unmarked, the Pennsylvania One Call System Inc. shall be notified at 1-800-242-1776 for the location of existing underground utilities.

3. Hold pre-construction conference with the Environmental Inspectors, local County Conservation District (CCD), PADEP, and Design Engineer.

4. Install orange construction fence around areas to be protected.

5. Locate staging areas and access points including construction entrances. Field locate limits of disturbance.

6. Install rock construction entrances (RCEs).

7. Remove brush to effectively install perimeter controls, level side cuts to grant access for vehicles and workers to safely perform the installation of sediment barriers on the Site as shown on the construction drawings.

8. The Compliance Manager shall provide PADEP and CCD at least three days' notice prior to bulk earth disturbance and upon completed installation of perimeter erosion controls.

9. * Install sediment basin, including clay core, antiseep collars, slope liners, cleanout stake, and associated improvements.

10. Install vegetated roadside swales, culverts and riprap outlet protection. Rough grade access roads.

11. Upon grading Infiltration Basin 2, install orange construction fence to prevent damage. Do not install OS 2. Install compost filter socks at interior toe of slope to minimize siltation of basin bottom.

12. * Install drainage channel aprons as soon as swale grading is complete.

13. Begin construction staking for grading.

14. Begin grading and strip and stockpile topsoil within the area of improvements and install sediment barriers around stockpiles.

15. Upon temporary cessation of an earth disturbance activity or any stage of an activity where the cessation of earth disturbance activities will exceed four days, the Site shall be immediately seeded, mulched, or otherwise protected from accelerated erosion and sedimentation pending future earth disturbance activities.

For an earth disturbance activity or any stage of an activity to be considered temporarily stabilized, the disturbed areas shall be covered with one of the following: A minimum uniform coverage of mulch and seed, with a density capable of resisting accelerated erosion and sedimentation, or an acceptable BMP which temporarily minimizes accelerated erosion and sedimentation. Temporary stabilization will not occur on active vehicular travel ways within the ROW. The on-Site environmental inspector will log daily activity within the LOD and notify the Contractor of areas requiring temporary stabilization (i.e., areas where work has ceased for at least four days).

16. Grade the compressor station pads, including stormwater runoff conveyance features as shown on the E&SC and PCSM/SR Plans (**Sections 2 and 3 of the ESCGP-2 NOI**).

17. Immediately stabilize side slopes with erosion control matting when slopes are 3:1 or greater. See PCSM/SR Plans and Detail Sheets, as provided in **Section 3 of the ESCGP-2 NOI**, (patterns differ by slope category). Install rip rap slope stabilization where shown on the PCSM/SR Plans.

18. Establish final grade.

19. Surface Stabilization, apply permanent stabilization measures immediately to any disturbed areas where work has reached final grade.

20. Upon completion of all earthwork activities and permanent stabilization of all disturbed areas, the Owner and/or Operators shall contact the local CCD for an inspection prior to the removal/conversion of the E&SC BMPs.

21. * After all upslope disturbed areas are stabilized, convert sediment basin to proposed stormwater management basin 1 including infiltration berms and amended soils.

22. * Install OS-2. Install amended soils. Reinstall compost filter sock in interior toe of slope to protect amended soil from siltation.

23. After finish grading and topsoil placement is completed, disturbed areas shall be fertilized, seeded, and mulched. Seed mixtures, fertilizer and mulch applications rates and dates shall conform to the tables provided on the PCSM/SR Plans and Detail Sheets (**Section 3 of the ESCGP-2 NOI**), land owner agreements and/or the **ECP** (**Section 4 of the ESCGP-2 NOI**).

24. After seeding, fertilizing and mulching is complete, install ECBs as required or ordered or on slopes of than 3:1 or greater.

25. After the Site is permanently stabilized and upon PADEP or local CCD and Owner approval of stabilization and re-vegetation, remove temporary erosion and sediment control measures and stabilize areas disturbed by removal.

26. * Complete Site stabilization, including soil amendment, seed application, ECB installing in basin, and mulching.

27. Upon completion of all earth disturbance activities and permanent stabilization of all disturbed areas, the Owner and/or Operators shall contact the local CCD for a final inspection.

28. Maintain E&SC BMPs until Site work is complete and uniform 70% perennial vegetative cover is established.

29. Remove and properly dispose/recycle E&SC BMPs. Remove orange construction fence. Repair and permanently stabilize areas disturbed during E&SC BMP removal upon establishment of uniform 70% vegetative cover.

*** indicates a critical stage of PCSM installation to be observed by a licensed professional or designee. Contractor to provide three working days' notice to Design Engineer.**

1.8 Supporting Calculations and Measurements

Supporting calculations are provided in Appendix A.

1.9 Plan Drawings

E&SC Plan Drawings are included in **Section 2 of the ESCGP-2 NOI**.

1.10 Maintenance Program

E&SC BMPs shall be maintained properly throughout the construction of the Site. The following inspection and maintenance shall be implemented to maintain E&SC BMPs.

- Maintenance and inspection of E&SC BMPs shall conform to the following:

- Federal Energy Regulatory Commission (FERC) regulations, Attachment 17 of the **ECP** as provided in **Section 4 of the ESCGP-2 NOI**;
- Transco's Project-specific Upland Erosion Control, Revegetation, and Maintenance Plan (Transco Plan) included as **Attachment 17 of the ECP** as provided in **Section 4 of the ESCGP-2 NOI**;
- Transco's Project-specific Wetland and Waterbody Construction and Mitigation Procedures, and Procedures (Transco Procedures) included as **Attachment 18 of the ECP** as provided in **Section 4 of the ESCGP-2 NOI**; and
- PA Code Chapter 102 and 105 regulations, including all conditions of the ESCGP-2.

- Until the Site is stabilized, all E&SC BMPs shall be maintained properly. Maintenance shall include inspections of all E&SC BMPs after each runoff event and on a weekly basis. All preventative and remedial maintenance work, including clean out, repair, replacement, regrading, reseeding, remulching and renetting must be initiated immediately. If the E&SC BMPs fail to perform as expected, replacement E&SC BMPs, or modifications of those installed will be required.

- Immediately upon discovering unforeseen circumstances posing the potential for accelerated erosion and/or sediment pollution, the Operator shall implement appropriate E&SC BMPs to minimize the potential for erosion and sediment pollution and notify the local CCD and/or the regional office of the PADEP.

- A log showing dates that E&SC BMPs were inspected as well as any deficiencies found and the date they were corrected shall be maintained with the Environmental Inspector's records on the Site and be made available to regulatory agency officials at the time of inspection.

- The reviewing agency (PADEP or local CCD) shall be notified of any changes to the approved E&SC Plan prior to implementation of those changes. The reviewing agency may require a written submittal of those changes for review and approval at its discretion.

- Refer to E&SC BMP Detail Sheets for inspection and maintenance procedures specific to each E&SC BMP (See **Section 2 of the ESCGP-2 NOI**).

- Sediment removed from E&SC BMPs shall be properly disposed of off-site or placed on-site up gradient of E&SC BMPs.

- All Site entrance and exit points will be inspected on a daily basis for evidence of off-site tracking of mud. The Contractor shall clean streets and roads of mud and/or dust and keep the streets and roads in a clean and dust-free condition.

- Access road gravel thickness shall be constantly maintained. A stockpile shall be maintained on-site for this purpose.

- E&SC BMPs shall remain functional as such until all areas tributary to them are permanently stabilized or until they are replaced by another E&SC BMP approved by the local CCD or PADEP.
- Permanent stabilization is defined as a minimum uniform, perennial 70 percent vegetative cover or other permanent non-vegetative cover with a density sufficient to resist accelerated erosion. Cut and fill slopes shall be capable of resisting failure due to slumping, sliding, or other movements. Any area not achieving a minimum uniform 70 percent perennial vegetative cover shall be reseeded and mulched within 24 hours of detection.

1.11 Material Recycling and Disposal

Transco has prepared a Spill Plan for Oil and Hazardous Materials to assist in prevention of any spills that may occur at the Site and to respond to any spills that do occur. The Contractor will be required to become familiar with the Spill Plan for Oil and Hazardous Materials and its contents prior to commencing any construction-related activities. The Spill Plan for Oil and Hazardous Materials is included as **Attachment 9 to the ECP** provided as **Section 4 of the ESCGP-2 NOI**.

Contractors are required to inventory and manage their construction site materials. The goal is to be aware of the materials on-site; ensure they are properly maintained, used, and disposed of; and to make sure the materials are not exposed to stormwater.

Materials Covered

The following materials or substances are expected to be present on-site during construction **(Note: this list is not an all-inclusive list and the Materials Management Practices can be modified to address additional materials used on-site)**:

- Acids
- Detergents
- Fertilizers (nitrogen/phosphorus)

- Hydroseeding mixtures
- Petroleum based products
- Sanitary wastes
- Soil stabilization additives
- Solder
- Solvents
- Other

These materials must be stored as appropriate and shall not contact storm or non-stormwater discharges. Contractor shall provide a weather proof container to store chemicals or erodible substances that must be kept on the Site. Contractor is responsible for reading, maintaining, and making employees and subcontractors aware of safety data sheets (SDSs).

Material Management Practices

The following are material management practices that will be used to reduce the risk of spills or other accidental exposure of materials and substances to stormwater runoff.

1. Good Housekeeping Practices

   The following good housekeeping practices will be followed on Site during construction:

   - Store only enough material required to do the job.
   - Store materials in a neat, orderly manner.
   - Store chemicals in watertight containers or in a storage shed, under a roof, completely enclosed, with appropriate secondary containment to prevent spill or leakage. Drip pans shall be provided under dispensers.
   - Substances will not be mixed with one another unless recommended by the Manufacturer.
   - Manufacturer's recommendations for proper use and disposal will be followed.
   - Inspections will be performed to ensure proper use and disposal of materials.

- Cover and berm loose stockpiled construction materials that are not actively being used (i.e. Soil, spoils, aggregate, etc.).

- Minimize exposure of construction materials to precipitation.

- Minimize the potential for off-site tracking of loose construction and landscape materials.

2. Hazardous Products

These practices will be used to reduce the risks associated with hazardous materials. SDSs for each substance with hazardous properties that is used on the job site(s) will be obtained and used for the proper management of potential wastes that may result from these products. A SDS will be posted in the immediate area where such product is stored and/or used and another copy of each SDS will be maintained in a file at the job site construction trailer office. Each employee, who must handle a substance with hazardous properties, will be instructed on the use of SDS and the specific information in the applicable SDS for the product he/she is using, particularly regarding spill control techniques.

- Products will be kept in original containers with the original labels in legible condition.

- Original labels and SDSs will be produced and used for each material.

- If surplus product must be disposed of, manufacturers or local/state/federal recommended methods for proper disposal will be followed.

3. Hazardous Wastes

All hazardous waste materials will be disposed of by the Contractor in the manner specified by local, state, and/or federal regulations and by the manufacturer of such products. Site personnel will be instructed.

4. Concrete and Other Wash Waters

Prevent disposal of rinse, wash waters, or materials on impervious or pervious surfaces, into streams, wetlands or other water bodies.

Concrete trucks will be allowed to wash out or discharge surplus concrete or drum wash water on the Site, but only in either (1) specifically designated diked areas which have been prepared to prevent contact between the concrete and/or washout and soil and stormwater having the potential to be discharged from the Site; or (2) in locations where waste concrete can be poured into forms to make riprap or other useful concrete products.

The hardened residue from the concrete washout diked areas will be disposed of in the same manner as other non-hazardous construction waste materials or may be broken up and used on the Site as deemed appropriate by the Contractor and Owner or Owner's representative. The Contractor will be responsible for seeing that these procedures are followed.

All concrete washout areas will be located in an area where the likelihood of the area contributing to stormwater discharge is negligible. If required, additional E&SC BMPs must be implemented to prevent concrete wastes from contributing to stormwater discharges. The location of the concrete washout area(s) must be identified, by the Contractor/Job Site Superintendent, on the job site copy of the E&SC Plans (**Section 2 of the ESCGP-2 NOI**) and in this E&SC Narrative.

5. Sanitary Wastes

All sanitary waste units will be located in an area where the likelihood of the unit contributing to stormwater discharges is negligible. Additional E&SC BMPs must be implemented, such as containment trays (provided by the rental company) or special containment created with 2" x 4" lumber, impervious plastic, and gravel. The location of the sanitary waste units must be identified on the job site copy of the E&SC Plans (**Section 2 of the ESCGP-2 NOI**), in this E&SC Narrative, by the Contractor/Job Site Superintendent.

6. Solid and Construction Wastes

All waste materials will be collected and stored in a securely lidded metal dumpster. The dumpster will comply with all local and state solid waste management regulations. The dumpster/container lids shall be closed at the end of every business day and during rain events. Appropriate measures shall be taken to prevent discharges from waste disposal containers to the receiving water.

7. Construction Access

A stabilized construction exit will be provided to help reduce vehicle tracking of sediments. The paved roads adjacent to the Site entrance will be inspected daily and swept as necessary to remove any excess mud, dirt, or rock tracked from the Site. Dump trucks hauling material from the construction site will be covered with a tarpaulin as necessary.

8. Petroleum Products

On-site vehicles will be monitored for leaks and receive regular preventative maintenance. Petroleum products will be stored in tightly sealed containers which are clearly labeled. Petroleum storage tanks on-site will have a dike or berm containment structure constructed around it to contain spills which may occur (containment volume to be 110% of volume stored). The dike or bermed area shall be lined with an impervious material such as a heavy duty plastic sheet. Drip pans shall be provided for all dispensers. Any asphalt substances used on the Site will be applied according to the manufacturer's recommendations.

9. Fertilizers and Landscape Materials

Fertilizers will be applied only in the minimum amounts recommended by the manufacturer. Once applied, fertilizer will be worked into the soil to minimize the potential for exposure to stormwater. Storage will be under cover. The contents of any partially used bags of fertilizer will be transferred to a sealable plastic bin to minimize the potential for spills. The bin shall be labeled appropriately.

Contain stockpiled materials, such as but not limited to, mulches, top soil, rocks and gravel, and decomposed granite, when they are not actively being used.

Apply erodible landscape material at quantities and application rates according to the manufacturer’s recommendations or based on written specifications by knowledgeable and experienced field personnel. Discontinue the application of any erodible landscape material within two days prior to a forecasted rain event or during periods of precipitation.

10. Paints, Paint Solvents and Cleaning Solvents

Containers will be tightly sealed and stored when not in use. Excess paint and solvents will be properly disposed of according to the manufacturer's recommendations or local, state, and/or federal regulations.

11. Contaminated Soils

    Any contaminated soils (resulting from spills of materials with hazardous properties) which may result from construction activities will be contained and cleaned up immediately in accordance with applicable local, state and federal regulations.

1.12 Soil Conditions and Geologic Formations

There are no naturally occurring geologic formations or soils on-site are expected that may have the potential to cause pollution during earth disturbance activities. See E&SC Detail Sheets (**Section 2 of the ESCGP-2 NOI**) for Acid-Producing Soils and Bedrock Control Plan should any unexpected acid runoff producing soils be encountered.

1.13 Thermal Impacts

Thermal impacts associated with CPL North, CPL South, and Associated Facilities will be avoided to the maximum extent practicable. The following provisions related to thermal impacts are included in the **E&SC Plan** within **Section 2 of the ESCGP-2 NOI**:

- The minimum permanent changes in land cover, necessary to construct the required facilities are being proposed.

- Runoff from the permanent impervious areas will be collected as part of the Post Construction Stormwater Management/Site Restoration (PCSM/SR) Plan and routed to PCSM/SR BMPs. In addition, impervious areas will be gravel instead of asphalt wherever practical.

- PCSM/SR BMPs incorporate the use of infiltration facilities such as basins and vegetated swales with Rock Filter Check Dams.

- The removal of vegetation, especially tree cover, will be limited to only that necessary for construction.

- The amount of impervious surfaces will be limited to only that necessary to support the construction of CPL North, CPL South, and Associated Facilities and/or operation of the pipeline.
- The impacts to existing riparian corridors will be limited to only that necessary for construction.

1.14 E&S Plan and PCSM/SR Plan Consistency

The E&SC Plans and Narrative have been designed and will be constructed to be consistent with the PCSM/SR Plans. Following completion of construction, disturbed areas shall be stabilized and the long-term maintenance of the PCSM/SR BMPs will begin.

1.15 Riparian Forest Buffers

There are no regulated riparian buffers within the Site area.

1.16 Antidegradation Requirements

The Site is not located in a special protection or siltation impaired watershed; therefore, no antidegradation analysis is necessary.

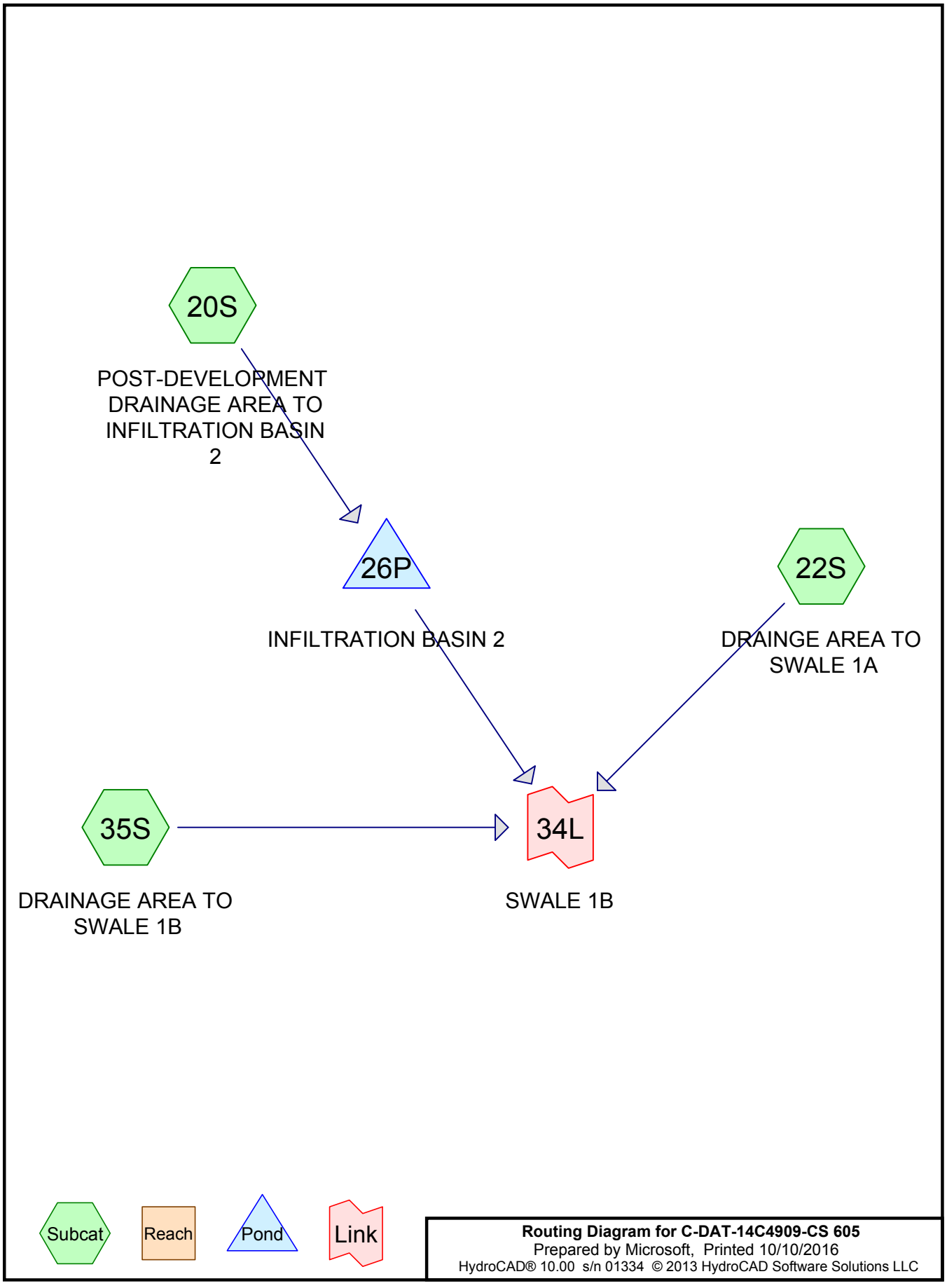
APPENDICES

Appendix A	Compressor Station 605 Supporting Calculations
	A.1 Swale Calculations A.2 Culvert Calculations A.3 Sediment Basin Calculations A.4 Sediment Barrier Table A.5 Supporting Information
Appendix B	Preparer Qualifications
Appendix C	Site Characterization Assessment
Appendix D	United States Department of Agriculture (USDA) Natural Resources Conservation Service (NRCS) Custom Soil Resource Report

APPENDIX A

Compressor Station 605 Supporting Calculations

A.1 Swale Calculations



Routing Diagram for C-DAT-14C4909-CS 605
Prepared by Microsoft, Printed 10/10/2016

E&S WORKSHEET # 11

Channel Design Data

PROJECT NAME: ATLANTIC SUNRISE PROJECT - COMPRESSOR STATION # 605

LOCATION: CLINTON TOWNSHIP, WYOMING COUNTY

PREPARED BY: AOE *DATE: 11/18/15*

CHECKED BY: AJB *DATE: 11/18/15*

CHANNEL OR CHANNEL SECTION		SWALE 1A LINING (MIN/MAX)	SWALE 1A GRASS/LINING (MIN/MAX)			
TEMPORARY OR PERMANENT?	(T OR P)	P	P			
DESIGN STORM	(2, 5, OR 10 YR)	10	10			
ACRES	(AC)	0.27	0.27			
MULTIPLIER[1]	(1.6, 2.25, or 2.75)[1]	N/A	N/A			
Qr (REQUIRED CAPACITY)	(CFS)	***1.21***	***1.21***			
Q (CALCULATED AT FLOW DEPTH d)	(CFS)	***1.19***	***1.25***			
PROTECTIVE LINING[2]		SC250	GRASS/SC250			
n (MANNING'S COEFFICIENT)[2]		0.04	0.159			
Va (ALLOWABLE VELOCITY)	(FPS)	N/A	N/A			
V (CALCULATED AT FLOW DEPTH d)	(FPS)	***2.80***	***1.08***			
τa (MAX ALLOWABLE SHEAR STRESS)	(LB/FT^2)	2.50	8.00			
τd (CALC'D SHEAR STRESS AT FLOW DEPTH d)	(LB/FT^2)	***0.84***	***1.82***			
CHANNEL BOTTOM WIDTH	(FT)	2	2			
CHANNEL SIDE SLOPES	(H:V)	3	3			
D (TOTAL DEPTH)	(FT)	1.0	1.0			
CHANNEL TOP WIDTH @ D	(FT)	8	8			
d (CALCULATED FLOW DEPTH)	(FT)	***0.17***	***0.37***			
CHANNEL TOP WIDTH @ FLOW DEPTH d	(FT)	***3.02***	***4.22***			
BOTTOM WIDTH: FLOW DEPTH RATIO	(12:1 MAX)	***11.76***	***5.41***			
d50 STONE SIZE	(IN)	N/A	N/A			
A (CROSS-SECTIONAL AREA)	(SQ. FT.)	**0.43**	**1.15**			
R (HYDRAULIC RADIUS)		**0.14**	**0.27**			
S (BED SLOPE)[3]	(FT/FT)	0.079	0.079			
Sc (CRITICAL SLOPE)	(FT/FT)	***0.046***	***0.589***			
.7Sc	(FT/FT)	***0.032***	***0.412***			
1.3Sc	(FT/FT)	***0.060***	***0.766***			
STABLE FLOW?	(Y/N)	Y	Y			
FREEBOARD BASED ON UNSTABLE FLOW	(FT)	***0.04***	***0.03***			
FREEBOARD BASED ON STABLE FLOW	(FT)	0.50	0.50			
MINIMUM REQUIRED FREEBOARD[4]	(FT)	0.50	0.50			
DESIGN METHOD FOR PROTECTIVE LINING[5] PERMISSIBLE VELOCITY (V) OR SHEAR STRESS	(S)	S	S			

1. Use 1.6 for Temporary Channels; 2.25 for Temporary Channels in Special Protection (HQ or EV) Watersheds; 2.75 for Permanent Channels. For Rational Method, enter "N/A" and attach E&S Worksheets 9 and 10. For TR-55 enter "N/A" and attach appropriate Worksheets.
2. Adjust "n" value for changes in channel liner and flow depth. For vegetated channels, provide data for manufactured linings without vegetation and with vegetation in separate columns.
3. Slopes may not be averaged.
4. Minimum Freeboard is 0.5 ft. or ¼ Total Channel Depth, whichever is greater
5. Permissible velocity lining design method is not acceptable for channels with a bed slope of 10% or greater. Shear stress lining design method is required for channels with a bed slope of 10% or greater. Shear stress lining design method may be used for any channel bed slope.

Source: 363-2134-008 / March 31, 2012 / Page 382

E&S WORKSHEET # 11

Channel Design Data

PROJECT NAME: ATLANTIC SUNRISE NATURAL GAS PIPELINE

LOCATION: CLINTON TOWNSHIP, WYOMING COUNTY

PREPARED BY: AOE DATE: 11/16/15

CHECKED BY: AJB DATE: 11/16/15

CHANNEL OR CHANNEL SECTION		SWALE 1B GRASS/LINING (MIN)	SWALE 1B GRASS/LINING (MAX)	SWALE 1B GRASS/LINING (MIN)	SWALE 1B GRASS/LINING (MAX)	
TEMPORARY OR PERMANENT?	(T OR P)	P	P	P	P	
DESIGN STORM	(2, 5, OR 10 YR)	10	10	100	100	
ACRES	(AC)	14.78	14.78	14.78	14.78	
MULTIPLIER[1]	(1.6, 2.25, or 2.75)[1]	N/A	N/A	N/A	N/A	
Qr (REQUIRED CAPACITY)	(CFS)	***27.07***	***27.07***	***47.37***	***47.37***	
Q (CALCULATED AT FLOW DEPTH d)	(CFS)	***28.18***	***29.16***	***49.09***	***48.35***	
PROTECTIVE LINING[2]		W3000/GRASS	W3000/GRASS	W3000/GRASS	W3000/GRASS	
n (MANNING'S COEFFICIENT)[2]		***0.054***	***0.052***	***0.047***	***0.045***	
Va (ALLOWABLE VELOCITY)	(FPS)	N/A	N/A	N/A	N/A	
V (CALCULATED AT FLOW DEPTH d)	(FPS)	***5.01***	***6.45***	***6.49***	***8.30***	
τa (MAX ALLOWABLE SHEAR STRESS)	(LB/FT^2)	16.00	16.00	16.00	16.00	
τd (CALC'D SHEAR STRESS AT FLOW DEPTH d)	(LB/FT^2)	***3.36***	***5.27***	***4.19***	***6.41***	
CHANNEL BOTTOM WIDTH	(FT)	5	5	5	5	
CHANNEL SIDE SLOPES	(H:V)	3	3	3	3	
D (TOTAL DEPTH)	(FT)	2.0	2.0	2.0	2.0	
CHANNEL TOP WIDTH @ D	(FT)	17	17	17	17	
d (CALCULATED FLOW DEPTH)	(FT)	***0.77***	***0.65***	***0.96***	***0.79***	
CHANNEL TOP WIDTH @ FLOW DEPTH d	(FT)	***9.62***	***8.90***	***10.76***	***9.74***	
BOTTOM WIDTH: FLOW DEPTH RATIO	(12:1 MAX)	***6.49***	***7.69***	***5.21***	***6.33***	
d50 STONE SIZE	(IN)	N/A	N/A	N/A	N/A	
A (CROSS-SECTIONAL AREA)	(SQ. FT.)	***5.63***	***4.52***	***7.56***	***5.82***	
R (HYDRAULIC RADIUS)		***0.57***	***0.50***	***0.68***	***0.58***	
S (BED SLOPE)[3]	(FT/FT)	0.07	0.13	0.07	0.13	
Sc (CRITICAL SLOPE)	(FT/FT)	***0.053***	***0.178***	***0.243***	***0.172***	
.7Sc	(FT/FT)	***0.037***	***0.124***	***0.170***	***0.120***	
1.3Sc	(FT/FT)	***0.068***	***0.231***	***0.316***	***0.223***	
STABLE FLOW?	(Y/N)	***Y***	***N***	***Y***	***N***	
FREEBOARD BASED ON UNSTABLE FLOW	(FT)	***0.29***	***0.3***	***0.5***	***0.5***	
FREEBOARD BASED ON STABLE FLOW	(FT)	0.50	0.5	0.5	0.5	
MINIMUM REQUIRED FREEBOARD[4]	(FT)	0.50	0.50	0.50	0.51	
DESIGN METHOD FOR PROTECTIVE LINING [5] PERMISSIBLE VELOCITY (V) OR SHEAR STRESS	(S)	S	S	S	S	

1. Use 1.6 for Temporary Channels; 2.25 for Temporary Channels in Special Protection (HQ or EV) Watersheds; 2.75 for Permanent Channels. For Rational Method, enter "N/A" and attach E&S Worksheets 9 and 10. For TR-55 enter "N/A" and attach appropriate Worksheets.
2. Adjust "n" value for changes in channel liner and flow depth. For vegetated channels, provide data for manufactured linings without vegetation and with vegetation in separate columns.
3. Slopes may not be averaged.
4. Minimum Freeboard is 0.5 ft. or ¼ Total Channel Depth, whichever is greater
5. Permissible velocity lining design method is not acceptable for channels with a bed slope of 10% or greater. Shear stress lining design method is required for channels with a bed slope of 10% or greater. Shear stress lining design method may be used for any channel bed slope.

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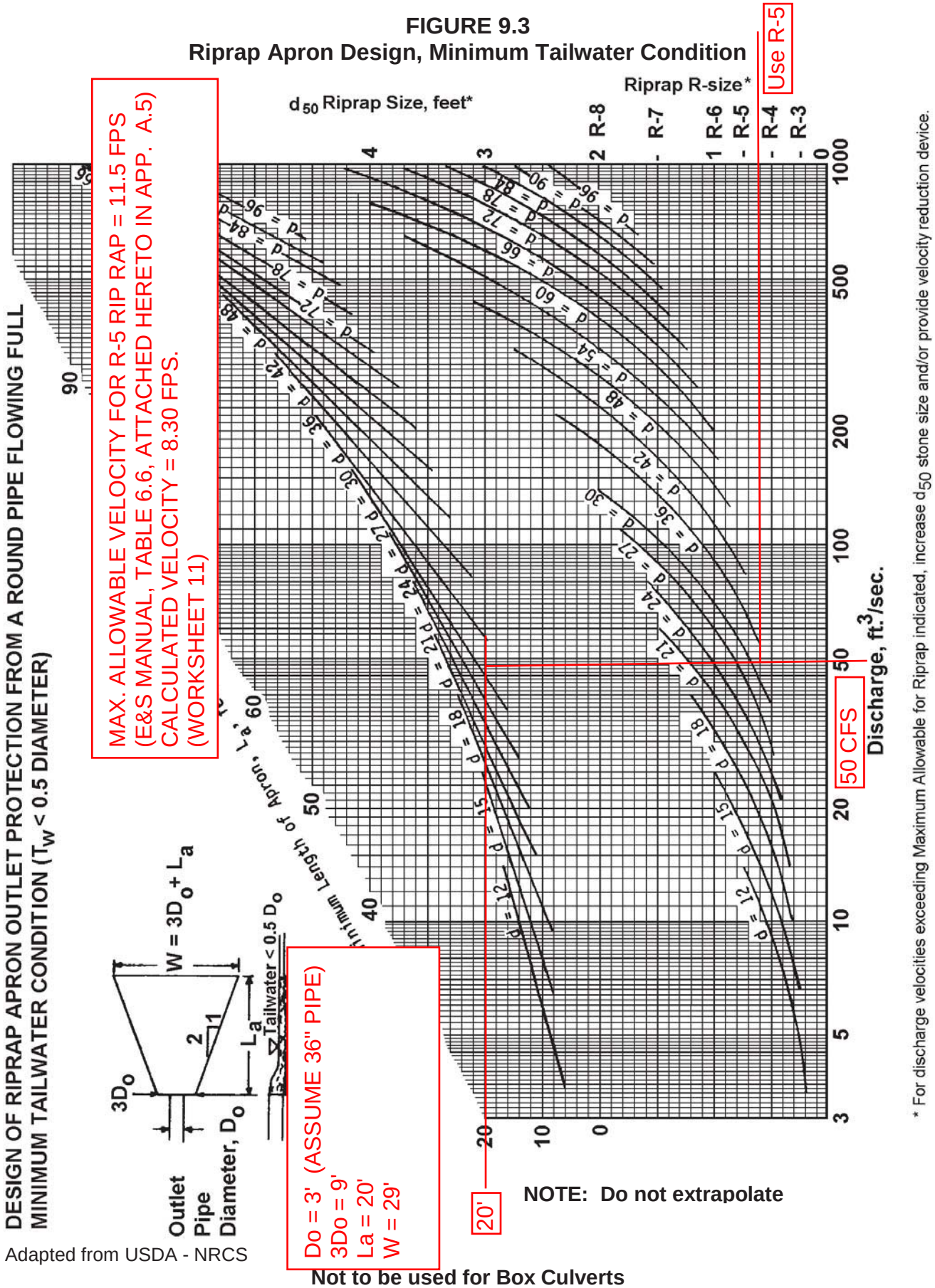
FIGURE 9.3
Riprap Apron Design, Minimum Tailwater Condition



Summary for Subcatchment 20S: POST-DEVELOPMENT DRAINAGE AREA TO INFILTRATION BASIN

[49] Hint: Tc<2dt may require smaller dt

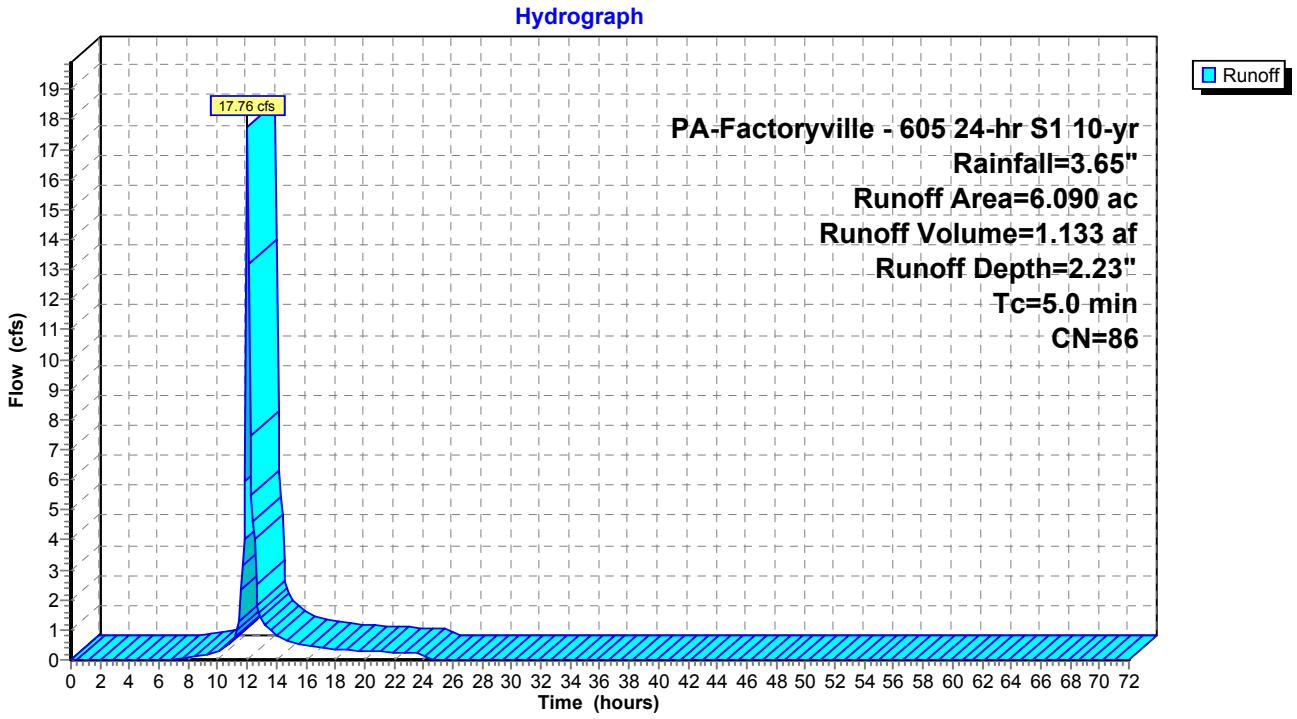
Runoff = 17.76 cfs @ 12.02 hrs, Volume= 1.133 af, Depth= 2.23"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs
PA-Factoryville - 605 24-hr S1 10-yr Rainfall=3.65"

	Area (ac)	CN	Description
*	0.370	98	Impervious, HSG C
	2.360	78	Meadow, non-grazed, HSG D
*	3.360	91	Gravel Areas, HSG D
	6.090	86	Weighted Average
	5.720		93.92% Pervious Area
	0.370		6.08% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					**Direct Entry,**

Subcatchment 20S: POST-DEVELOPMENT DRAINAGE AREA TO INFILTRATION BASIN 2



Summary for Subcatchment 22S: DRAINGE AREA TO SWALE 1A

[49] Hint: Tc<2dt may require smaller dt

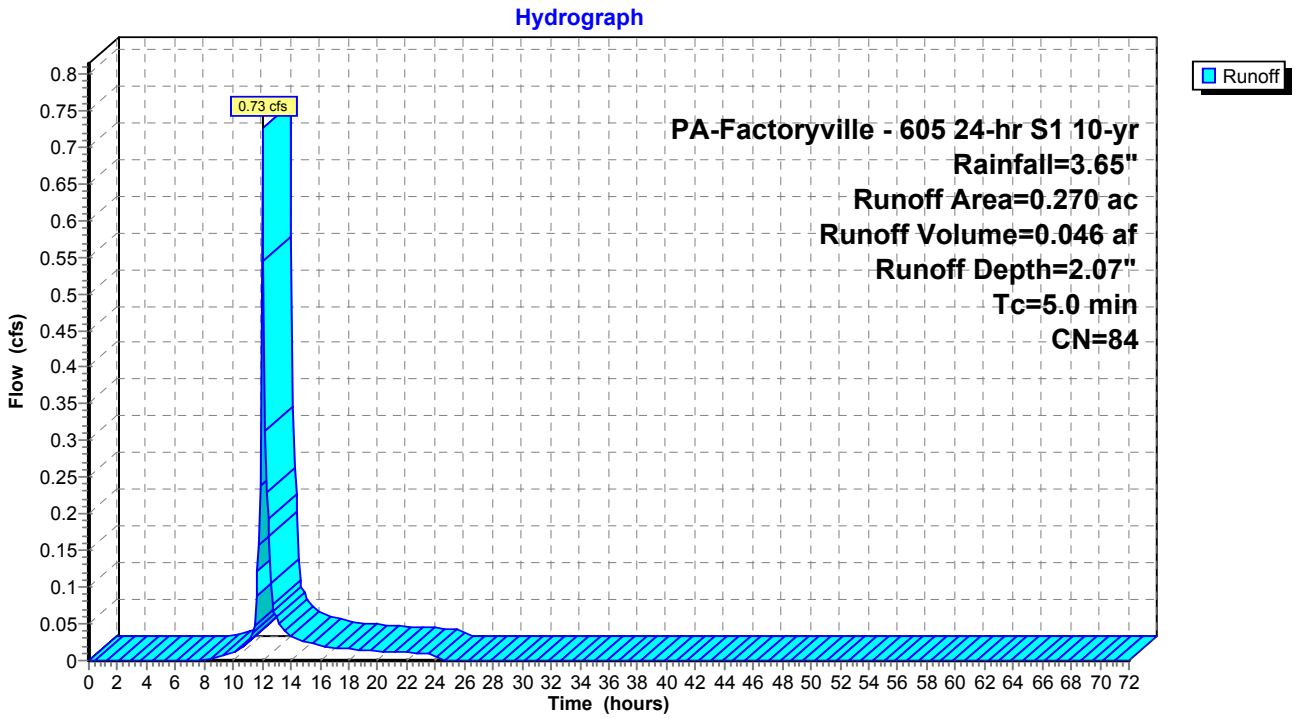
Runoff = 0.73 cfs @ 12.02 hrs, Volume= 0.046 af, Depth= 2.07"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs
PA-Factoryville - 605 24-hr S1 10-yr Rainfall=3.65"

	Area (ac)	CN	Description
	0.190	78	Meadow, non-grazed, HSG D
*	0.080	98	Impervious areas, HSG D
	0.270	84	Weighted Average
	0.190		70.37% Pervious Area
	0.080		29.63% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					**Direct Entry,**

Subcatchment 22S: DRAINGE AREA TO SWALE 1A



Summary for Subcatchment 35S: DRAINAGE AREA TO SWALE 1B

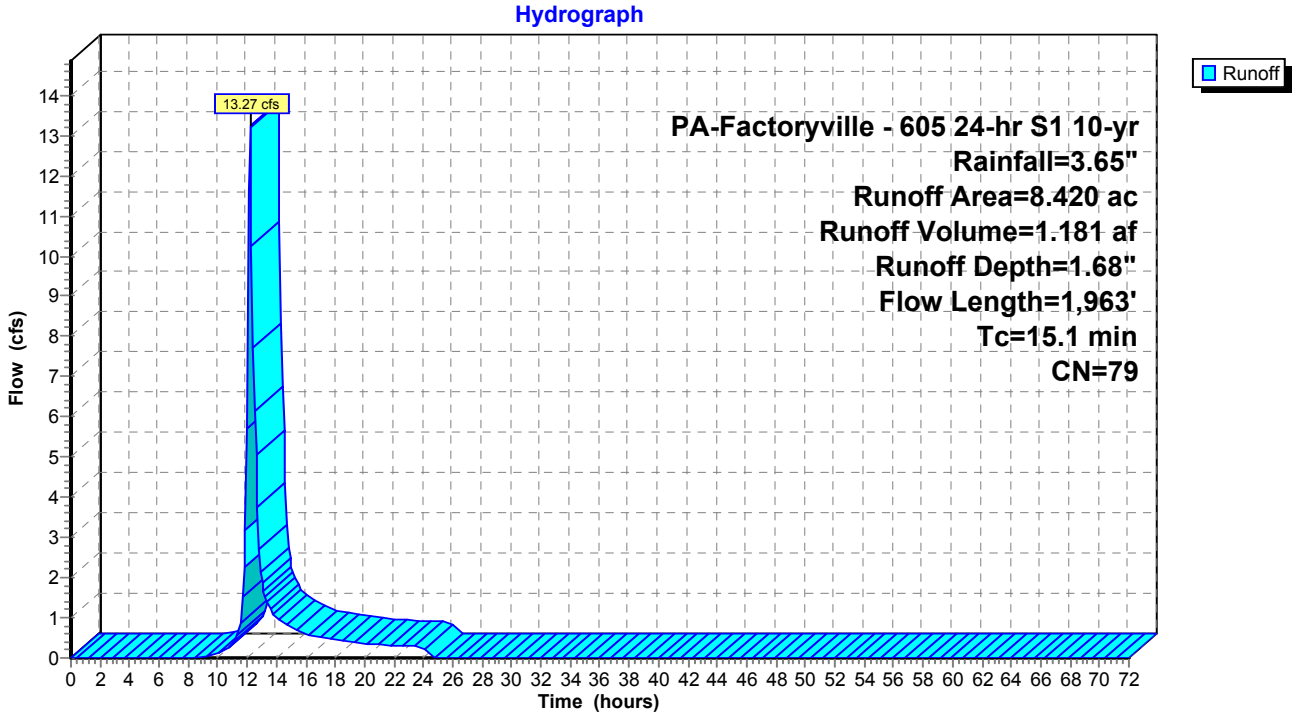
Runoff = 13.27 cfs @ 12.18 hrs, Volume= 1.181 af, Depth= 1.68"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs
PA-Factoryville - 605 24-hr S1 10-yr Rainfall=3.65"

	Area (ac)	CN	Description
	5.626	78	Meadow, non-grazed, HSG D
	2.364	77	Woods, Good, HSG D
*	0.430	98	Impervious areas, HSG D
	8.420	79	Weighted Average
	7.990		94.89% Pervious Area
	0.430		5.11% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.4	100	0.0400	0.22		**Sheet Flow, SHT 1** Range n= 0.130 P2= 2.54"
4.1	686	0.1574	2.78		**Shallow Concentrated Flow, SCF 1** Short Grass Pasture Kv= 7.0 fps
3.6	1,177	0.1290	5.39		**Shallow Concentrated Flow, SCF 2** Grassed Waterway Kv= 15.0 fps
15.1	1,963	Total			

Subcatchment 35S: DRAINAGE AREA TO SWALE 1B



Summary for Pond 26P: INFILTRATION BASIN 2

Inflow Area = 6.090 ac, 6.08% Impervious, Inflow Depth = 2.23" for 10-yr event
Inflow = 17.76 cfs @ 12.02 hrs, Volume= 1.133 af
Outflow = 14.82 cfs @ 12.10 hrs, Volume= 1.133 af, Atten= 17%, Lag= 4.8 min
Discarded = 0.50 cfs @ 12.10 hrs, Volume= 0.536 af
Primary = 14.33 cfs @ 12.10 hrs, Volume= 0.597 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs
Peak Elev= 1,120.52' @ 12.10 hrs Surf.Area= 8,068 sf Storage= 9,967 cf

Plug-Flow detention time= 110.1 min calculated for 1.133 af (100% of inflow)
Center-of-Mass det. time= 110.0 min (931.2 - 821.2)

Volume	Invert	Avail.Storage	Storage Description
#1	1,118.00'	56,769 cf	**Custom Stage Data (Prismatic)** Listed below (Recalc)

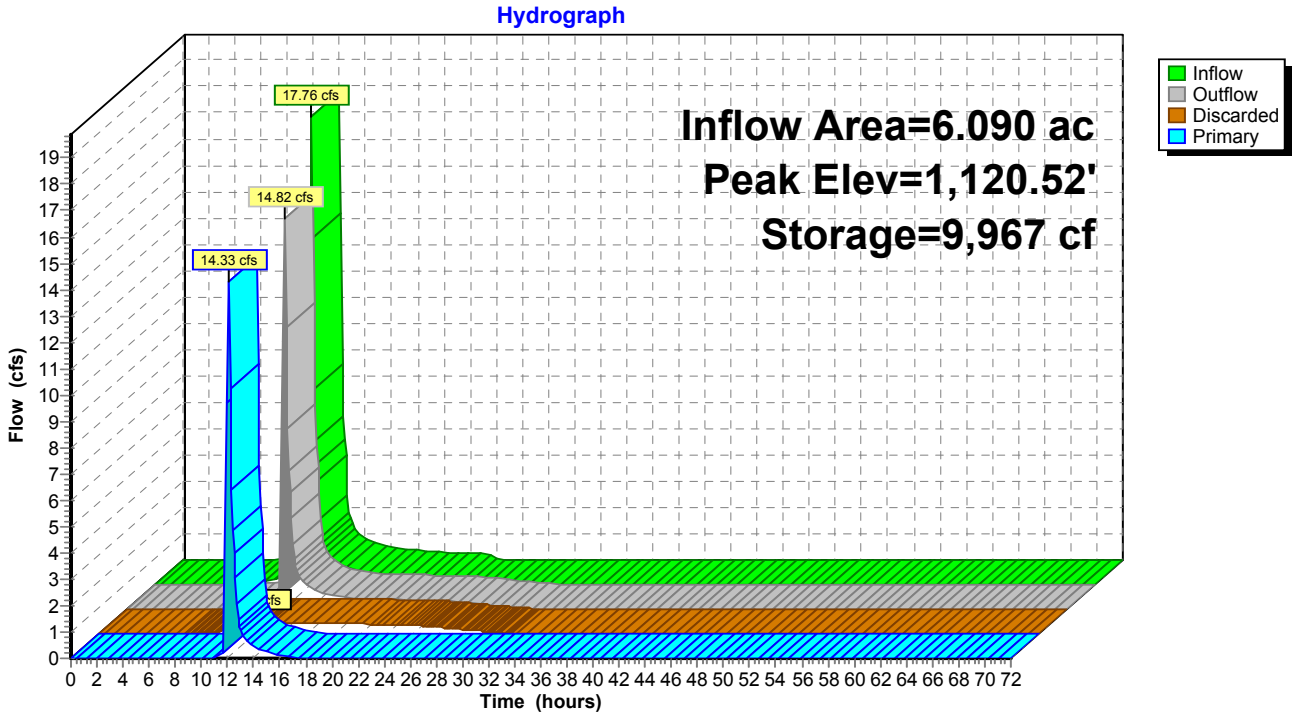
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
1,118.00	0	0	0
1,120.00	6,243	6,243	6,243
1,122.00	13,256	19,499	25,742
1,124.00	17,771	31,027	56,769

Device	Routing	Invert	Outlet Devices
#1	Primary	1,117.00'	**18.0" Round Culvert** L= 126.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 1,117.00' / 1,106.00' S= 0.0873 '/' Cc= 0.900 n= 0.012, Flow Area= 1.77 sf
#2	Discarded	1,118.00'	**2.660 in/hr Exfiltration over Surface area**
#3	Device 1	1,120.00'	**24.0" x 48.0" Horiz. Orifice/Grate** C= 0.600 Limited to weir flow at low heads
#4	Primary	1,120.50'	**20.0' long x 17.0' breadth Broad-Crested Rectangular Weir** Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Discarded OutFlow Max=0.50 cfs @ 12.10 hrs HW=1,120.52' (Free Discharge)
└**2=Exfiltration** (Exfiltration Controls 0.50 cfs)

Primary OutFlow Max=14.27 cfs @ 12.10 hrs HW=1,120.52' (Free Discharge)
└**1=Culvert** (Inlet Controls 14.15 cfs @ 8.01 fps)
└**3=Orifice/Grate** (Passes 14.15 cfs of 14.58 cfs potential flow)
└**4=Broad-Crested Rectangular Weir** (Weir Controls 0.12 cfs @ 0.35 fps)

Pond 26P: INFILTRATION BASIN 2

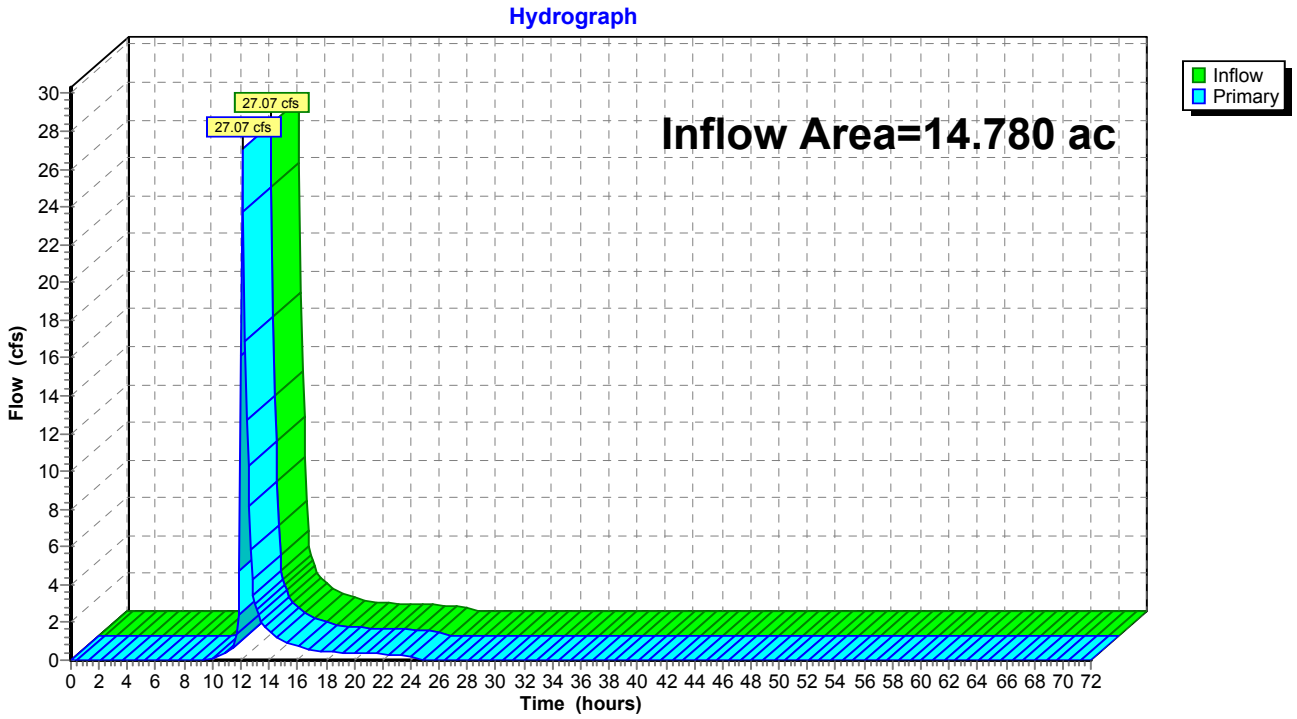


Summary for Link 34L: SWALE 1B

Inflow Area = 14.780 ac, 5.95% Impervious, Inflow Depth = 1.48" for 10-yr event
Inflow = 27.07 cfs @ 12.13 hrs, Volume= 1.825 af
Primary = 27.07 cfs @ 12.13 hrs, Volume= 1.825 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs

Link 34L: SWALE 1B



Summary for Subcatchment 20S: POST-DEVELOPMENT DRAINAGE AREA TO INFILTRATION BASIN

[49] Hint: Tc<2dt may require smaller dt

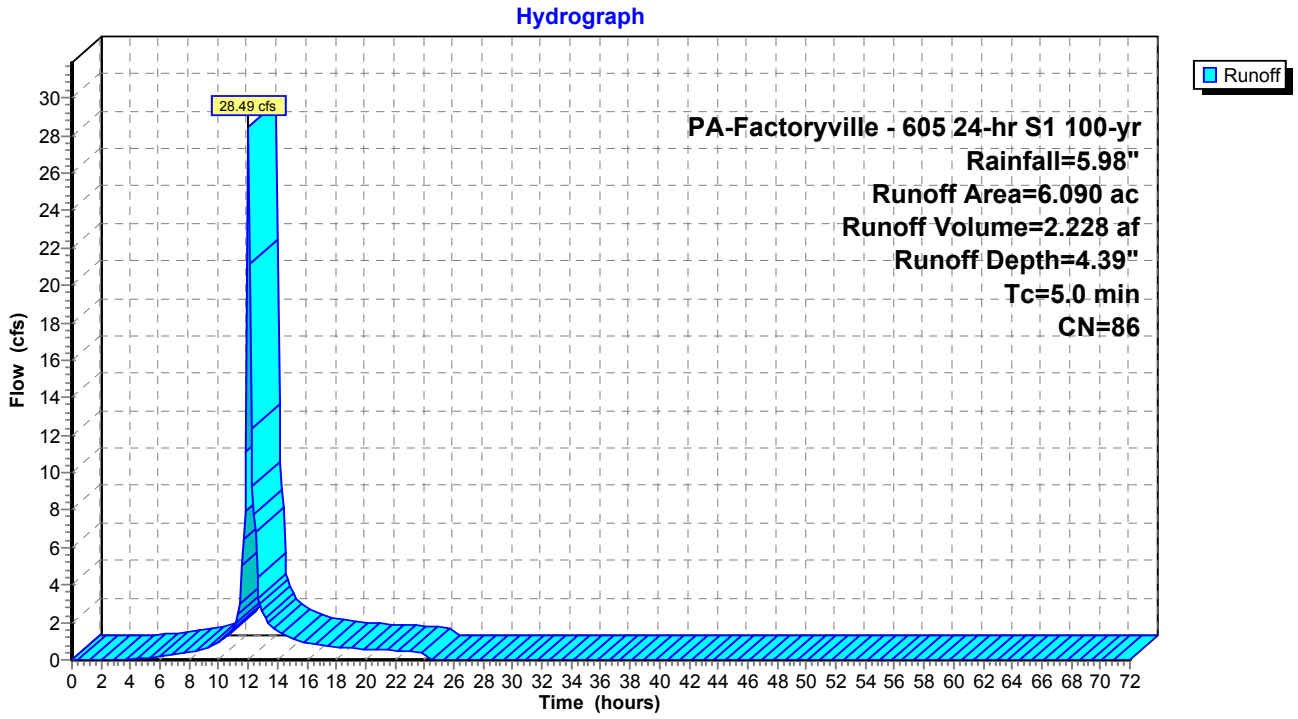
Runoff = 28.49 cfs @ 12.02 hrs, Volume= 2.228 af, Depth= 4.39"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs
PA-Factoryville - 605 24-hr S1 100-yr Rainfall=5.98"

	Area (ac)	CN	Description
*	0.370	98	Impervious, HSG C
	2.360	78	Meadow, non-grazed, HSG D
*	3.360	91	Gravel Areas, HSG D
	6.090	86	Weighted Average
	5.720		93.92% Pervious Area
	0.370		6.08% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					**Direct Entry,**

Subcatchment 20S: POST-DEVELOPMENT DRAINAGE AREA TO INFILTRATION BASIN 2



Summary for Subcatchment 22S: DRAINGE AREA TO SWALE 1A

[49] Hint: Tc<2dt may require smaller dt

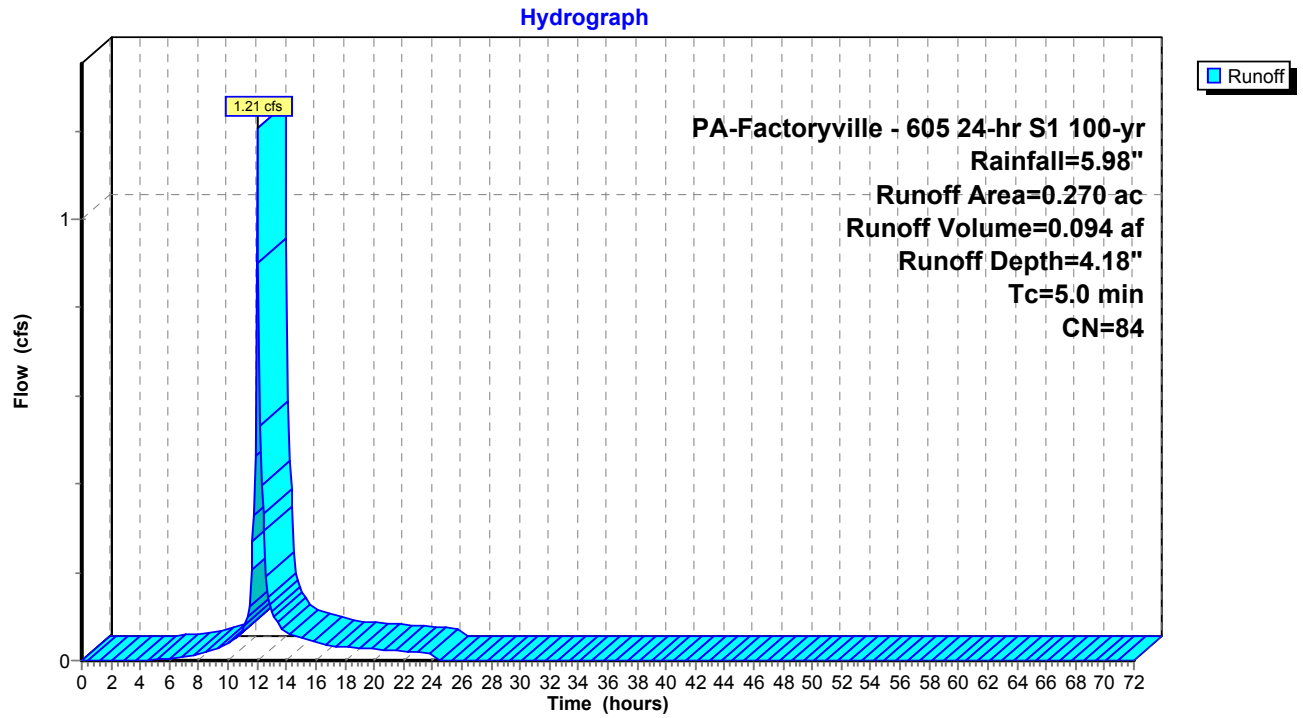
Runoff = 1.21 cfs @ 12.02 hrs, Volume= 0.094 af, Depth= 4.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs
PA-Factoryville - 605 24-hr S1 100-yr Rainfall=5.98"

	Area (ac)	CN	Description
	0.190	78	Meadow, non-grazed, HSG D
*	0.080	98	Impervious areas, HSG D
	0.270	84	Weighted Average
	0.190		70.37% Pervious Area
	0.080		29.63% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					**Direct Entry,**

Subcatchment 22S: DRAINGE AREA TO SWALE 1A



Summary for Subcatchment 35S: DRAINAGE AREA TO SWALE 1B

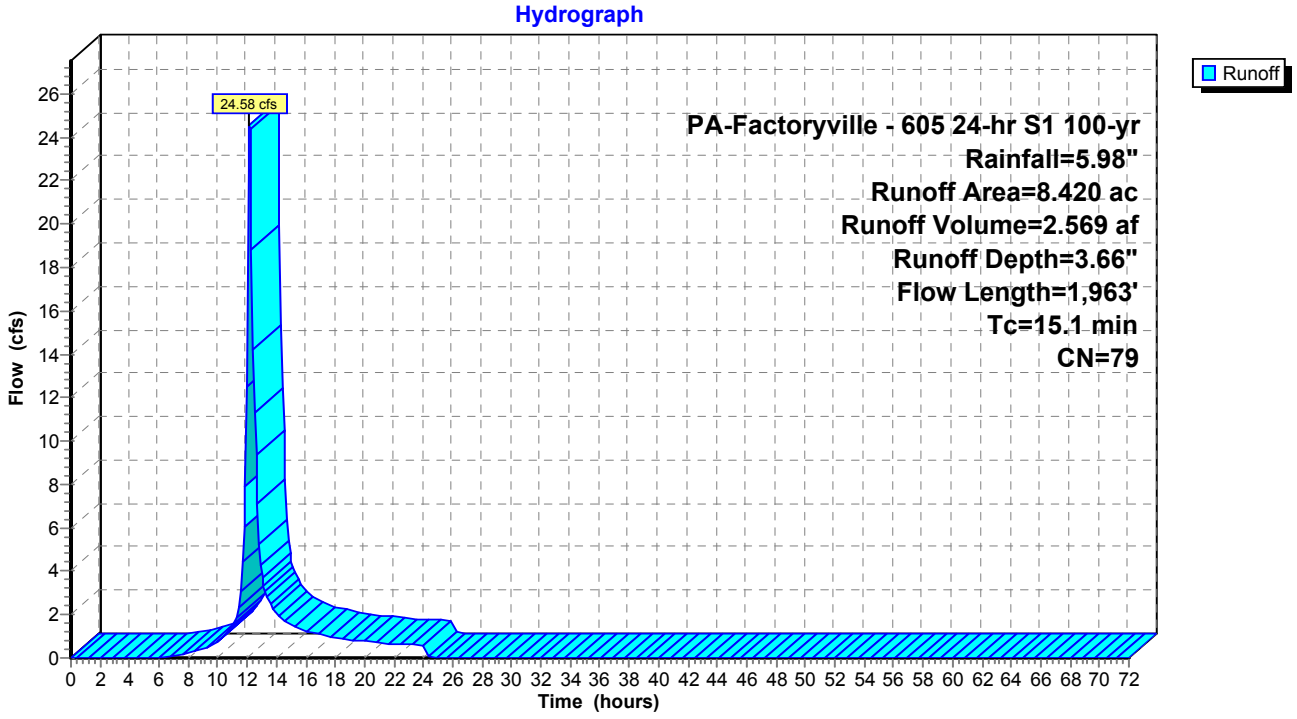
Runoff = 24.58 cfs @ 12.18 hrs, Volume= 2.569 af, Depth= 3.66"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs
PA-Factoryville - 605 24-hr S1 100-yr Rainfall=5.98"

	Area (ac)	CN	Description
	5.626	78	Meadow, non-grazed, HSG D
	2.364	77	Woods, Good, HSG D
*	0.430	98	Impervious areas, HSG D
	8.420	79	Weighted Average
	7.990		94.89% Pervious Area
	0.430		5.11% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.4	100	0.0400	0.22		**Sheet Flow, SHT 1** Range n= 0.130 P2= 2.54"
4.1	686	0.1574	2.78		**Shallow Concentrated Flow, SCF 1** Short Grass Pasture Kv= 7.0 fps
3.6	1,177	0.1290	5.39		**Shallow Concentrated Flow, SCF 2** Grassed Waterway Kv= 15.0 fps
15.1	1,963	Total			

Subcatchment 35S: DRAINAGE AREA TO SWALE 1B



Summary for Pond 26P: INFILTRATION BASIN 2

Inflow Area = 6.090 ac, 6.08% Impervious, Inflow Depth = 4.39" for 100-yr event
Inflow = 28.49 cfs @ 12.02 hrs, Volume= 2.228 af
Outflow = 23.89 cfs @ 12.10 hrs, Volume= 2.228 af, Atten= 16%, Lag= 4.7 min
Discarded = 0.56 cfs @ 12.10 hrs, Volume= 0.681 af
Primary = 23.33 cfs @ 12.10 hrs, Volume= 1.547 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs
Peak Elev= 1,120.79' @ 12.10 hrs Surf.Area= 9,018 sf Storage= 12,282 cf

Plug-Flow detention time= 74.1 min calculated for 2.225 af (100% of inflow)
Center-of-Mass det. time= 74.7 min (881.3 - 806.7)

Volume	Invert	Avail.Storage	Storage Description
#1	1,118.00'	56,769 cf	**Custom Stage Data (Prismatic)** Listed below (Recalc)

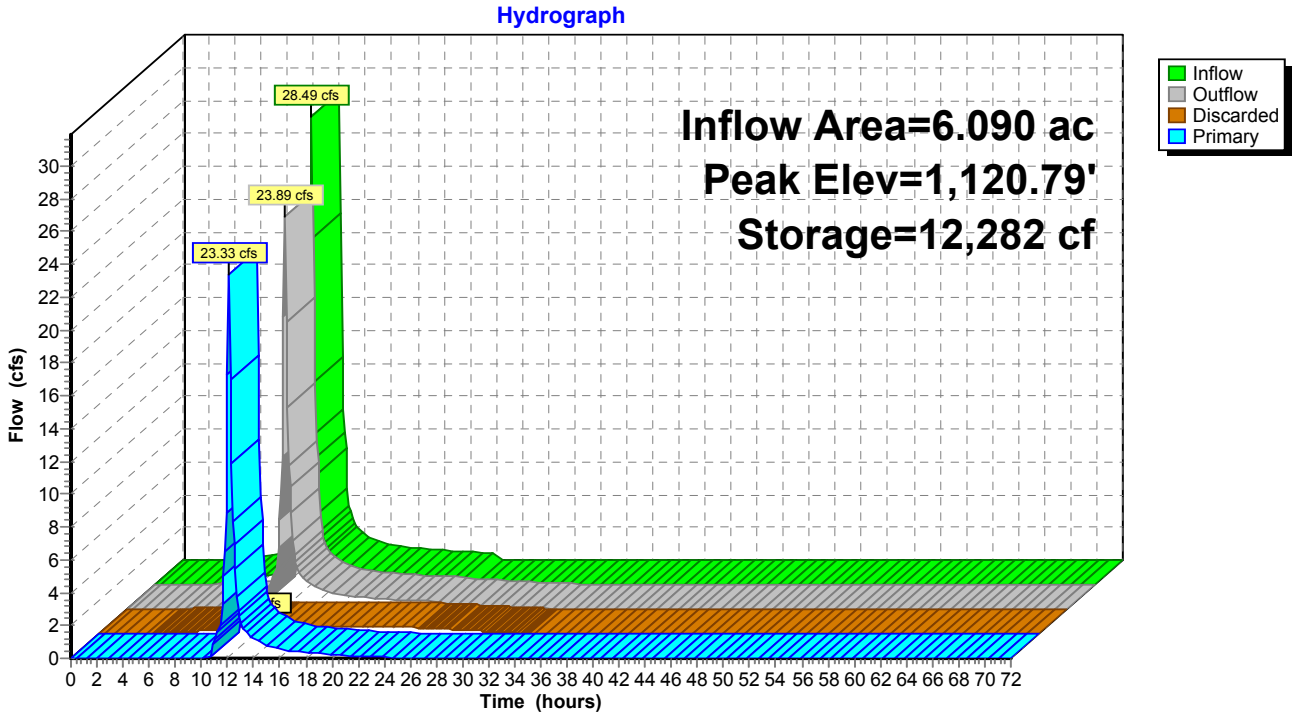
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
1,118.00	0	0	0
1,120.00	6,243	6,243	6,243
1,122.00	13,256	19,499	25,742
1,124.00	17,771	31,027	56,769

Device	Routing	Invert	Outlet Devices
#1	Primary	1,117.00'	**18.0" Round Culvert** L= 126.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 1,117.00' / 1,106.00' S= 0.0873 '/' Cc= 0.900 n= 0.012, Flow Area= 1.77 sf
#2	Discarded	1,118.00'	**2.660 in/hr Exfiltration over Surface area**
#3	Device 1	1,120.00'	**24.0" x 48.0" Horiz. Orifice/Grate** C= 0.600 Limited to weir flow at low heads
#4	Primary	1,120.50'	**20.0' long x 17.0' breadth Broad-Crested Rectangular Weir** Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Discarded OutFlow Max=0.55 cfs @ 12.10 hrs HW=1,120.79' (Free Discharge)
└**2=Exfiltration** (Exfiltration Controls 0.55 cfs)

Primary OutFlow Max=23.21 cfs @ 12.10 hrs HW=1,120.79' (Free Discharge)
└**1=Culvert** (Inlet Controls 14.83 cfs @ 8.39 fps)
└**3=Orifice/Grate** (Passes 14.83 cfs of 27.53 cfs potential flow)
└**4=Broad-Crested Rectangular Weir** (Weir Controls 8.38 cfs @ 1.45 fps)

Pond 26P: INFILTRATION BASIN 2

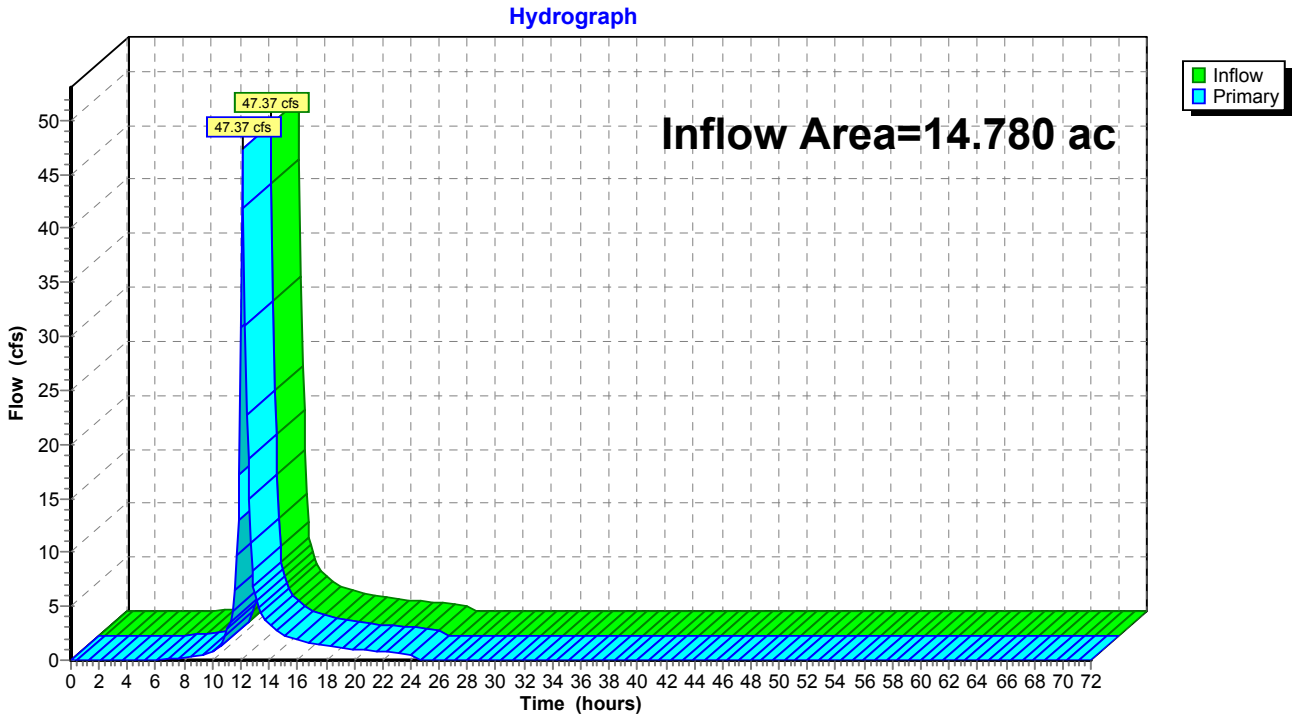


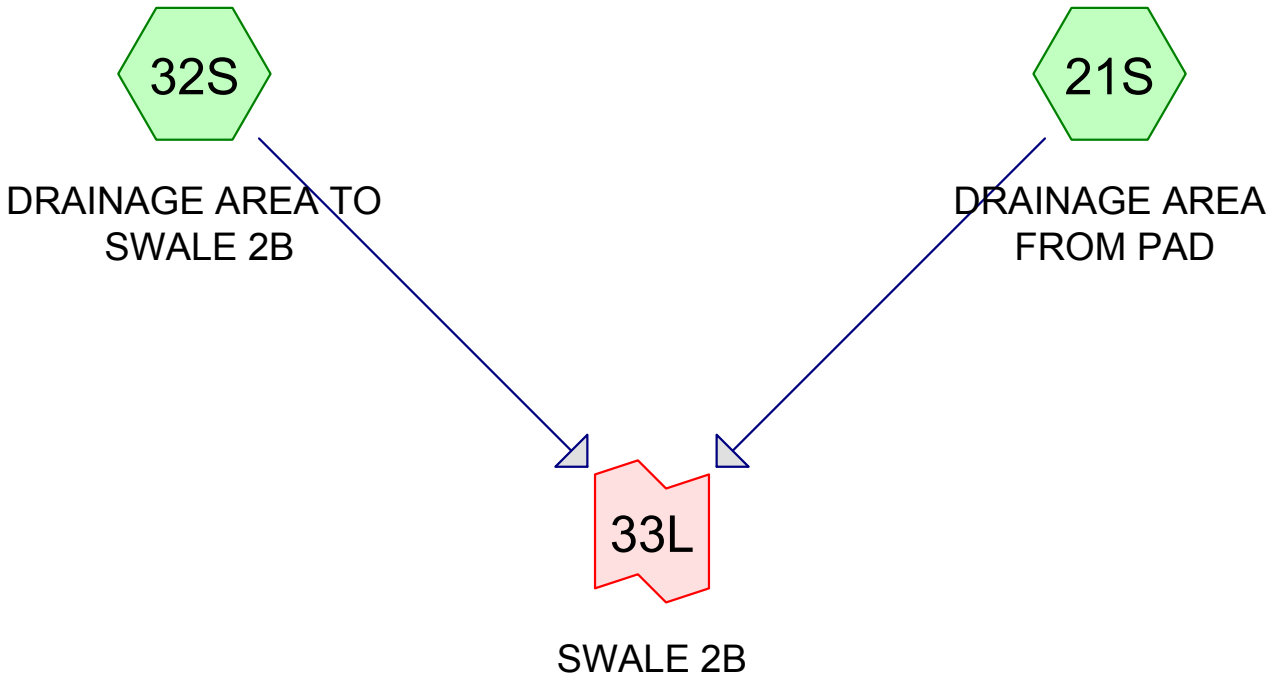
Summary for Link 34L: SWALE 1B

Inflow Area = 14.780 ac, 5.95% Impervious, Inflow Depth = 3.42" for 100-yr event
Inflow = 47.37 cfs @ 12.13 hrs, Volume= 4.210 af
Primary = 47.37 cfs @ 12.13 hrs, Volume= 4.210 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs

Link 34L: SWALE 1B





Subcat Reach Pond Link

Routing Diagram for C-DAT-14C4909-CS 605
Prepared by Microsoft, Printed 10/10/2016

E&S WORKSHEET # 11

Channel Design Data

PROJECT NAME: ATLANTIC SUNRISE NATURAL GAS PIPELINE

PROJECT NAME: ATLANTIC SUNRISE PROJECT - COMPRESSOR STATION # 605

PREPARED BY: AOE DATE: 08/12/15

CHECKED BY: AJB DATE: 08/12/15

CHANNEL OR CHANNEL SECTION		SWALE 2A LINING (MIN/MAX)	SWALE 2A GRASS (MIN/MAX)			
TEMPORARY OR PERMANENT?	(T OR P)	P	P			
DESIGN STORM	(2, 5, OR 10 YR)	10	10			
ACRES	(AC)	1.17	1.17			
MULTIPLIER[1]	(1.6, 2.25, or 2.75)[1]	2.75	2.75			
Qr (REQUIRED CAPACITY)	(CFS)	3.22	3.22			
Q (CALCULATED AT FLOW DEPTH d)	(CFS)	3.20	3.25			
PROTECTIVE LINING[2]		S75	GRASS			
n (MANNING'S COEFFICIENT)[2]		0.055	0.13			
Va (ALLOWABLE VELOCITY)	(FPS)	N/A	N/A			
V (CALCULATED AT FLOW DEPTH d)	(FPS)	1.44	0.77			
τa (MAX ALLOWABLE SHEAR STRESS)	(LB/FT^2)	1.55	1.00			
τd (CALC'D SHEAR STRESS AT FLOW DEPTH d)	(LB/FT^2)	0.37	0.56			
CHANNEL BOTTOM WIDTH	(FT)	2	2			
CHANNEL SIDE SLOPES	(H:V)	3	3			
D (TOTAL DEPTH)	(FT)	1.5	1.5			
CHANNEL TOP WIDTH @ D	(FT)	11	11			
d (CALCULATED FLOW DEPTH)	(FT)	0.59	0.90			
CHANNEL TOP WIDTH @ FLOW DEPTH d	(FT)	5.54	7.40			
BOTTOM WIDTH: FLOW DEPTH RATIO	(12:1 MAX)	3.39	2.22			
d50 STONE SIZE	(IN)	N/A	N/A			
A (CROSS-SECTIONAL AREA)	(SQ. FT.)	2.22	4.23			
R (HYDRAULIC RADIUS)		0.39	0.55			
S (BED SLOPE)[3]	(FT/FT)	0.01	0.01			
Sc (CRITICAL SLOPE)	(FT/FT)	0.062	1.041			
.7Sc	(FT/FT)	0.044	0.729			
1.3Sc	(FT/FT)	0.081	1.353			
STABLE FLOW?	(Y/N)	Y	Y			
FREEBOARD BASED ON UNSTABLE FLOW	(FT)	0.06	0.05			
FREEBOARD BASED ON STABLE FLOW	(FT)	0.50	0.50			
MINIMUM REQUIRED FREEBOARD[4]	(FT)	0.50	0.50			
DESIGN METHOD FOR PROTECTIVE LINING [5] PERMISSIBLE VELOCITY (V) OR SHEAR STRESS	(S)	S	S			

1. Use 1.6 for Temporary Channels; 2.25 for Temporary Channels in Special Protection (HQ or EV) Watersheds; 2.75 for Permanent Channels. For Rational Method, enter "N/A" and attach E&S Worksheets 9 and 10. For TR-55 enter "N/A" and attach appropriate Worksheets.
2. Adjust "n" value for changes in channel liner and flow depth. For vegetated channels, provide data for manufactured linings without vegetation and with vegetation in separate columns.
3. Slopes may not be averaged.
4. Minimum Freeboard is 0.5 ft. or ¼ Total Channel Depth, whichever is greater
5. Permissible velocity lining design method is not acceptable for channels with a bed slope of 10% or greater. Shear stress lining design method is required for channels with a bed slope of 10% or greater. Shear stress lining design method may be used for any channel bed slope.

Source: 363-2134-008 / March 31, 2012 / Page 382

E&S WORKSHEET # 11

Channel Design Data

PROJECT NAME: ATLANTIC SUNRISE NATURAL GAS PIPELINE

PROJECT NAME: ATLANTIC SUNRISE PROJECT - COMPRESSOR STATION # 605

PREPARED BY: AOE DATE: 08/12/15

CHECKED BY: AJB DATE: 08/12/15

CHANNEL OR CHANNEL SECTION		SWALE 2B GRASS/LINING (MIN)	SWALE 2B GRASS/LINING (MAX)	SWALE 2B GRASS/LINING (MIN)	SWALE 2B GRASS/LINING (MAX)	
TEMPORARY OR PERMANENT?	(T OR P)	P	P	P	P	
DESIGN STORM	(2, 5, OR 10 YR)	10	10	100	100	
ACRES	(AC)	14.46	14.46	14.46	14.46	
MULTIPLIER[1]	(1.6, 2.25, or 2.75)[1]	N/A	N/A	N/A	N/A	
Qr (REQUIRED CAPACITY)	(CFS)	31.68	31.68	53.00	53.00	
Q (CALCULATED AT FLOW DEPTH d)	(CFS)	32.15	31.66	53.87	53.13	
PROTECTIVE LINING[2]		W3000	W3000/GRASS	W3000	W3000/GRASS	
n (MANNING'S COEFFICIENT)[2]		0.06	0.049	0.052	0.043	
Va (ALLOWABLE VELOCITY)	(FPS)	N/A	N/A	N/A	N/A	
V (CALCULATED AT FLOW DEPTH d)	(FPS)	2.40	8.66	3.06	11.10	
τa (MAX ALLOWABLE SHEAR STRESS)	(LB/FT^2)	16.00	16.00	16.00	16.00	
τd (CALC'D SHEAR STRESS AT FLOW DEPTH d)	(LB/FT^2)	0.90	8.58	1.08	10.61	
CHANNEL BOTTOM WIDTH	(FT)	5	5	5	5	
CHANNEL SIDE SLOPES	(H:V)	3	3	3	3	
D (TOTAL DEPTH)	(FT)	2.0	2.0	2.0	2.0	
CHANNEL TOP WIDTH @ D	(FT)	17	17	17	17	
d (CALCULATED FLOW DEPTH)	(FT)	1.44	0.55	1.73	0.68	
CHANNEL TOP WIDTH @ FLOW DEPTH d	(FT)	13.64	8.30	15.38	9.08	
BOTTOM WIDTH: FLOW DEPTH RATIO	(12:1 MAX)	3.47	9.09	2.89	7.35	
d50 STONE SIZE	(IN)	N/A	N/A	N/A	N/A	
A (CROSS-SECTIONAL AREA)	(SQ. FT.)	13.42	3.66	17.63	4.79	
R (HYDRAULIC RADIUS)		0.95	0.43	1.11	0.51	
S (BED SLOPE)[3]	(FT/FT)	0.01	0.25	0.01	0.25	
Sc (CRITICAL SLOPE)	(FT/FT)	0.055	0.128	0.039	0.129	
.7Sc	(FT/FT)	0.039	0.090	0.028	0.090	
1.3Sc	(FT/FT)	0.072	0.166	0.051	0.168	
STABLE FLOW?	(Y/N)	Y	Y	Y	Y	
FREEBOARD BASED ON UNSTABLE FLOW	(FT)	0.26	0.36	0.40	0.57	
FREEBOARD BASED ON STABLE FLOW	(FT)	0.50	0.50	0.50	0.50	
MINIMUM REQUIRED FREEBOARD[4]	(FT)	0.50	0.50	0.50	0.57	
DESIGN METHOD FOR PROTECTIVE LINING [5] PERMISSIBLE VELOCITY (V) OR SHEAR STRESS	(S)	S	S	S	S	

1. Use 1.6 for Temporary Channels; 2.25 for Temporary Channels in Special Protection (HQ or EV) Watersheds; 2.75 for Permanent Channels. For Rational Method, enter "N/A" and attach E&S Worksheets 9 and 10. For TR-55 enter "N/A" and attach appropriate Worksheets.
2. Adjust "n" value for changes in channel liner and flow depth. For vegetated channels, provide data for manufactured linings without vegetation and with vegetation in separate columns.
3. Slopes may not be averaged.
4. Minimum Freeboard is 0.5 ft. or ¼ Total Channel Depth, whichever is greater
5. Permissible velocity lining design method is not acceptable for channels with a bed slope of 10% or greater. Shear stress lining design method is required for channels with a bed slope of 10% or greater. Shear stress lining design method may be used for any channel bed slope.

Source: 363-2134-008 / March 31, 2012 / Page 382

Summary for Subcatchment 21S: DRAINAGE AREA FROM PAD

[49] Hint: Tc<2dt may require smaller dt

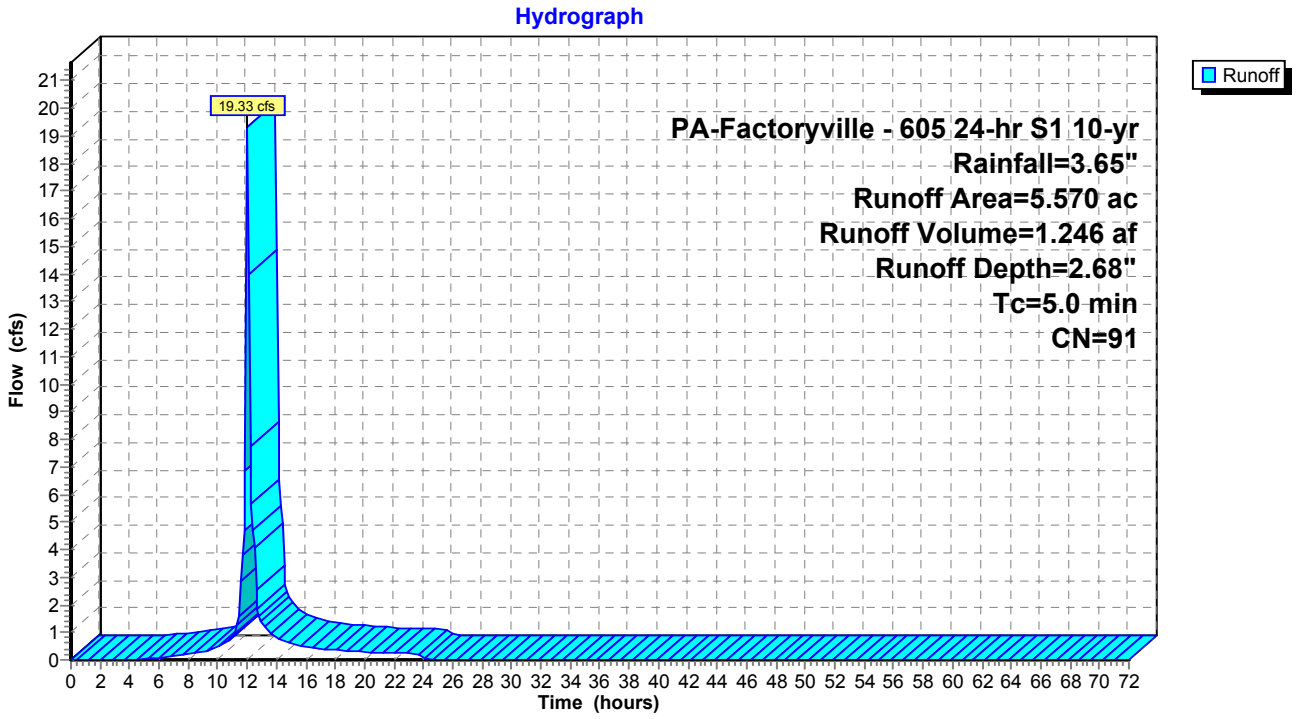
Runoff = 19.33 cfs @ 12.02 hrs, Volume= 1.246 af, Depth= 2.68"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs
PA-Factoryville - 605 24-hr S1 10-yr Rainfall=3.65"

	Area (ac)	CN	Description
	0.760	78	Meadow, non-grazed, HSG D
*	3.180	91	Gravel areas, HSG D
*	1.630	98	Impervious areas, HSG D
	5.570	91	Weighted Average
	3.940		70.74% Pervious Area
	1.630		29.26% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					**Direct Entry,**

Subcatchment 21S: DRAINAGE AREA FROM PAD



Summary for Subcatchment 32S: DRAINAGE AREA TO SWALE 2B

[49] Hint: Tc<2dt may require smaller dt

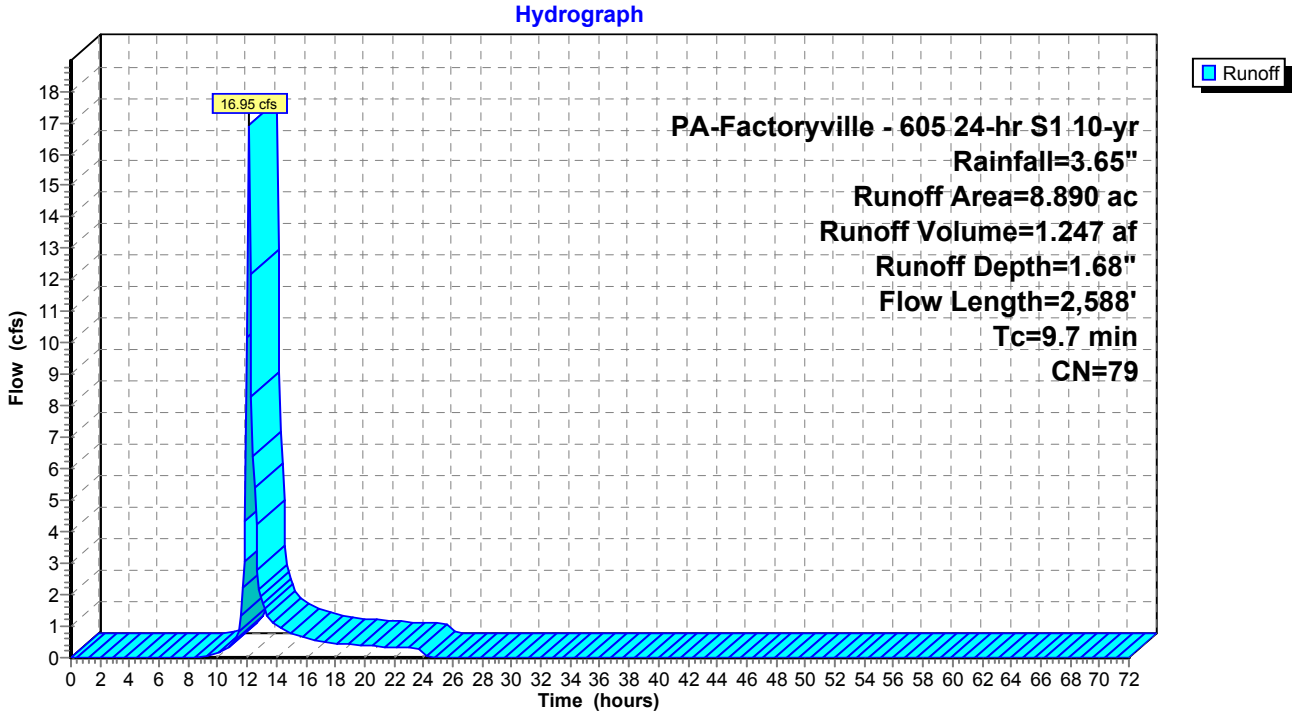
Runoff = 16.95 cfs @ 12.11 hrs, Volume= 1.247 af, Depth= 1.68"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs
PA-Factoryville - 605 24-hr S1 10-yr Rainfall=3.65"

	Area (ac)	CN	Description
	8.250	78	Meadow, non-grazed, HSG D
*	0.640	98	Impervious areas, HSG D
	8.890	79	Weighted Average
	8.250		92.80% Pervious Area
	0.640		7.20% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.0	266	0.0100	1.50		**Shallow Concentrated Flow, SCF-1** Grassed Waterway Kv= 15.0 fps
6.7	2,322	0.0700	5.82	40.72	**Channel Flow,** Area= 7.0 sf Perim= 11.0' r= 0.64' n= 0.050
9.7	2,588	Total			

Subcatchment 32S: DRAINAGE AREA TO SWALE 2B

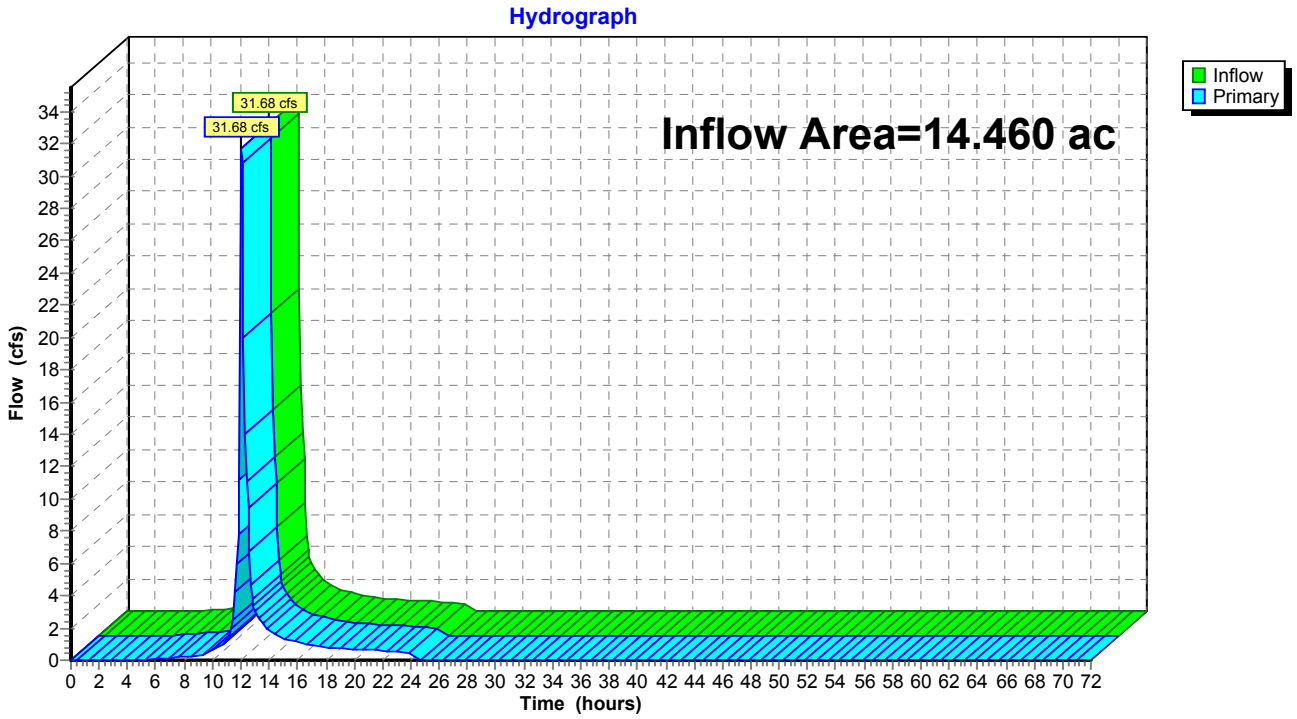


Summary for Link 33L: SWALE 2B

Inflow Area = 14.460 ac, 15.70% Impervious, Inflow Depth = 2.07" for 10-yr event
Inflow = 31.68 cfs @ 12.06 hrs, Volume= 2.493 af
Primary = 31.68 cfs @ 12.06 hrs, Volume= 2.493 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs

Link 33L: SWALE 2B



Summary for Subcatchment 21S: DRAINAGE AREA FROM PAD

[49] Hint: Tc<2dt may require smaller dt

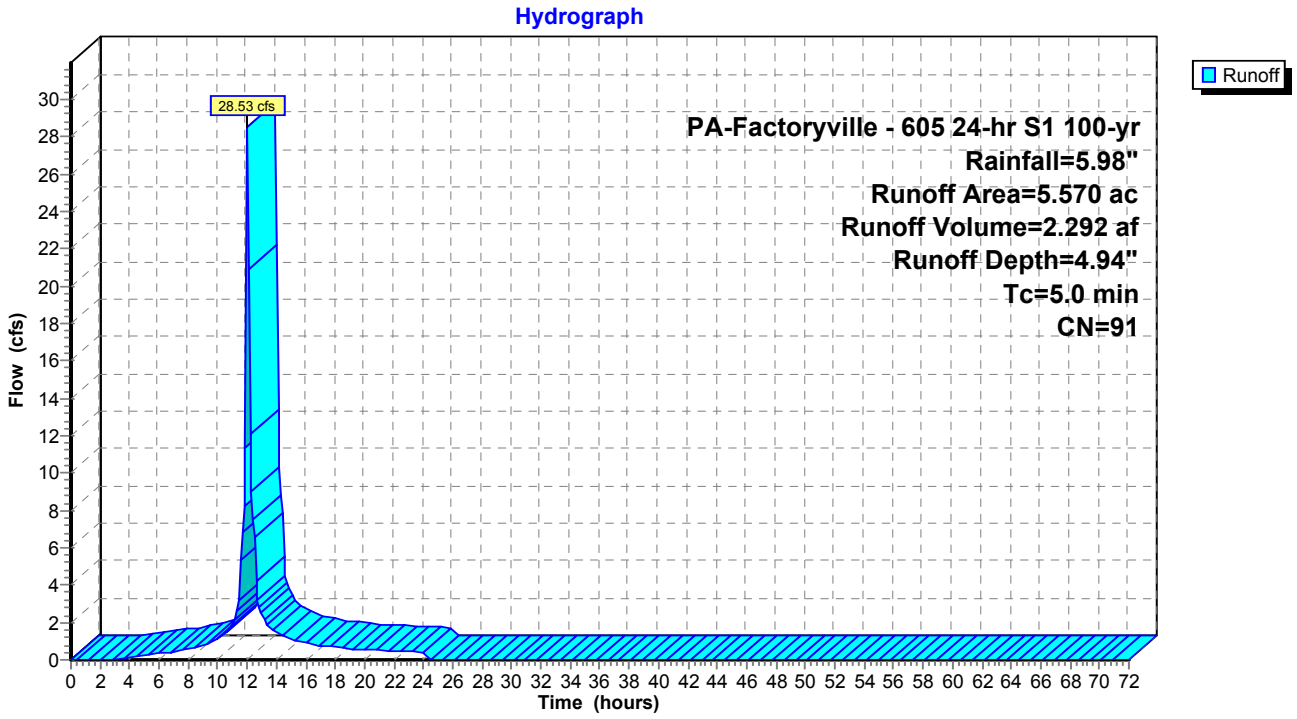
Runoff = 28.53 cfs @ 12.02 hrs, Volume= 2.292 af, Depth= 4.94"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs
PA-Factoryville - 605 24-hr S1 100-yr Rainfall=5.98"

	Area (ac)	CN	Description
	0.760	78	Meadow, non-grazed, HSG D
*	3.180	91	Gravel areas, HSG D
*	1.630	98	Impervious areas, HSG D
	5.570	91	Weighted Average
	3.940		70.74% Pervious Area
	1.630		29.26% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					**Direct Entry,**

Subcatchment 21S: DRAINAGE AREA FROM PAD



Summary for Subcatchment 32S: DRAINAGE AREA TO SWALE 2B

[49] Hint: Tc<2dt may require smaller dt

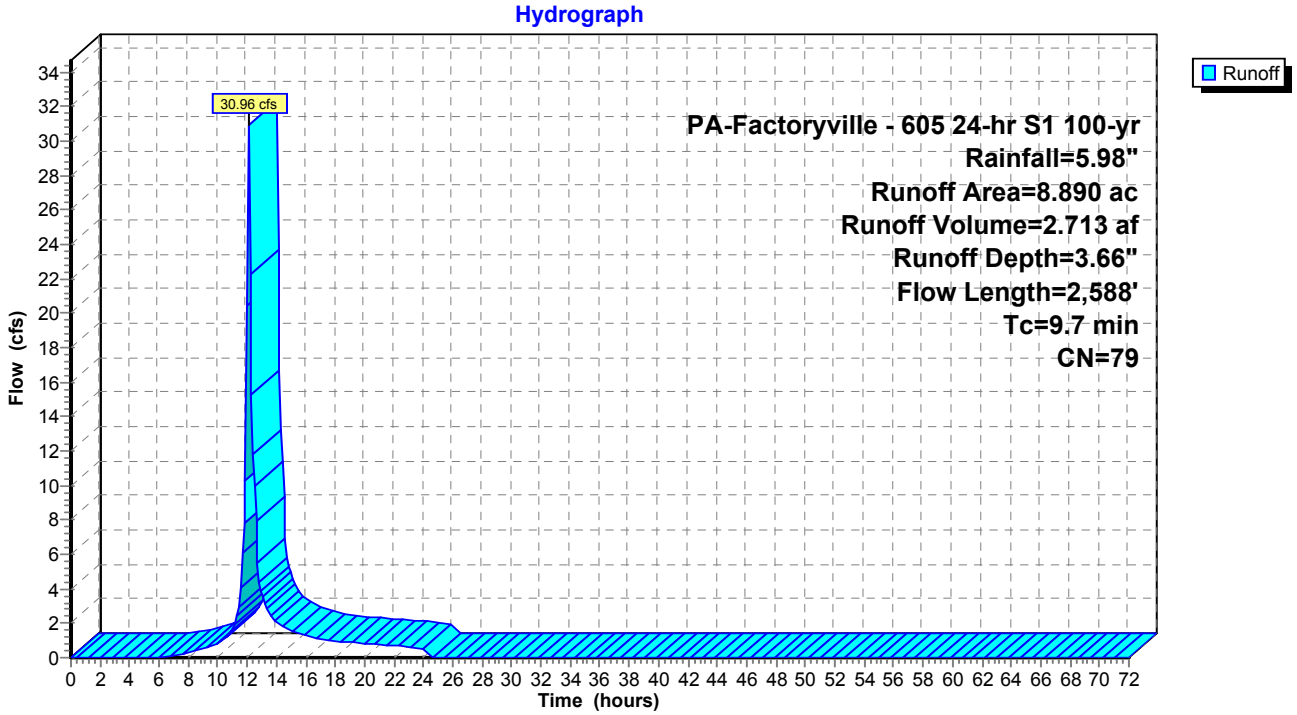
Runoff = 30.96 cfs @ 12.10 hrs, Volume= 2.713 af, Depth= 3.66"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs
PA-Factoryville - 605 24-hr S1 100-yr Rainfall=5.98"

	Area (ac)	CN	Description
	8.250	78	Meadow, non-grazed, HSG D
*	0.640	98	Impervious areas, HSG D
	8.890	79	Weighted Average
	8.250		92.80% Pervious Area
	0.640		7.20% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.0	266	0.0100	1.50		**Shallow Concentrated Flow, SCF-1** Grassed Waterway Kv= 15.0 fps
6.7	2,322	0.0700	5.82	40.72	**Channel Flow,** Area= 7.0 sf Perim= 11.0' r= 0.64' n= 0.050
9.7	2,588	Total			

Subcatchment 32S: DRAINAGE AREA TO SWALE 2B

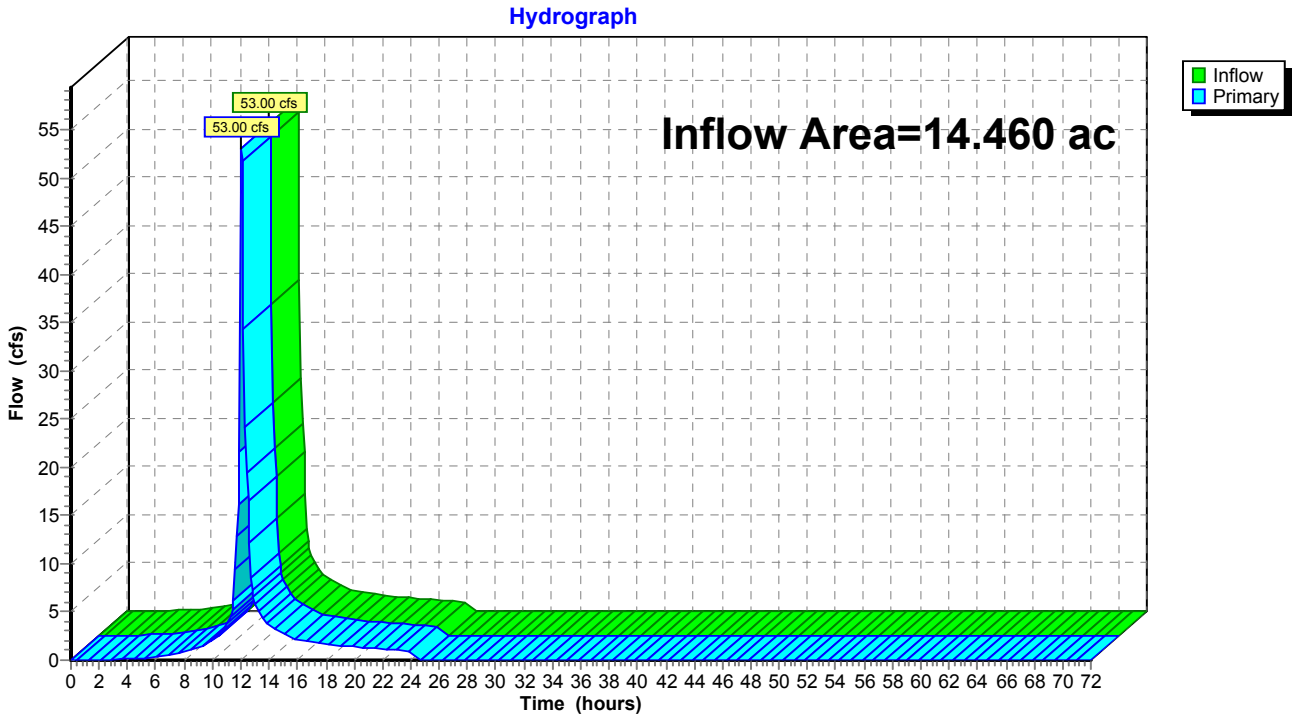


Summary for Link 33L: SWALE 2B

Inflow Area = 14.460 ac, 15.70% Impervious, Inflow Depth = 4.15" for 100-yr event
Inflow = 53.00 cfs @ 12.07 hrs, Volume= 5.005 af
Primary = 53.00 cfs @ 12.07 hrs, Volume= 5.005 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs

Link 33L: SWALE 2B



E&S WORKSHEET # 11
Channel Design Data

PROJECT NAME: ATLANTIC SUNRISE PROJECT - COMPRESSOR STATION # 605

LOCATION: CLINTON TOWNSHIP, WYOMING COUNTY, PA

PREPARED BY: AOE DATE: 02/05/16

CHECKED BY: AJB DATE: 02/05/16

CHANNEL OR CHANNEL SECTION		DITCH 1	DITCH 3	DITCH 5	DITCH 6	DITCH 8
TEMPORARY OR PERMANENT?	(T OR P)	P	P	P	P	P
DESIGN STORM	(2, 5, OR 10 YR)	10	10	10	10	10
ACRES	(AC)	0.34	4.06	1.65	1.38	1.08
MULTIPLIER[1]	(1.6, 2.25, or 2.75)[1]	2.75	2.75	2.75	2.75	2.75
Qr (REQUIRED CAPACITY)	(CFS)	0.94	11.17	4.54	3.80	2.97
Q (CALCULATED AT FLOW DEPTH d)	(CFS)	0.90	7.44	4.61	3.81	2.98
PROTECTIVE LINING[2]		R-4	R-4	R-4	R-4	R-4
n (MANNING'S COEFFICIENT)[2]		0.063	0.05	0.063	0.063	0.063
Va (ALLOWABLE VELOCITY)	(FPS)	N/A	N/A	N/A	N/A	N/A
V (CALCULATED AT FLOW DEPTH d)	(FPS)	1.60	2.07	2.99	2.47	2.50
τa (MAX ALLOWABLE SHEAR STRESS)	(LB/FT^2)	2.00	2.00	2.00	2.00	2.00
τd (CALC'D SHEAR STRESS AT FLOW DEPTH d)	(LB/FT^2)	0.62	0.58	2.00	1.37	1.42
CHANNEL BOTTOM WIDTH	(FT)	2	2	2	2	2
CHANNEL SIDE SLOPES	(H:V)	2	2	2	2	2
D (TOTAL DEPTH)	(FT)	3.0	3.0	4.0	5.0	4.0
CHANNEL TOP WIDTH @ D	(FT)	14	14	18	22	18
d (CALCULATED FLOW DEPTH)	(FT)	0.23	0.93	0.51	0.51	0.42
CHANNEL TOP WIDTH @ FLOW DEPTH d	(FT)	2.92	5.72	4.04	4.04	3.68
BOTTOM WIDTH: FLOW DEPTH RATIO	(12:1 MAX)	8.70	2.15	3.92	3.92	4.76
d50 STONE SIZE	(IN)	6	6	6	6	6
A (CROSS-SECTIONAL AREA)	(SQ. FT.)	0.57	3.59	1.54	1.54	1.19
R (HYDRAULIC RADIUS)		0.19	0.58	0.36	0.36	0.31
S (BED SLOPE)[3]	(FT/FT)	0.043	0.01	0.063	0.043	0.054
Sc (CRITICAL SLOPE)	(FT/FT)	0.033	0.131	0.089	0.089	0.069
.7Sc	(FT/FT)	0.023	0.091	0.062	0.062	0.048
1.3Sc	(FT/FT)	0.043	0.170	0.116	0.116	0.090
STABLE FLOW?	(Y/N)	Y	Y	N	Y	N
FREEBOARD BASED ON UNSTABLE FLOW	(FT)	0.0	0.1	0.1	0.1	0.1
FREEBOARD BASED ON STABLE FLOW	(FT)	0.5	0.5	0.5	0.5	0.5
MINIMUM REQUIRED FREEBOARD[4]	(FT)	0.50	0.5	0.5	0.5	0.5
DESIGN METHOD FOR PROTECTIVE LINING [5] PERMISSIBLE VELOCITY (V) OR SHEAR STRESS	(S)	S	S	S	S	S

1. Use 1.6 for Temporary Channels; 2.25 for Temporary Channels in Special Protection (HQ or EV) Watersheds; 2.75 for Permanent Channels. For Rational Method, enter "N/A" and attach E&S Worksheets 9 and 10. For TR-55 enter "N/A" and attach appropriate Worksheets.
2. Adjust "n" value for changes in channel liner and flow depth. For vegetated channels, provide data for manufactured linings without vegetation and with vegetation in separate columns.
3. Slopes may not be averaged.
4. Minimum Freeboard is 0.5 ft. or ¼ Total Channel Depth, whichever is greater
5. Permissible velocity lining design method is not acceptable for channels with a bed slope of 10% or greater. Shear stress lining design method is required for channels with a bed slope of 10% or greater. Shear stress lining design method may be used for any channel bed slope.

Source: 363-2134-008 / March 31, 2012 / Page 382

E&S WORKSHEET # 11

Channel Design Data

PROJECT NAME: ATLANTIC SUNRISE PROJECT - COMPRESSOR STATION # 605

LOCATION: CLINTON TOWNSHIP, WYOMING COUNTY, PA

PREPARED BY: AOE DATE: 08/16/15

CHECKED BY: AJB DATE: 08/16/15

CHANNEL OR CHANNEL SECTION		DITCH 9	DITCH 10	DITCH 11	DITCH 13	DITCH 14
TEMPORARY OR PERMANENT?	(T OR P)	P	P	P	P	P
DESIGN STORM	(2, 5, OR 10 YR)	10	10	10	10	10
ACRES	(AC)	0.86	4.40	0.42	0.91	0.54
MULTIPLIER[1]	(1.6, 2.25, or 2.75)[1]	2.75	2.75	2.75	2.75	2.75
Qr (REQUIRED CAPACITY)	(CFS)	2.37	12.10	1.16	2.50	1.49
Q (CALCULATED AT FLOW DEPTH d)	(CFS)	2.38	12.02	1.21	2.56	1.53
PROTECTIVE LINING[2]		R-4	R-4	R-4	R-4	R-4
n (MANNING'S COEFFICIENT)[2]		0.063	0.047	0.063	0.063	0.063
Va (ALLOWABLE VELOCITY)	(FPS)	N/A	N/A	N/A	N/A	N/A
V (CALCULATED AT FLOW DEPTH d)	(FPS)	1.88	2.46	1.55	2.15	1.24
τa (MAX ALLOWABLE SHEAR STRESS)	(LB/FT^2)	2.00	2.00	2.00	2.00	2.00
τd (CALC'D SHEAR STRESS AT FLOW DEPTH d)	(LB/FT^2)	0.80	0.71	0.56	1.05	0.35
CHANNEL BOTTOM WIDTH	(FT)	2	2	2	2	2
CHANNEL SIDE SLOPES	(H:V)	2	2	2	2	2
D (TOTAL DEPTH)	(FT)	5.0	5.0	6.0	5.0	2.0
CHANNEL TOP WIDTH @ D	(FT)	22	22	26	22	10
d (CALCULATED FLOW DEPTH)	(FT)	0.44	1.14	0.30	0.42	0.43
CHANNEL TOP WIDTH @ FLOW DEPTH d	(FT)	3.76	6.56	3.20	3.68	3.72
BOTTOM WIDTH: FLOW DEPTH RATIO	(12:1 MAX)	4.55	1.75	6.67	4.76	4.65
d50 STONE SIZE	(IN)	6	6	6	6	6
A (CROSS-SECTIONAL AREA)	(SQ. FT.)	1.27	4.88	0.78	1.19	1.23
R (HYDRAULIC RADIUS)		0.32	0.69	0.23	0.31	0.31
S (BED SLOPE)[3]	(FT/FT)	0.029	0.01	0.03	0.04	0.013
Sc (CRITICAL SLOPE)	(FT/FT)	0.073	0.157	0.045	0.069	0.071
.7Sc	(FT/FT)	0.051	0.110	0.032	0.048	0.050
1.3Sc	(FT/FT)	0.095	0.204	0.059	0.090	0.092
STABLE FLOW?	(Y/N)	Y	Y	Y	Y	Y
FREEBOARD BASED ON UNSTABLE FLOW	(FT)	0.1	0.2	0.0	0.1	0.0
FREEBOARD BASED ON STABLE FLOW	(FT)	0.5	0.5	0.5	0.5	0.5
MINIMUM REQUIRED FREEBOARD[4]	(FT)	0.50	0.5	0.5	0.5	0.5
DESIGN METHOD FOR PROTECTIVE LINING [5] PERMISSIBLE VELOCITY (V) OR SHEAR STRESS	(S)	S	S	S	S	S

1. Use 1.6 for Temporary Channels; 2.25 for Temporary Channels in Special Protection (HQ or EV) Watersheds; 2.75 for Permanent Channels. For Rational Method, enter "N/A" and attach E&S Worksheets 9 and 10. For TR-55 enter "N/A" and attach appropriate Worksheets.
2. Adjust "n" value for changes in channel liner and flow depth. For vegetated channels, provide data for manufactured linings without vegetation and with vegetation in separate columns.
3. Slopes may not be averaged.
4. Minimum Freeboard is 0.5 ft. or ¼ Total Channel Depth, whichever is greater
5. Permissible velocity lining design method is not acceptable for channels with a bed slope of 10% or greater. Shear stress lining design method is required for channels with a bed slope of 10% or greater. Shear stress lining design method may be used for any channel bed slope.

Source: 363-2134-008 / March 31, 2012 / Page 382

E&S WORKSHEET # 11

Channel Design Data

PROJECT NAME: ATLANTIC SUNRISE PROJECT - COMPRESSOR STATION # 605

LOCATION: CLINTON TOWNSHIP, WYOMING COUNTY

PREPARED BY: AOE **DATE:** 11/16/15

CHECKED BY: AJB **DATE:** 11/16/15

CHANNEL OR CHANNEL SECTION		EX. ROADSIDE SWALE				
TEMPORARY OR PERMANENT?	(T OR P)	P				
DESIGN STORM	(2, 5, OR 10 YR)	10				
ACRES	(AC)	106.43				
MULTIPLIER[1]	(1.6, 2.25, or 2.75)[1]	N/A				
Qr (REQUIRED CAPACITY)	(CFS)	68 - 10 YEAR DESIGN STORM, SEE CULVERT A HYDROCAD REPORT				
Q (CALCULATED AT FLOW DEPTH d)	(CFS)	68.00				
PROTECTIVE LINING[2]		N/A				
n (MANNING'S COEFFICIENT)[2]		0.106	SEE CHANNEL REPORT			
Va (ALLOWABLE VELOCITY)	(FPS)	3				
V (CALCULATED AT FLOW DEPTH d)	(FPS)	2.41				
τa (MAX ALLOWABLE SHEAR STRESS)	(LB/FT^2)	N/A				
τd (CALC'D SHEAR STRESS AT FLOW DEPTH d)	(LB/FT^2)	N/A				
CHANNEL BOTTOM WIDTH	(FT)	11				
CHANNEL SIDE SLOPES	(H:V)	VARIES	SEE CHANNEL REPORT			
D (TOTAL DEPTH)	(FT)	1.9				
CHANNEL TOP WIDTH @ D	(FT)	23.26				
d (CALCULATED FLOW DEPTH)	(FT)	1.88				
CHANNEL TOP WIDTH @ FLOW DEPTH d	(FT)	23.26				
BOTTOM WIDTH: FLOW DEPTH RATIO	(12:1 MAX)	5.85				
d50 STONE SIZE	(IN)	N/A				
A (CROSS-SECTIONAL AREA)	(SQ. FT.)	28.20				
R (HYDRAULIC RADIUS)		1.18				
S (BED SLOPE)[3]	(FT/FT)	0.024				
Sc (CRITICAL SLOPE)	(FT/FT)	0.159				
.7Sc	(FT/FT)	0.111				
1.3Sc	(FT/FT)	0.207				
STABLE FLOW?	(Y/N)	Y				
FREEBOARD BASED ON UNSTABLE FLOW	(FT)	0.34				
FREEBOARD BASED ON STABLE FLOW	(FT)	0.50				
MINIMUM REQUIRED FREEBOARD[4]	(FT)	0.50				
DESIGN METHOD FOR PROTECTIVE LINING [5] PERMISSIBLE VELOCITY (V) OR SHEAR STRESS	(S)	V				

1. Use 1.6 for Temporary Channels; 2.25 for Temporary Channels in Special Protection (HQ or EV) Watersheds; 2.75 for Permanent Channels. For Rational Method, enter "N/A" and attach E&S Worksheets 9 and 10. For TR-55 enter "N/A" and attach appropriate Worksheets.
2. Adjust "n" value for changes in channel liner and flow depth. For vegetated channels, provide data for manufactured linings without vegetation and with vegetation in separate columns.
3. Slopes may not be averaged.
4. Minimum Freeboard is 0.5 ft. or ¼ Total Channel Depth, whichever is greater
5. Permissible velocity lining design method is not acceptable for channels with a bed slope of 10% or greater. Shear stress lining design method is required for channels with a bed slope of 10% or greater. Shear stress lining design method may be used for any channel bed slope.

Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc. Monday, Nov 16 2015

EXISTING ROAD SWALE 10 YEAR STORM

User-defined

Invert Elev (ft)	= 941.17
Slope (%)	= 2.40
N-Value	= 0.106

Calculations

Compute by:	Known Q
Known Q (cfs)	= 68.00

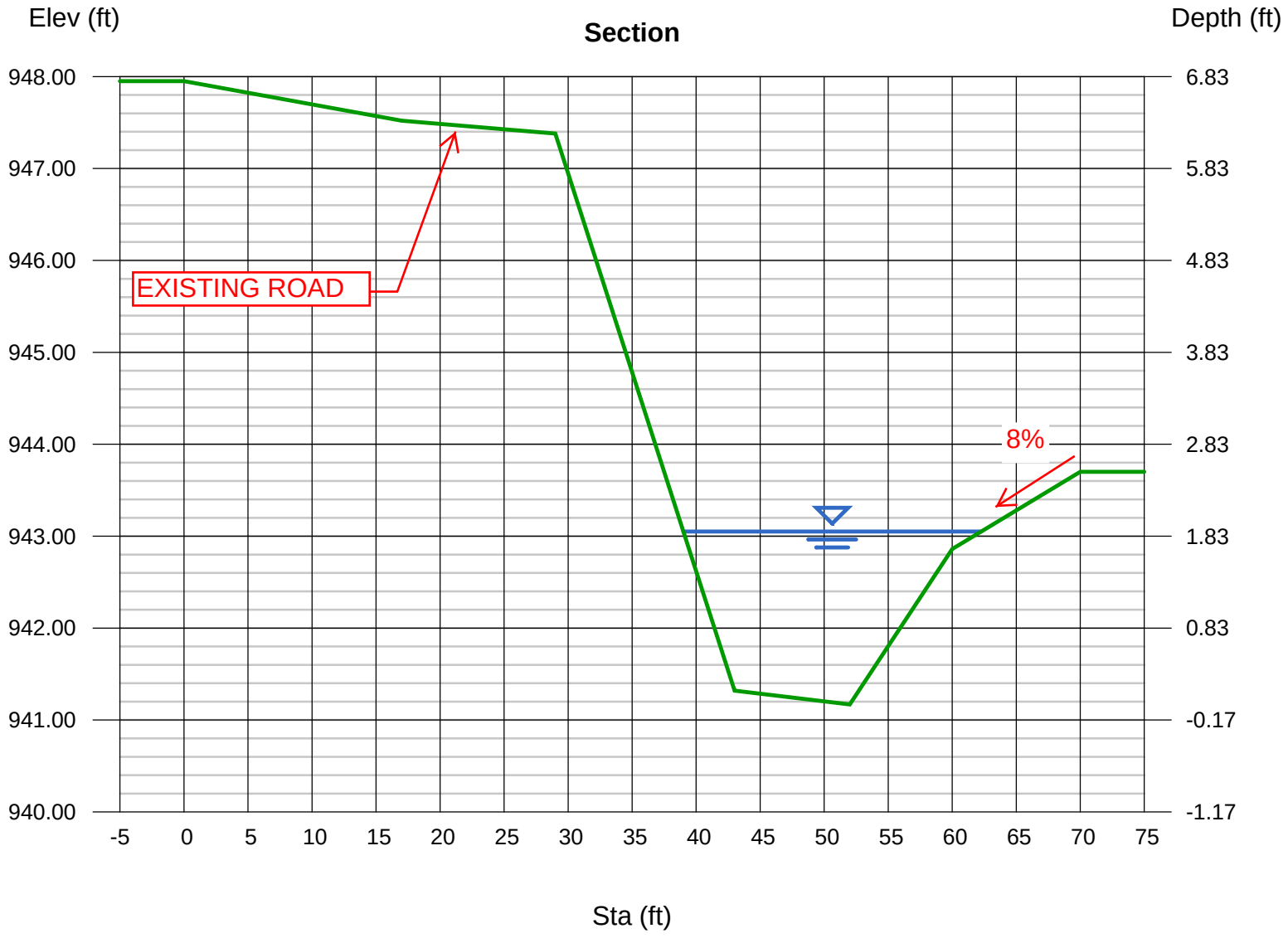
Highlighted

Depth (ft)	= 1.88
Q (cfs)	= 68.00
Area (sqft)	= 28.20
Velocity (ft/s)	= 2.41
Wetted Perim (ft)	= 23.80
Crit Depth, Yc (ft)	= 1.12
Top Width (ft)	= 23.26
EGL (ft)	= 1.97

(Sta, El, n)-(Sta, El, n)...

(0.00, 947.95)-(17.00, 947.52, 0.015)-(29.00, 947.38, 0.015)-(43.00, 941.32, 0.065)-(52.00, 941.17, 0.065)-(60.00, 942.86, 0.150)-(70.00, 943.70, 0.150)

THE FLOW TO THE EXISTING ROAD SIDE SWALE IS THE DISCHARGE FROM PROPOSED CULVERT A DURING A 10 YEAR STORM. THE FLOW VELOCITY IS LESS THAN 3 FPS THEREFORE THE SWALE IS STABLE.



A.2 Culvert Calculations

Culvert Report

CULVERT A - 50 YEAR STORM ANALYSIS

Invert Elev Dn (ft)	=	942.30
Pipe Length (ft)	=	64.00
Slope (%)	=	1.48
Invert Elev Up (ft)	=	943.25
Rise (in)	=	38.0
Shape	=	Elliptical
Span (in)	=	60.0
No. Barrels	=	1
n-Value	=	0.012
Culvert Type	=	Horizontal Ellipse Concrete
Culvert Entrance	=	Square edge w/headwall (H)
Coeff. K,M,c,Y,k	=	0.01, 2, 0.0398, 0.67, 0.5

Embankment

Top Elevation (ft)	=	948.00
Top Width (ft)	=	24.00
Crest Width (ft)	=	50.00

Calculations

Qmin (cfs)	=	82.00
Qmax (cfs)	=	82.00
Tailwater Elev (ft)	=	(dc+D)/2

Highlighted

Qtotal (cfs)	=	82.00
Qpipe (cfs)	=	82.00
Qovertop (cfs)	=	0.00
Veloc Dn (ft/s)	=	7.58
Veloc Up (ft/s)	=	10.22
HGL Dn (ft)	=	944.83
HGL Up (ft)	=	945.15
Hw Elev (ft)	=	947.19
Hw/D (ft)	=	1.24
Flow Regime	=	Inlet Control

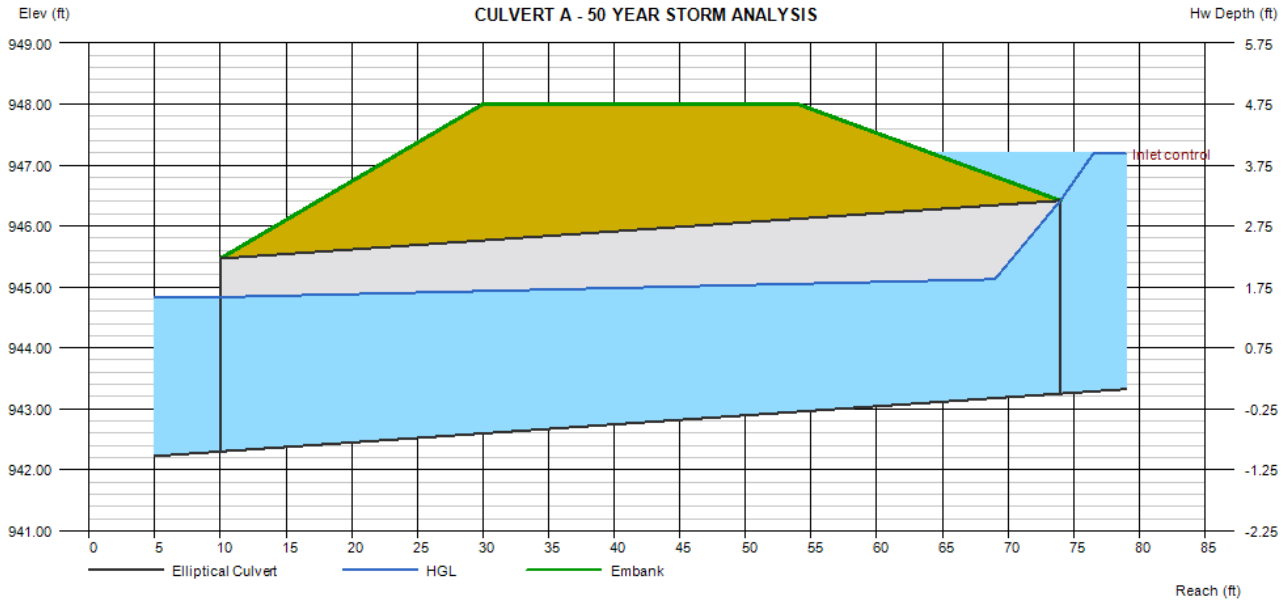
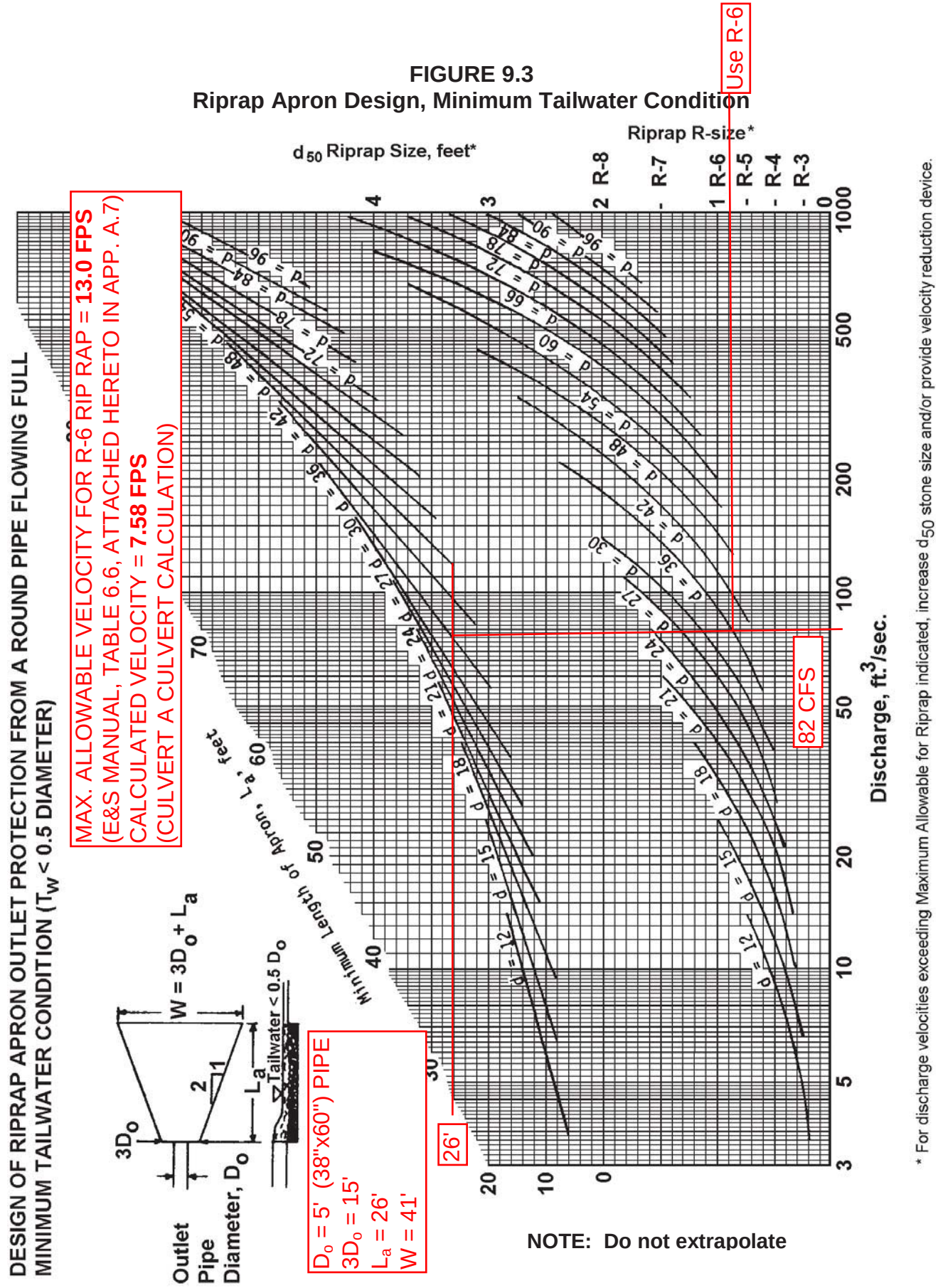
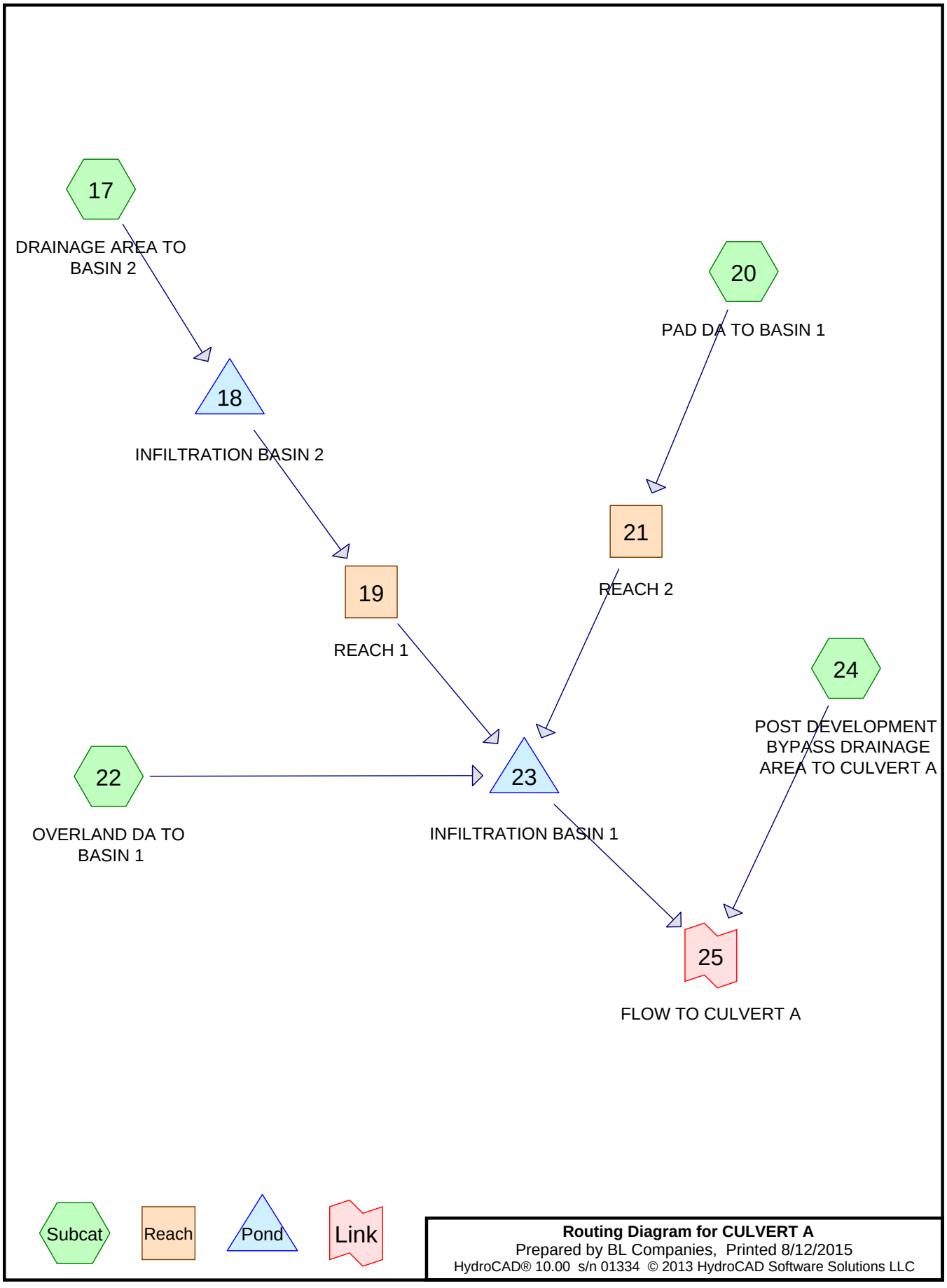


FIGURE 9.3
Riprap Apron Design, Minimum Tailwater Condition



Adapted from USDA - NRCS

Not to be used for Box Culverts



Routing Diagram for CULVERT A
Prepared by BL Companies, Printed 8/12/2015

Summary for Subcatchment 17: DRAINAGE AREA TO BASIN 2

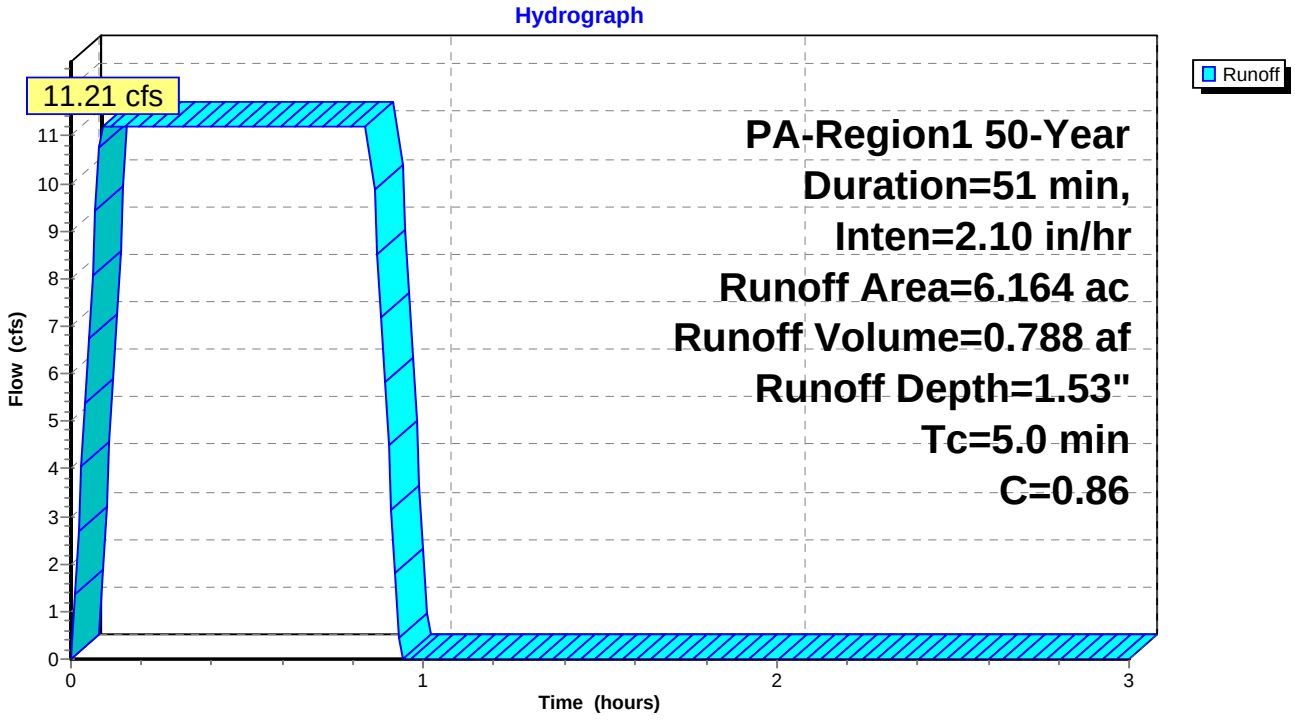
Runoff = 11.21 cfs @ 0.09 hrs, Volume= 0.788 af, Depth= 1.53"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
PA-Region1 50-Year Duration=51 min, Inten=2.10 in/hr

Area (ac)	C	Description
0.880	0.95	Impervious, HSG D
1.506	0.70	Grass/Meadow/Pasture, HSG D
3.778	0.90	Gravel Areas, HSG D
6.164	0.86	Weighted Average
5.284		85.72% Pervious Area
0.880		14.28% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					**Direct Entry,**

Subcatchment 17: DRAINAGE AREA TO BASIN 2



Summary for Subcatchment 20: PAD DA TO BASIN 1

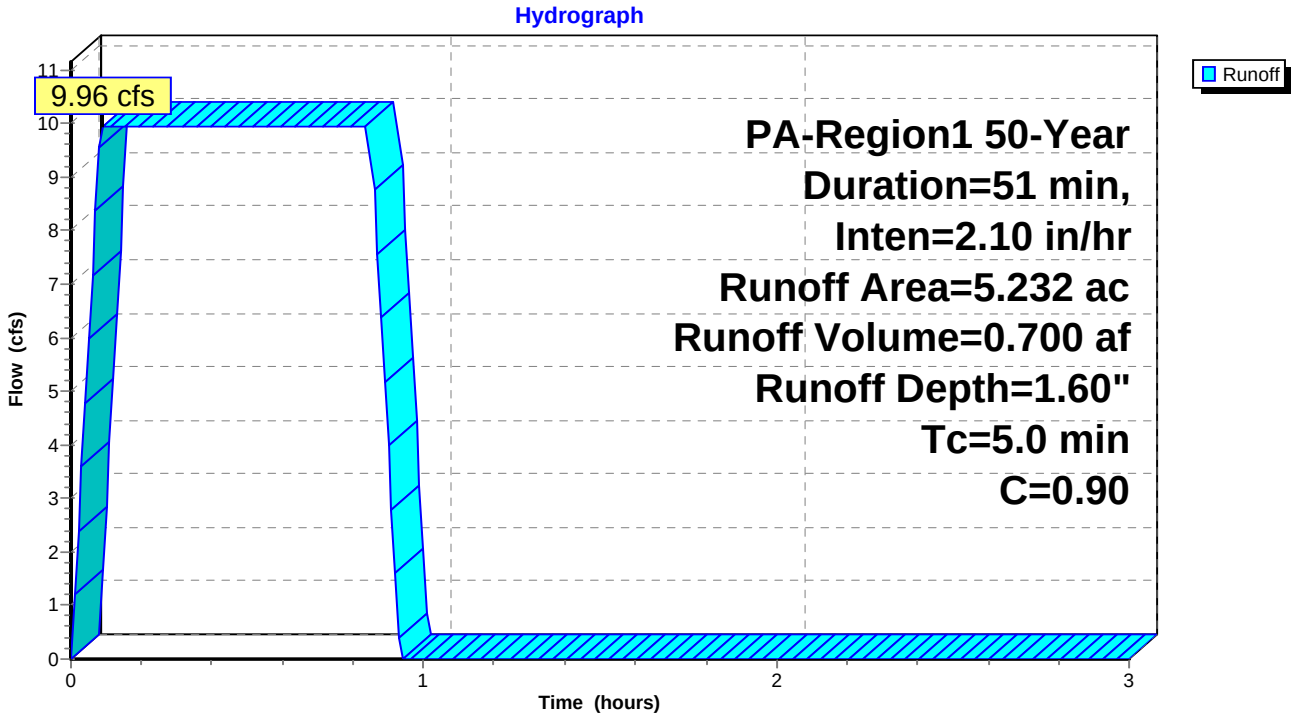
Runoff = 9.96 cfs @ 0.09 hrs, Volume= 0.700 af, Depth= 1.60"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
PA-Region1 50-Year Duration=51 min, Inten=2.10 in/hr

Area (ac)	C	Description
0.481	0.70	Meadow/grassland/range, Good, HSG D
3.149	0.90	Gravel areas, HSG D
1.602	0.95	Impervious areas, HSG D
5.232	0.90	Weighted Average
3.630		69.38% Pervious Area
1.602		30.62% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					**Direct Entry,**

Subcatchment 20: PAD DA TO BASIN 1



Summary for Subcatchment 22: OVERLAND DA TO BASIN 1

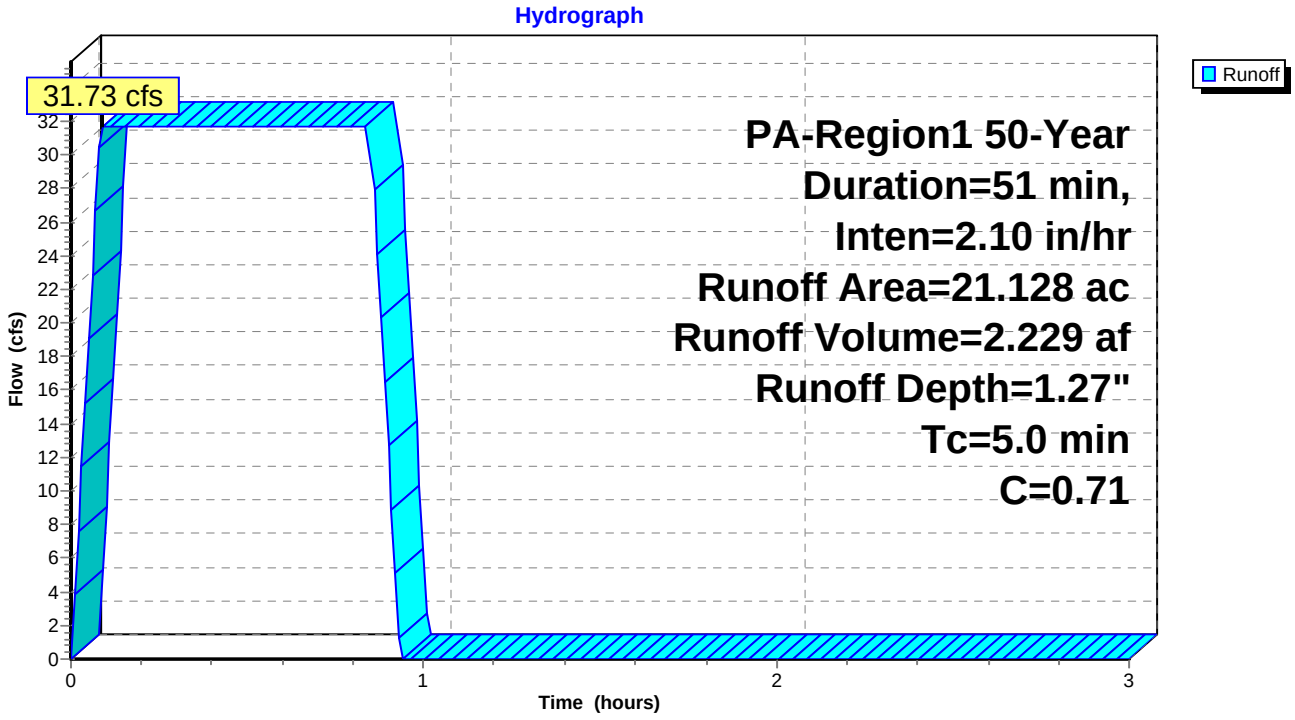
Runoff = 31.73 cfs @ 0.09 hrs, Volume= 2.229 af, Depth= 1.27"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
PA-Region1 50-Year Duration=51 min, Inten=2.10 in/hr

Area (ac)	C	Description
19.580	0.70	Meadow/grassland/range, Good, HSG D
0.269	0.30	Woods, Good, HSG D
1.279	0.95	Impervious areas, HSG D
21.128	0.71	Weighted Average
19.849		93.95% Pervious Area
1.279		6.05% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					**Direct Entry,**

Subcatchment 22: OVERLAND DA TO BASIN 1



Summary for Subcatchment 24: POST DEVELOPMENT BYPASS DRAINAGE AREA TO CULVERT A

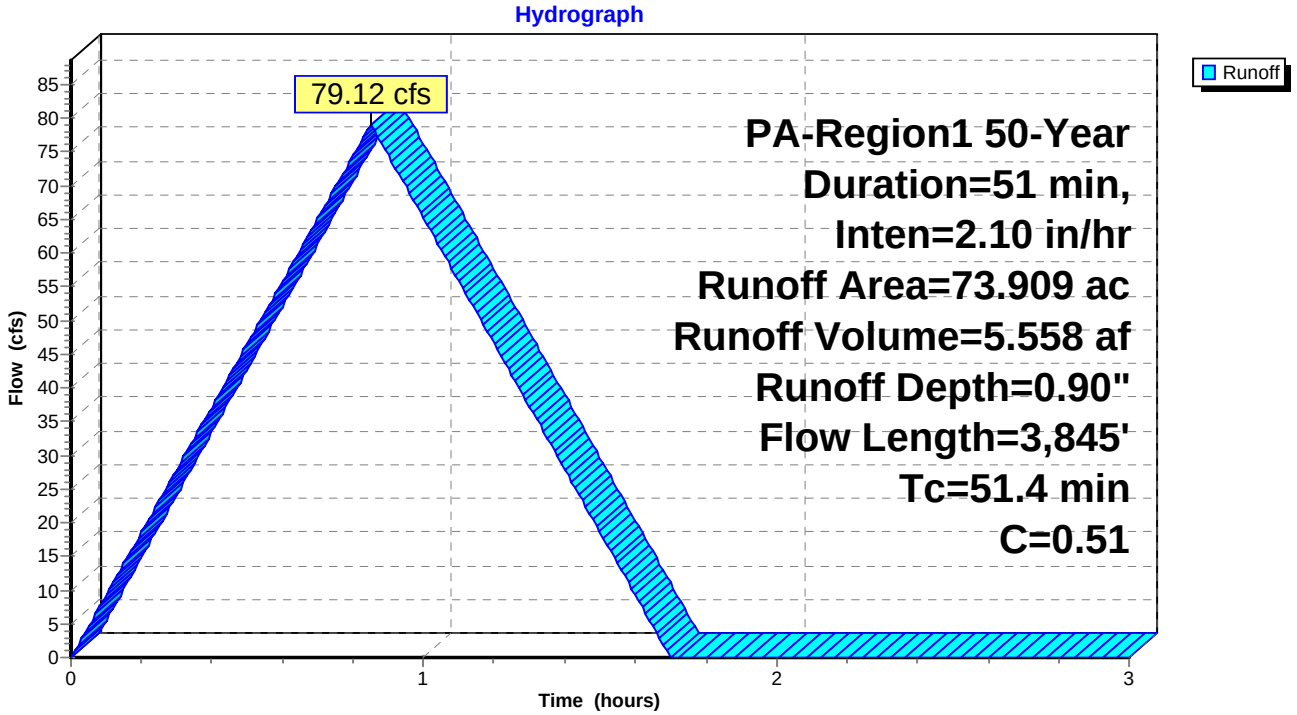
Runoff = 79.12 cfs @ 0.85 hrs, Volume= 5.558 af, Depth= 0.90"

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
PA-Region1 50-Year Duration=51 min, Inten=2.10 in/hr

Area (ac)	C	Description
36.847	0.30	Woods, Good, HSG D
35.556	0.70	Pasture/grassland/range, Good, HSG D
1.506	0.95	Impervious areas, HSG D
73.909	0.51	Weighted Average
72.403		97.96% Pervious Area
1.506		2.04% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
11.9	100	0.0420	0.14		**Sheet Flow, SHT 1** Grass: Dense n= 0.240 P2= 2.54"
6.2	685	0.0700	1.85		**Shallow Concentrated Flow, SCF 1** Short Grass Pasture Kv= 7.0 fps
8.8	1,028	0.1500	1.94		**Shallow Concentrated Flow, SCF 2** Woodland Kv= 5.0 fps
24.5	2,032	0.0085	1.38		**Shallow Concentrated Flow, SCF 3** Grassed Waterway Kv= 15.0 fps
51.4	3,845	Total			

Subcatchment 24: POST DEVELOPMENT BYPASS DRAINAGE AREA TO CULVERT A



Summary for Reach 19: REACH 1

Inflow Area = 6.164 ac, 14.28% Impervious, Inflow Depth = 1.17" for 50-Year event
Inflow = 10.74 cfs @ 0.85 hrs, Volume= 0.602 af
Outflow = 10.72 cfs @ 0.96 hrs, Volume= 0.601 af, Atten= 0%, Lag= 6.4 min

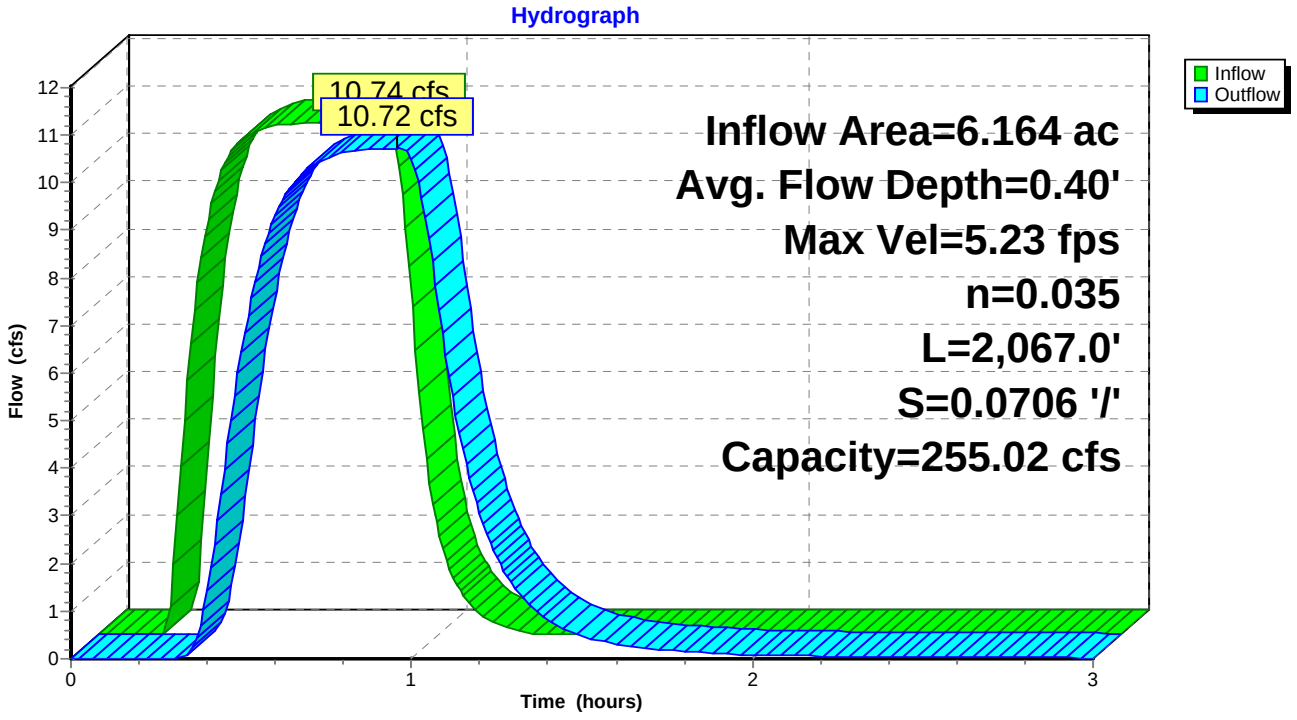
Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
Max. Velocity= 5.23 fps, Min. Travel Time= 6.6 min
Avg. Velocity = 2.22 fps, Avg. Travel Time= 15.5 min

Peak Storage= 4,239 cf @ 0.85 hrs
Average Depth at Peak Storage= 0.40'
Bank-Full Depth= 2.00' Flow Area= 20.0 sf, Capacity= 255.02 cfs

4.00' x 2.00' deep channel, n= 0.035
Side Slope Z-value= 3.0 '/' Top Width= 16.00'
Length= 2,067.0' Slope= 0.0706 '/'
Inlet Invert= 1,106.00', Outlet Invert= 960.00'

‡

Reach 19: REACH 1



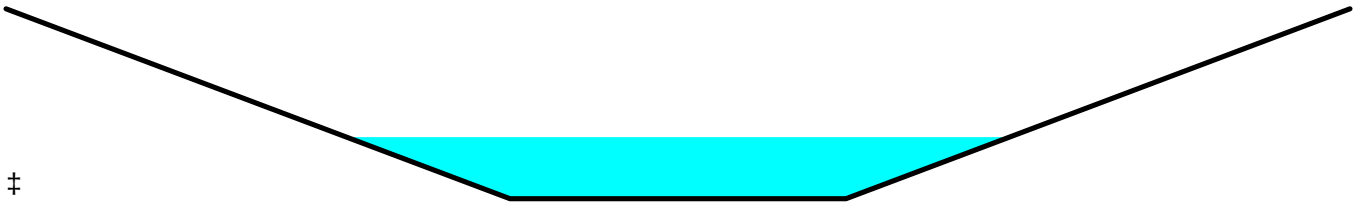
Summary for Reach 21: REACH 2

Inflow Area = 5.232 ac, 30.62% Impervious, Inflow Depth = 1.60" for 50-Year event
Inflow = 9.96 cfs @ 0.09 hrs, Volume= 0.700 af
Outflow = 9.79 cfs @ 1.10 hrs, Volume= 0.691 af, Atten= 2%, Lag= 60.3 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
Max. Velocity= 2.53 fps, Min. Travel Time= 14.8 min
Avg. Velocity = 1.32 fps, Avg. Travel Time= 28.4 min

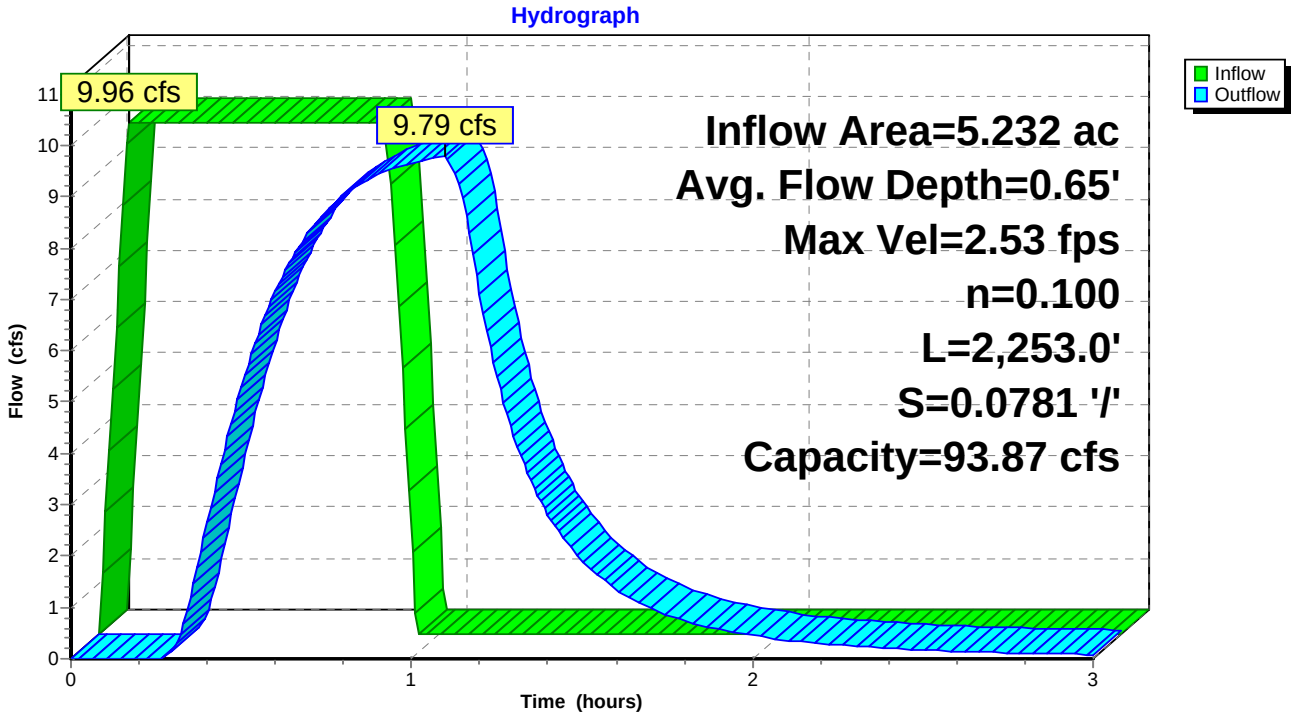
Peak Storage= 8,703 cf @ 0.85 hrs
Average Depth at Peak Storage= 0.65'
Bank-Full Depth= 2.00' Flow Area= 20.0 sf, Capacity= 93.87 cfs

4.00' x 2.00' deep channel, n= 0.100
Side Slope Z-value= 3.0 '/' Top Width= 16.00'
Length= 2,253.0' Slope= 0.0781 '/'
Inlet Invert= 1,130.00', Outlet Invert= 954.00'



‡

Reach 21: REACH 2



Summary for Pond 18: INFILTRATION BASIN 2

Inflow Area = 6.164 ac, 14.28% Impervious, Inflow Depth = 1.53" for 50-Year event
Inflow = 11.21 cfs @ 0.09 hrs, Volume= 0.788 af
Outflow = 11.21 cfs @ 0.85 hrs, Volume= 0.694 af, Atten= 0%, Lag= 45.6 min
Discarded = 0.48 cfs @ 0.85 hrs, Volume= 0.093 af
Primary = 10.74 cfs @ 0.85 hrs, Volume= 0.602 af

Routing by Stor-Ind method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
Peak Elev= 1,120.42' @ 0.85 hrs Surf.Area= 7,719 sf Storage= 9,182 cf

Plug-Flow detention time= 18.2 min calculated for 0.692 af (88% of inflow)
Center-of-Mass det. time= 15.6 min (43.6 - 28.0)

Volume	Invert	Avail.Storage	Storage Description
#1	1,118.00'	56,769 cf	**Custom Stage Data (Prismatic)**Listed below (Recalc)

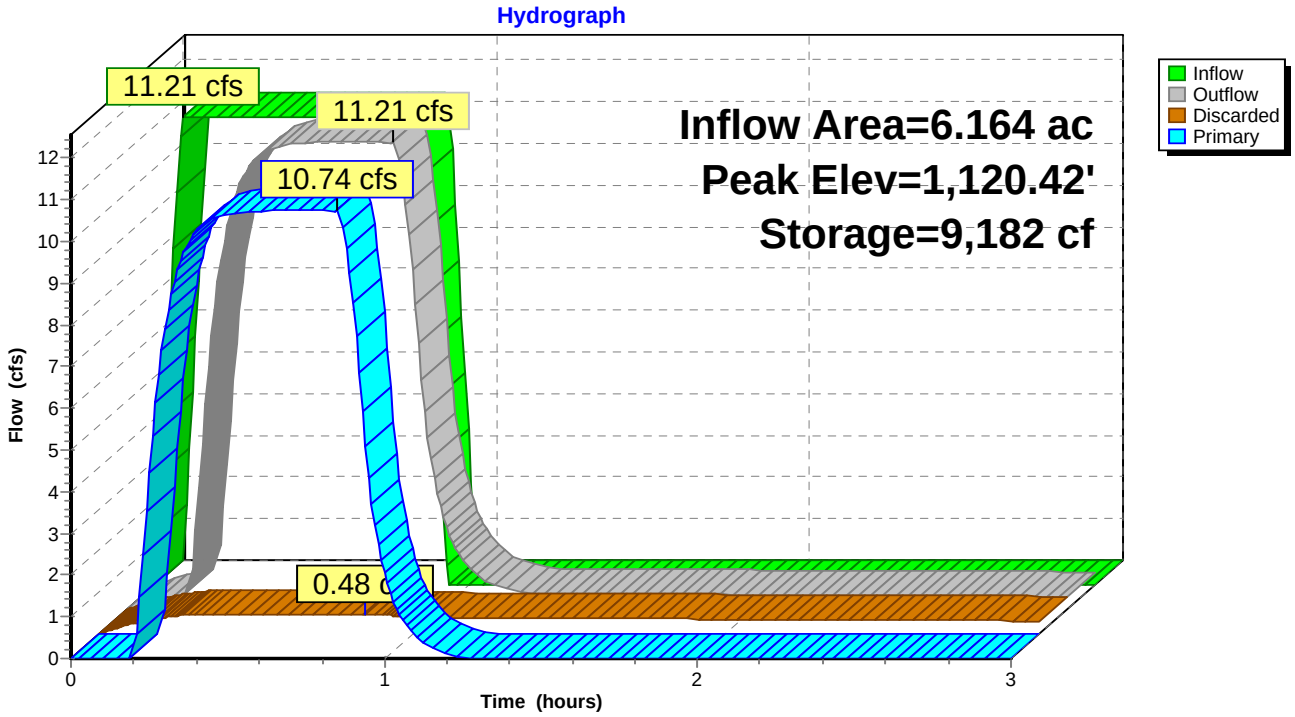
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
1,118.00	0	0	0
1,120.00	6,243	6,243	6,243
1,122.00	13,256	19,499	25,742
1,124.00	17,771	31,027	56,769

Device	Routing	Invert	Outlet Devices
#1	Primary	1,117.00'	**18.0" Round Culvert** L= 66.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 1,117.00' / 1,111.00' S= 0.0909 '/' Cc= 0.900 n= 0.012, Flow Area= 1.77 sf
#2	Discarded	1,118.00'	**2.660 in/hr Exfiltration over Surface area**
#3	Device 1	1,120.00'	**24.0" x 48.0" Horiz. Orifice/Grate** C= 0.600 Limited to weir flow at low heads
#4	Primary	1,120.50'	**20.0' long x 17.0' breadth Broad-Crested Rectangular Weir** Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Discarded OutFlow Max=0.48 cfs @ 0.85 hrs HW=1,120.42' (Free Discharge)
└**2=Exfiltration** (Exfiltration Controls 0.48 cfs)

Primary OutFlow Max=10.72 cfs @ 0.85 hrs HW=1,120.42' (Free Discharge)
└**1=Culvert** (Passes 10.72 cfs of 13.91 cfs potential flow)
└**3=Orifice/Grate** (Weir Controls 10.72 cfs @ 2.12 fps)
└**4=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)

Pond 18: INFILTRATION BASIN 2



Summary for Pond 23: INFILTRATION BASIN 1

Inflow Area = 32.524 ac, 11.56% Impervious, Inflow Depth > 1.30" for 50-Year event
Inflow = 51.67 cfs @ 0.85 hrs, Volume= 3.521 af
Outflow = 4.48 cfs @ 1.35 hrs, Volume= 0.837 af, Atten= 91%, Lag= 30.2 min
Discarded = 1.16 cfs @ 1.35 hrs, Volume= 0.248 af
Primary = 3.32 cfs @ 1.35 hrs, Volume= 0.590 af

Routing by Stor-Ind method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
Peak Elev= 954.38' @ 1.35 hrs Surf.Area= 41,605 sf Storage= 137,009 cf

Plug-Flow detention time= 93.6 min calculated for 0.835 af (24% of inflow)
Center-of-Mass det. time= 67.8 min (105.9 - 38.1)

Volume	Invert	Avail.Storage	Storage Description
#1	949.00'	314,703 cf	**Custom Stage Data (Prismatic)**Listed below (Recalc)

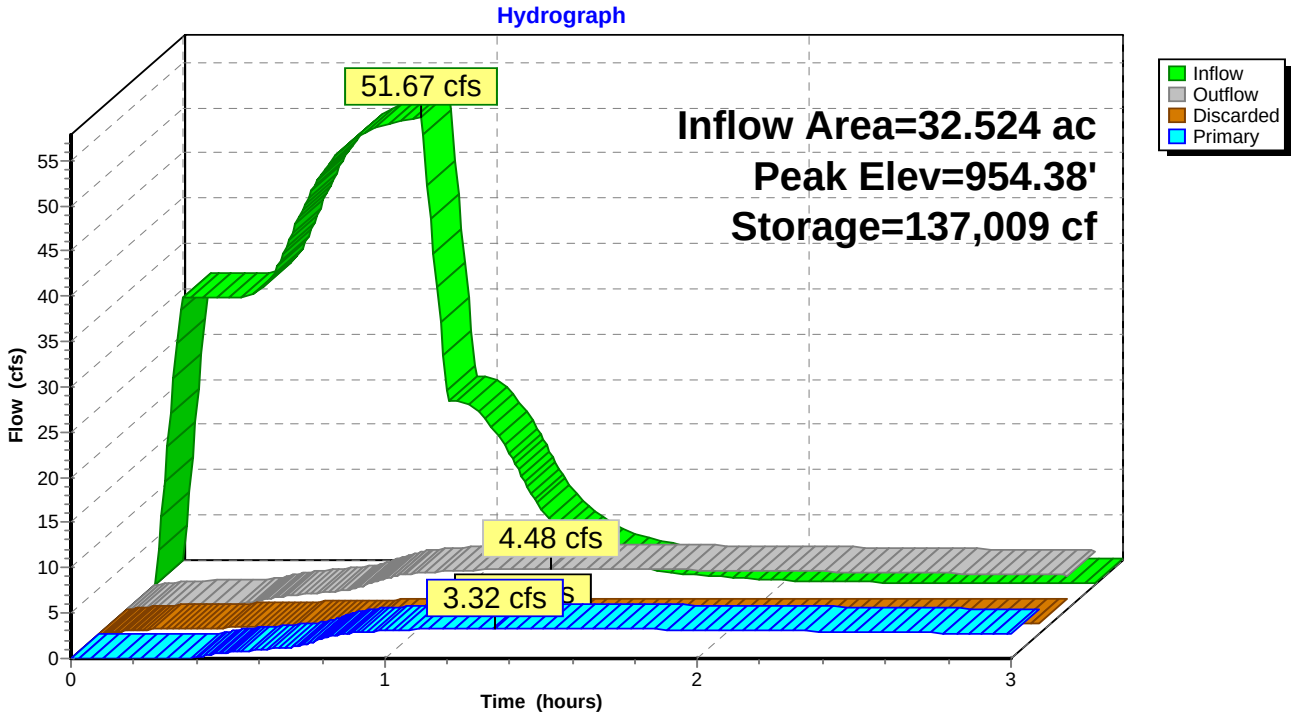
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
949.00	5,082	0	0
950.00	16,872	10,977	10,977
952.00	27,255	44,127	55,104
954.00	39,375	66,630	121,734
956.00	51,198	90,573	212,307
958.00	51,198	102,396	314,703

Device	Routing	Invert	Outlet Devices
#1	Primary	948.00'	**18.0" Round Culvert** L= 77.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 948.00' / 947.50' S= 0.0065 '/' Cc= 0.900 n= 0.012, Flow Area= 1.77 sf
#2	Discarded	949.00'	**1.200 in/hr Exfiltration over Surface area**
#3	Device 1	951.25'	**6.0" Vert. Orifice/Grate** C= 0.600
#4	Device 1	953.00'	**8.0" Vert. Orifice/Grate** C= 0.600
#5	Device 1	955.00'	**8.0" Vert. Orifice/Grate** C= 0.600
#6	Primary	957.00'	**30.0' long x 15.5' breadth Broad-Crested Rectangular Weir** Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Discarded OutFlow Max=1.16 cfs @ 1.35 hrs HW=954.38' (Free Discharge)
└**2=Exfiltration** (Exfiltration Controls 1.16 cfs)

Primary OutFlow Max=3.32 cfs @ 1.35 hrs HW=954.38' (Free Discharge)
├**1=Culvert** (Passes 3.32 cfs of 20.01 cfs potential flow)
│ ├**3=Orifice/Grate** (Orifice Controls 1.60 cfs @ 8.17 fps)
│ ├**4=Orifice/Grate** (Orifice Controls 1.72 cfs @ 4.92 fps)
│ └**5=Orifice/Grate** (Controls 0.00 cfs)
└**6=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)

Pond 23: INFILTRATION BASIN 1

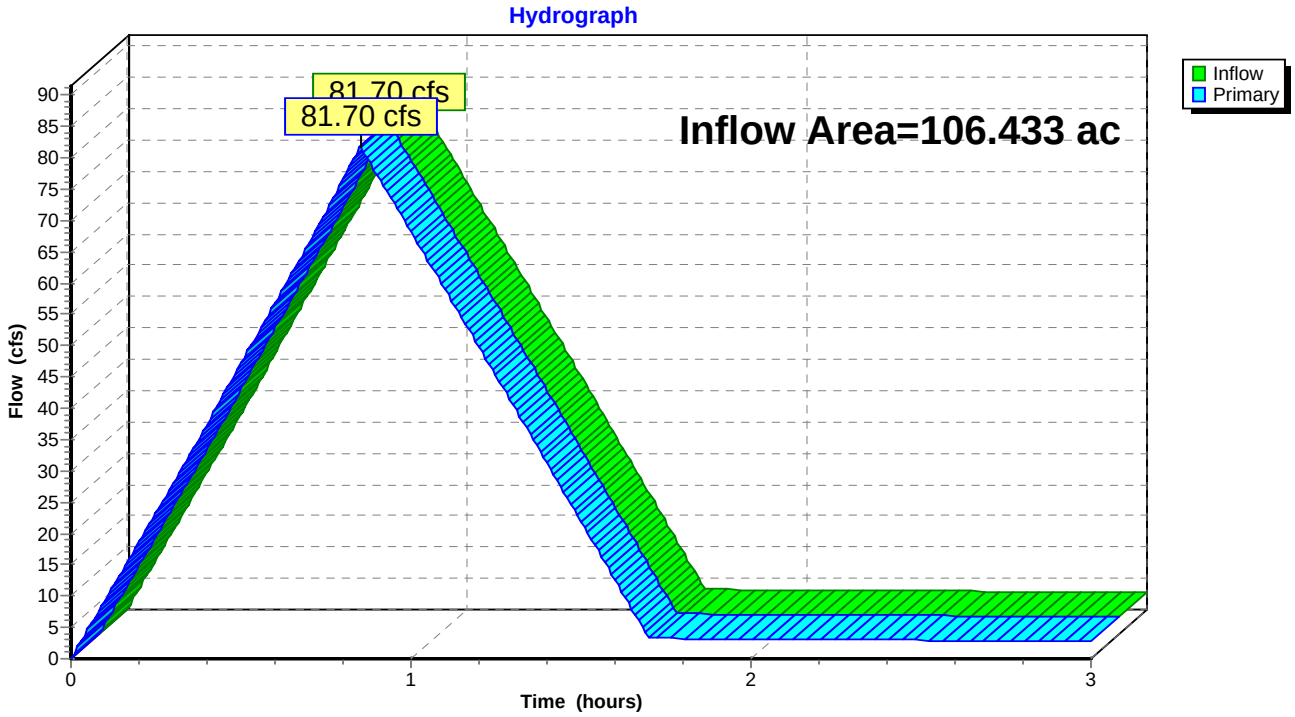


Summary for Link 25: FLOW TO CULVERT A

Inflow Area = 106.433 ac, 4.95% Impervious, Inflow Depth > 0.69" for 50-Year event
Inflow = 81.70 cfs @ 0.85 hrs, Volume= 6.148 af
Primary = 81.70 cfs @ 0.85 hrs, Volume= 6.148 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

Link 25: FLOW TO CULVERT A



Culvert Report

CULVERT B - 100 YEAR STORM ANAYLSIS

Invert Elev Dn (ft)	=	952.00
Pipe Length (ft)	=	82.00
Slope (%)	=	3.66
Invert Elev Up (ft)	=	955.00
Rise (in)	=	36.0
Shape	=	Circular
Span (in)	=	36.0
No. Barrels	=	1
n-Value	=	0.012
Culvert Type	=	Circular Culvert
Culvert Entrance	=	Smooth tapered inlet throat
Coeff. K,M,c,Y,k	=	0.534, 0.555, 0.0196, 0.9, 0.2

Embankment

Top Elevation (ft)	=	960.00
Top Width (ft)	=	24.00
Crest Width (ft)	=	50.00

Calculations

Qmin (cfs)	=	52.49
Qmax (cfs)	=	52.49
Tailwater Elev (ft)	=	(dc+D)/2

Highlighted

Qtotal (cfs)	=	52.49
Qpipe (cfs)	=	52.49
Qovertop (cfs)	=	0.00
Veloc Dn (ft/s)	=	7.88
Veloc Up (ft/s)	=	8.82
HGL Dn (ft)	=	954.68
HGL Up (ft)	=	957.35
Hw Elev (ft)	=	958.73
Hw/D (ft)	=	1.24
Flow Regime	=	Inlet Control

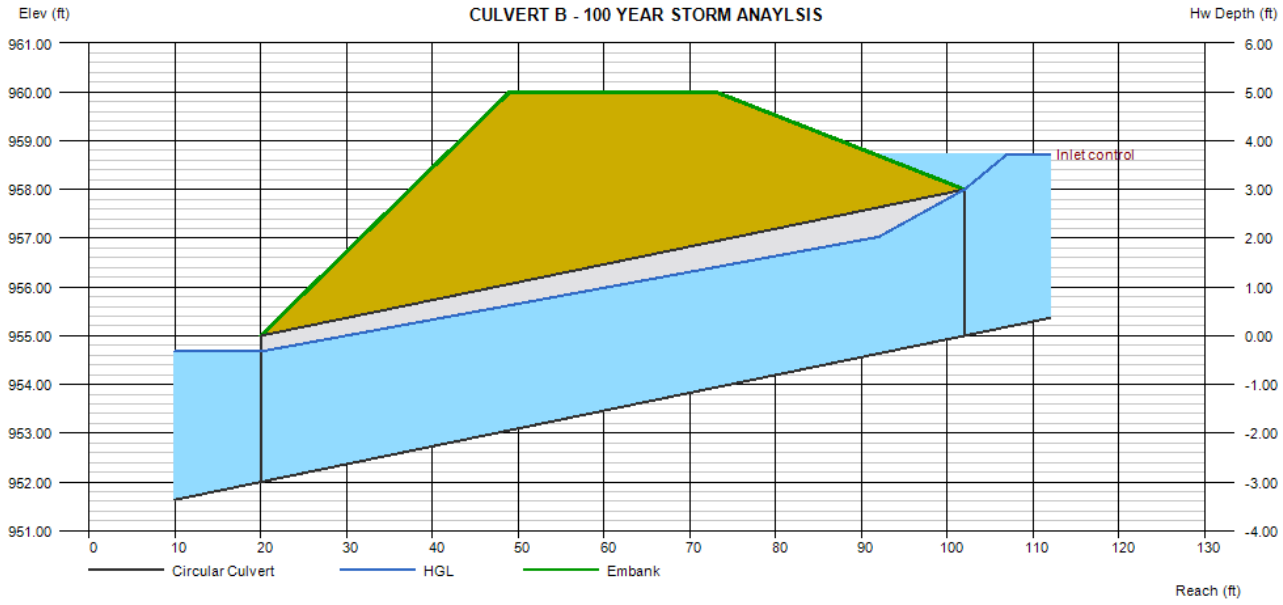
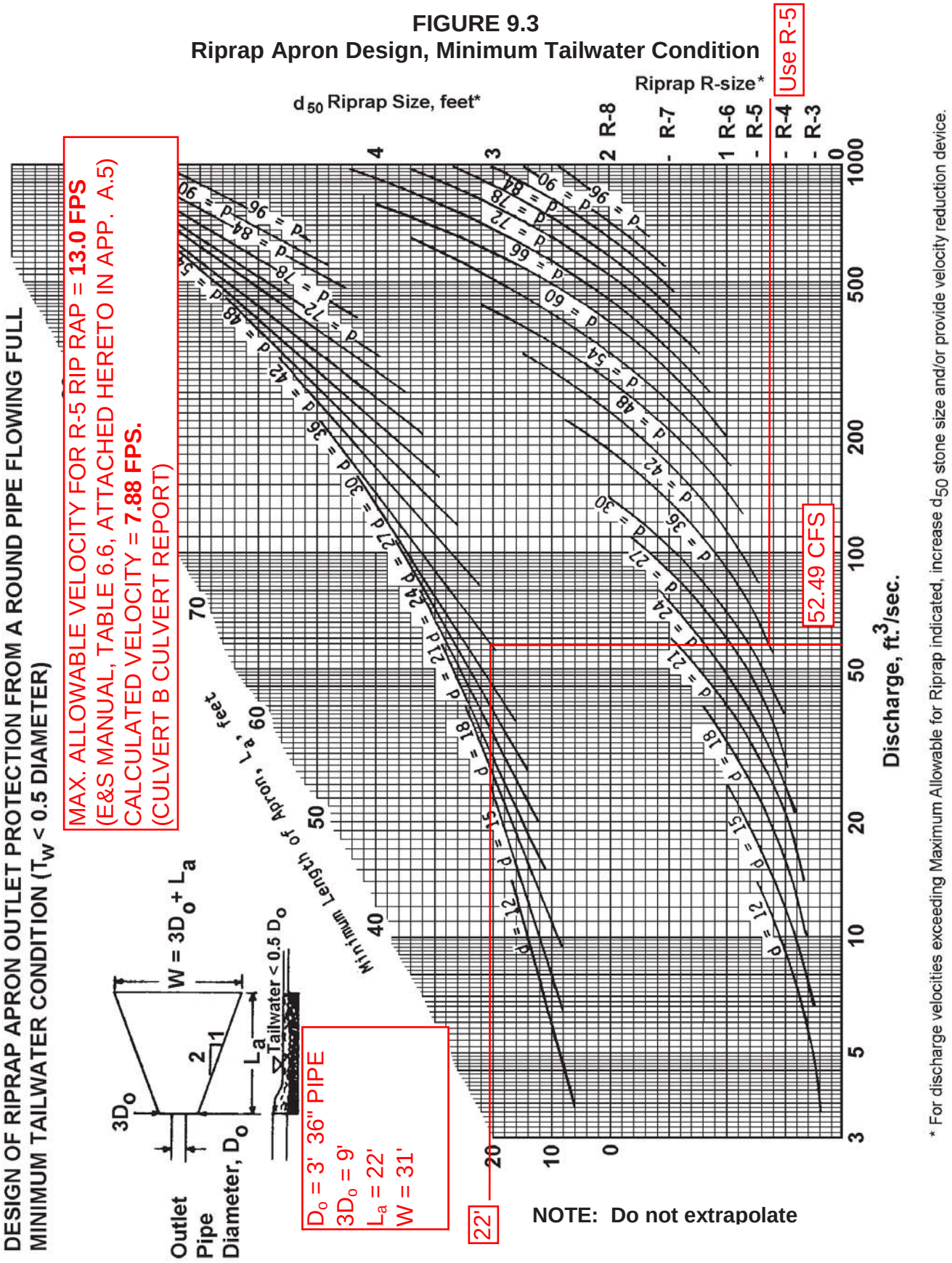
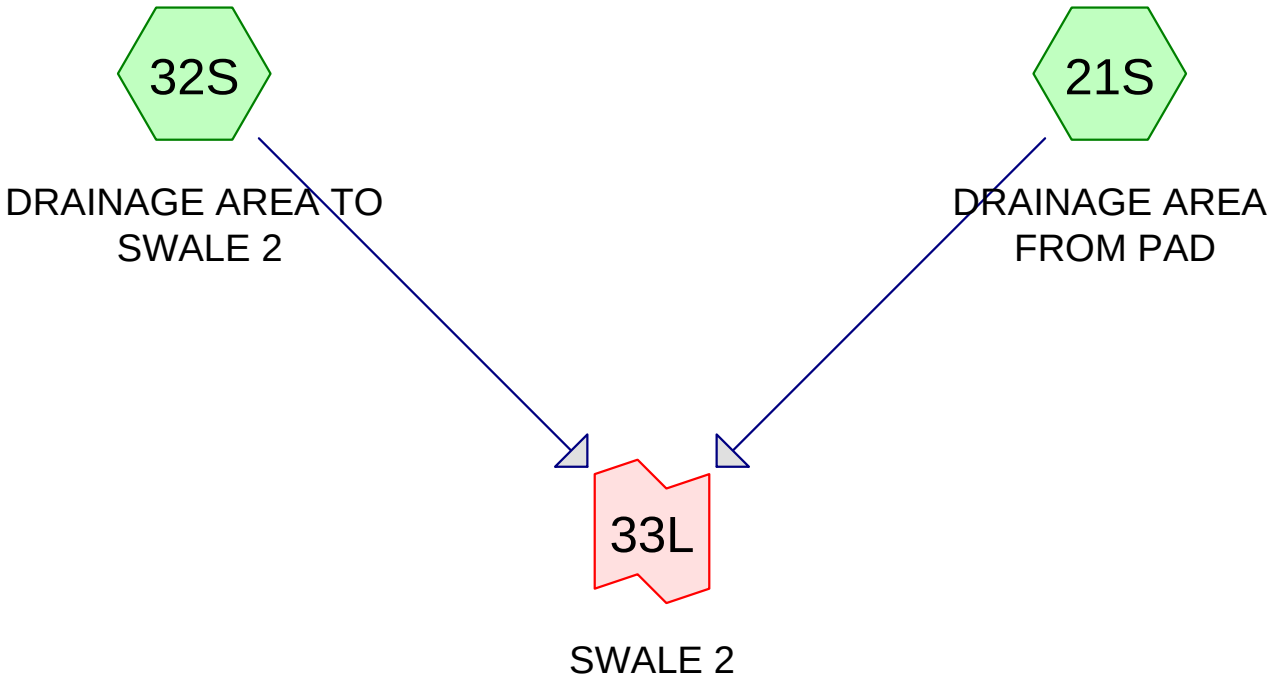


FIGURE 9.3
Riprap Apron Design, Minimum Tailwater Condition



Adapted from USDA - NRCS

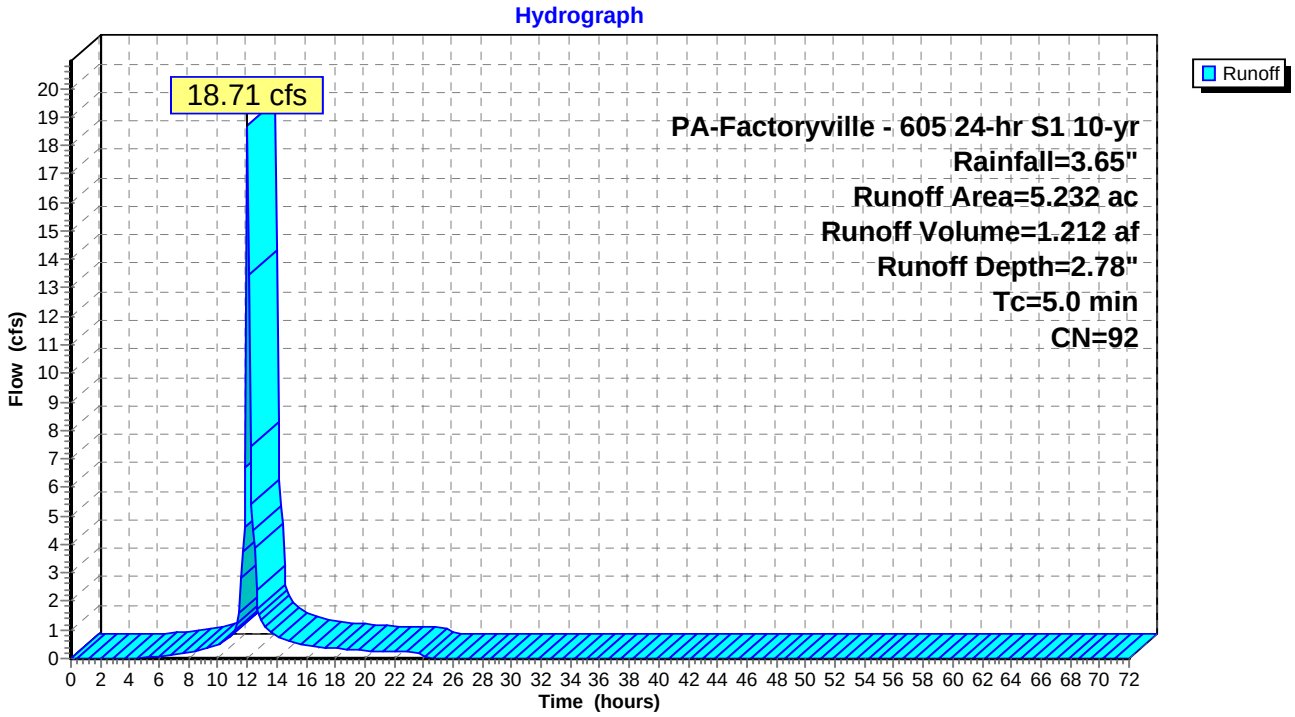
Not to be used for Box Culverts



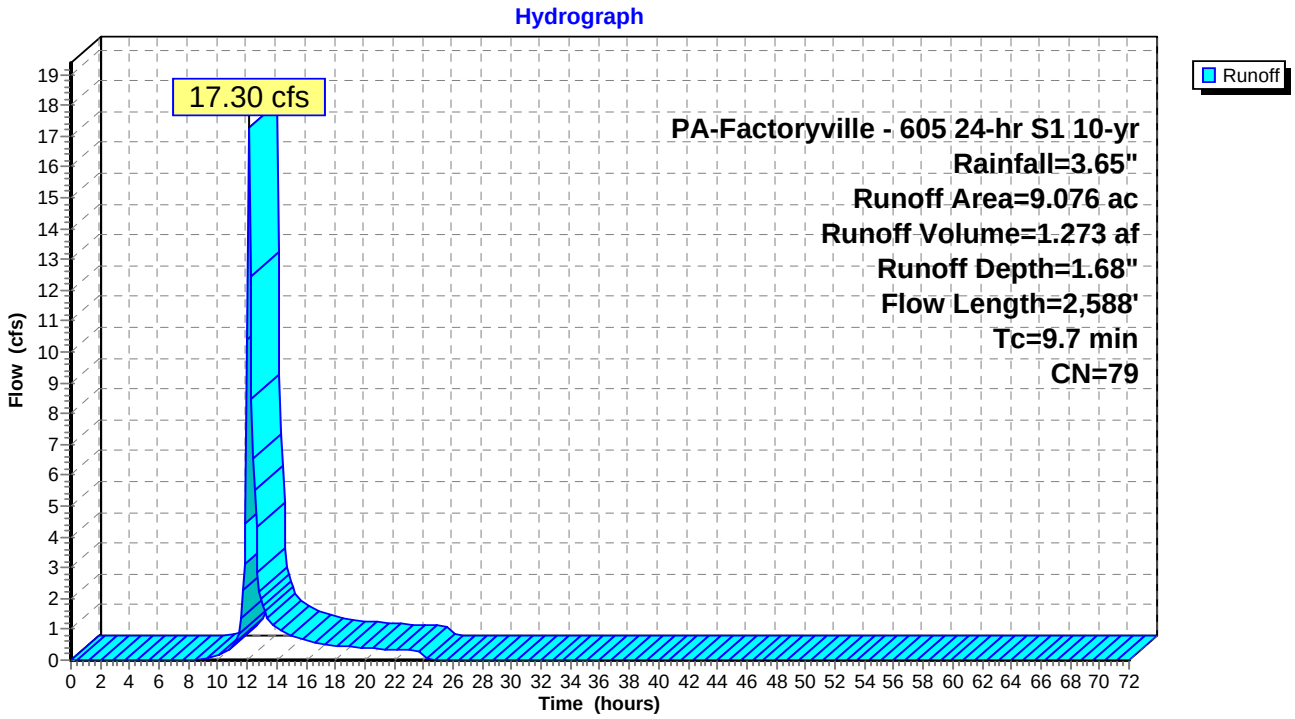
Subcat Reach Pond Link

Routing Diagram for C-DAT-14C4909-CS 605
Prepared by BL Companies, Printed 8/12/2015

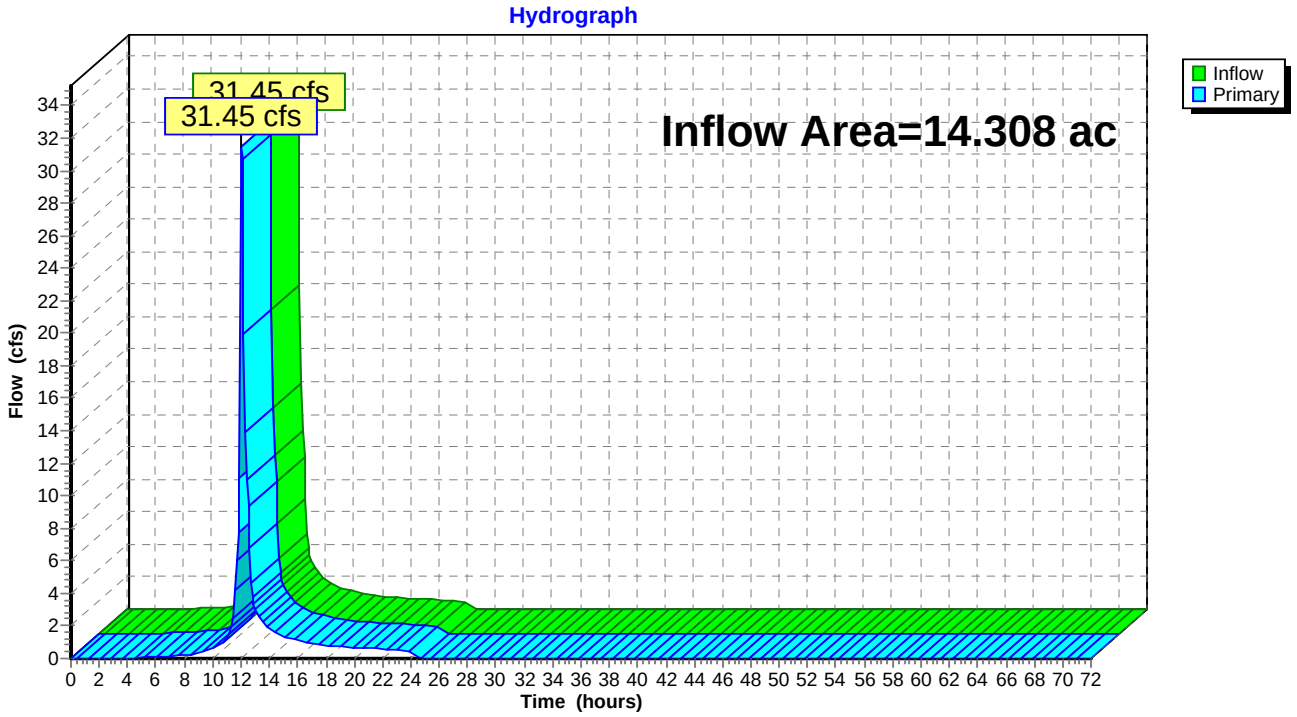
Subcatchment 21S: DRAINAGE AREA FROM PAD



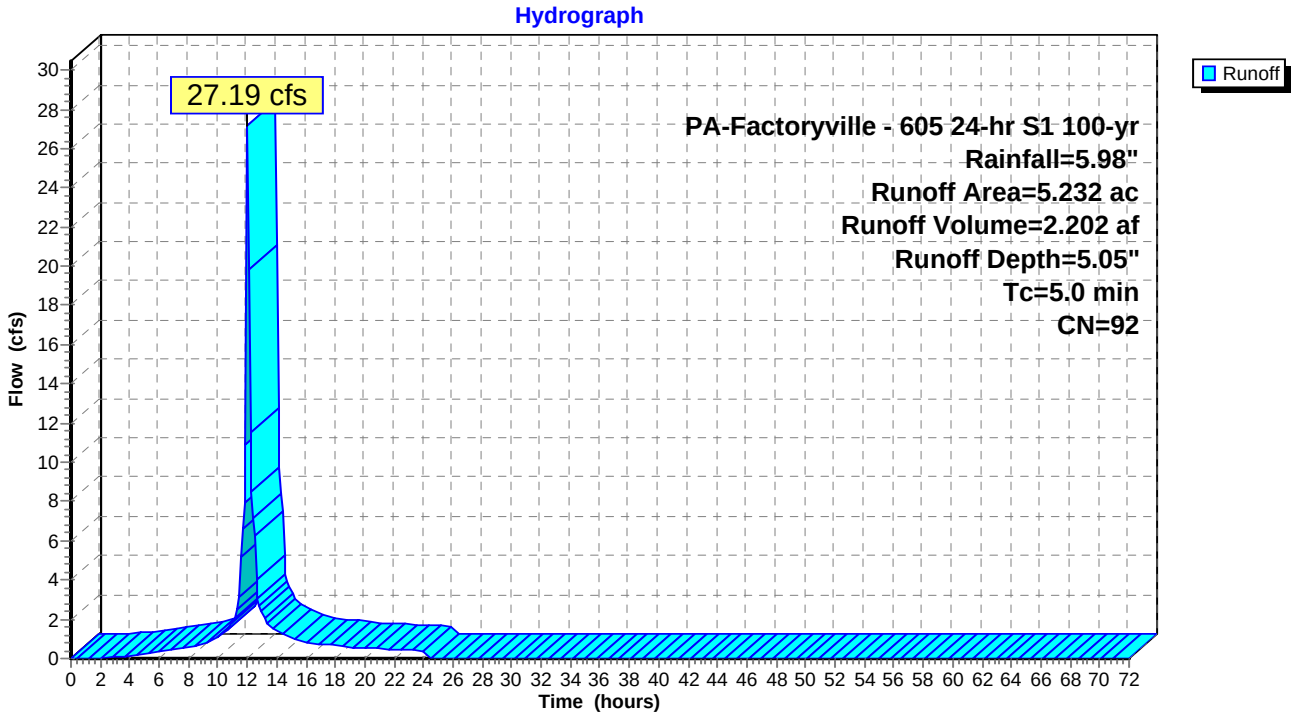
Subcatchment 32S: DRAINAGE AREA TO SWALE 2



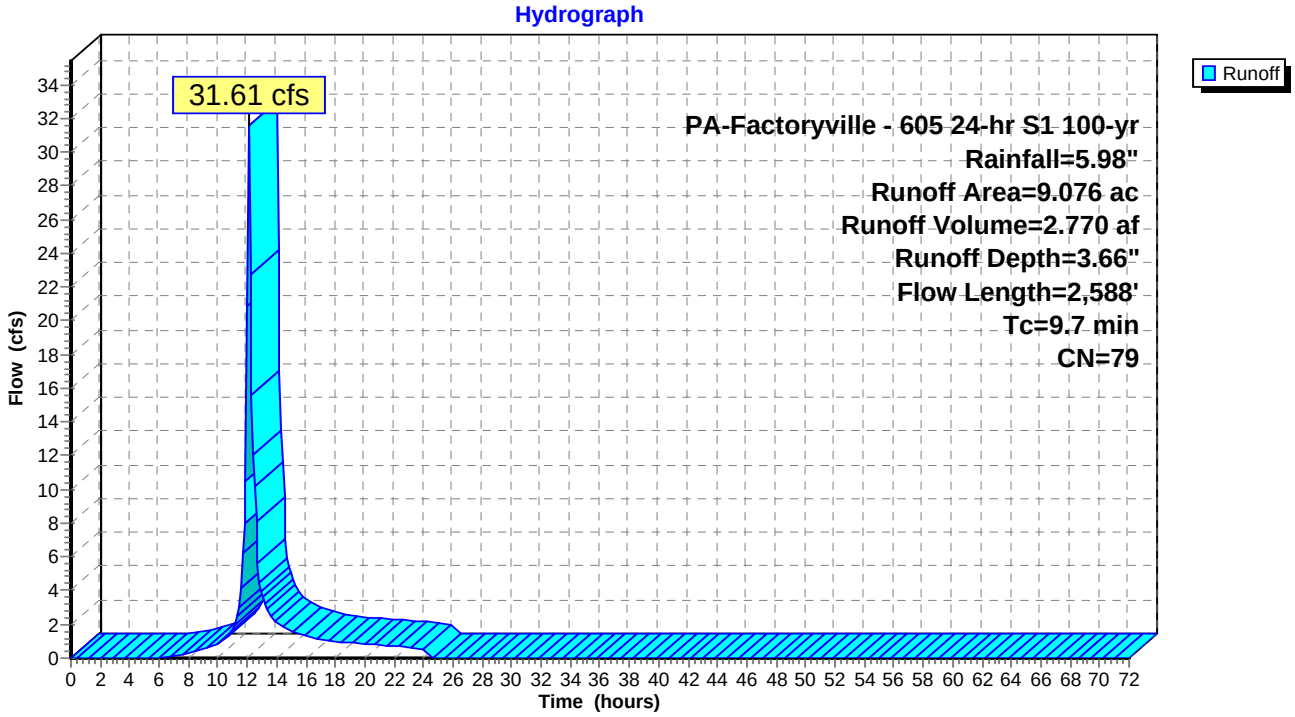
Link 33L: SWALE 2



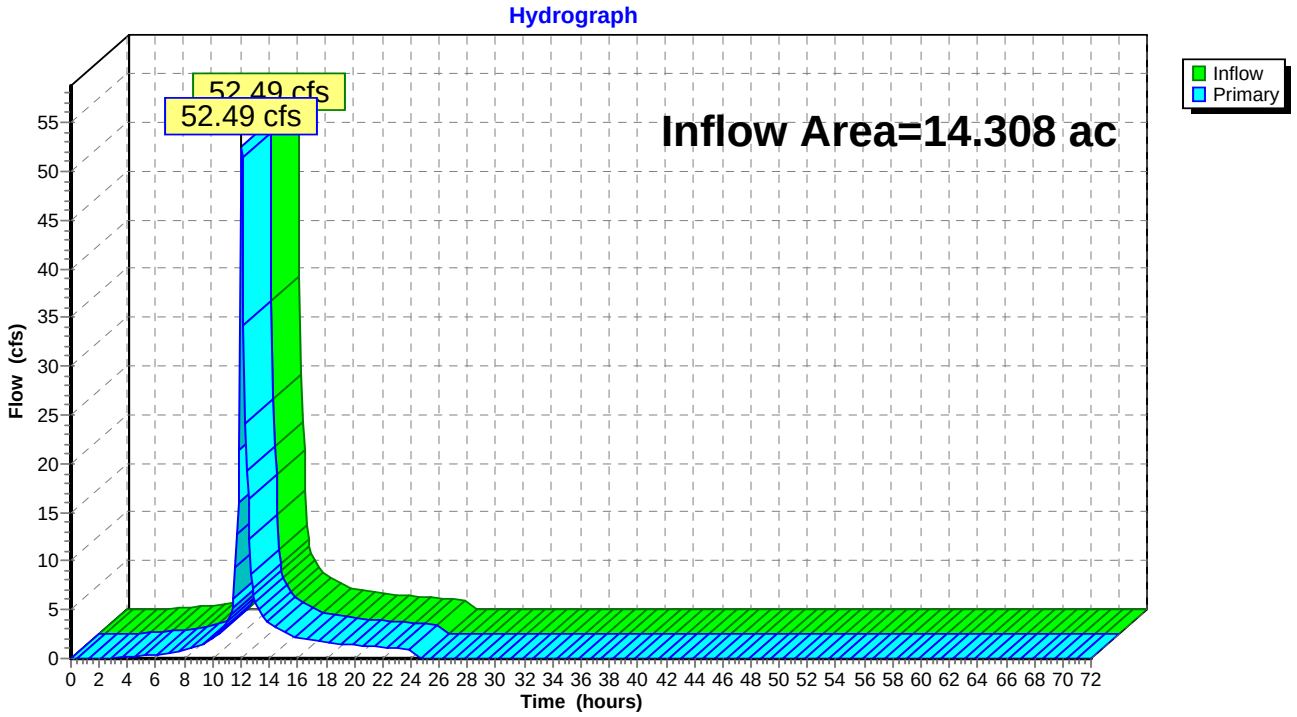
Subcatchment 21S: DRAINAGE AREA FROM PAD



Subcatchment 32S: DRAINAGE AREA TO SWALE 2



Link 33L: SWALE 2



Culvert Report

CULVERT C - 100 YEAR STORM ANAYLSIS

Invert Elev Dn (ft)	=	1128.00
Pipe Length (ft)	=	80.00
Slope (%)	=	1.25
Invert Elev Up (ft)	=	1129.00
Rise (in)	=	24.0
Shape	=	Circular
Span (in)	=	24.0
No. Barrels	=	1
n-Value	=	0.012
Culvert Type	=	Circular Culvert
Culvert Entrance	=	Smooth tapered inlet throat
Coeff. K,M,c,Y,k	=	0.534, 0.555, 0.0196, 0.9, 0.2

Embankment

Top Elevation (ft)	=	1132.00
Top Width (ft)	=	24.00
Crest Width (ft)	=	50.00

Calculations

Qmin (cfs)	=	24.03
Qmax (cfs)	=	24.03
Tailwater Elev (ft)	=	(dc+D)/2

Highlighted

Qtotal (cfs)	=	24.03
Qpipe (cfs)	=	24.03
Qovertop (cfs)	=	0.00
Veloc Dn (ft/s)	=	7.87
Veloc Up (ft/s)	=	8.30
HGL Dn (ft)	=	1129.87
HGL Up (ft)	=	1130.74
Hw Elev (ft)	=	1131.93
Hw/D (ft)	=	1.47
Flow Regime	=	Inlet Control

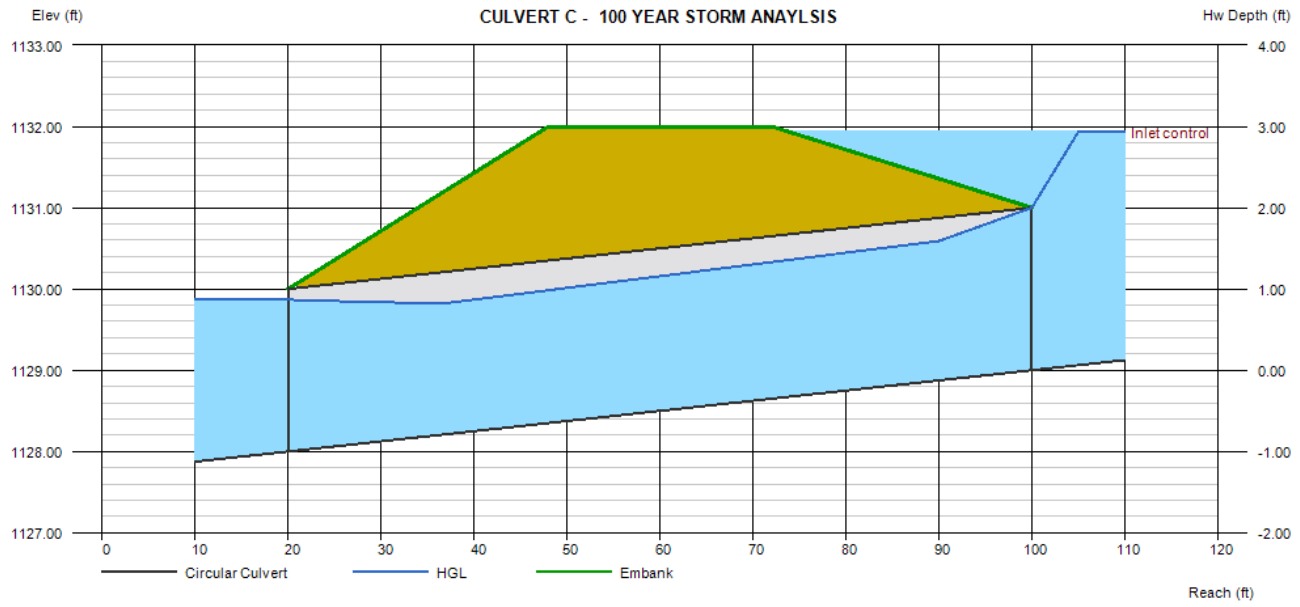
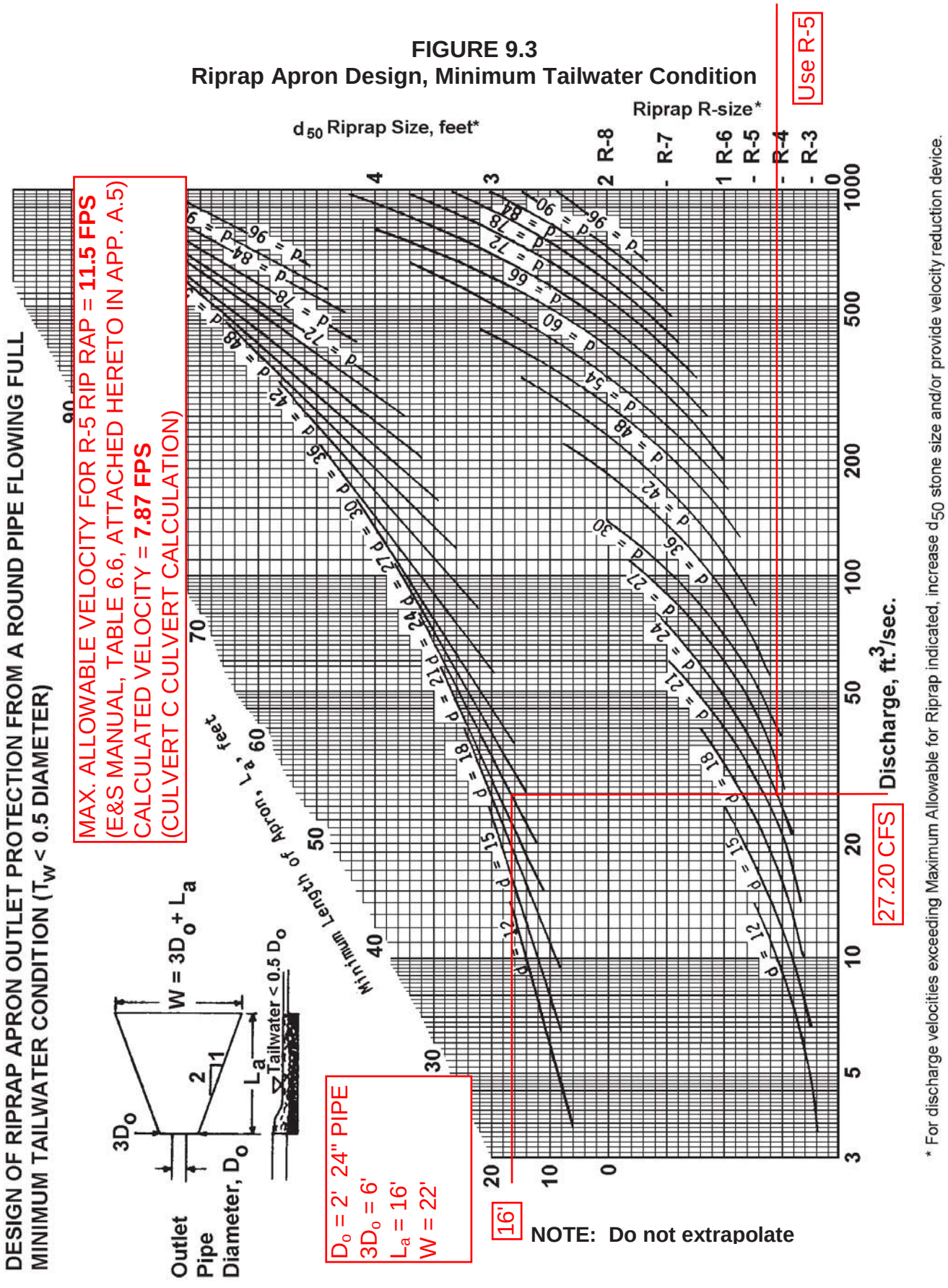


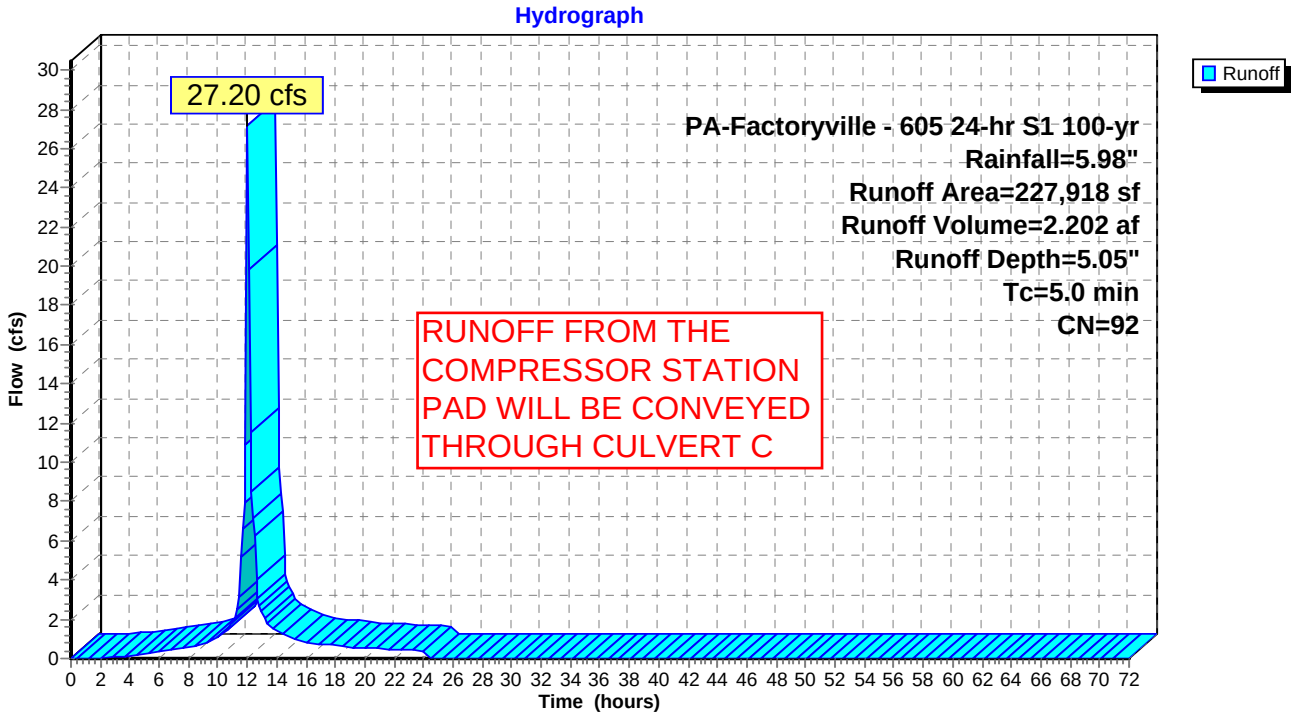
FIGURE 9.3
Riprap Apron Design, Minimum Tailwater Condition



Adapted from USDA - NRCS

Not to be used for Box Culverts

Subcatchment 7: PAD DA TO BASIN 1



Culvert Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc. Thursday, Aug 20 2015

CULVERT D - 100 YEAR STORM ANALYSIS

Invert Elev Dn (ft)	=	1122.00
Pipe Length (ft)	=	45.00
Slope (%)	=	14.07
Invert Elev Up (ft)	=	1128.33
Rise (in)	=	30.0
Shape	=	Circular
Span (in)	=	30.0
No. Barrels	=	1
n-Value	=	0.012
Culvert Type	=	Circular Concrete
Culvert Entrance	=	Square edge w/headwall (C)
Coeff. K,M,c,Y,k	=	0.0098, 2, 0.0398, 0.67, 0.5

Embankment

Top Elevation (ft)	=	1132.00
Top Width (ft)	=	10.00
Crest Width (ft)	=	100.00

Calculations

Qmin (cfs)	=	31.00
Qmax (cfs)	=	31.00
Tailwater Elev (ft)	=	(dc+D)/2

Highlighted

Qtotal (cfs)	=	31.00
Qpipe (cfs)	=	31.00
Qovertop (cfs)	=	0.00
Veloc Dn (ft/s)	=	6.78
Veloc Up (ft/s)	=	7.76
HGL Dn (ft)	=	1124.20
HGL Up (ft)	=	1130.23
Hw Elev (ft)	=	1131.42
Hw/D (ft)	=	1.23
Flow Regime	=	Inlet Control

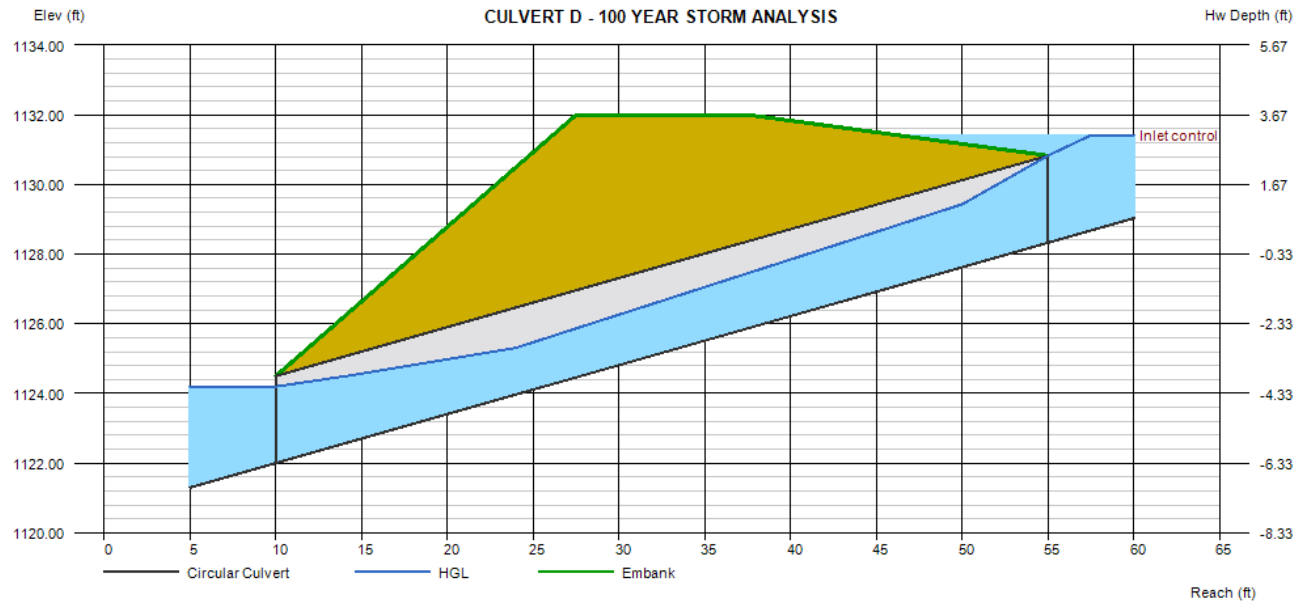
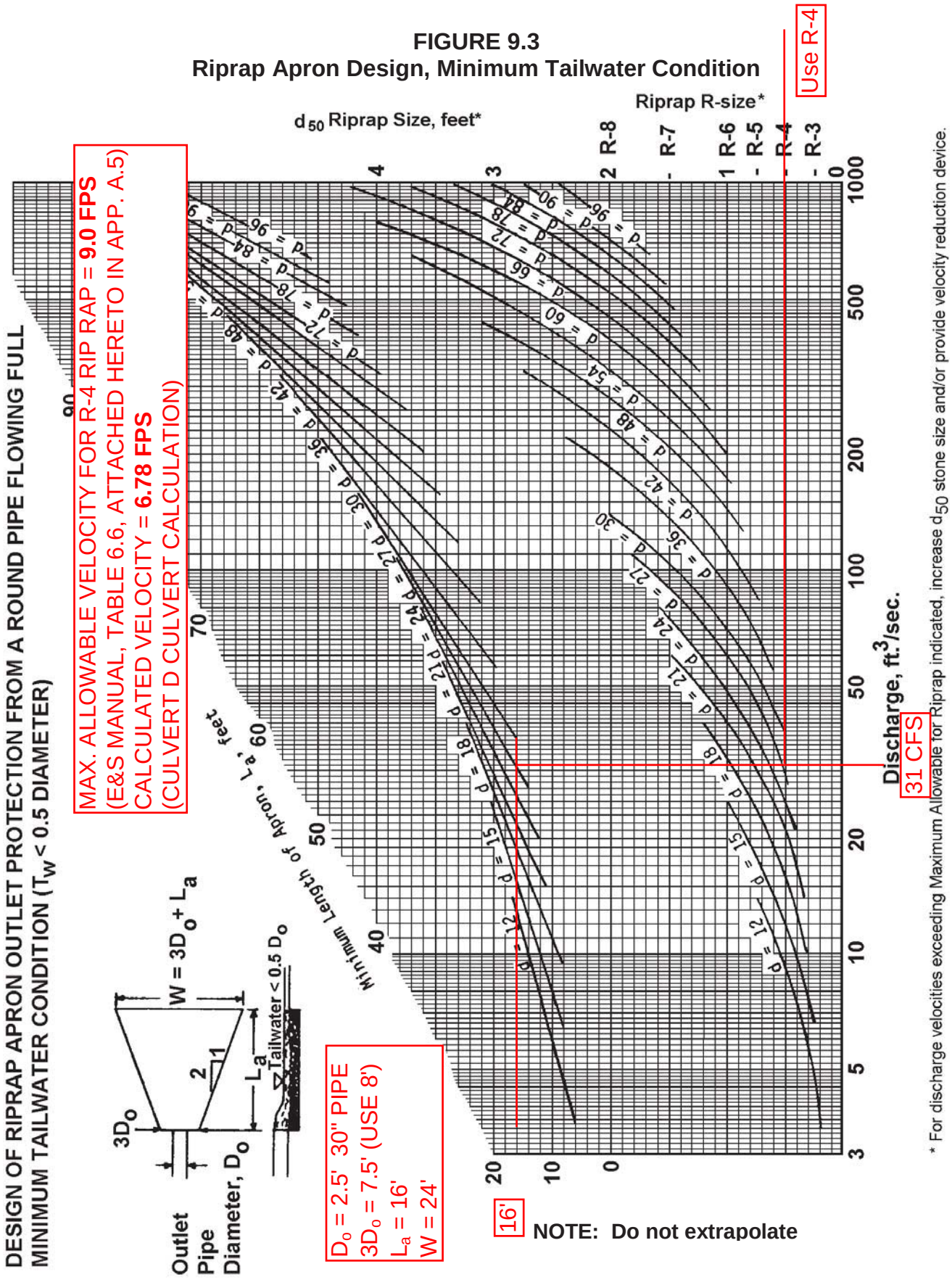


FIGURE 9.3
Riprap Apron Design, Minimum Tailwater Condition



Adapted from USDA - NRCS

Not to be used for Box Culverts

Summary for Subcatchment 4: POST-DEVELOPMENT DRAINAGE AREA TO INFILTRATION BASIN 2

Runoff = 30.54 cfs @ 12.02 hrs, Volume= 2.422 af, Depth= 4.72"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs
PA-Factoryville - 605 24-hr S1 100-yr Rainfall=5.98"

	Area (ac)	CN	Description
*	0.880	98	Impervious, HSG C
	1.506	78	Meadow, non-grazed, HSG D
*	3.778	91	Gravel Areas, HSG D
	6.164	89	Weighted Average
	5.284		85.72% Pervious Area
	0.880		14.28% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					**Direct Entry,**

Subcatchment 4: POST-DEVELOPMENT DRAINAGE AREA TO INFILTRATION BASIN 2

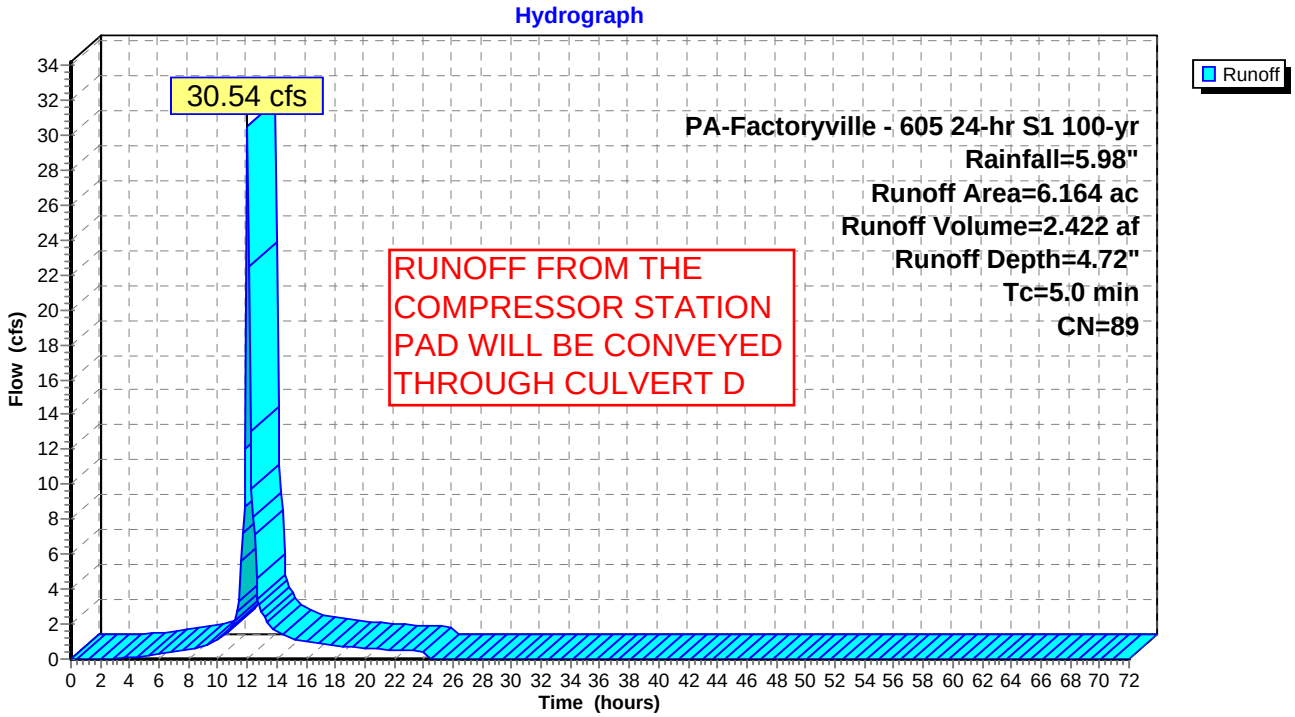
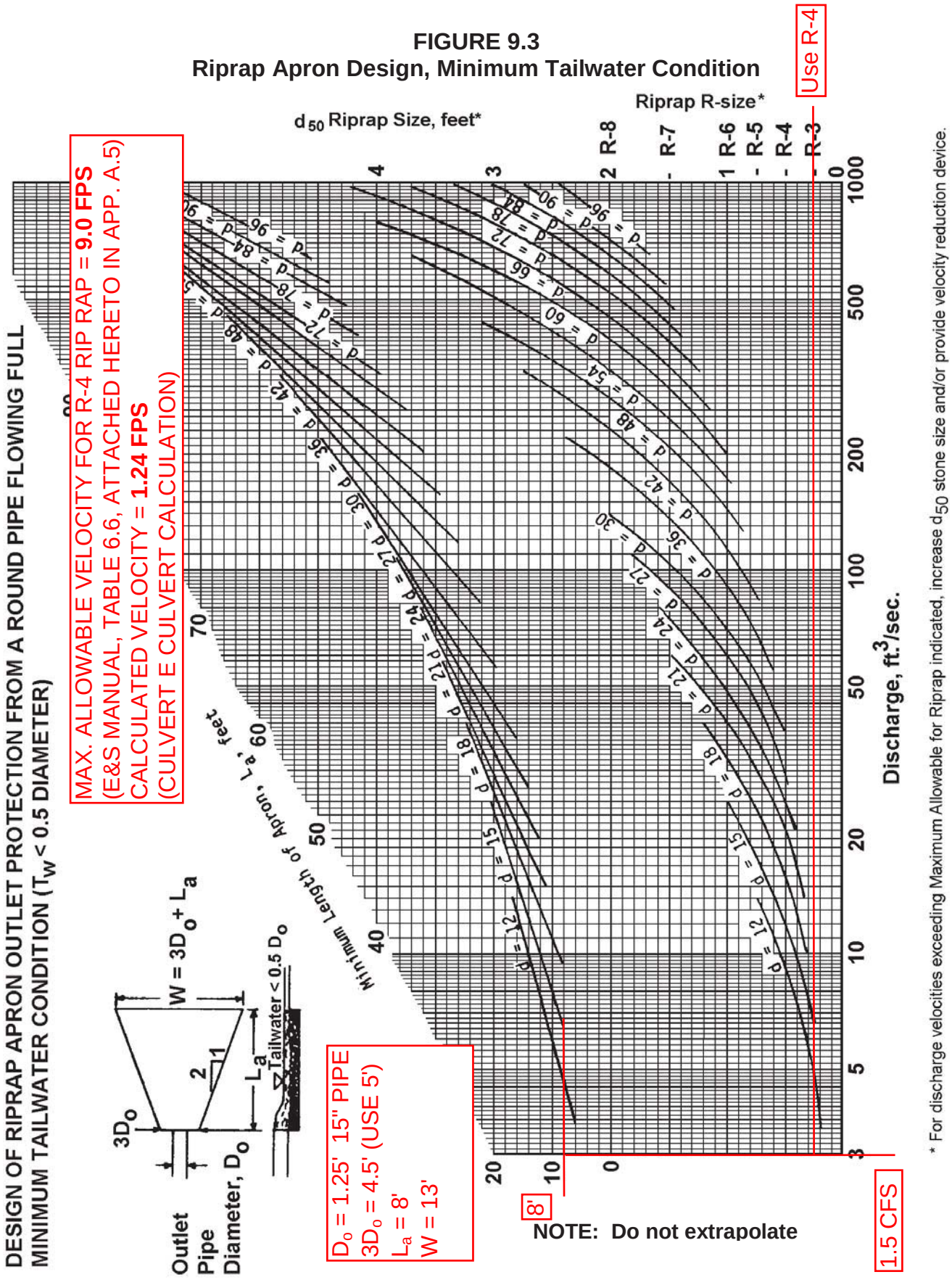


FIGURE 9.3
Riprap Apron Design, Minimum Tailwater Condition



Adapted from USDA - NRCS

Not to be used for Box Culverts

A.3 Sediment Basin Calculations

E&S WORKSHEET #12
Sediment Basin Capacity Requirements

PROJECT NAME: ATLANTIC SUNRISE PROJECT
LOCATION: CLINTON TOWNSHIP, WYOMING COUNTY
PREPARED BY: AOE DATE: 11/18/15
CHECKED BY: AJB DATE: 11/18/15

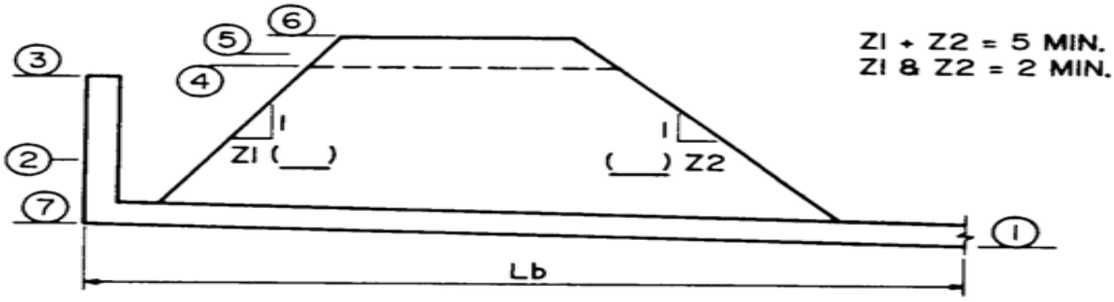
BASIN NUMBER		1	
PERMANENT OR TEMPORARY BASIN?	(P or T)	P	
SPECIAL PROTECTION WATERSHED?	(YES OR NO)	N	
KARST SOILS?	(YES OR NO)	N	
(A) MAXIMUM TOTAL DRAINAGE AREA	(AC)	32.56	
IS DRAINAGE AREA (A) MORE THAN 10% LARGER THAN THE PRECONSTRUCTION CONDITION	(YES OR NO)	Y	
(A_1) DISTURBED ACRES IN DRAINAGE AREA	(AC)	23.00	
(I) INITIAL REQ'D DEWATERING ZONE (5,000 X A)	(CF)	162,800	
(T) REDUCTION FOR TOP DEWATERING (-700 X A)	(CF)	-22,792	
(P) REDUCTION FOR PERMANENT POOL (-700 X A)	(CF)	0	
(L) REDUCTION FOR 4:1 FLOW LENGTH:WIDTH (-350 X A)	(CF)	-11,396	
(D) REDUCTION FOR 4 TO 7 DAY DEWATERING (-350 X A)	(CF)	-11,396	
(Sv) REQUIRED DEWATERING ZONE [I - (T+P+L+D)][1]	(CF)	117,216	
(Sd) REQUIRED SEDIMENT STORAGE VOLUME (1000 X A_1)	(CF)	23,000	
(St) TOTAL REQUIRED STORAGE VOLUME (Sv + Sd)	(CF)	140,216	
TOTAL STORAGE VOLUME PROVIDED (@ ELEV 3)[2]	(CF)	**164,827**	
DEWATERING TIME FOR DEWATERING ZONE	(DAYS)	7.0	
REQUIRED DISCHARGE CAPACITY (2 X A)	(CFS)[3]	***23.99 (25 YR STORM)***	
PRINCIPAL SPILLWAY TYPE (PERFORATED RISER, SKIMMER, etc.)		SKIMMER	
PEAK FLOW FROM 10 YR/24 HR STORM FOR DRAINAGE AREA (A)		122.27	
PRINCIPAL SPILLWAY CAPACITY (@ ELEV 5)	(CFS)[4]	***22.77***	
EMERGENCY SPILLWAY CAPACITY (@ ELEV 5)	(CFS)	0.00	
TOTAL BASIN DISCHARGE CAPACITY (@ ELEV 5)	(CFS)	***22.77***	
EMERGENCY SPILLWAY PROTECTIVE LINING[5]		P550	
OUTLET TO A SURFACE WATER?	(YES OR NO)[6]	YES	
PEAK FLOW FROM A 100 YR/24 HR STORM FOR DRG. AREA (A)	(CFS)	173.22	

1 The minimum dewatering zone capacity for sediment basins is (3,600 X A). No reduction is permitted in Special Protection (HQ and EV) Watersheds.
2 Total Storage Volume provided at riser crest.
3 Or provide calculations to show peak flow from 25 yr./24 hr. storm for area (A) is routed through the
4 Provide supporting computations.
5 If grass lining is proposed, spillway should be constructed in original ground unless a suitable TRM lining is used. Wherever a TRM is used, riprap should be placed at the bottom of the embankment to prevent scour.
6 If no, and basin is permanent or drainage area is more than 10% larger than pre-construction, provide supporting calculations to show accelerated erosion will not result from the proposed discharge. For discharges increasing volume or rate of flow onto a neighboring property prior to entering a surface water, an easement should be obtained prior to plan submittal.

E&S WORKSHEET #13

Sediment Basin Dimensions and Elevations

PROJECT NAME: ATLANTIC SUNRISE PROJECT CS 605
LOCATION: CLINTON TOWNSHIP, WYOMING COUNTY
PREPARED BY: AOE DATE: 111/18/15
CHECKED BY: AJB DATE: 11/18/15



BASIN NUMBER		1	
1. DISCHARGE PIPE ELEVATION	(FT)	***947.50***	
2. ELEVATION AT TOP OF SEDIMENT STORAGE ZONE (@ Sd) (MIN. 1.0' ABOVE ELEVATION 7)	(FT)	***951.25***	
3. ELEVATION AT TOP OF DEWATERING ZONE (St) (CREST OF PRINCIPAL SPILLWAY)	(FT)	***955.00***	
4. EMERGENCY SPILLWAY CREST ELEVATION	(FT)	***957.00***	
5. 2 CFS/ACRE OR 25-YR/24-HR FLOW ELEVATION	(FT)	***956.52***	
6. TOP OF EMBANKMENT ELEVATION	(FT)	***958.00***	
7. BASIN BOTTOM ELEVATION	(FT)	***949.25***	
AVERAGE BOTTOM WIDTH	(FT)	104	
AVERAGE BOTTOM LENGTH	(FT)	277	
(SA_{min}) REQUIRED SURFACE AREA AT ELEVATION 2	(SQ. FT.)	***4,400***	
SURFACE AREA PROVIDED AT ELEVATION 2	122.27	***23,361***	
AVERAGE BASIN WIDTH (W) AT ELEVATION 3	22.77	135	
FLOW LENGTH (L) AT ELEVATION 3	(FT)	300	
FLOW LENGTH:WIDTH RATIO AT ELEVATION 3	22.77	5:1	
SILT CURTAIN OR FOREBAY? (IF YES, INDICATE WHICH)		NO	
EMBANKMENT TOP WIDTH	(FT, 8' MIN.)	10	
EMBANKMENT SOIL TYPE(S)		ON SITE	
KEY TRENCH DEPTH	(FT, 2' MIN.)	***4***	
KEY TRENCH WIDTH	(FT, 4' MIN.)	10	
RISER DIAMETER/TYPE	(15" MIN.)	24" X 48"	
BARREL DIAMETER/TYPE	(12" MIN.)	18" RCP	
Lb (BARREL LENGTH)	(FT)	***61***	
EMERGENCY SPILLWAY WIDTH	(FT)	15	
EMERGENCY SPILLWAY SIDE SLOPES	(H:V)	3:1	
EMERGENCY SPILLWAY DEPTH	(FT)	1.0	

For irregular shaped traps, provide stage storage data

Source: 363-2134-008 / March 31, 2012 / Page 384

E&S WORKSHEET # 14

Sediment Basin/Sediment Trap Storage Data

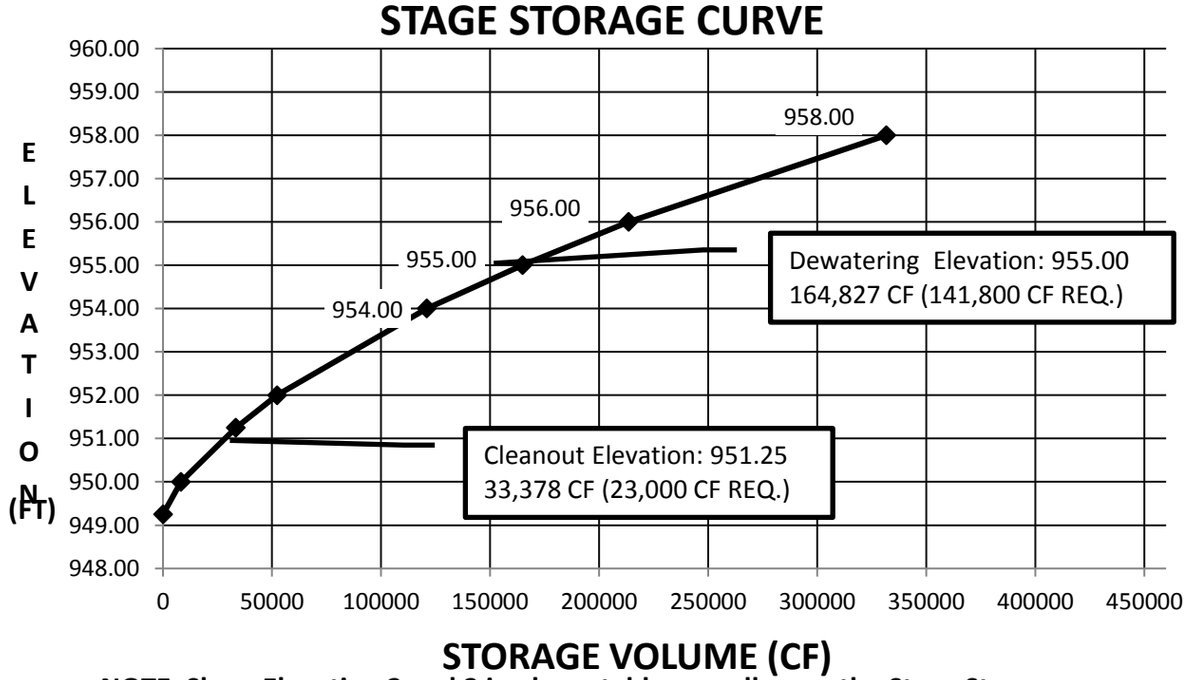
PROJECT NAME: ATLANTIC SUNRISE PROJECT

LOCATION: CLINTON TOWNSHIP, WYOMING COUNTY

PREPARED BY: AOE *DATE: 11/18/15*

CHECKED BY: AJB *DATE: 11/18/15*

WATER SURFACE ELEVATION (FEET)	AREA (SQ. FT.)	AVERAGE AREA (SQ. FT.)	DIFFERENCE IN ELEVATION (FEET)	STORAGE VOLUME (CUBIC FEET)	
				INCREMENTAL	TOTAL
949.25	*5,082*				*0*
950.00	*16,872*	*10977*	*0.75*	*8233*	*8233*
951.25	*23,361*	*20117*	*1.25*	*25146*	*33378*
952.00	*27,255*	*25308*	*0.75*	*18981*	*52359*
954.00	*41,379*	*34317*	*2.00*	*68634*	*120993*
955.00	*46,288*	*43834*	*1.00*	*43834*	*164827*
956.00	*51,198*	*48743*	*1.00*	*48743*	*213570*
958.00	*66,983*	*59091*	*2.00*	*118181*	*331751*



NOTE: Show Elevation 2 and 3 in above table as well as on the Stage Storage Curve.

Source: 363-2134-008/March 31, 2012/Page 385

MINIMUM SEDIMENT BASIN SURFACE AREA AT SEDIMENT STORAGE ELEVATION (SA_{min})

SKIMMER DISCHARGE

Orifice Equation: $q_{out} = CA(2gh)^{0.5}$

D =	4	in.	Orifice diameter
C =	0.59		Orifice coefficient
A =	0.087	sf.	Orifice area
g =	32.2	ft./sec.^{2}	Gravitational constant
h =	***0.42***	ft.	Head above orifice
q_{out} =	***0.27***	cfs.	Skimmer Orifice discharge

MINIMUM SURFACE AREA AT TOP OF SEDIMENT STORAGE

Minimum Surface Area: $SA_{min} = 1.2(q_{out}/y_s)$

q_{out} =	***0.27***	cfs.	Orifice discharge
y_s*=	7.30E-05	ft./sec.	Settling velocity
SA_{min} =	**4,400**	sf.	Minimum surface area

*Values for y_s are given below:

For sand, loamy sand and sandy loam soils: $y_s = 1.2 \times 10^{-3}$ ft./sec.

For loam, silt and silt loam soils: $y_s = 7.3 \times 10^{-5}$ ft./sec.

For clay loam, silty clay and clay soils: $y_s = 1.2 \times 10^{-5}$ ft./sec.

SKIMMER ARM LENGTH

The minimum skimmmer arm length (L) = max storage depth X $2^{0.5}$ (Page 166, E&S Manual)

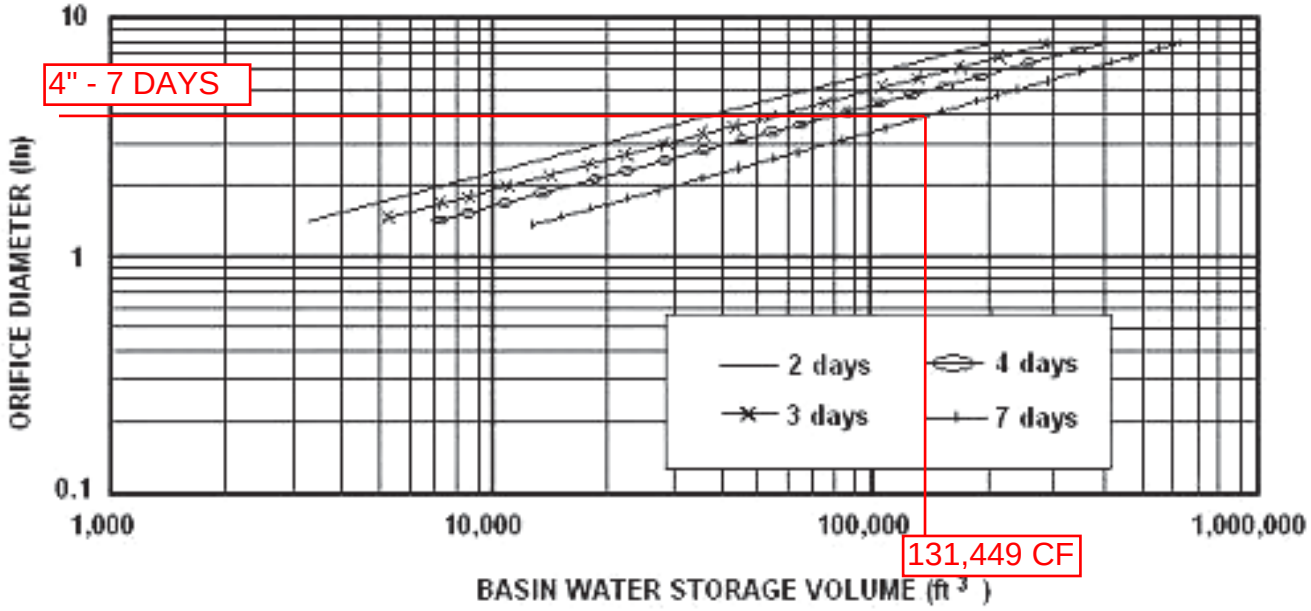
Max storage depth (d) = 25 yr storm water surface elevation - temporary stub elevation

d = ***956.52*** - ***951.25*** = ***5.27*** ft.

$2^{0.5}$ = 1.414

L = ***7.5*** ft. ***Use 8'***

FIGURE 7.2
Skimmer Orifice Design Chart



Adapted from Penn State Agricultural and Biological Fact Sheet F-253

Figure 7.2 is for use in designing the orifice plate for the skimmer shown in Standard Construction Detail # 7-1 or # 7-2. It assumes a 2" to 5" head (depending upon the size of the skimmer). The required head for use of Figure 7.2 varies as follows: For a skimmer with a dewatering tube $\leq$ 2 ½" diameter, use a 2" head. For a 3" diameter tube, use a 2.5" head; 4" tube, use 3.3" head; 5" tube use 4" head, and 6" diameter tube use 5" head.

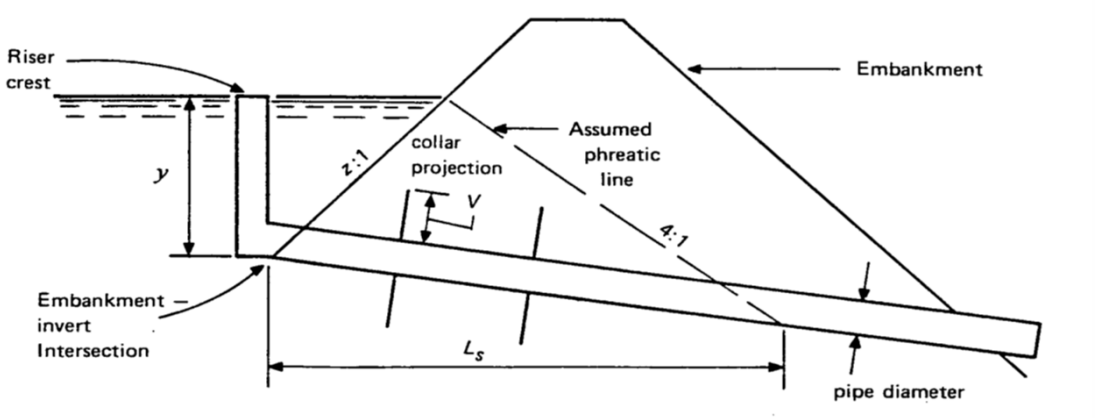
Find the vertical line representing the basin's dewatering zone volume. At the intersection of the vertical line with the desired dewatering time, read horizontally to the left to find the required skimmer orifice diameter.

Skimmer Orifice Design Example:

For a basin with a dewatering volume of 40,000 cubic feet and a desired dewatering time of two days, the required skimmer orifice diameter is 4 inches. Indicate this dimension on the plan drawings (as a note on the typical or in the summary table). There must be a sufficient number of holes in the underside of the water entry unit of the skimmer to allow water to enter freely into the skimmer orifice. The outlet pipe or barrel must be capable of discharging at the rate permitted by the skimmer and in all cases must be equal to or larger in dimension than the orifice diameter. This dimension should also be indicated on the plan drawings. Anti-seep collars are recommended for the barrel.

When erodible soils or soils having a high content of fine silts will be disturbed in the drainage area of a sediment basin, longer settling times will result in a higher percentage of suspended solids removal. Therefore, settling times of 4 to 7 days are recommended in such situations.

WORKSHEET #18
Anti-seep Collar Design



BASIN NO.	TEMP. OR PERM.	Y (FT)	Z	Ls (FT)	Lf (FT)	V (IN)	BARRELL DIA. (IN)	COLLAR SIZE (IN)	NO. COLLARS	COLLAR SPACING (FT)	DISTANCE TO 1ST COLLAR (FT)
1	P	***8.37***	3	***60***	***69***	***18***	22	***58***	3	10	***20***
2	p	3.81	3	41	47	20	22	61	2	10	15

Source: 363-2134-008 / March 31, 2012 / Page 389

COMPRESSOR STATION 605
INFILTRATION BASIN 1 OUTLET STRUCTURE FLOTATION CALCULATIONS

Assumptions

24" X 48" concrete inlet box riser

Total area of 24" x 48" inlet box = 10 sf

6" concrete wall thickness

6" thick bottom

Density of water = 62.4 lb/cf

Density of concrete = 150 lb/cf

Area of concrete in a 2' X 4' inlet box with a 6" thick wall = 3.5 sf

Volume of concrete per vertical foot of inlet box = 1' X 3.5 sf = 3.5 cf.

Weight of concrete per vertical foot of inlet box = 3.5 cf X 150 lb/cf = 525 Lbs

Buoyant force from water per vertical foot of inlet box = 62.4lb/cf X 10 sf X 1 ft = 624 lb.

Volume of bottom of inlet = 10 sf X 0.5 ft = 5 cf

Weight of bottom of inlet = 150 lb/cf X 5 cf = 750 lb

Buoyant force on bottom of inlet = 62.4 lb/cf X 5 = 312 lb

Basin 1 outlet structure height = 7.50 ft

Weight of outlet structure = 7.50 X 525 + 750 = 4,687 lb

Buoyant force = 312 + 624 X 7.50 = 4,992 lb

Weight of outlet structure with foot of concrete below invert:

4,687 + 150 X 10 = 6,187 lb OK

COMPRESSOR STATION 605
INFILTRATION BASIN 2 OUTLET STRUCTURE FLOTATION CALCULATIONS

Assumptions

24" X 48" concrete inlet box riser

Total area of 24" x 48" inlet box = 10 sf

6" concrete wall thickness

6" thick bottom

Density of water = 62.4 lb/cf

Density of concrete = 150 lb/cf

Area of concrete in a 2' X 4' inlet box with a 6" thick wall = 3.5 sf

Volume of concrete per vertical foot of inlet box = 1' X 3.5 sf = 3.5 cf.

Weight of concrete per vertical foot of inlet box = 3.5 cf X 150 lb/cf = 525 Lbs

Buoyant force from water per vertical foot of inlet box = 62.4lb/cf X 10 sf X 1 ft = 624 lb.

Volume of bottom of inlet = 10 sf X 0.5 ft = 5 cf

Weight of bottom of inlet = 150 lb/cf X 5 cf = 750 lb

Buoyant force on bottom of inlet = 62.4 lb/cf X 5 = 312 lb

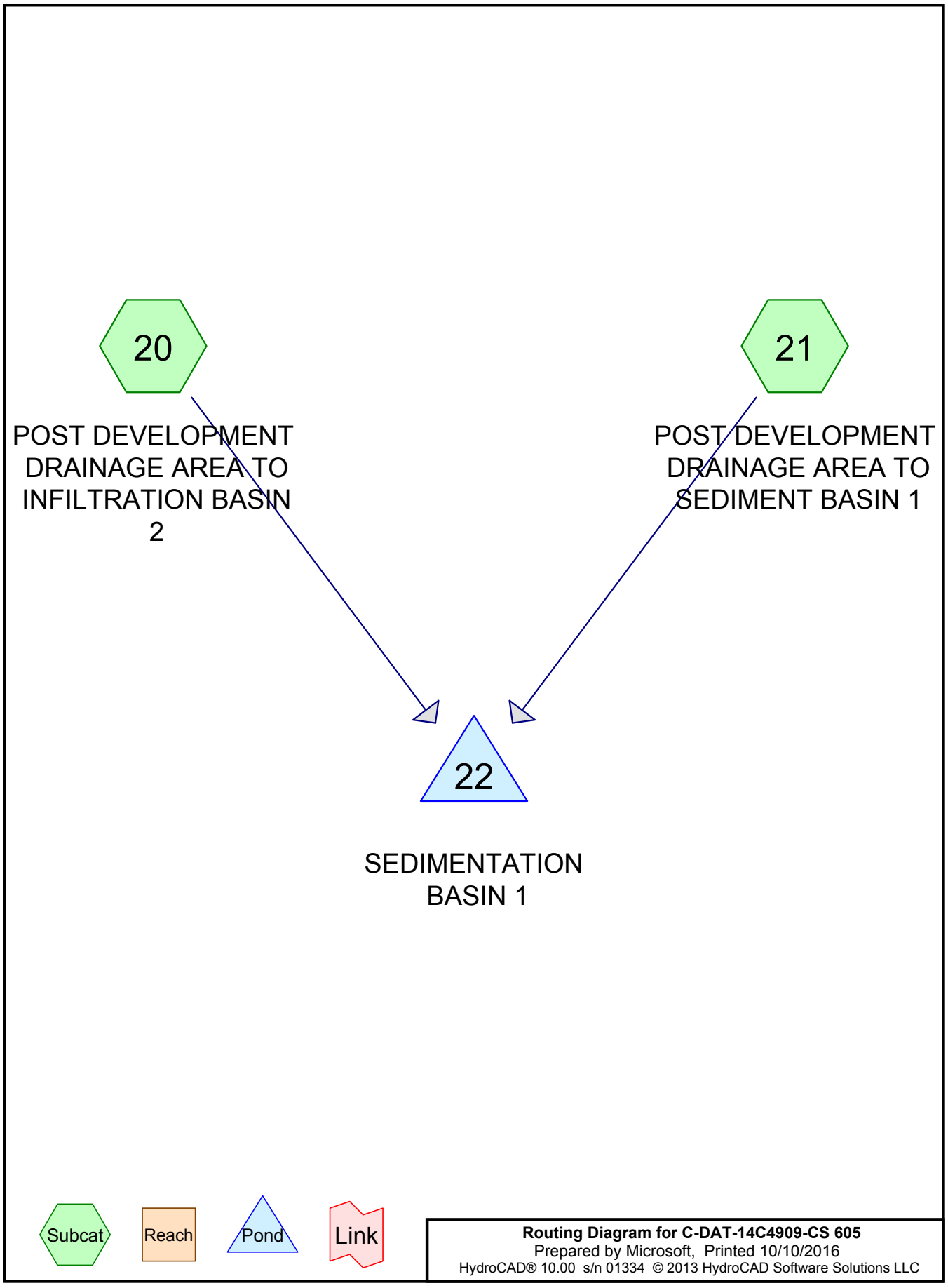
Basin 2 outlet structure height = 3.00 ft

Weight of outlet structure = 3.00 X 525 + 750 = 2325 lb

Buoyant force = 312 + 624 X 3.00 = 2184 lb

Weight of outlet structure with foot of concrete below invert:

4,687 + 150 X 10 = 3,825 lb OK


20
POST DEVELOPMENT DRAINAGE AREA TO INFILTRATION BASIN 2
21
POST DEVELOPMENT DRAINAGE AREA TO SEDIMENT BASIN 1
22
SEDIMENTATION BASIN 1
Subcat
Reach
Pond
Link
Routing Diagram for C-DAT-14C4909-CS 605
Prepared by Microsoft, Printed 10/10/2016
HydroCAD® 10.00 s/n 01334 © 2013 HydroCAD Software Solutions LLC

Summary for Subcatchment 20: POST DEVELOPMENT DRAINAGE AREA TO INFILTRATION BASIN 2

[49] Hint: Tc<2dt may require smaller dt

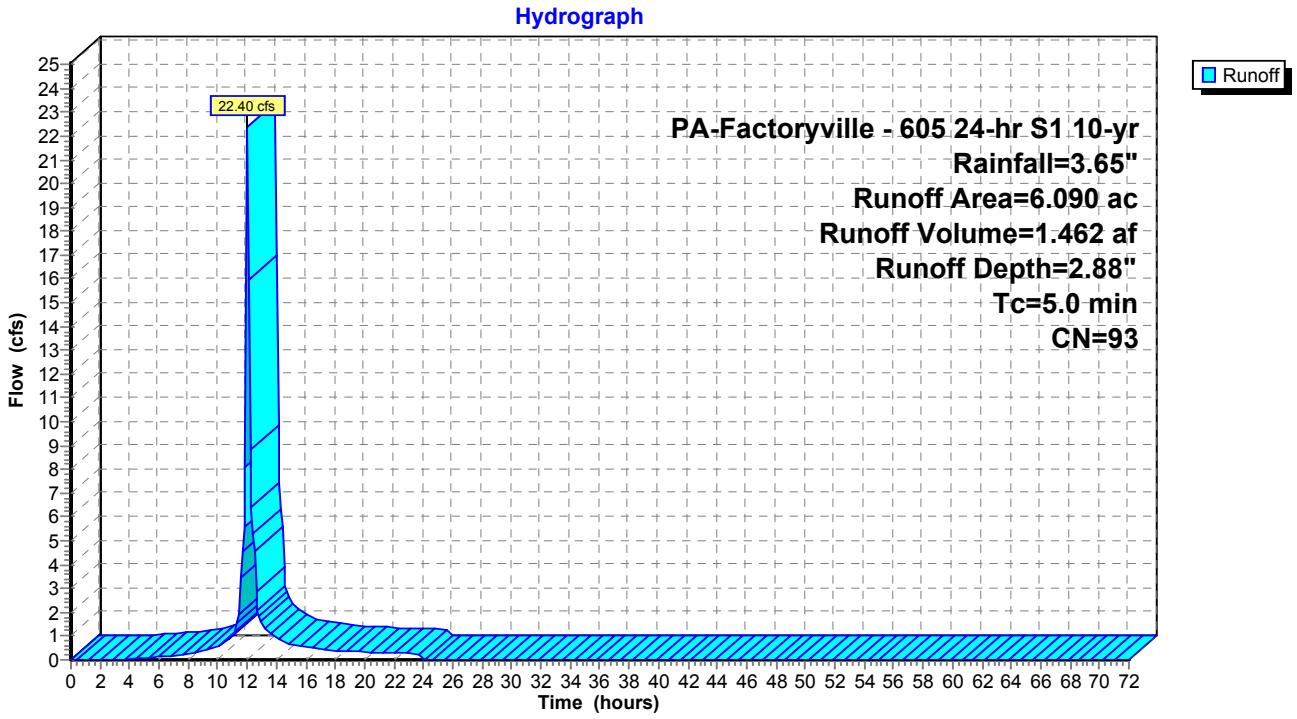
Runoff = 22.40 cfs @ 12.02 hrs, Volume= 1.462 af, Depth= 2.88"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs
PA-Factoryville - 605 24-hr S1 10-yr Rainfall=3.65"

	Area (ac)	CN	Description
*	0.370	98	Impervious, HSG C
	2.360	94	Newly graded area, HSG D
*	3.360	91	Gravel Areas, HSG D
	6.090	93	Weighted Average
	5.720		93.92% Pervious Area
	0.370		6.08% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					**Direct Entry,**

Subcatchment 20: POST DEVELOPMENT DRAINAGE AREA TO INFILTRATION BASIN 2



Summary for Subcatchment 21: POST DEVELOPMENT DRAINAGE AREA TO SEDIMENT BASIN 1

[49] Hint: Tc<2dt may require smaller dt

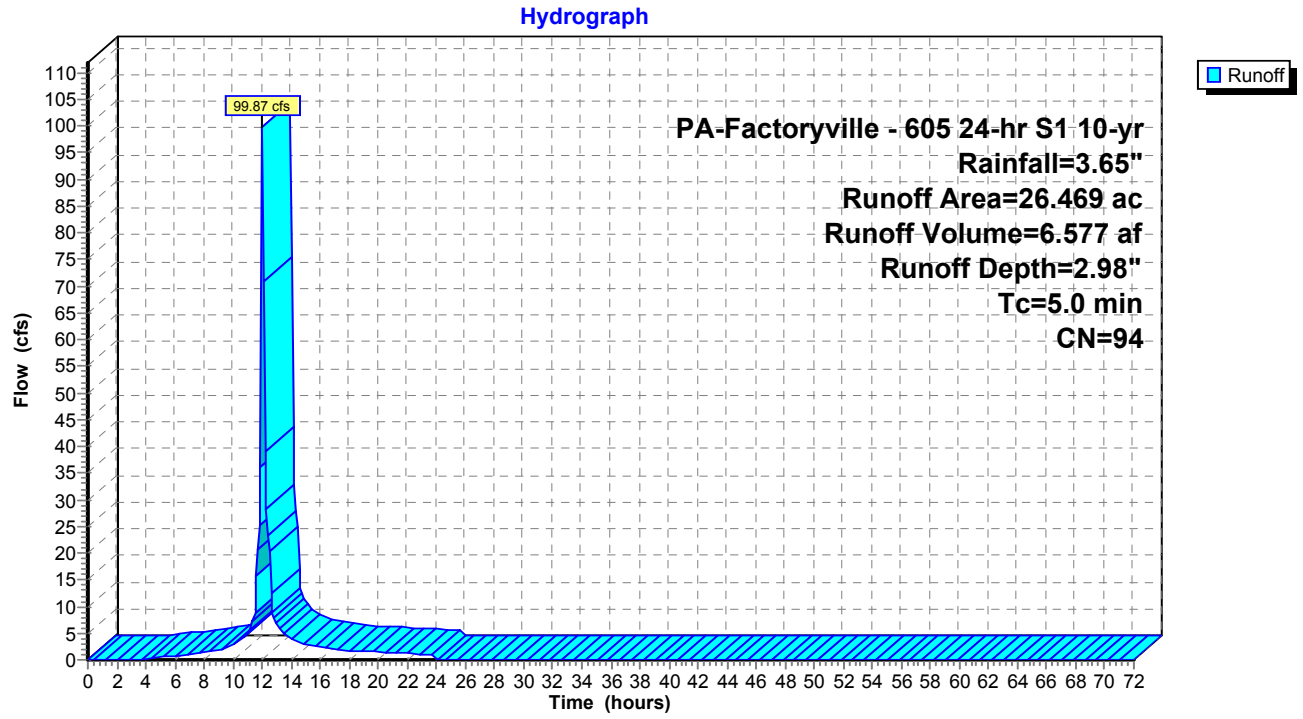
Runoff = 99.87 cfs @ 12.02 hrs, Volume= 6.577 af, Depth= 2.98"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs
PA-Factoryville - 605 24-hr S1 10-yr Rainfall=3.65"

	Area (ac)	CN	Description
	19.284	94	Newly graded area, HSG D
*	3.905	91	Gravel areas, HSG D
*	3.280	98	Impervious areas, HSG D
	26.469	94	Weighted Average
	23.189		87.61% Pervious Area
	3.280		12.39% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					**Direct Entry,**

Subcatchment 21: POST DEVELOPMENT DRAINAGE AREA TO SEDIMENT BASIN 1



Summary for Pond 22: SEDIMENTATION BASIN 1

Inflow Area = 32.559 ac, 11.21% Impervious, Inflow Depth = 2.96" for 10-yr event
Inflow = 122.27 cfs @ 12.02 hrs, Volume= 8.039 af
Outflow = 22.77 cfs @ 12.52 hrs, Volume= 5.282 af, Atten= 81%, Lag= 29.9 min
Primary = 22.77 cfs @ 12.52 hrs, Volume= 5.282 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs
Peak Elev= 955.73' @ 12.51 hrs Surf.Area= 49,877 sf Storage= 199,975 cf

Plug-Flow detention time= 641.2 min calculated for 5.282 af (66% of inflow)
Center-of-Mass det. time= 537.8 min (1,323.4 - 785.6)

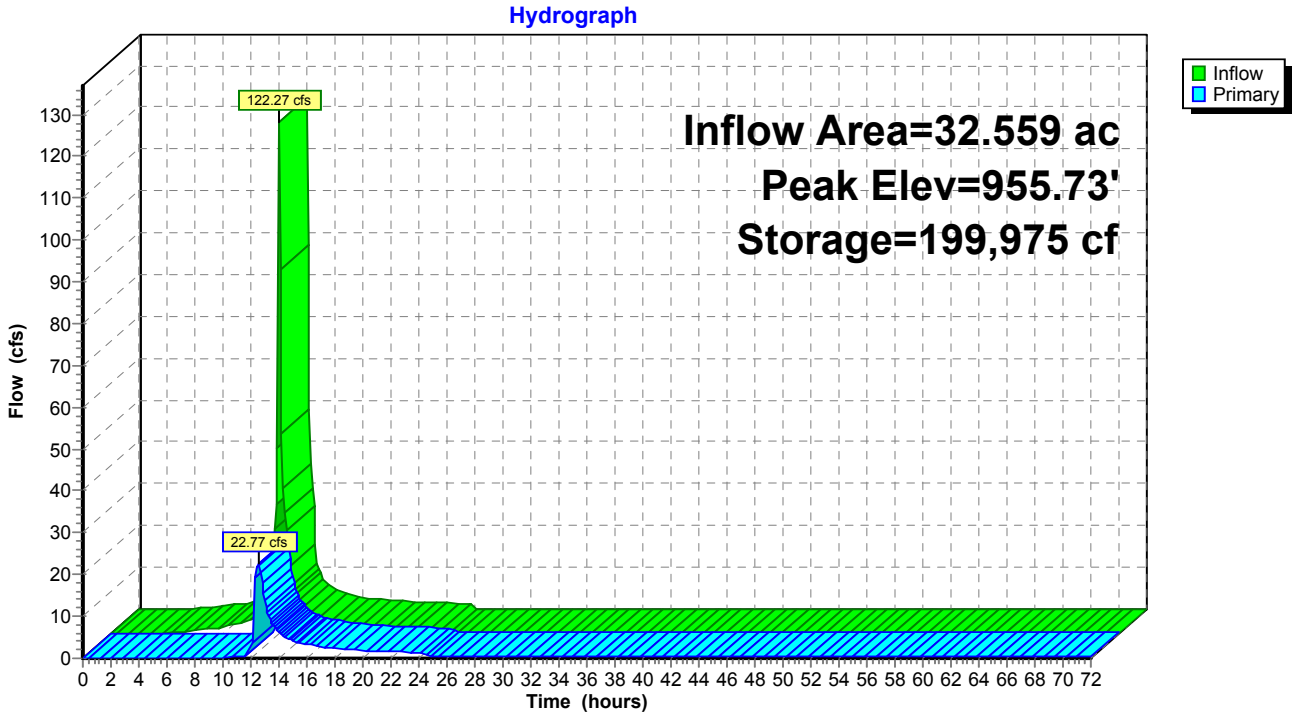
Volume	Invert	Avail.Storage	Storage Description
#1	949.25'	331,752 cf	**Custom Stage Data (Prismatic)** Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
949.25	5,082	0	0
950.00	16,872	8,233	8,233
952.00	27,255	44,127	52,360
954.00	41,379	68,634	120,994
956.00	51,198	92,577	213,571
958.00	66,983	118,181	331,752

Device	Routing	Invert	Outlet Devices
#1	Primary	948.00'	**18.0" Round Culvert** L= 61.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 948.00' / 947.50' S= 0.0082 '/' Cc= 0.900 n= 0.012, Flow Area= 1.77 sf
#2	Primary	951.25'	**0.270 cfs Constant Flow/Skimmer**
#3	Device 1	955.00'	**24.0" x 48.0" Horiz. Orifice/Grate** C= 0.600 Limited to weir flow at low heads
#4	Primary	957.00'	**30.0' long x 15.0' breadth Broad-Crested Rectangular Weir** Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=22.75 cfs @ 12.52 hrs HW=955.73' (Free Discharge)
- **1=Culvert** (Inlet Controls 22.48 cfs @ 12.72 fps)
  - **3=Orifice/Grate** (Passes 22.48 cfs of 24.34 cfs potential flow)
- **2=Constant Flow/Skimmer** (Constant Controls 0.27 cfs)
- **4=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)

Pond 22: SEDIMENTATION BASIN 1



Summary for Subcatchment 20: POST DEVELOPMENT DRAINAGE AREA TO INFILTRATION BASIN 2

[49] Hint: Tc<2dt may require smaller dt

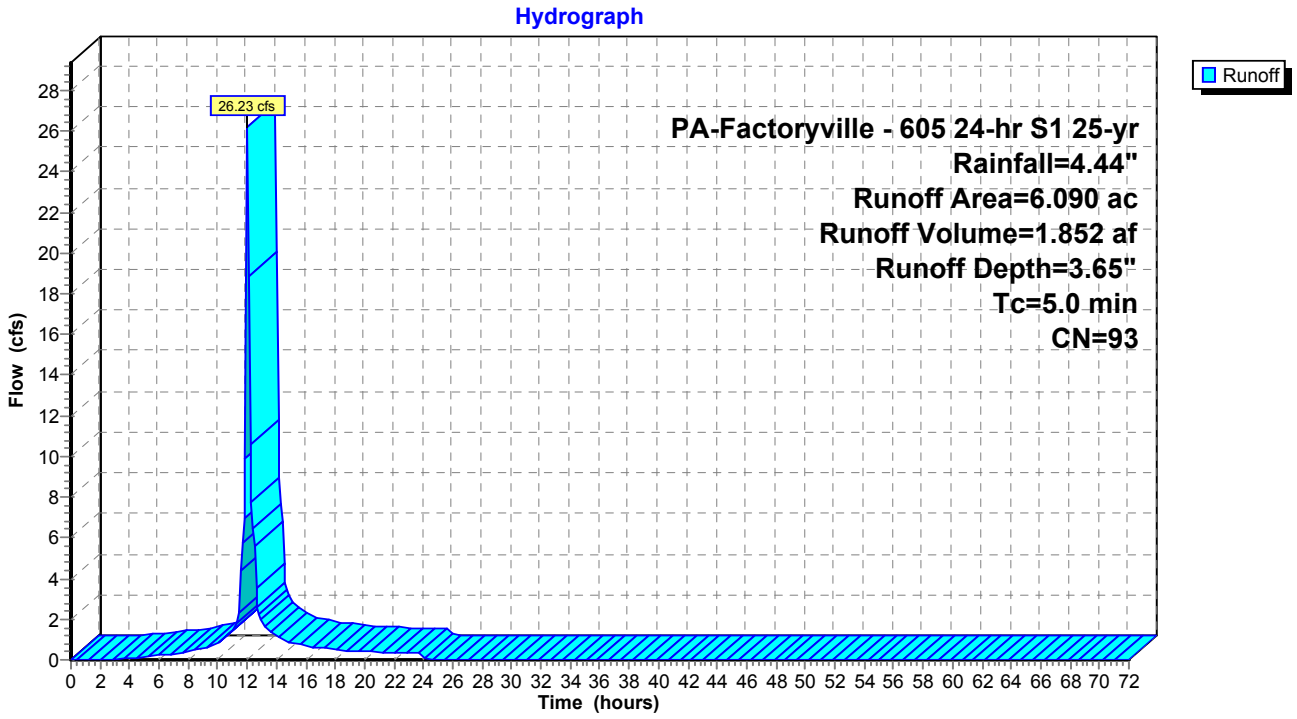
Runoff = 26.23 cfs @ 12.02 hrs, Volume= 1.852 af, Depth= 3.65"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs
PA-Factoryville - 605 24-hr S1 25-yr Rainfall=4.44"

	Area (ac)	CN	Description
*	0.370	98	Impervious, HSG C
	2.360	94	Newly graded area, HSG D
*	3.360	91	Gravel Areas, HSG D
	6.090	93	Weighted Average
	5.720		93.92% Pervious Area
	0.370		6.08% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					**Direct Entry,**

Subcatchment 20: POST DEVELOPMENT DRAINAGE AREA TO INFILTRATION BASIN 2



Summary for Subcatchment 21: POST DEVELOPMENT DRAINAGE AREA TO SEDIMENT BASIN 1

[49] Hint: Tc<2dt may require smaller dt

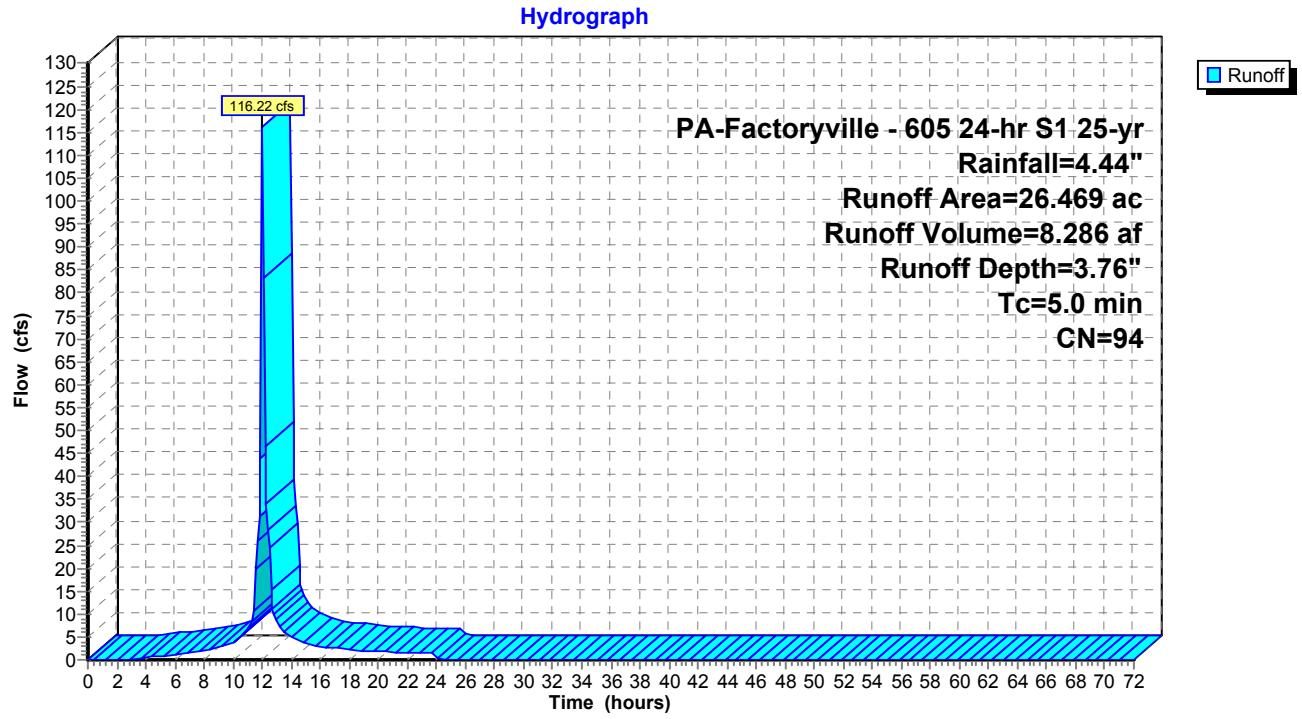
Runoff = 116.22 cfs @ 12.02 hrs, Volume= 8.286 af, Depth= 3.76"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs
PA-Factoryville - 605 24-hr S1 25-yr Rainfall=4.44"

	Area (ac)	CN	Description
	19.284	94	Newly graded area, HSG D
*	3.905	91	Gravel areas, HSG D
*	3.280	98	Impervious areas, HSG D
	26.469	94	Weighted Average
	23.189		87.61% Pervious Area
	3.280		12.39% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					**Direct Entry,**

Subcatchment 21: POST DEVELOPMENT DRAINAGE AREA TO SEDIMENT BASIN 1



Summary for Pond 22: SEDIMENTATION BASIN 1

Inflow Area = 32.559 ac, 11.21% Impervious, Inflow Depth = 3.74" for 25-yr event
Inflow = 142.45 cfs @ 12.02 hrs, Volume= 10.137 af
Outflow = 24.03 cfs @ 12.56 hrs, Volume= 7.376 af, Atten= 83%, Lag= 32.2 min
Primary = 24.03 cfs @ 12.56 hrs, Volume= 7.376 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs
Peak Elev= 956.55' @ 12.56 hrs Surf.Area= 55,511 sf Storage= 242,724 cf

Plug-Flow detention time= 511.0 min calculated for 7.376 af (73% of inflow)
Center-of-Mass det. time= 413.2 min (1,193.5 - 780.3)

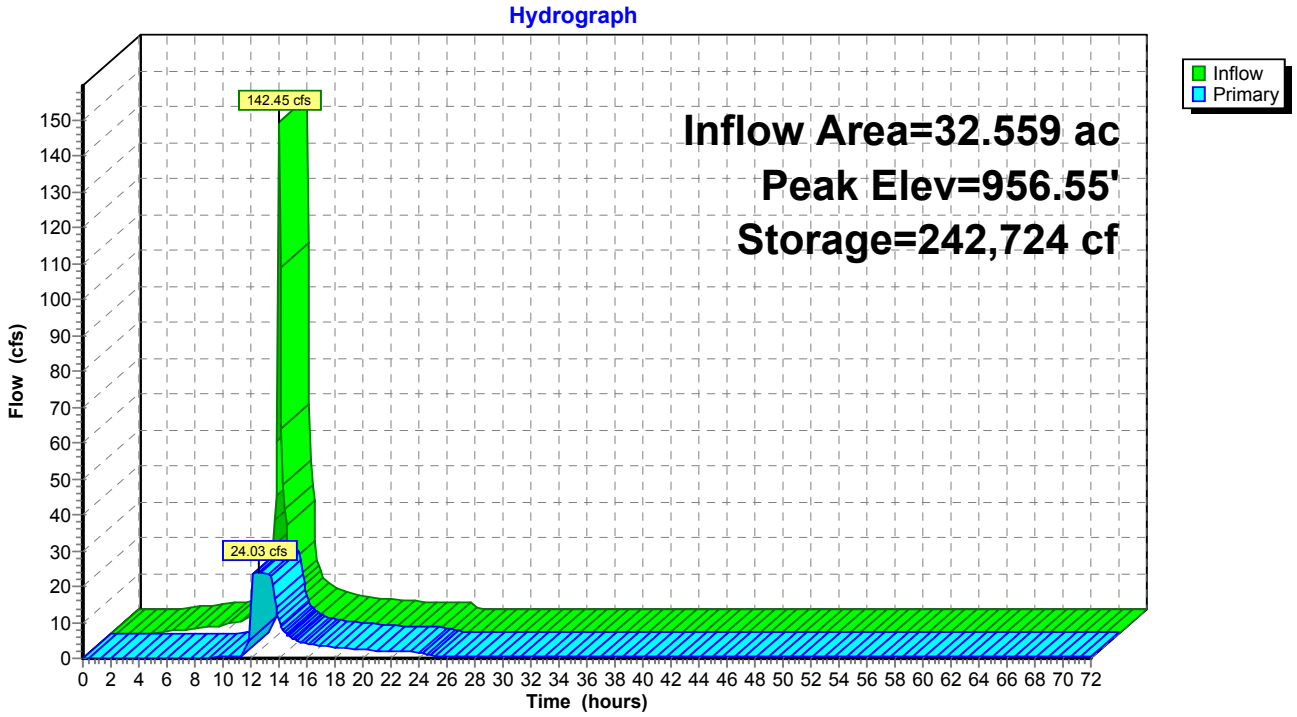
Volume	Invert	Avail.Storage	Storage Description
#1	949.25'	331,752 cf	**Custom Stage Data (Prismatic)** Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
949.25	5,082	0	0
950.00	16,872	8,233	8,233
952.00	27,255	44,127	52,360
954.00	41,379	68,634	120,994
956.00	51,198	92,577	213,571
958.00	66,983	118,181	331,752

Device	Routing	Invert	Outlet Devices
#1	Primary	948.00'	**18.0" Round Culvert** L= 61.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 948.00' / 947.50' S= 0.0082 '/' Cc= 0.900 n= 0.012, Flow Area= 1.77 sf
#2	Primary	951.25'	**0.270 cfs Constant Flow/Skimmer**
#3	Device 1	955.00'	**24.0" x 48.0" Horiz. Orifice/Grate** C= 0.600 Limited to weir flow at low heads
#4	Primary	957.00'	**30.0' long x 15.0' breadth Broad-Crested Rectangular Weir** Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=24.02 cfs @ 12.56 hrs HW=956.54' (Free Discharge)
- **1=Culvert** (Inlet Controls 23.75 cfs @ 13.44 fps)
  - **3=Orifice/Grate** (Passes 23.75 cfs of 47.80 cfs potential flow)
- **2=Constant Flow/Skimmer** (Constant Controls 0.27 cfs)
- **4=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)

Pond 22: SEDIMENTATION BASIN 1



Summary for Subcatchment 20: POST DEVELOPMENT DRAINAGE AREA TO INFILTRATION BASIN 2

[49] Hint: Tc<2dt may require smaller dt

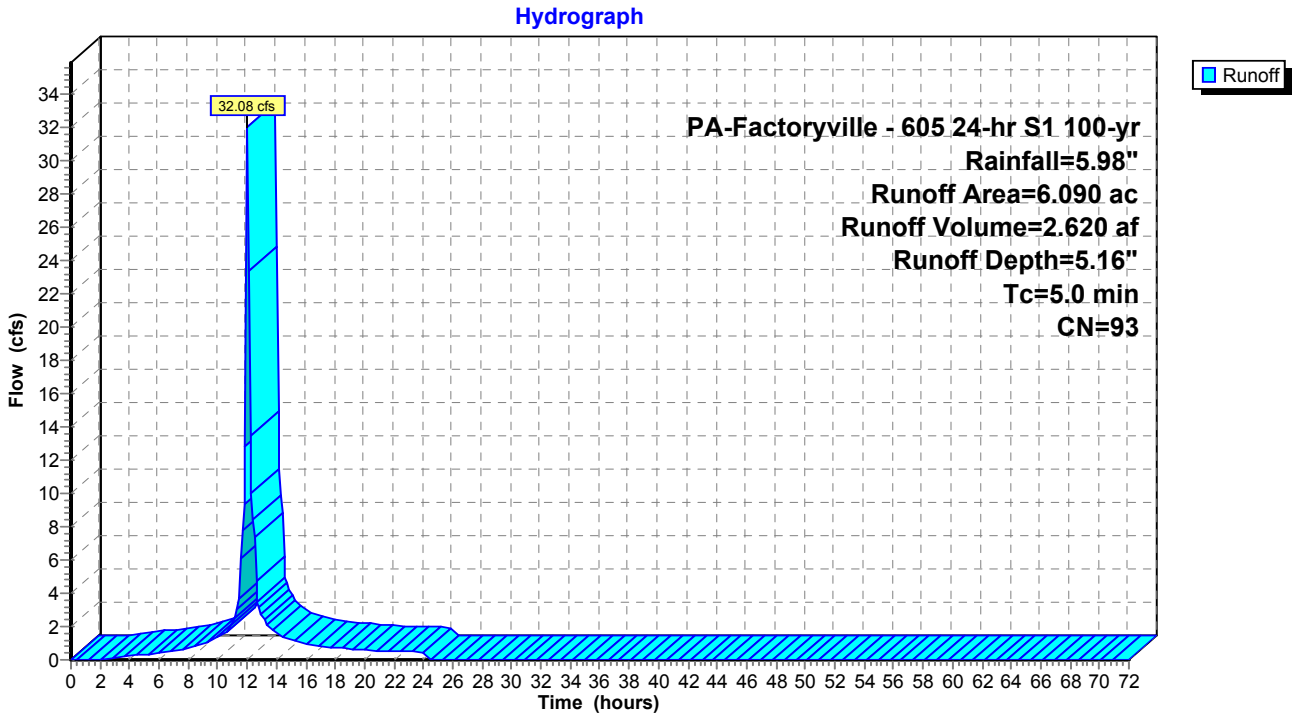
Runoff = 32.08 cfs @ 12.02 hrs, Volume= 2.620 af, Depth= 5.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs
PA-Factoryville - 605 24-hr S1 100-yr Rainfall=5.98"

	Area (ac)	CN	Description
*	0.370	98	Impervious, HSG C
	2.360	94	Newly graded area, HSG D
*	3.360	91	Gravel Areas, HSG D
	6.090	93	Weighted Average
	5.720		93.92% Pervious Area
	0.370		6.08% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					**Direct Entry,**

Subcatchment 20: POST DEVELOPMENT DRAINAGE AREA TO INFILTRATION BASIN 2



Summary for Subcatchment 21: POST DEVELOPMENT DRAINAGE AREA TO SEDIMENT BASIN 1

[49] Hint: Tc<2dt may require smaller dt

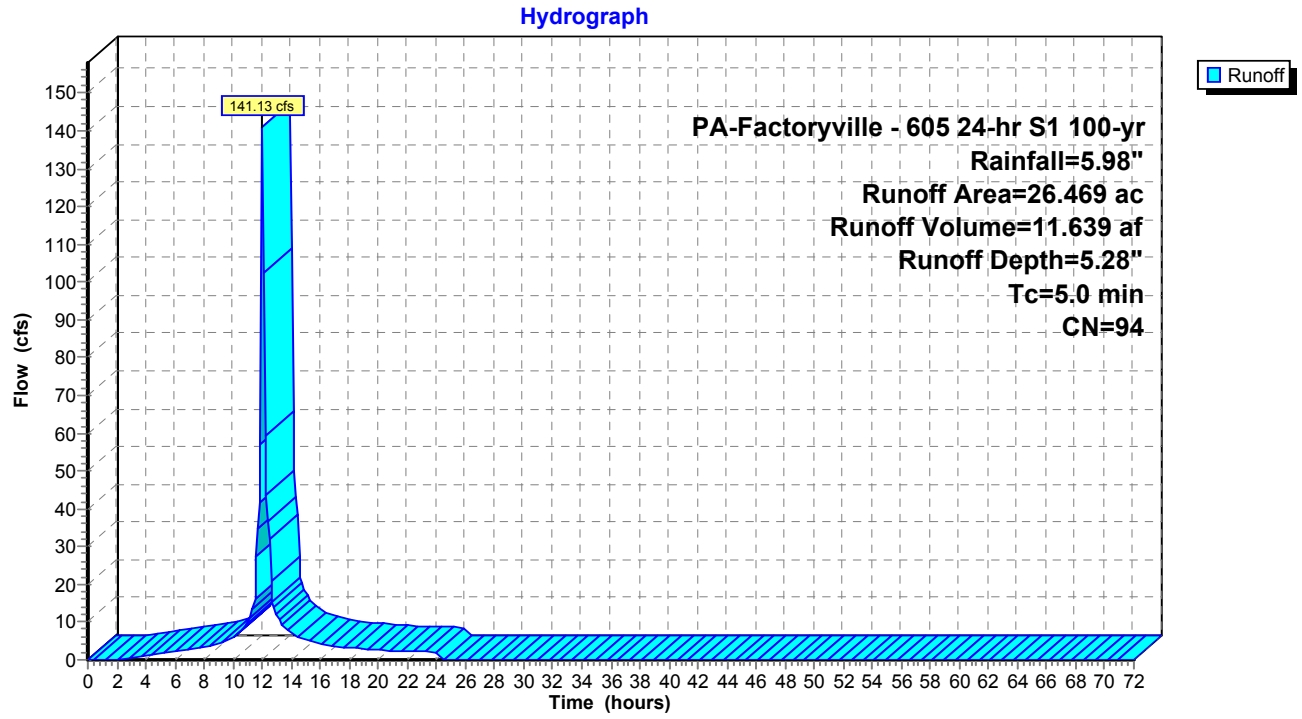
Runoff = 141.13 cfs @ 12.02 hrs, Volume= 11.639 af, Depth= 5.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs
PA-Factoryville - 605 24-hr S1 100-yr Rainfall=5.98"

	Area (ac)	CN	Description
	19.284	94	Newly graded area, HSG D
*	3.905	91	Gravel areas, HSG D
*	3.280	98	Impervious areas, HSG D
	26.469	94	Weighted Average
	23.189		87.61% Pervious Area
	3.280		12.39% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					**Direct Entry,**

Subcatchment 21: POST DEVELOPMENT DRAINAGE AREA TO SEDIMENT BASIN 1



Summary for Pond 22: SEDIMENTATION BASIN 1

Inflow Area = 32.559 ac, 11.21% Impervious, Inflow Depth = 5.26" for 100-yr event
Inflow = 173.22 cfs @ 12.02 hrs, Volume= 14.259 af
Outflow = 55.85 cfs @ 12.32 hrs, Volume= 11.493 af, Atten= 68%, Lag= 17.8 min
Primary = 55.85 cfs @ 12.32 hrs, Volume= 11.493 af

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.10 hrs
Peak Elev= 957.52' @ 12.32 hrs Surf.Area= 63,189 sf Storage= 300,462 cf

Plug-Flow detention time= 387.6 min calculated for 11.477 af (80% of inflow)
Center-of-Mass det. time= 305.0 min (1,077.6 - 772.6)

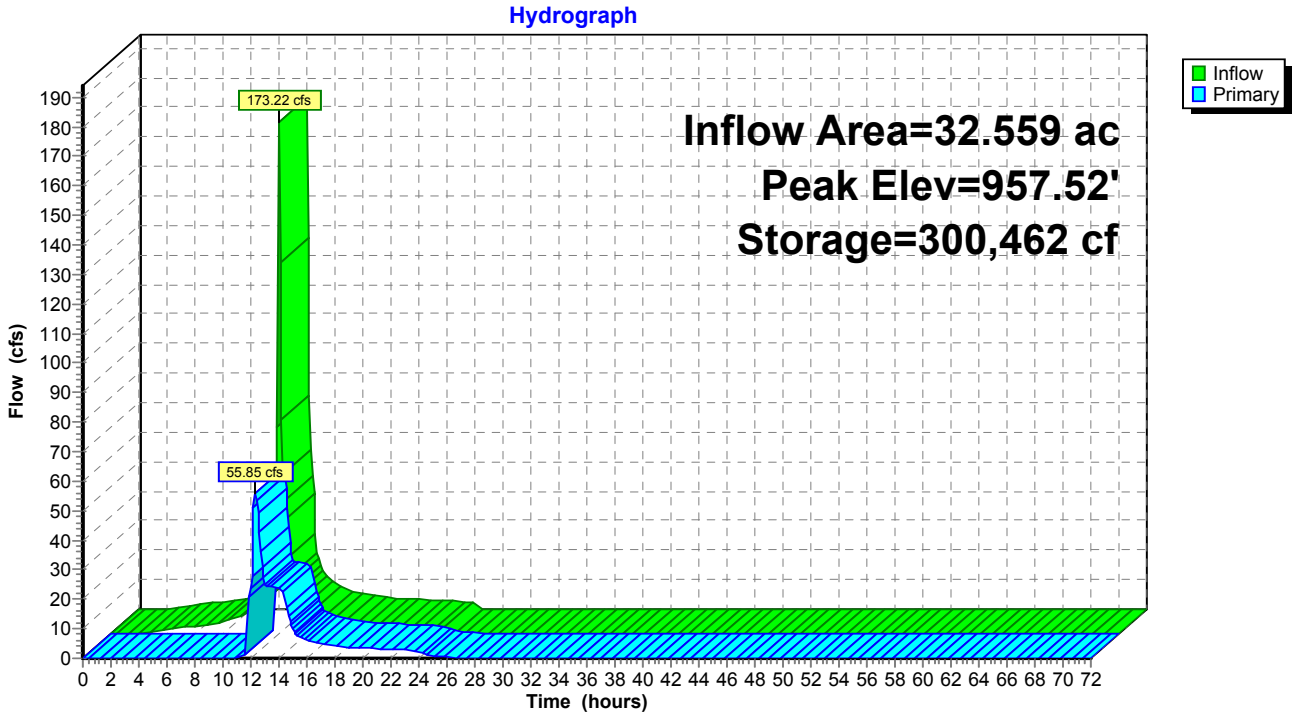
Volume	Invert	Avail.Storage	Storage Description
#1	949.25'	331,752 cf	**Custom Stage Data (Prismatic)** Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
949.25	5,082	0	0
950.00	16,872	8,233	8,233
952.00	27,255	44,127	52,360
954.00	41,379	68,634	120,994
956.00	51,198	92,577	213,571
958.00	66,983	118,181	331,752

Device	Routing	Invert	Outlet Devices
#1	Primary	948.00'	**18.0" Round Culvert** L= 61.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 948.00' / 947.50' S= 0.0082 '/' Cc= 0.900 n= 0.012, Flow Area= 1.77 sf
#2	Primary	951.25'	**0.270 cfs Constant Flow/Skimmer**
#3	Device 1	955.00'	**24.0" x 48.0" Horiz. Orifice/Grate** C= 0.600 Limited to weir flow at low heads
#4	Primary	957.00'	**30.0' long x 15.0' breadth Broad-Crested Rectangular Weir** Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=55.28 cfs @ 12.32 hrs HW=957.51' (Free Discharge)
- **1=Culvert** (Inlet Controls 25.19 cfs @ 14.25 fps)
  - **3=Orifice/Grate** (Passes 25.19 cfs of 61.07 cfs potential flow)
- **2=Constant Flow/Skimmer** (Constant Controls 0.27 cfs)
- **4=Broad-Crested Rectangular Weir** (Weir Controls 29.82 cfs @ 1.94 fps)

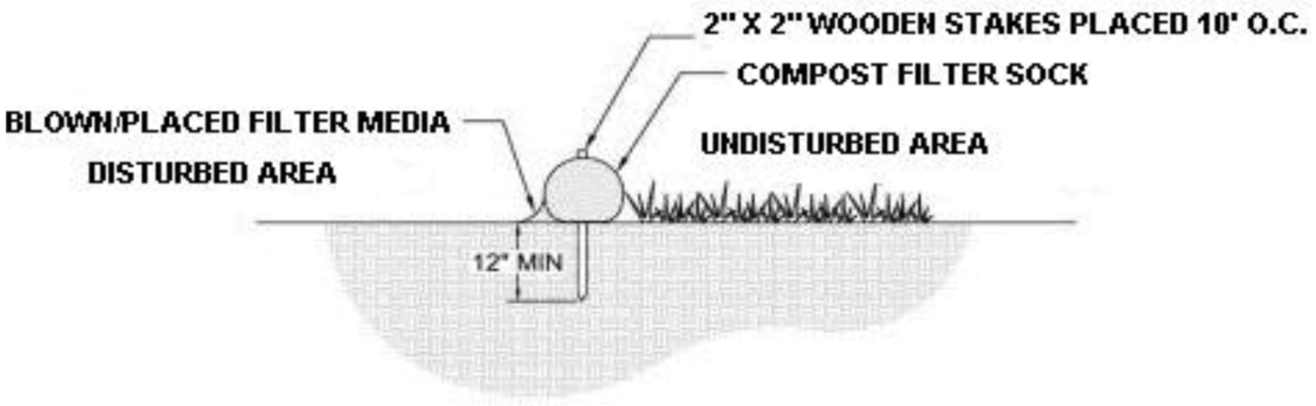
Pond 22: SEDIMENTATION BASIN 1



A.4 Sediment Barrier Table

E&S WORKSHEET #1
Compost Filter Sock

PROJECT NAME: ATLANTIC SUNRISE PROJECT
LOCATION: CLINTON TOWNSHIP, WYOMING COUNTY
PREPARED BY: AOE DATE: 06/15/15
CHECKED BY: AJB DATE: 06/15/15



SOCK NO.	Dia. In.	LOCATION	SLOPE PERCENT	SLOPE LENGTH ABOVE BARRIER (FT)
1	18	BELOW SEDIMENT BASIN 1	33	40
2	12	NEAR CULVERT A DISCHARGE	4	350
3	32	BELOW ACCESS ROAD SW OF THE PAD	33	97
4	24	SOUTH EAST OF PAD	8	200
5	24	SOUTH EAST/EAST OF PAD	5	340
6	32	BELOW NORTHERN CORNER OF PAD	3	500
7	12	NORTH OF NORTH EASTERN STOCKPILE	2:1 MAX	35' MAX
8	18	EAST OF PAD AND STOCKPILES	10	154
9	12	TOPSOIL STOCKPILE	2:1 MAX	35' MAX
10	12	WEST OF MIDDLE STOCKPILE	2:1 MAX	35' MAX
11	32	WEST OF EASTERN STOCKPILE	26	151
12	12	NEAR CULVERT A DISCHARGE	22	32
13	12	TOPSOIL STOCKPILE	2:1 MAX	35' MAX
14	12	BASIN 1 & 2 INFILTRATION AREAS	33	16'

SOURCE: Pennsylvania Erosion and Sediment Pollution Control Manual, Page 372

A.5 Supporting Information

E&S WORKSHEET # 11

Channel Design Data

PROJECT NAME: ATLANTIC SUNRISE PROJECT - COMPRESSOR STATION 605

LOCATION: CLINTON TOWNSHIP, WYOMING COUNTY, PENNSYLVANIA

PREPARED BY: AOE **DATE:** 11/18/2015

CHECKED BY: AJB **DATE:** 11/18/2015

CHANNEL OR CHANNEL SECTION		EMERGENCY SPILLWAY BASIN 1 WEIR	EMERGENCY SPILLWAY BASIN 1 CHANNEL	EMERGENCY SPILLWAY BASIN 2 WEIR	EMERGENCY SPILLWAY BASIN 12CHANNEL	
TEMPORARY OR PERMANENT?	(T OR P)	P	P	P	P	
DESIGN STORM	(2, 5, OR 10 YR)	100	100	100	100	
ACRES	(AC)	THE REQUIRED CAPACITY IS THE 100 YEAR STORM DISCHARGE THROUGH THE EMERGENCY SPILLWAY IF THE OUTLET STRUCTURE IS NOT FUNCTIONING				
MULTIPLIER[1]	(1.6, 2.25, or 2.75)[1]					
Qr (REQUIRED CAPACITY)	(CFS)	***7.27***	***7.27***	***26.96***	***26.96***	
Q (CALCULATED AT FLOW DEPTH d)	(CFS)	***7.27***	***7.32***	***27.18***	***27.64***	
PROTECTIVE LINING[2]		***GRASS/ P550***	***GRASS/ P550***	***GRASS/ P550***	***GRASS/ P550***	
n (MANNING'S COEFFICIENT)[2]		***0.136***	***0.121***	***0.076***	***0.067***	
Va (ALLOWABLE VELOCITY)	(FPS)	N/A	N/A	N/A	N/A	
V (CALCULATED AT FLOW DEPTH d)	(FPS)	***0.72***	***2.35***	***1.66***	***5.60***	
τa (MAX ALLOWABLE SHEAR STRESS)	(LB/FT^2)	12.00	12.00	12.00	12.00	
τd (CALC'D SHEAR STRESS AT FLOW DEPTH d)	(LB/FT^2)	***0.37***	***4.12***	***0.57***	***6.38***	
CHANNEL BOTTOM WIDTH	(FT)	15	15	15	15	
CHANNEL SIDE SLOPES	(H:V)	3	3	3	3	
D (TOTAL DEPTH)	(FT)	1.0	1.0	1.0	1.0	
CHANNEL TOP WIDTH @ D	(FT)	21	21	21	21	
d (CALCULATED FLOW DEPTH)	(FT)	***0.60***	***0.20***	***0.92***	***0.31***	
CHANNEL TOP WIDTH @ FLOW DEPTH d	(FT)	***18.60***	***16.20***	***20.52***	***16.86***	
BOTTOM WIDTH: FLOW DEPTH RATIO	(12:1 MAX)	***25.00***	***75.00***	***16.30***	***48.39***	
d50 STONE SIZE	(IN)	N/A	N/A	N/A	N/A	
A (CROSS-SECTIONAL AREA)	(SQ. FT.)	***10.08***	***3.12***	***16.34***	***4.94***	
R (HYDRAULIC RADIUS)		***0.54***	***0.19***	***0.78***	***0.29***	
S (BED SLOPE)[3]	(FT/FT)	0.01	0.33	0.01	0.33	
Sc (CRITICAL SLOPE)	(FT/FT)	***0.335***	***0.371***	***0.092***	***0.099***	
.7Sc	(FT/FT)	***0.234***	***0.260***	***0.065***	***0.069***	
1.3Sc	(FT/FT)	***0.435***	***0.482***	***0.120***	***0.129***	
STABLE FLOW?	(Y/N)	***Y***	***N***	***Y***	***Y***	
FREEBOARD BASED ON UNSTABLE FLOW	(FT)	***0.03***	***0.04***	***0.11***	***0.13***	
FREEBOARD BASED ON STABLE FLOW	(FT)	0.50	0.50	0.50	0.50	
MINIMUM REQUIRED FREEBOARD[4]	(FT)	0.50	0.50	0.50	0.50	
DESIGN METHOD FOR PROTECTIVE LINING [5] PERMISSIBLE VELOCITY (V) OR SHEAR STRESS	(S)	S	S	S	S	

1. Use 1.6 for Temporary Channels; 2.25 for Temporary Channels in Special Protection (HQ or EV) Watersheds; 2.75 for Permanent Channels. For Rational Method, enter "N/A" and attach E&S Worksheets 9 and 10. For TR-55 enter "N/A" and attach appropriate Worksheets.
2. Adjust "n" value for changes in channel liner and flow depth. For vegetated channels, provide data for manufactured linings without vegetation and with vegetation in separate columns.
3. Slopes may not be averaged.
4. Minimum Freeboard is 0.5 ft. or ¼ Total Channel Depth, whichever is greater
5. Permissible velocity lining design method is not acceptable for channels with a bed slope of 10% or greater. Shear stress lining design method is required for channels with a bed slope of 10% or greater. Shear stress lining design method may be used for any channel bed slope.

Source: 363-2134-008 / March 31, 2012 / Page 382

TABLE 6.6
Riprap Gradation, Filter Blanket Requirements, Maximum Velocities

Percent Passing (Square Openings)						
Class, Size NO. / **Rock Size (Inches)**	**R-8**	**R-7**	**R-6**	**R-5**	**R-4**	**R-3**
42	100					
30		100				
24	15-50		100			
18		15-50		100		
15	0-15					
12		0-15	15-50		100	
9				15-50		
6			0-15		15-50	100
4				0-15		
3					0-15	15-50
2						0-15
Nominal Placement Thickness (inches)	63	45	36	27	18	9
Filter Stone[1]	AASHTO #1	AASHTO #1	AASHTO #1	AASHTO #3	AASHTO #3	AASHTO #57
V_{max} (ft/sec)	17.0	14.5	13.0	11.5	9.0	6.5

Adapted from PennDOT Pub. 408, Section 703.2(c), Table C

1 This is a general standard. Soil conditions at each site should be analyzed to determine actual filter size. A suitable woven or non-woven geotextile underlayment, used according to the manufacturer's recommendations, may be substituted for the filter stone for gradients < 10%.

TABLE 6.7
Comparison of Various Gradations of Coarse Aggregates

Total Percent Passing															
AASHTO NUMBER	**6 ½**	**4"**	**3 ½"**	**2 ½**	**2"**	**1 ½ "**	**1"**	**3/4 "**	**1/2"**	**3/8"**	**#4**	**#8**	**#16**	**#30**	**#100**
1		100	90-100	25-60		0-15		0-5							
3				100	90-100	35-70	0-15		0-5						
5						100	90-100	20-55	0-10	0-5					
57						100	90-100		25-60		0-10	0-5			
67							100	90-100		20-55	0-10	0-5			
7								100	90-100	40-70	0-15	0-5			
8									100	85-100	10-30	0-10	0-5		
10										100	75-100				10-30

PennDOT Publication 408, Section 703.2(c), Table C

Tables 6.6 and 6.7 should be placed on the plan drawings of all sites where riprap channel linings are proposed.

TABLE 6.3
Manning's "n" for Trapezoidal Channels with Vegetative Stabilization (Retardance C)

Flow Depth (FT)	Channel Bed Slope (FT/FT)									
	0.01	**0.02**	**0.03**	**0.04**	**0.05**	**0.06**	**0.07**	**0.08**	**0.09**	**0.10**
0.1	0.15	0.11	0.10	0.09	0.08	0.07	0.07	0.07	0.06	0.06
0.2	0.12	0.09	0.08	0.07	0.06	0.06	0.05	0.05	0.05	0.05
0.3	0.10	0.08	0.07	0.06	0.05	0.05	0.05	0.04	0.04	0.04
0.4	0.09	0.07	0.06	0.05	0.05	0.05	0.04	0.04	0.04	0.04
0.5	0.08	0.07	0.06	0.05	0.05	0.04	0.04	0.04	0.04	0.03
0.6	0.08	0.06	0.05	0.05	0.04	0.04	0.04	0.04	0.03	0.03
0.7	0.08	0.06	0.05	0.04	0.04	0.04	0.04	0.03	0.03	0.03
0.8	0.07	0.06	0.05	0.04	0.04	0.04	0.03	0.03	0.03	0.03
0.9	0.07	0.05	0.05	0.04	0.04	0.04	0.03	0.03	0.03	0.03
1.0	0.07	0.05	0.04	0.04	0.04	0.03	0.03	0.03	0.03	0.03
2.0	0.06	0.04	0.04	0.03	0.03	0.03	0.03	0.02	0.02	0.02
3.0	0.05	0.04	0.03	0.03	0.03	0.02	0.02	0.02	0.02	0.02
4.0	0.04	0.03	0.03	0.03	0.02	0.02	0.02	0.02	0.02	0.02
5.0	0.04	0.03	0.03	0.02	0.02	0.02	0.02	0.02	0.02	0.02
6.0	0.04	0.03	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02
7.0	0.04	0.03	0.02	0.02	0.02	0.02	0.02	0.02	0.01	0.01
8.0	0.03	0.02	0.02	0.02	0.02	0.02	0.02	0.01	0.01	0.01
9.0	0.03	0.02	0.02	0.02	0.02	0.02	0.02	0.01	0.01	0.01
10.0	0.03	0.02	0.02	0.02	0.02	0.02	0.01	0.01	0.01	0.01

PA DEP

NOTE: For vegetated channels that are not anticipated to have a retardance C value (e.g. frequently mowed channels), the equation on page 134 and Table 6.3 should not be used. The designer is referred to NRCS publications for guidance on designing vegetative channels with Retardances other than C.

Westmoreland Conservation District

Weir Report

BERM 4 WEIR FLOW (100 YR DISCHARGE FROM SWALE 1B)

Rectangular Weir

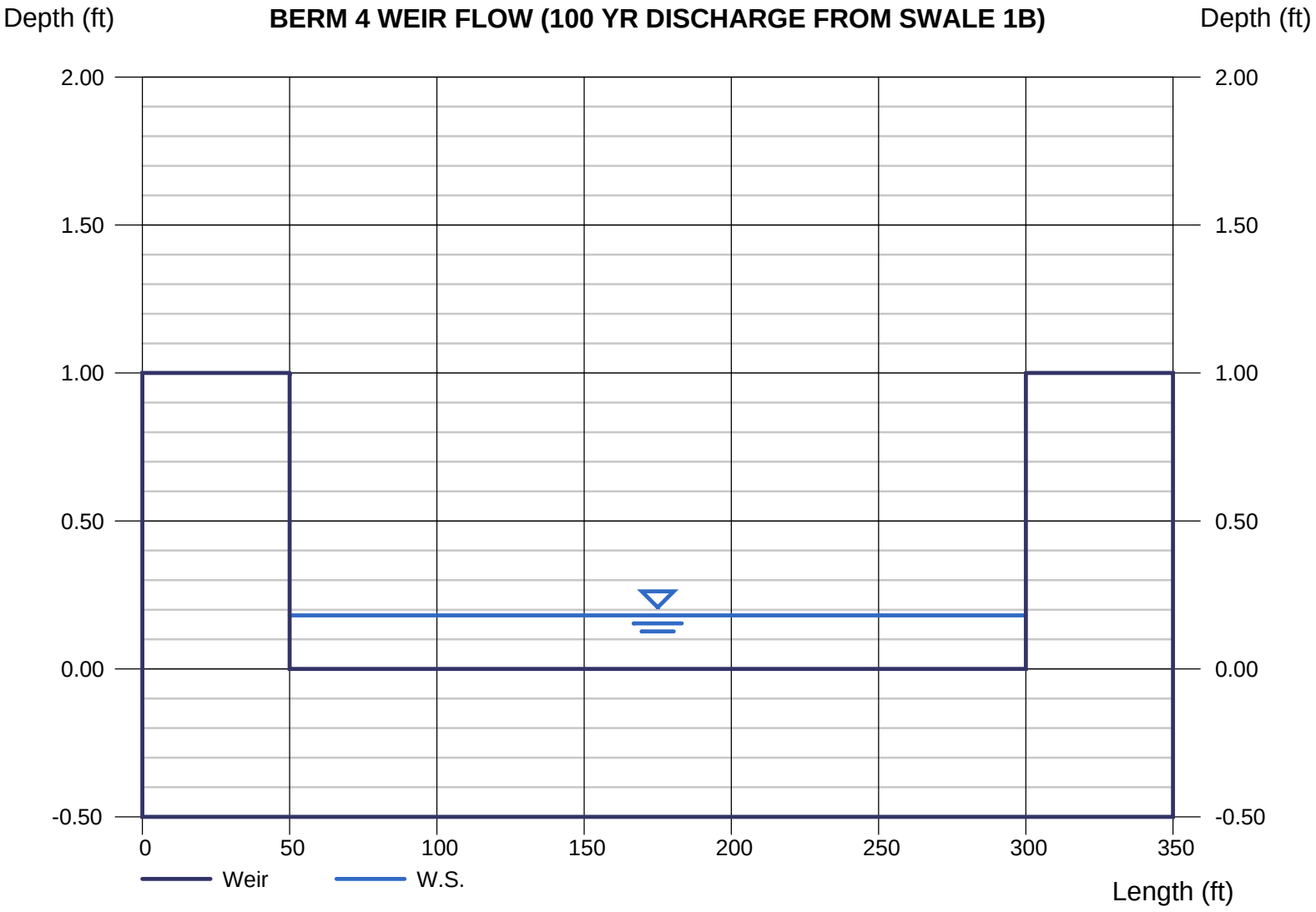
Crest	= Broad
Bottom Length (ft)	= 250.00
Total Depth (ft)	= 1.00

Calculations

Weir Coeff. Cw	= 2.60
Compute by:	Known Q
Known Q (cfs)	= 50.00

Highlighted

Depth (ft)	= 0.18
Q (cfs)	= 50.00
Area (sqft)	= 45.18
Velocity (ft/s)	= 1.11
Top Width (ft)	= 250.00



Weir Report

BERM 3 WEIR FLOW (100 YR DISCHARGE FROM SWALE 1B)

Rectangular Weir

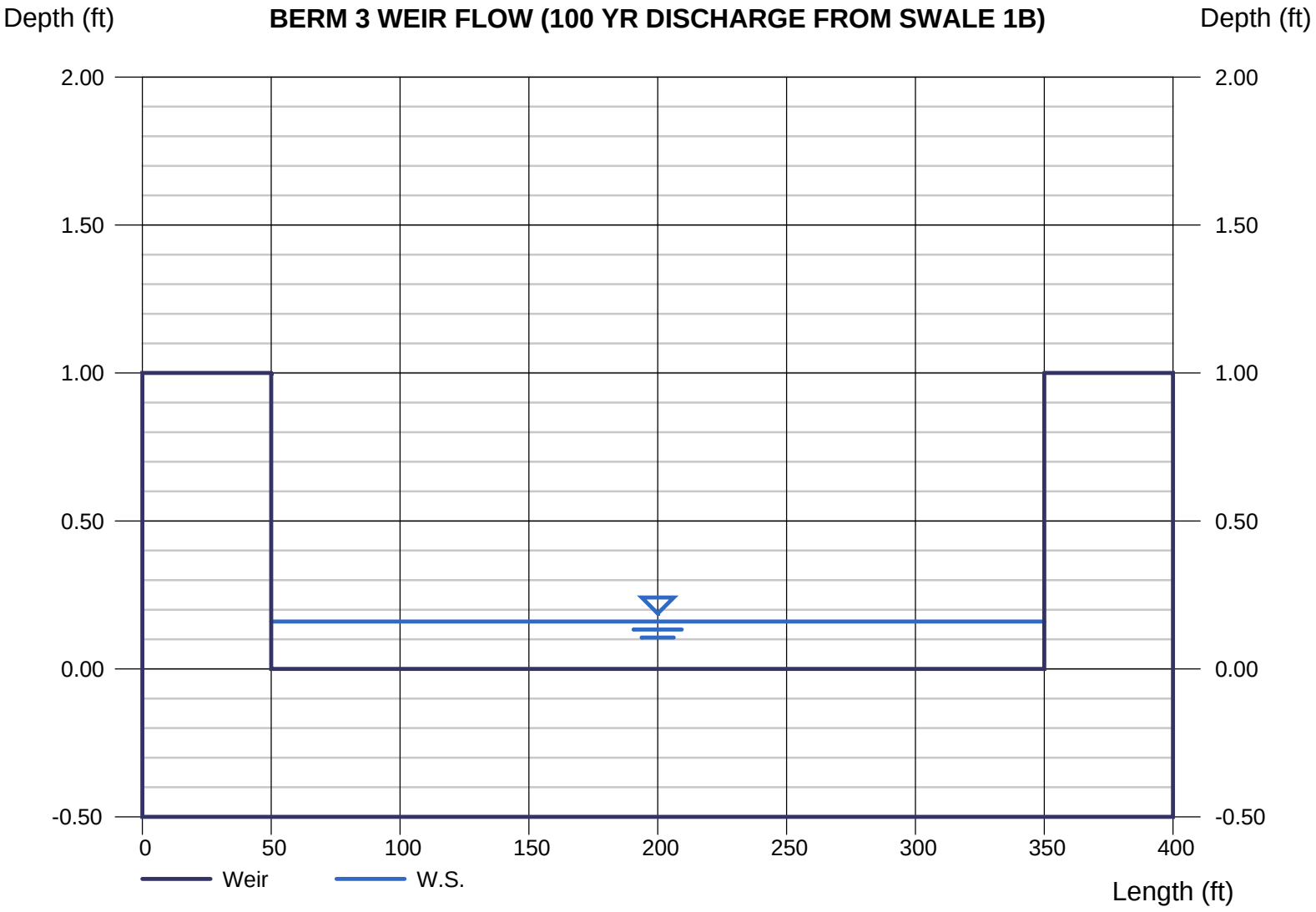
Crest	= Broad
Bottom Length (ft)	= 300.00
Total Depth (ft)	= 1.00

Calculations

Weir Coeff. Cw	= 2.60
Compute by:	Known Q
Known Q (cfs)	= 50.00

Highlighted

Depth (ft)	= 0.16
Q (cfs)	= 50.00
Area (sqft)	= 48.01
Velocity (ft/s)	= 1.04
Top Width (ft)	= 300.00



Weir Report

BERM 2 WEIR FLOW (100 YR DISCHARGE FROM SWALE 1B)

Rectangular Weir

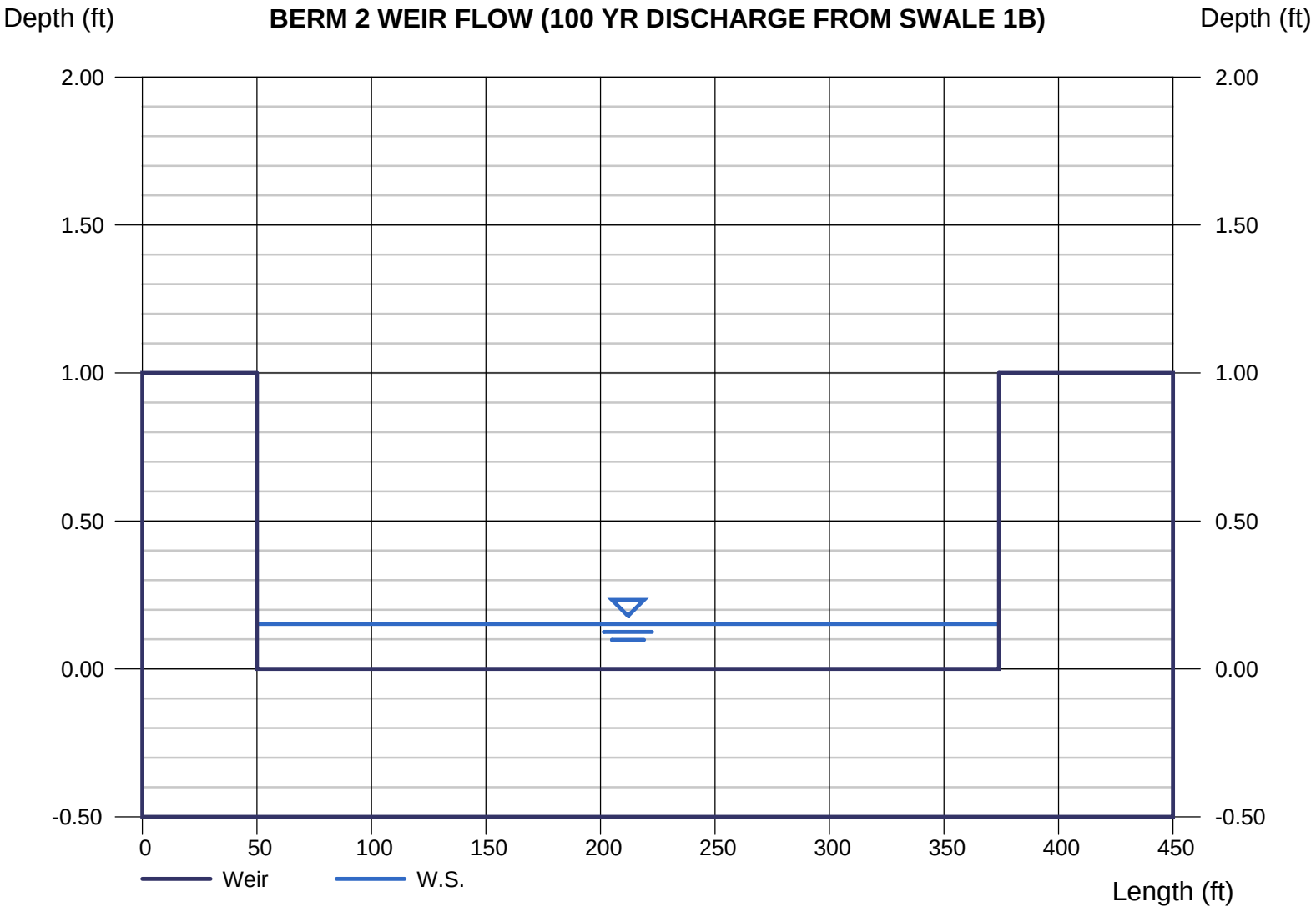
Crest	= Broad
Bottom Length (ft)	= 324.00
Total Depth (ft)	= 1.00

Calculations

Weir Coeff. Cw	= 2.60
Compute by:	Known Q
Known Q (cfs)	= 50.00

Highlighted

Depth (ft)	= 0.15
Q (cfs)	= 50.00
Area (sqft)	= 49.25
Velocity (ft/s)	= 1.02
Top Width (ft)	= 324.00



Weir Report

BERM 1 WEIR FLOW (100 YR DISCHARGE FROM SWALE 1B)

Rectangular Weir

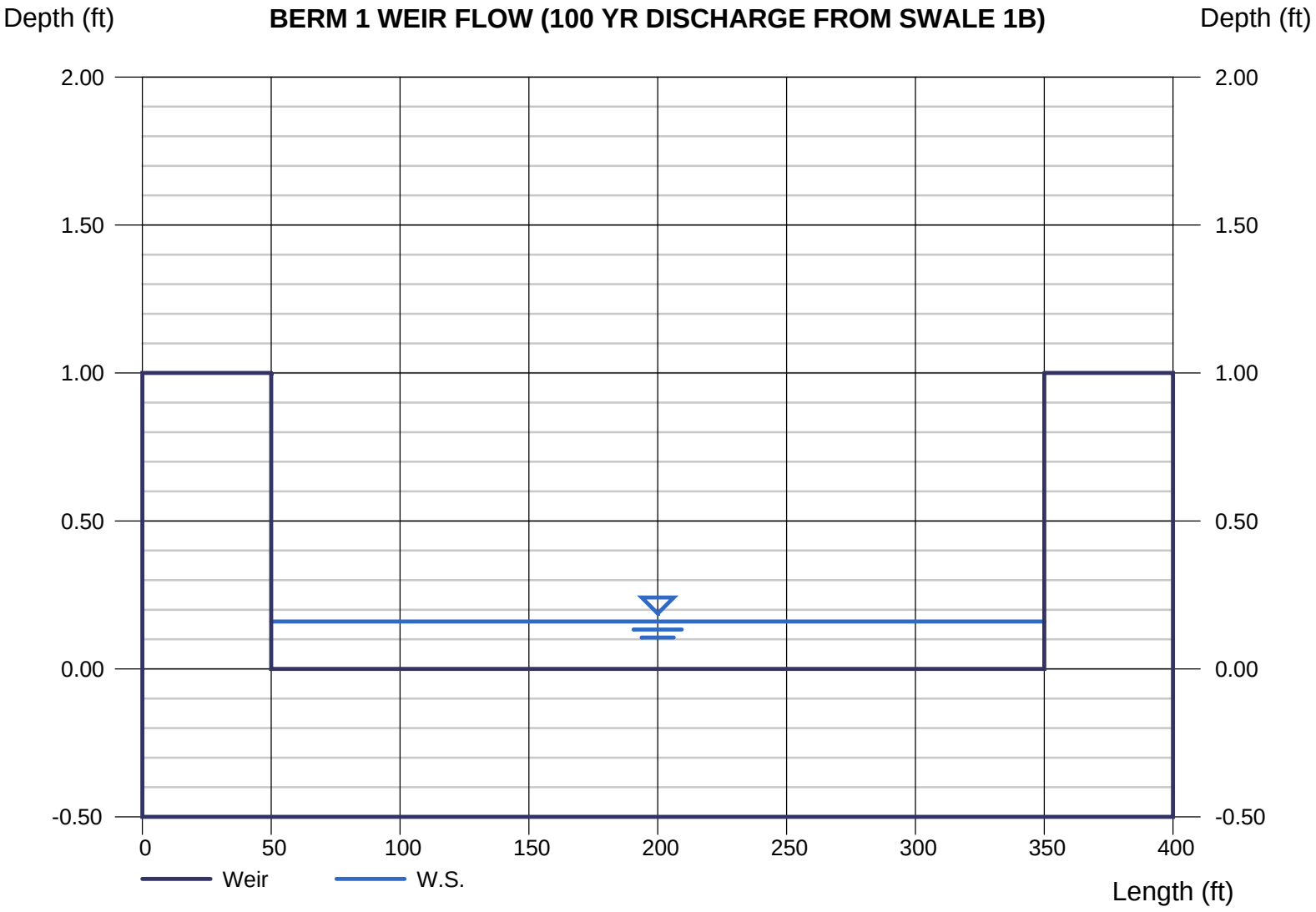
Crest	= Broad
Bottom Length (ft)	= 300.00
Total Depth (ft)	= 1.00

Calculations

Weir Coeff. Cw	= 2.60
Compute by:	Known Q
Known Q (cfs)	= 50.00

Highlighted

Depth (ft)	= 0.16
Q (cfs)	= 50.00
Area (sqft)	= 48.01
Velocity (ft/s)	= 1.04
Top Width (ft)	= 300.00



Weir Report

BERM 5 WEIR FLOW (100 YR DISCHARGE FROM SWALE 1B)

Rectangular Weir

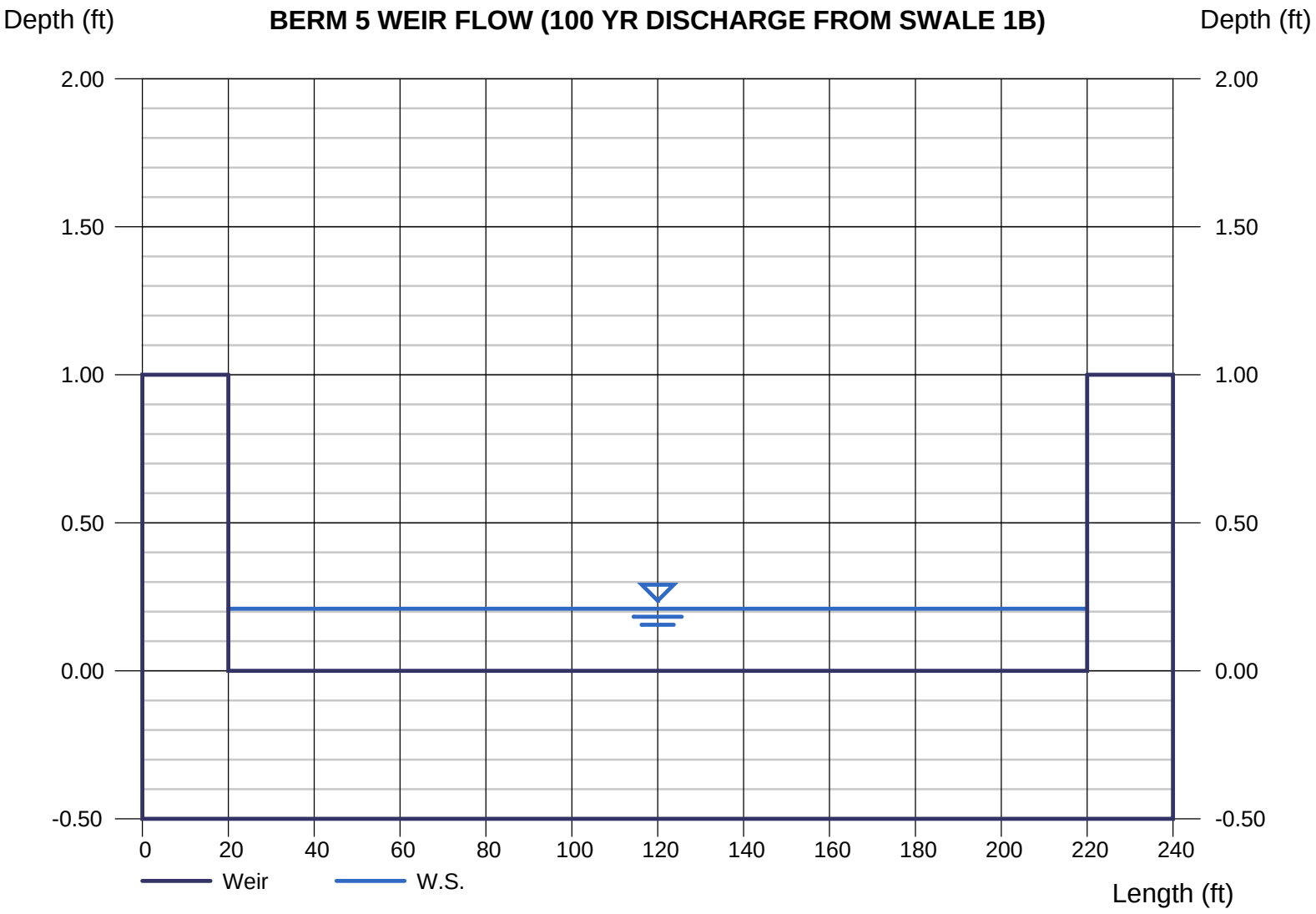
Crest	= Broad
Bottom Length (ft)	= 200.00
Total Depth (ft)	= 1.00

Calculations

Weir Coeff. Cw	= 2.60
Compute by:	Known Q
Known Q (cfs)	= 50.00

Highlighted

Depth (ft)	= 0.21
Q (cfs)	= 50.00
Area (sqft)	= 41.94
Velocity (ft/s)	= 1.19
Top Width (ft)	= 200.00



Busher, Al

From: Jill Pack <JPack@tensarcorp.com>
Sent: Monday, November 17, 2014 12:15 PM
To: abuser@blcompanies.com
Subject: Performance of SC150

Mr. Busher,

As we spoke about on the phone, there are a lot of factors that could influence the performance and life of our products. Generally speaking the 24 month longevity of the SC150 is the average functional longevity, and so the stated design values should stay near 100% during that time frame. But as we know climates and conditions vary, so if you are in conditions where the erosion control blanket would see increases in degradation time (extreme UV conditions, large shifts in moisture and temperature, etc.) then the functionality would be reduced to some degree. This is difficult to measure as no current testing standards for temporary products test beyond initial product installation. Also since these products are typically used in conjunction with establishing vegetation, the vegetation would have an impact on the performance of the system together and would typically strengthen the system once the vegetation develops.

I would also note that we do offer a longevity warranty on all of our temporary products that equates to 75% of the stated functional longevity. So for a 24 month product we do warranty that it will last and perform a minimum of 18 months. This further supports our confidence in the quality and performance of our products.

If you have any additional questions, please feel free to contact me.

Thanks,

Jill Pack, CPESC | Product Manager - Erosion Control

Tensar | NORTH AMERICAN GREEN

Tensar International Corporation | 5401 St. Wendel – Cynthiana Road | Poseyville, IN 47633 | Office: 812-867-6632 | Toll Free: 800-772-2040 | Fax: 812-867-0247 | jpack@tensarcorp.com | www.nagreen.com

ROLLMAX™
ROLLED EROSION CONTROL

ROLLED
EROSION CONTROL

SYSTEMS BROCHURE

Tensar®

When It Rains (or Blows, Flows or Washes), It Pours

Erosion not only wears away slopes, degrades shorelines and steals precious topsoil, it can also threaten water sources, damage man-made structures, reconfigure landscapes and disrupt wildlife habitats. Add the stiff penalties at stake for violating Environmental Protection Agency (EPA) or local enforcement agency regulations, and the costs of erosion can quickly climb out of control.

WE ROLL AGAINST THE FLOW

Tensar International Corporation (Tensar) is the world's leading provider of performance-guaranteed erosion control solutions. For more than 25 years, the Tensar® North American Green® line of erosion and sediment control products has kept our customers on solid ground.

The RollMax™ Systems' family of Rolled Erosion Control Products (RECPs) is solid evidence of Tensar's ongoing investment in innovation. Our short-term and long-term erosion control blankets and turf reinforcement mats keep you one step ahead of just about any erosion challenge.

ALL THE HELP YOU NEED

Of all the RECP manufacturers out there, none can match Tensar's customer service and technical knowhow. Our support team will assist with project design and product specification or, if you'd rather do it yourself, use our Erosion Control Materials Design Software (ECMDS®) (the industry's first) for selecting material, and planning your project.

Tensar products are sold exclusively through nearly 200 Tensar Erosion Control authorized distributors worldwide. The Tensar Erosion Solutions Specialist program certifies our distributors and their sales representatives to design erosion control measures that comply with the EPA's National Pollutant Discharge Elimination System (NPDES) and other industry regulations.

Tensar is a proud member of the Erosion Control Technology Council (ECTC) and the International Erosion Control Association (IECA).

NEW NAME – SAME GREAT PERFORMANCE AND SERVICE

Tensar International Corporation acquired North American Green (NAG) in 2004 to enhance our position as the premier provider of technology-driven site solutions. We are proud to continue offering the same NAG level of service, quality and high-performance erosion control products under the name of Tensar.

Site erosion can be costly, with the RollMax Systems full line of rolled erosion control products we can keep you in compliance.

For more than 25 years, our Tensar North American Green line of products has kept our customers on solid ground.

Applications Welcome

For nearly every erosion application, there's a RollMax™ Systems solution. Permanent turf reinforcement mats provide long-term protection and vegetation establishment; temporary Erosion Control Blankets (ECBs) give immediate protection and assist with vegetation establishment before degrading naturally. Tensar's extensive selection of RollMax products almost guarantees you'll find the answer to your erosion problems.

Typical erosion control applications include these and many more:

- Highway and other DOT projects
- Commercial and residential developments
- Shorelines and waterways
- Golf course turf management
- Oil and gas pipeline restoration
- Mine and fire reclamation
- Military base construction

AND SPEAKING OF GUARANTEES . . .

Tensar's Ultimate Assurance Guarantee is the most comprehensive in the industry. It says if any properly specified and installed Tensar® North American Green® rolled erosion control product designed by a qualified engineer or Tensar technical representative in accordance with our Erosion Control Materials Design Software (ECMDS®) fails to perform under the conditions in the Guarantee, then we will replace the failed product with our next higher-performance RECP product, along with the cost of seed, fertilizer, topsoil and other amendments lost due to such product failure. Our Guarantee warrants in accordance with its terms and conditions all registered projects designed with the latest version of our ECMDS and properly installed.

Tensar turf reinforcement mats are also guaranteed to reinforce vegetation for five years after installation, and the functional longevity of these products' permanent structures is warranted for a minimum of 10 years after installation, subject to the terms and conditions set forth in the Guarantee.

From challenging roadway improvements to concentrated flow channels, there is a RollMax product ready to handle the job – and it's guaranteed.

Permanent RollMax™ Solutions

Back in the day, rock riprap, articulated concrete blocks and poured concrete were the only way to deal with erosion in high-flow channels, on shorelines and other areas where water and/or wind exceed the shear limits of unreinforced vegetation.

Not anymore. Tensar's permanent Turf Reinforcement Mats (TRMs) use 100% synthetic components or a composite of synthetic and natural materials for long-term erosion protection and vegetation establishment. Whether compared to rock riprap or concrete, the RollMax™ Systems' permanent TRMs offer a number of significant advantages:

- Prevent loss of precious topsoil to wind and water erosion
- Permanently reinforce vegetation root and stem structures
- Provide excellent conditions for quick, healthy vegetation growth
- Stabilize slopes from erosion to keep roadways safe and clean
- Protect water quality in lakes, rivers and streams
- Protect dormant seeding during winter months
- Easily conform to landscape features
- Lightweight for easy handling and transportation

VMAX® COMPOSITE TURF REINFORCEMENT MATS

VMax® C-TRMs combine three-dimensional matting with fiber matrix material for permanent erosion control on severe slopes, spillways, stream banks, shorelines and in high- to extreme-flow channels. These extensively tested products provide maximum performance through all three phases of reinforced vegetative lining development: unvegetated, establishment, and maturity. Incorporating the best performance features of temporary and permanent Tensar erosion control products, VMax C-TRMs deliver these tangible benefits:

- Surface-applied for the highest level of immediate soil protection
- Less than one third of the installed cost of rock or concrete
- No heavy equipment needed to install
- More attractive and effective "Green" alternative than rock riprap or concrete
- Exceeds FHWA and ECTC standards for TRMs
- An EPA Best Management Practice (BMP) for National Pollutant Discharge Elimination System (NPDES) regulations
- No threat to pedestrians or automobiles when used near travel routes
- Naturally filters runoff water

The TRMs easily conform to various landscape features to prevent the loss of precious topsoil.

The RollMax TRMs are installed in a one-step operation directly over the prepared seedbed saving time and money and ensuring the highest level of erosion control and vegetation reinforcement.

VMax® P550® Permanent TRM

Our top of the line P550® TRM has a polypropylene fiber matrix augmenting the permanent netting structure with permanent mulching and erosion control performance. Unvegetated, the P550 TRM reduces soil loss to less than 0.5 in. (12.7 mm) under shear stress up to 4.0 lbs/ft^2 (191 Pa). The ultra-strong structure drives the vegetated shear resistance up to 14 lbs/ft^2 (672 Pa), establishing a new maximum for vegetation reinforcement. The P550 TRM may be used as an alternative for poured concrete or articulated concrete blocks in extreme erosion control projects.

VMax® C350® Permanent TRM

A 100% coconut fiber matrix supplements the C350's permanent three-dimensional netting structure with initial mulching and erosion control performance for up to 36 months. Unvegetated, the C350® TRM reduces soil loss to less than 0.5 in. (12.7 mm) under shear stress up to 3.2 lbs/ft^2 (153 Pa) and boosts permanent vegetation performance up to 12 lbs/ft^2 (576 Pa). This environmentally friendly alternative to 30 in. (76 cm) or larger rock riprap is ideal for severe erosion control projects.

VMax® SC250® Permanent TRM

The SC250® permanent TRM has a 70% straw/30% coconut fiber matrix to enhance initial mulching and erosion control performance for up to 24 months. Unvegetated, SC250 TRMs reduce soil loss to less than 0.5 in. (12.7 mm) under shear stress up to 3.0 lbs/ft^2, and increases permanent vegetation performance up to 10 lbs/ft^2 (480 Pa) for a green alternative to rock riprap.

ERONET™ PERMANENT EROSION CONTROL BLANKETS

The EroNet™ Permanent ECB provides immediate erosion protection and vegetation establishment assistance until vegetation roots and stems mature.

EroNet™ P300® Permanent Erosion Control Blankets

The P300® permanent erosion control blanket consists of UV-stabilized polypropylene fiber stitched between heavy-weight UV-stabilized polypropylene top and bottom nets. These mats reduce soil loss and protect vegetation from being washed away or uprooted, even under high stress. Unvegetated, they reduce soil loss to less than 0.5 in. (12.7 mm) under shear stress up to 3.0 lbs/ft^2 (144 Pa), and protect vegetation from being washed away or uprooted when exposed to shear stresses up to 8 lbs/ft^2 (383 Pa).

To boost performance of the VMax turf reinforcement mats in critical applications, combine with our ShoreMax® flexible transition mat to create a system that can dramatically elevate the permissible shear stress and velocity protection beyond many hard armor solutions.

VMax Mats are perfect for pipe outlets, channel bottoms, shoreline transition zones, and other areas subjected to highly turbulent water flows.

Temporary RollMax™ Solutions

Erosion control has never been so simple yet effective. Tensar's RollMax™ temporary Erosion Control Blankets (ECBs) provide immediate erosion protection and vegetation establishment assistance, then degrade once the vegetation's root and stem systems are mature enough to stabilize the soil.

Our high-quality temporary solutions are available in varying functional longevities and materials:

- Short-term photodegradable blankets with a functional longevity of 45 days up to 12 months
- Extended-term and long-term photodegradable blankets for protection up to 36 months
- Short-term biodegradable blankets for protection up to 12 months
- Extended-term and long-term biodegradable products for protection and mulching from 18 to 24 months

ERONET™ EROSION CONTROL BLANKETS

Tensar's EroNet™ ECBs incorporate photodegradable nettings, which means they are broken down by the ultraviolet rays in sunlight. These temporary products can be used in a variety of scenarios, including moderate to steep slopes, medium- to high-flow channels, shorelines and other areas needing protection until permanent vegetation establishment.

EroNet™ C125® Long-Term Photodegradable Double-Net Coconut Blanket

The C125® ECB is made of 100% coconut fiber stitched between heavyweight UV-stabilized polypropylene nets. It offers excellent durability, erosion control and longevity for severe slopes, steep embankments, high-flow channels and other areas where vegetation may take up to 36 months to grow in.

The EroNet temporary ECBs are designed to provide immediate erosion protection and vegetation establishment assistance, and then degrade after the vegetation is mature enough to permanently stabilize the underlying soil. Both short-term and extended-term ECBs are available.

EroNet™ SC150® Extended-Term Photodegradable Double-Net Straw/Coconut Blanket

With a layer of 70% straw and 30% coconut fiber stitched between a heavyweight UV-stabilized polypropylene top net and a lightweight photodegradable polypropylene bottom net, the SC150® ECB has increased durability, erosion control capabilities and longevity. It is suitable for steeper slopes, medium-flow channels and other areas where it may take vegetation up to 24 months to grow in.

EroNet™ S150® Short-Term Photodegradable Double-Net Straw Blanket

The S150 ECB is made with a 100% straw fiber matrix stitched between lightweight photodegradable polypropylene top and bottom nets. The S150 ECB's double-net construction has greater structural integrity than single net blankets for use on steeper slopes and in channels with moderate water flow. It provides erosion protection and mulching for up to 12 months.

EroNet™ DS150™ Ultra Short-Term Photodegradable Double-Net Straw Blanket

The DS150™ ECB is suitable for high maintenance areas where close mowing will occur soon after installation. Special additives in the thread and top and bottom net ensure it degrades in adequate sunlight within 60 days.

EroNet™ S75® Short-Term Photodegradable Single-Net Straw Blanket

The S75® ECB protects and mulches moderate slopes and low-flow channels in low maintenance areas for up to 12 months. It is constructed of 100% straw fiber stitched with degradable thread to a lightweight photodegradable polypropylene top net.

EroNet™ DS75™ Ultra Short-Term Photodegradable Single-Net Straw Blanket

Designed for high maintenance areas where close mowing will occur soon after installation, the DS75™ ECB degrades within 45 days because of special additives in the thread and top net that facilitate rapid breakdown in adequate sunlight.

Every site has its own unique characteristics and challenges. EroNet Erosion Control Blankets are available in varying longevities to suit a variety of scenarios and conditions.

With our Erosion Control Materials Design Software (ECMDS), you can select either short-term, extended-term or long-term EroNet blankets based on your specific design needs.

Temporary RollMax™ Solutions

BIONET® EROSION CONTROL BLANKETS

BioNet® 100% biodegradable ECBs provide effective and all-natural erosion control and vegetation establishment in an environmentally and wildlife friendly manner. All products in the line are made of organic, biodegradable materials perfect for bioengineering applications, environmentally sensitive sites, shaded areas, stream banks and shorelines. Other advantages are:

- Little to no risk of wildlife entrapment
- Easy to sprig or plant through
- High durability, fiber retention and mechanical stability with Leno weave technology
- Increased water absorption with jute netting vs. polypropylene netting
- Improved blanket conformance and adherence to soil vs. polypropylene netting
- Enhanced erosion protection and mulching capabilities vs. polypropylene netting
- Durable, flexible and 100% biodegradable
- Lightweight jute netting requires no direct sunlight exposure to initiate degradation

BioNet® C125BN™ Long-Term Biodegradable Double-Net Coconut Blanket

A dense layer of coconut fiber stitched between jute nettings allows the C125BN™ ECB to provide more effective erosion protection and mulch than open weave coir nettings. This product performs in critical applications for up to 24 months.

BioNet® SC150BN™ Extended-Term Biodegradable Double-Net Straw/Coconut Blanket

The SC150BN™ ECB features a layer of 70% straw and 30% coconut fiber stitched between biodegradable jute top and bottom nettings. It provides erosion protection and mulching for up to 18 months in applications requiring extra strength and erosion control properties.

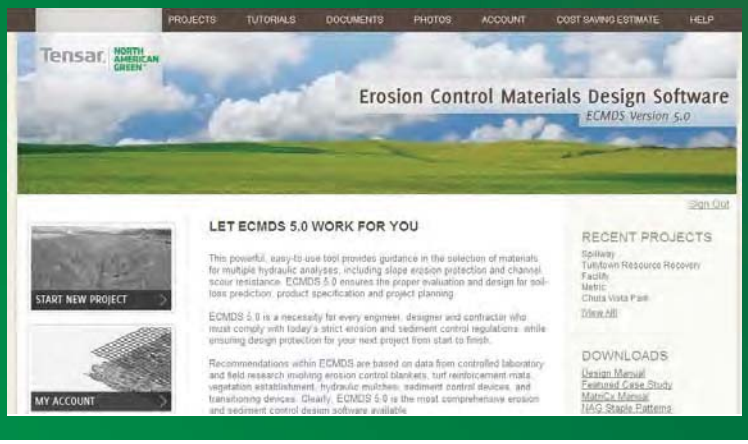
BioNet® S150BN™ Short-Term Biodegradable Double-Net Straw Blanket

The S150BN™ ECB is used for applications requiring greater durability and performance than a single-net biodegradable ECB can provide. Made with a 100% straw fiber matrix stitched between biodegradable jute top and bottom nettings, it offers up to 12 months of erosion protection and mulching action.

BioNet® S75BN™ Short-Term Biodegradable Single-Net Straw Blanket

Consisting of a 100% straw fiber matrix stitched to a biodegradable jute top nettings, the S75BN™ ECB provides better erosion protection and mulching action than conventional open weave jute nettings alone. The S75BN ECB provides up to 12 months of erosion control and vegetation growth support.

Design and Installation Tools



SHIFT, CONTROL, ENTER

Professional guidance on RECP selection, design and project planning is at your fingertips with Tensar's proprietary Erosion Control Materials Design Software (ECMDS®). This web-based program incorporates design methodologies from the Federal Highway Administration and United States Department of Agriculture to analyze your specific site conditions, and make quantified recommendations based on data from controlled laboratory and field research. ECMDS is a must-have if you face tough erosion and sediment control regulations. Best of all, it's free of charge, compliments of Tensar. To learn more and access the software directly, go to **www.ECMDS.com**.

INSTRUCTIONS INCLUDED

Proper anchoring patterns and rates must be used to achieve optimal results in RECP installation. View our installation guides for stapling patterns. Site specific staple pattern recommendations based on soil type and severity of application may be acquired through our ECMDS.

HOLD ON TIGHT

When under the pressure of severe conditions, even the best erosion control products can't function to their full potential without proper installation and anchoring. Tensar supplies a wide variety of fastener options for nearly every application and soil type.

For use in cohesive soils, wire staples are a cost-effective means to fasten RECPs. Available in 6 in., 8 in., 10 in. and 12 in. lengths, our U-shaped staples can reach to various depths to ensure adequate pull-out resistance. For installation using our handy Pin Pounder installation tool, 6 in. V-top staples or 6 in. circle top pins are available.

Our biodegradable BioStakes® are available in 4 in. and 6 in. lengths and provide an environmentally friendly alternative to metal staples. For an even more durable, deeper reaching yet all-natural anchoring option, our wood EcoStakes® are available in 6 in., 12 in., 18 in. and 24 in. lengths.

For severe applications needing the ultimate, long-lasting hold, try our 12 and 18 in. rebar staples, our 12 in. plastic ShoreMax® stakes, or our complete line of percussion earth anchors. The Tensar earth anchors reach deep into the soil strata to offer enhanced anchoring in the worst conditions. Our variety of earth anchors are designed for durability and holding power under extreme hydraulic stresses and adverse soil conditions *(Table 1)*.

For more information on the RollMax Systems or other systems within the Tensar Erosion Control Solutions, call **800-TENSAR-1** or visit **www.tensarcorp.com**.

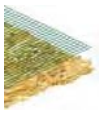
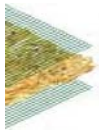
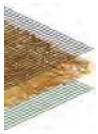
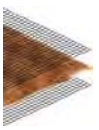
Earth Anchor Options

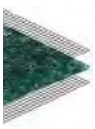
					EA 400		EA 680	
	Tendon Type (3/32 in. x 36 in.)	**Assembly Description**	**Fast Install**	**Economic Anchor**	**Stainless**	**Galvanized**	**Stainless**	**Galvanized**
End Piece Options with a PVC Face Plate	**Copper Stop Sleeve** with Stainless Steel Washer	Manually crimped to the stainless steel cable to secure the face plate.		X	X		X	
	Grip End Piece with Stainless Steel Washer	Three-dimensional, self-securing metal end piece that does not require manual crimping for tendon tensioning.	X	X	X	X	X	X
	Wedge Grip Piece	Self-securing end piece that installs flush to the face plate. Does not require manual crimping for tendon tensioning.	X		X	X	X	X
	Aluminum Stop Sleeve with Stainless Steel Washer	Manually crimped to the galvanized cable to secure the face plate.		X		X		X

TABLE 1

The complete line of RollMax™ products offers a variety of options for both short-term and permanent erosion control needs. Reference the RollMax Products Chart below to find the right solution for your next project.

RollMax Product Selection Chart

	TEMPORARY						
	ERONET						BIONET
							
	DS75	**DS150**	**S75**	**S150**	**SC150**	**C125**	**S75BN**
Longevity	45 days	60 days	12 mo.	12 mo.	24 mo.	36 mo.	12 mo.
Applications	Low Flow Channels 4:1-3:1 Slopes	Moderate Flow Channels 3:1-2:1 Slopes	Low Flow Channels 4:1-3:1 Slopes	Moderate Flow Channels 3:1-2:1 Slopes	Medium Flow Channels 2:1-1:1 Slopes	High-Flow Channels 1:1 and Greater Slopes	Low Flow Channels 4:1-3:1 Slopes
Design Permissible Shear Stress lbs/ft² (Pa)	Unvegetated 1.55 (74)	Unvegetated 1.75 (84)	Unvegetated 1.55 (74)	Unvegetated 1.75 (84)	Unvegetated 2.00 (96)	Unvegetated 2.25 (108)	Unvegetated 1.60 (76)
Design Permissible Velocity ft/s (m/s)	Unvegetated 5.00 (1.52)	Unvegetated 6.00 (1.52)	Unvegetated 5.00 (1.2)	Unvegetated 6.00 (1.83)	Unvegetated 8.00 (2.44)	Unvegetated 10.00 (3.05)	Unvegetated 5.00 (1.52)
Top Net	Lightweight accelerated photodegradable polypropylene 1.50 lbs/1000 ft² (0.73 kg/100 m²) approx wt	Lightweight accelerated photodegradable polypropylene 1.50 lbs/1000 ft² (0.73 kg/100 m²) approx wt	Lightweight photodegradable polypropylene 1.50 lbs/1000 ft² (0.73 kg/100 m²) approx wt	Lightweight photodegradable polypropylene 1.50 lbs/1000 ft² (0.73 kg/100 m²) approx wt	Heavyweight UV-stabilized polypropylene 2.9 lbs/1000 ft² (1.47 kg/100 m²) approx wt	Heavyweight UV-stabilized polypropylene 2.9 lbs/1000 ft² (1.47 kg/100 m²) approx wt	Leno woven. 100% biodegradable jute fiber 9.30 lbs/1000 ft² (4.53 kg/100 m²) approx wt
Center Net	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Fiber Matrix	Straw fiber 0.50 lbs/yd² (0.27 kg/m²)	Straw fiber 0.50 lbs/yd² (0.27 kg/m²)	Straw fiber 0.50 lbs/yd² (0.27 kg/m²)	Straw fiber 0.50 lbs/yd² (0.27 kg/m²)	Straw/coconut matrix 70% Straw 0.35 lbs/yd² (0.19 kg/m²) 30% Coconut 0.15 lbs/yd² (0.08 kg/m²)	Coconut fiber 0.50 lbs/yd² (0.27 kg/m²)	Straw fiber 0.50 lbs/yd² (0.27 kg/m²)
Bottom Net	N/A	Lightweight accelerated photodegradable polypropylene 1.50 lbs/1000 ft² (0.73 kg/100 m²) approx wt	N/A	Lightweight photodegradable polypropylene 1.50 lbs/1000 ft² (0.73 kg/100 m²) approx wt	Lightweight photodegradable polypropylene 1.50 lbs/1000 ft² (0.73 kg/100 m²) approx wt	Heavyweight UV-stabilized polypropylene 2.9 lbs/1000 ft² (1.47 kg/100 m²) approx wt	N/A
Thread	Accelerated degradable	Accelerated degradable	Degradable	Degradable	Degradable	UV-stabilized polypropylene	Biodegradable

	TEMPORARY			PERMANENT			
	BIONET			ERONET	VMAX		
							
	S150BN	**SC150BN**	**C125BN**	**P300**	**SC250**	**C350**	**P550**
Longevity	12 mo.	18 mo.	24 mo.	Permanent	Permanent	Permanent	Permanent
Applications	Moderate Flow Channels 3:1-2:1 Slopes	Medium Flow Channels 2:1-1:1 Slopes	High-Flow Channels 1:1 and Greater Slopes	High-Flow Channels 1:1 Slopes	High-Flow Channels 1:1 and Greater Slopes	High-Flow Channels 1:1 and Greater Slopes	Extreme High-Flow Channels 1:1 and Greater Slopes
Design Permissible Shear Stress lbs/ft² (Pa)	Unvegetated 1.85 (88)	Unvegetated 2.10 (100)	Unvegetated 2.35 (112)	Unvegetated 3.0 (144) Vegetated 8.0 (383)	Unvegetated 3.0 (144) Vegetated 10.0 (480)	Unvegetated 3.2 (153) Vegetated 12.0 (576)	Unvegetated 4.0 (191) Vegetated 14.0 (672)
Design Permissible Velocity ft/s (m/s)	Unvegetated 6.00 (1.83)	Unvegetated 8.00 (2.44)	Unvegetated 10.00 (3.05)	Unvegetated 9.00 (2.7) Vegetated 16.0 (4.9)	Unvegetated 9.5 (2.9) Vegetated 15.0 (4.6)	Unvegetated 10.5 (3.2) Vegetated 20.0 (6.0)	Unvegetated 12.5 (3.8) Vegetated 25.0 (7.6)
Top Net	Leno woven. 100% biodegradable jute fiber 9.30 lbs/1000 ft² (4.53 kg/100 m²) approx wt	Leno woven. 100% biodegradable jute fiber 9.30 lbs/1000 ft² (4.53 kg/100 m²) approx wt	Leno woven. 100% biodegradable jute fiber 9.30 lbs/1000 ft² (4.53 kg/100 m²) approx wt	Heavyweight UV-stabilized polypropylene 5.0 lbs/1000 ft² (2.44 kg/100 m²) approx wt	Heavyweight polypropylene 5.0 lbs/1000 ft² (2.44 kg/100 m²) approx wt	Extra heavyweight polypropylene 8.0 lbs/1000 ft² (3.91 kg/100 m²) approx wt	Ultra heavyweight polypropylene 24.0 lbs/1000 ft² (11.7 kg/100 m²) approx wt
Center Net	N/A	N/A	N/A	N/A	Ultra heavyweight polypropylene – corrugated 24.0 lbs/1000 ft² (11.7 kg/100 m²)	Ultra heavyweight polypropylene – corrugated 24.0 lbs/1000 ft² (11.7 kg/100 m²)	Ultra heavyweight polypropylene – corrugated 24.0 lbs/1000 ft² (11.7 kg/100 m²)
Fiber Matrix	Straw fiber 0.50 lbs/yd² (0.27 kg/m²)	Straw/coconut matrix 70% Straw 0.35 lbs/yd² (0.19 kg/m²) 30% Coconut 0.15 lbs/yd² (0.08 kg/m²)	Coconut fiber 0.50 lbs/yd² (0.27 kg/m²)	UV-stabilized polypropylene fiber 0.70 lbs/yd² (0.38 kg/m²)	Straw/coconut matrix 70% Straw 0.35 lbs/yd² (0.19 kg/m²) 30% Coconut 0.15 lbs/yd² (0.08 kg/m²)	Coconut fiber 0.50 lbs/yd² (0.27 kg/m²)	UV-stabilized polypropylene fiber 0.50 lbs/yd² (0.27 kg/m²)
Bottom Net	Woven. 100% biodegradable jute fiber 7.70 lbs/1000 ft² (3.76 kg/100 m²) approx wt	Woven. 100% biodegradable jute fiber 7.70 lbs/1000 ft² (3.76 kg/100 m²) approx wt	Woven. 100% biodegradable jute fiber 7.70 lbs/1000 ft² (3.76 kg/100 m²) approx wt	Heavyweight UV-stabilized polypropylene 3.0 lbs/1000 ft² (1.47 kg/100 m²) approx wt	Heavyweight UV-stabilized polypropylene 5.0 lbs/1000 ft² (2.44 kg/100 m²) approx wt	Extra heavyweight polypropylene 8.0 lbs/1000 ft² (3.91 kg/100 m²) approx wt	Ultra heavyweight polypropylene 24.0 lbs/1000 ft² (11.7 kg/100 m²) approx wt
Thread	Biodegradable	Biodegradable	Biodegradable	UV-stabilized polypropylene	UV-stabilized polypropylene	UV-stabilized polypropylene fiber	UV-stabilized polypropylene

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ROLLMAX™
ROLLED EROSION CONTROL

Specification Sheet – EroNet™ DS75™ Erosion Control Blanket

DESCRIPTION

The ultra short-term single net erosion control blanket shall be a machine-produced mat of 100% agricultural straw with a functional longevity of up to 45 days. (NOTE: functional longevity may vary depending upon climatic conditions, soil, geographical location, and elevation). The blanket shall be of consistent thickness with the straw evenly distributed over the entire area of the mat. The blanket shall be covered on the top side with a polypropylene netting having an approximate 0.50 x 0.50 (1.27 x 1.27 cm) mesh with photodegradable accelerators to provide breakdown of the netting within approximately 45 days, depending upon geographical location and elevation. The blanket shall be sewn together on 1.50 inch (3.81 cm) centers with degradable thread. The blanket shall be manufactured with a colored thread stitched along both outer edges (approximately 2-5 inches [5-12.5 cm] from the edge) as an overlap guide for adjacent mats.

The DS75 shall meet Type 1.C specification requirements established by the Erosion Control Technology Council (ECTC) and Federal Highway Administration's (FHWA) FP-03 Section 713.17

Material Content		
Matrix	100% Straw Fiber	0.5 lbs/sq yd (0.27 kg/sm)
Netting	Top side only, lightweight photodegradable with photo accelerators	1.5 lb/1000 sq ft (0.73 g/sm)
Thread	Degradable	

Standard Roll Sizes			
Width	6.67 (2.03 m)	8.0 ft (2.4 m)	16 ft (4.87 m)
Length	108 ft (32.92 m)	112 ft (34.14 m)	108 ft (32.92 m)
Weight ± 10%	40 lbs (18.14 kg)	50 lbs (22.68 kg)	96 lbs (43.54 kg)
Area	80 sq yd (66.9 sm)	100 sq yd (83.61 sm)	192 sq yd (165.5 sm)

Index Property	Test Method	Typical
Thickness	ASTM D6525	0.45 in. (11.43 mm)
Resiliency	ECTC Guidelines	78.8%
Water Absorbency	ASTM D1117	375%
Mass/Unit Area	ASTM 6475	8.57 oz/sy (291 g/sm)
Swell	ECTC Guidelines	15%
Smolder Resistance	ECTC Guidelines	Yes
Stiffness	ASTM D1388	6.31 oz-in
Light Penetration	ASTM D6567	10%
Tensile Strength - MD	ASTM D6818	105.6 lbs/ft (1.57 kN/m)
Elongation - MD	ASTM D6818	34%
Tensile Strength - TD	ASTM D6818	42.0 lbs/ft (0.62 kN/m)
Elongation - TD	ASTM D6818	25.2%
Biomass Improvement	ASTM D7322	286%

Design Permissible Shear Stress	
Unvegetated Shear Stress	1.55 psf (74 Pa)
Unvegetated Velocity	5.00 fps (1.52 m/s)

Slope Design Data: C Factors			
	Slope Gradients (S)		
Slope Length (L)	≤ 3:1	3:1 – 2.1	≥ 2:1
≤ 20 ft (6 m)	0.029	N/A	N/A
20-50 ft	0.11	N/A	N/A
≥ 50 ft (15.2 m)	0.19	N/A	N/A

Roughness Coefficients – Unveg.	
Flow Depth	Manning's n
≤ 0.50 ft (0.15 m)	0.055
0.50 – 2.0 ft	0.055-0.021
≥ 2.0 ft (0.60 m)	0.021

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ROLLMAX™
ROLLED EROSION CONTROL

Specification Sheet – EroNet™ C125® Erosion Control Blanket

DESCRIPTION

The long-term double net erosion control blanket shall be a machine-produced mat of 100% coconut fiber with a functional longevity of up to 36 months. (NOTE: functional longevity may vary depending upon climatic conditions, soil, geographical location, and elevation). The blanket shall be of consistent thickness with the coconut evenly distributed over the entire area of the mat. The blanket shall be covered on the top and bottom sides with a heavyweight photodegradable polypropylene netting having ultraviolet additives to delay breakdown and an approximate 0.63 x 0.63 in (1.59 x 1.59 cm) mesh. The blanket shall be sewn together on 1.50 inch (3.81 cm) centers with degradable thread. The blanket shall be manufactured with a colored thread stitched along both outer edges (approximately 2-5 inches [5-12.5 cm] from the edge) as an overlap guide for adjacent mats.

The C125 shall meet Type 4 specification requirements established by the Erosion Control Technology Council (ECTC) and Federal Highway Administration's (FHWA) FP-03 Section 713.17

Material Content		
Matrix	100% Coconut Fiber	0.5 lbs/sq yd (0.27 kg/sm)
Netting	Heavyweight photodegradable with UV additives	3 lbs/1000 sq ft (1.47 g/sm)
Thread	Black polypropylene	

Standard Roll Sizes		
Width	6.67 (2.03 m)	8 ft (2.44 m)
Length	108 ft (32.92 m)	112 ft (35.14 m)
Weight ± 10%	44 lbs (19.95 kg)	56.25 (25.5 kg)
Area	80 sq yd (66.9 sm)	100 sq yd (83.61 sm)

Index Property	Test Method	Typical
Thickness	ASTM D6525	0.22 in. (5.59 mm)
Resiliency	ECTC Guidelines	82%
Water Absorbency	ASTM D1117	167%
Mass/Unit Area	ASTM 6475	7.73 oz/sy (262.8 g/sm)
Swell	ECTC Guidelines	13%
Smolder Resistance	ECTC Guidelines	Yes
Stiffness	ASTM D1388	0.75 oz-in
Light Penetration	ASTM D6567	16.6%
Tensile Strength - MD	ASTM D6818	472.8 lbs/ft (7.01 kN/m)
Elongation - MD	ASTM D6818	25.6%
Tensile Strength - TD	ASTM D6818	225.6 lbs/ft (3.35 kN/m)
Elongation - TD	ASTM D6818	33.9%
Biomass Improvement	ASTM 7322	257%

Design Permissible Shear Stress	
Unvegetated Shear Stress	2.25 psf (108 Pa)
Unvegetated Velocity	10.0 fps (3.05 m/s)

Slope Design Data: C Factors			
	Slope Gradients (S)		
Slope Length (L)	≤ 3:1	3:1 – 2:1	≥ 2:1
≤ 20 ft (6 m)	0.001	0.029	0.082
20-50 ft	0.036	0.060	0.096
≥ 50 ft (15.2 m)	0.070	0.090	0.110

Roughness Coefficients – Unveg.	
Flow Depth	Manning's n
≤ 0.50 ft (0.15 m)	0.022
0.50 – 2.0 ft	0.022-0.014
≥ 2.0 ft (0.60 m)	0.014

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ROLLMAX™
ROLLED EROSION CONTROL

Specification Sheet – VMax® C350® Turf Reinforcement Mat

DESCRIPTION

The composite turf reinforcement mat (C-TRM) shall be a machine-produced mat of 100% coconut fiber matrix incorporated into permanent three-dimensional turf reinforcement matting. The matrix shall be evenly distributed across the entire width of the matting and stitch bonded between super heavy duty UV-stabilized nettings with 0.50 x 0.50 in. (1.27 x 1.27 cm) openings, an ultra heavy duty UV-stabilized, dramatically corrugated (crimped) intermediate netting with 0.5 x 0.5 in. (1.27 x 1.27 cm) openings, and covered by a super heavy duty UV-stabilized nettings with 0.50 x 0.50 in. (1.27 x 1.27 cm) openings. The middle corrugated netting shall form prominent closely spaced ridges across the entire width of the mat. The three nettings shall be stitched together on 1.50 in. (3.81 cm) centers with UV-stabilized polypropylene thread to form permanent three-dimensional turf reinforcement matting. All mats shall be manufactured with colored thread stitched along both outer edges as an overlap guide for adjacent mats.

The C350 shall meet Type 5A, B and C specification requirements established by the Erosion Control Technology Council (ECTC) and Federal Highway Administration's (FHWA) *FP-03 Section 713.18*.

Material Content		
Matrix	100% Coconut Fiber	0.5 lb/sy (0.27 kg/sm)
Netting	Top and Bottom, UV-Stabilized Polypropylene	8 lb/1000 sf (3.91 kg/100 sm)
	Middle, Corrugated UV-Stabilized Polypropylene	24 lb/1000 sf (11.7 kg/100 sm)
Thread	Polypropylene, UV Stable	

Standard Roll Sizes	
Width	6.5 ft (2.0 m)
Length	55.5 ft (16.9 m)
Weight ± 10%	37 lbs (16.8 kg)
Thread	40 sy (33.4 sm)

Index Property	Test Method	Typical
Thickness	ASTM D6525	0.73 in. (18.54 mm)
Resiliency	ASTM D6524	90%
Density	ASTM D792	0.917 g/cm^3
Mass/Unit Area	ASTM D6566	18.36 oz/sy (624 g/sm)
UV Stability	ASTM D4355/ 1000 HR	86%
Porosity	ECTC Guidelines	99%
Stiffness	ASTM D1388	0.24 in.-lb (275990 mg-cm)
Light Penetration	ASTM D6567	7.2%
Tensile Strength – MD	ASTM D6818	585.8 lbs/ft (8.70 kN/m)
Elongation – MD	ASTM D6818	45.3%
Tensile Strength – TD	ASTM D6818	687.6 lbs/ft (10.20 kN/m)
Elongation – TD	ASTM D6818	19.5%
Biomass Improvement	ASTM D7322	380%

Design Permissible Shear Stress		
	Short Duration	**Long Duration**
Phase 1 Unvegetated	3.2 psf (153 Pa)	3.0 psf (144 Pa)
Phase 2 Partially Veg.	10.0 psf (480 Pa)	10.0 psf (480 Pa)
Phase 3 Fully Veg.	12.0 psf (576 Pa)	10.0 psf (480 Pa)
Unvegetated Velocity	10.5 fps (3.2 m/s)	
Vegetated Velocity	20 fps (6.0 m/s)	

Slope Design Data: C Factors			
	Slope Gradients (S)		
Slope Length (L)	≤ 3:1	3:1 – 2:1	≥ 2:1
≤ 20 ft (6 m)	0.0005	0.015	0.043
20-50 ft	0.018	0.031	0.050
≥ 50 ft (15.2 m)	0.035	0.047	0.057

Roughness Coefficients – Unveg.	
Flow Depth	Manning's n
≤ 0.50 ft (0.15 m)	0.041
0.50 – 2.0 ft	0.040-0.013
≥ 2.0 ft (0.60 m)	0.012

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ROLLMAX™
ROLLED EROSION CONTROL

Specification Sheet – EroNet™ SC150® Erosion Control Blanket

DESCRIPTION

The extended-term double net erosion control blanket shall be a machine-produced mat of 70% agricultural straw and 30% coconut fiber with a functional longevity of up to 24 months. (NOTE: functional longevity may vary depending upon climatic conditions, soil, geographical location, and elevation). The blanket shall be of consistent thickness with the straw and coconut evenly distributed over the entire area of the mat. The blanket shall be covered on the top side with a heavyweight photodegradable polypropylene netting having ultraviolet additives to delay breakdown and an approximate 0.63 x 0.63 in (1.59 x 1.59 cm) mesh, and on the bottom side with a lightweight photodegradable polypropylene netting with an approximate 0.50 x 0.50 (1.27 x 1.27 cm) mesh. The blanket shall be sewn together on 1.50 inch (3.81 cm) centers with degradable thread. The blanket shall be manufactured with a colored thread stitched along both outer edges (approximately 2-5 inches [5-12.5 cm] from the edge) as an overlap guide for adjacent mats.

The SC150 shall meet Type 3.B specification requirements established by the Erosion Control Technology Council (ECTC) and Federal Highway Administration's (FHWA) FP-03 Section 713.17

Material Content		
Matrix	70% Straw Fiber 30% Coconut Fiber	0.35 lbs/sq yd (0.19 kg/sm) 0.15 lbs/sq yd (0.08 kg/sm)
Netting	Top: Heavyweight photodegradable with UV additives	3 lbs/1000 sq ft (1.47 kg/100 sm)
	Bottom: lighweight photodegradable	1.5 lb/1000 sq ft (0.73 kg/100 sm)
Thread	Degradable	

Standard Roll Sizes			
Width	6.67 ft (2.03 m)	8 ft (2.4 m)	16.0 ft (4.87 m)
Length	108 ft (32.92 m)	112 ft (34.14 m)	108 ft (32.92 m)
Weight ± 10%	44 lbs (19.95 kg)	55 lbs (24.95 kg)	105.6 lbs (47.9 kg)
Area	80 sq yd (66.9 sm)	100 sq yd (83.61 sm)	192 sq yd (165.6 sm)

Index Property	Test Method	Typical
Thickness	ASTM D6525	0.35 in. (8.89 mm)
Resiliency	ECTC Guidelines	75%
Water Absorbency	ASTM D1117	342%
Mass/Unit Area	ASTM D6475	7.87 oz/sy (267.6 g/sm)
Swell	ECTC Guidelines	30%
Smolder Resistance	ECTC Guidelines	Yes
Stiffness	ASTM D1388	1.11 oz-in
Light Penetration	ASTM D6567	6.2%
Tensile Strength - MD	ASTM D6818	362.4 lbs/ft (5.37 kN/m)
Elongation - MD	ASTM D6818	29.4%
Tensile Strength - TD	ASTM D6818	136.8 lbs/ft (2.03 kN/m)
Elongation - TD	ASTM D6818	27.6%
Biomass Improvement	ASTM D7322	481%

Design Permissible Shear Stress	
Unvegetated Shear Stress	2.00 psf (96 Pa)
Unvegetated Velocity	8.0 fps (2.44 m/s)

Slope Design Data: C Factors			
	Slope Gradients (S)		
Slope Length (L)	≤ 3:1	3:1 – 2:1	≥ 2:1
≤ 20 ft (6 m)	0.001	0.048	0.100
20-50 ft	0.051	0.079	0.145
≥ 50 ft (15.2 m)	0.10	0.110	0.190

NTPEP Large-Scale Slope
ASTM D6459 - C-factor = 0.031

Roughness Coefficients – Unveg.	
Flow Depth	Manning's n
≤ 0.50 ft (0.15 m)	0.050
0.50 – 2.0 ft	0.050-0.018
≥ 2.0 ft (0.60 m)	0.018

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ROLLMAX™
ROLLED EROSION CONTROL

Specification Sheet – VMax® SC250® Turf Reinforcement Mat

DESCRIPTION

The composite turf reinforcement mat (C-TRM) shall be a machine-produced mat of 70% straw and 30% coconut fiber matrix incorporated into permanent three-dimensional turf reinforcement matting. The matrix shall be evenly distributed across the entire width of the matting and stitch bonded between a heavy duty UV stabilized nettings with 0.50 x 0.50 inch (1.27 x 1.27 cm) openings, an ultra heavy UV stabilized, dramatically corrugated (crimped) intermediate netting with 0.5 x 0.5 inch (1.27 x 1.27 cm) openings, and covered by an heavy duty UV stabilized nettings with 0.50 x 0.50 inch (1.27 x 1.27 cm) openings. The middle corrugated netting shall form prominent closely spaced ridges across the entire width of the mat. The three nettings shall be stitched together on 1.50 inch (3.81cm) centers with UV stabilized polypropylene thread to form permanent three-dimensional turf reinforcement matting. All mats shall be manufactured with a colored thread stitched along both outer edges as an overlap guide for adjacent mats.

The SC250 shall meet Type 5A, 5B, and 5C specification requirements established by the Erosion Control Technology Council (ECTC) and Federal Highway Administration's (FHWA) FP-03 Section 713.18

Material Content		
Matrix	70% Straw Fiber	0.35 lb/sq yd (0.19 kg/sm)
	30% Coconut Fiber	0.15 lbs/sq yd (0.08 kg/sm)
Netting	Top and Bottom, UV-Stabilized Polypropylene	5 lb/1000 sq ft (2.44 kg/100 sm)
	Middle, Corrugated UV-Stabilized Polypropylene	24 lb/1000 sf (11.7 kg/100 sm)
Thread	Polypropylene, UV Stable	

Standard Roll Sizes	
Width	6.5 ft (2.0 m)
Length	55.5 ft (16.9 m)
Weight ± 10%	34 lbs (15.42 kg)
Area	40 sq yd (33.4 sm)

Index Property	Test Method	Typical
Thickness	ASTM D6525	0.62 in. (15.75 mm)
Resiliency	ASTM 6524	95.2%
Density	ASTM D792	0.891 g/cm^3
Mass/Unit Area	ASTM 6566	16.13 oz/sy (548 g/sm)
UV Stability	ASTM D4355/ 1000 HR	100%
Porosity	ECTC Guidelines	99%
Stiffness	ASTM D1388	222.65 oz-in.
Light Penetration	ASTM D6567	4.1%
Tensile Strength – MD	ASTM D6818	709 lbs/ft (10.51 kN/m)
Elongation – MD	ASTM D6818	23.9%
Tensile Strength – TD	ASTM D6818	712 lbs/ft (10.56 kN/m)
Elongation – TD	ASTM D6818	36.9%
Biomass Improvement	ASTM D7322	441%

Design Permissible Shear Stress		
	Short Duration	**Long Duration**
Phase 1: Unvegetated	3.0 psf (144 Pa)	2.5 psf (120 Pa)
Phase 2: Partially Veg.	8.0 psf (383 Pa)	8.0 psf (383 Pa)
Phase 3: Fully Veg.	10.0 psf (480 Pa)	8.0 psf (383 Pa)
Unvegetated Velocity	9.5 fps (2.9 m/s)	
Vegetated Velocity	15 fps (4.6 m/s)	

Slope Design Data: C Factors

	Slope Gradients (S)		
Slope Length (L)	≤ 3:1	3:1 – 2.1	≥ 2:1
≤ 20 ft (6 m)	0.0010	0.0209	0.0507
20-50 ft	0.0081	0.0266	0.0574
≥ 50 ft (15.2 m)	0.0455	0.0555	0.081

Roughness Coefficients – Unveg.

Flow Depth	Manning's n
≤ 0.50 ft (0.15 m)	0.040
0.50 – 2.0 ft	0.040-0.012
≥ 2.0 ft (0.60 m)	0.011

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ROLLMAX™
ROLLED EROSION CONTROL

Specification Sheet – VMax® P550® Turf Reinforcement Mat

DESCRIPTION

The composite turf reinforcement mat (C-TRM) shall be a machine-produced mat of 100% UV stable polypropylene fiber matrix incorporated into permanent three-dimensional turf reinforcement matting. The matrix shall be evenly distributed across the entire width of the matting and stitch bonded between a ultra heavy duty UV stabilized nettings with 0.50 x 0.50 inch (1.27 x 1.27 cm) openings, an ultra heavy UV stabilized, dramatically corrugated (crimped) intermediate netting with 0.5 x 0.5 inch (1.27 x 1.27 cm) openings, and covered by an ultra heavy duty UV stabilized nettings with 0.50 x 0.50 inch (1.27 x 1.27 cm) openings. The middle corrugated netting shall form prominent closely spaced ridges across the entire width of the mat. The three nettings shall be stitched together on 1.50 inch (3.81cm) centers with UV stabilized polypropylene thread to form permanent three-dimensional turf reinforcement matting. All mats shall be manufactured with a colored thread stitched along both outer edges as an overlap guide for adjacent mats.

The P550 shall meet Type 5A, 5B, and 5C specification requirements established by the Erosion Control Technology Council (ECTC) and Federal Highway Administration's (FHWA) FP-03 Section 713.18

Material Content		
Matrix	100% UV stable polypropylene fiber	0.5 lb/sy (0.27 kg/sm)
Netting	Top and Bottom, UV-Stabilized Polypropylene	24 lb/1000 sf (11.7 kg/100 sm)
	Middle, Corrugated UV-Stabilized Polypropylene	24 lb/1000 sf (11.7 kg/100 sm)
Thread	Polypropylene, UV Stable	

Standard Roll Sizes	
Width	6.5 ft (2.0 m)
Length	55.5 ft (16.9 m)
Weight ± 10%	52 lbs (23.59 kg)
Area	40 sy (33.4 sm)

Index Property	Test Method	Typical
Thickness	ASTM D6525	0.72 in. (18.29 mm)
Resiliency	ASTM 6524	95%
Density	ASTM D792	0.892 g/cm^3
Mass/Unit Area	ASTM 6566	21.25 oz/sy (723 g/sm)
UV Stability	ASTM D4355/ 1000 HR	100%
Porosity	ECTC Guidelines	96%
Stiffness	ASTM D1388	366.3 oz-in.
Light Penetration	ASTM D6567	16.5%
Tensile Strength – MD	ASTM D6818	1421 lbs/ft (21.07 kN/m)
Elongation – MD	ASTM D6818	40.5%
Tensile Strength – TD	ASTM D6818	1191.6 lbs/ft (17.67 kN/m)
Elongation – TD	ASTM D6818	28.8%
Biomass Improvement	ASTM D7322	378%

Design Permissible Shear Stress		
	Short Duration	**Long Duration**
Phase 1: Unvegetated	4.0 psf (191 Pa)	3.25 psf (156 Pa)
Phase 2: Partially Veg.	12.0 psf (576 Pa)	12.0 psf (576 Pa)
Phase 3: Fully Veg.	14.0 psf (672 Pa)	12.0 psf (576 Pa)
Unvegetated Velocity	12.5 fps (3.8 m/s)	
Vegetated Velocity	25 fps (7.6 m/s)	

NTPEP ASTM D6460 Large Scale Channel	
Vegetated Shear Stress	>13.2 psf (632 Pa)
Vegetated Velocity	>24.5 fps (7.47 m/s)

Slope Design Data: C Factors			
	Slope Gradients (S)		
Slope Length (L)	≤ 3:1	3:1 – 2.1	≥ 2:1
≤ 20 ft (6 m)	0.0005	0.015	0.043
20-50 ft	0.0173	0.031	0.050
≥ 50 ft (15.2 m)	0.035	0.047	0.057

Roughness Coefficients – Unveg.	
Flow Depth	Manning's n
≤ 0.50 ft (0.15 m)	0.041
0.50 – 2.0 ft	0.040-0.013
≥ 2.0 ft (0.60 m)	0.013

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Filtrexx® Runoff Diversion

Runoff & Erosion Control Technology

PURPOSE & DESCRIPTION

Filtrexx® Runoff diversion is a three-dimensional tubular runoff and erosion control device used for diversion or redirection of runoff otherwise flowing to disturbed or highly erodable areas on and around construction activities. Filtrexx® Runoff diversion can be used as temporary or permanent runoff diversion device used to prevent soil erosion during excavation, or prior to erosion control practice installation, vegetation establishment, or final stabilization.

APPLICATION

Filtrexx® Runoff diversion is generally used upslope of areas undergoing excavation. Runoff diversion is effective at diverting sheet flow runoff coming from stabilized areas and otherwise flowing to unstable or bare soils while excavation and grading is in progress. Runoff diversion should direct runoff flows to stabilized channels, heavily vegetated areas, on to flat surfaces, infiltration zones, collection ponds, or storm inlets. Runoff diversion can also be used for temporary diversion on paved surfaces to protect disturbed soils adjacent to paved areas. Where hill slopes are greater than 5%, hydraulic shear stress is greater than 3 lbs/ft2 (15 kg/m2), or runoff velocity is greater than 6 CFS (0.17 CMS) additional erosion control measures to help stabilize the area where flow is being directed and potentially concentrated or channeled should be utilized (KY TC, 2006). Filtrexx® Channel protection may be used to stabilize channels where runoff is conveyed or concentrated. Runoff diversion devices and practices should be utilized early in the soil disturbance and construction process. Appropriate applications for runoff diversion devices include (Fifield, 2001):

- diversion of runoff away from disturbed areas and to stabilized outlets or storm inlets,
- diversion of sediment-laden water to a sediment containment or storm water treatment system,
- diversion of runoff into a conveyance channel to improve site working conditions (but does not otherwise increase erosion).
- prevention of sediment-laden runoff or storm water from leaving site perimeter.

For temporary applications, Runoff diversion does not need to be seeded; however, for permanent runoff diversion the device should be direct seeded at the time of application, as vegetation will prevent UV degradation of the device. Runoff diversion may also be used in sensitive environmental areas, where migration of wildlife may be impeded by the use of fences or trenching may damage plant roots.

It is possible to drive over Runoff diversion during construction; however, these areas should be immediately repaired by manually moving back into place, if disturbed. Continued heavy construction traffic may destroy the fabric, reduce the dimensions, and reduce the effectiveness of the Filtrexx® Runoff diversion.

ADVANTAGES AND DISADVANTAGES

Advantages

- Runoff diversion can be used on hill slopes to divert storm water runoff and prevent soil erosion in unprotected or highly erodable soils.
- Tubular construction allows for heavier and denser barrier for added stability on slopes subject to storm water runoff flows.
- Greater surface area contact with soil than typical runoff control devices, reducing potential for runoff to create rills under the device.
- No trenching is required, therefore soil and plant roots are not disturbed upon installation.
- Runoff diversion can be installed year-round in difficult soil conditions such as frozen or wet ground, and dense and compacted soils,

as long as stakes can be driven.

- Runoff diversion is easily implemented as a treatment in a greater treatment train approach to any erosion and sediment control plan.
- Runoff diversion can be easily installed on top of rolled erosion control blankets, bonded fiber matrices, soil stabilizers, Slope protection, and Channel protection; or adjacent to rip rap.
- Soxx™ (mesh netting containment system) allow Runoff diversion to be placed in areas of high sheet flow and low concentrated flow, unlike conventional (lose) filter berms.
- Runoff diversion can be direct seeded at time of application to provide greater stability and anchoring once vegetation is established.
- Runoff diversion can be used as a temporary or permanent runoff and erosion control practice.
- GrowingMedia™ is organic and can be left on site after permanent stabilization is complete, used in landscape design, and/or seeded and planted with permanent vegetation.
- GrowingMedia™ improves existing soil structure if spread out and used as a soil amendment after construction activity is complete.
- Biodegradable Runoff diversion can be left on site after construction activity eliminating the need for removal and labor and disposal costs.
- Runoff diversion is less likely to obstruct wildlife movement and migration than planar/ fence runoff control devices.
- Runoff diversion is available in 8 in.(200mm), 12 in. (300mm), 18 in. (450mm), 24 in (600mm), and 32 in (800mm). diameters for customized applications and challenging situations.
- Runoff diversion is available in 200 ft. (61 m) lengths to prevent weak sections and creation of concentrated flow situations typical to low points in runs of other runoff control devices. End points are sleeved together to create continuous unlimited lengths.
- Runoff diversion may assist in qualification for LEED® Green Building Rating and Certification credits under LEED® New Construction 2.2. Awarded credits may be possible from SS Prerequisite 1, SS Credit 5.1, MR Credit 4.1, MR Credit 4.2, MR Credit 5.1, MR Credit 5.2, and MR Credit 6. *Note: LEED® is an independent program offered through the US Green Building Council. LEED® credits are determined on a per project basis by an independent auditing committee. Filtrexx® neither guarantees nor assures LEED® credits from the use of its products.*

ADVANTAGES			
	LOW	MED	HIGH
Installation Difficulty	✓		
Durability			✓
Runoff Control		✓	
Erosion Control		✓	
Sediment Control		✓	
Soluble Pollutant Control		✓	

Disadvantages

- If filler material of Runoff diversion is not GrowingMedia™, runoff diversion and/or vegetation growth may be diminished.
- If not installed correctly, maintained or used for a purpose or intention that does not meet s pecifications, performance may be diminished.
- If land surface is extremely bumpy, rocky, or changes elevation abruptly ground surface contact to Runoff diversion may be diminished, thereby adversely effecting performance.
- Runoff diversion should not be the only form of site erosion control.
- Runoff diversion should not be used for filtration of storm water runoff.
- Runoff diversion is not used for perimeter control of sediment.
- Runoff diversion should only be used on hill slopes and never in intermittent, ephemeral, or perennial streams.
- Runoff diversion which concentrate runoff flow may require additional erosion control or soil stabilization practices such as erosion control blankets, turf reinforcement mats, Filtrexx® Channel protection, or rip rap.

MATERIAL SPECIFICATIONS

Filtrexx® Runoff diversion use only photodegradable or biodegradable netting materials available from Filtrexx® International, LLC and are the only mesh materials accepted in creating Filtrexx® Runoff diver-

sion for any purpose. For Soxx™ Material Specifications see Table 6.1.

GROWINGMEDIA™ CHARACTERISTICS

Filtrexx® Runoff diversion typically use only Filtrexx® GrowingMedia™ which is a fine composted material that is specifically designed for diversion of storm water runoff,and establishment and sustainability of plant vegetation. At the discretion of the Engineer, soil or sand may be added to the GrowingMedia™ to add weight and ballast to the Runoff diversion. Performance parameters include: hydraulic flow-though rate, percent cover of vegetation, water holding capacity, pH, organic matter, soluble salts, moisture content, biological stability, percent inert material, bulk density and particle size distribution. For information onthe physical, chemical, and biological properties of Filtrexx® GrowingMedia™ refer to Filtrexx® GrowingMedia™ Specifications in Appendix 5.26.

PERFORMANCE

Testing conducted at the Soil Control Lab, Inc. under simulated runoff conditions of sediment-laden water found that hydraulic flow-through rates for GrowingMedia™ used in Runoff diversion is less than 1 gpm/linear ft (1 L/min/m). Adding soil to the GrowingMedia™ may further reduce hydraulic flow-through rates. Field testing conducted by Filtrexx® International has shown that vegetation establishment can be near 100%. Figure 6.2 depicts a vegetated Runoff diversion.

For a summary of design specifications and performance testing results see Table 6.1 and Table 6.2 Note: the Contractor is responsible for establishing a working erosion and sediment control system and may, with approval of the Engineer, work outside the minimum construction requirements as needed. Where the Filtrexx® Runoff diversion deteriorates or fails, it shall be repaired or replaced with an effective alternative.

DESIGN CRITERIA

Runoff diversion is physical barriers designed to redirect or divert sheet flow runoff away from soil surfaces that have not been stabilized or are prone to water erosion. Runoff diversion should be used to intercept and convey runoff flows to non-erodable surfaces, drainage channels, or sediment ponds. This practice will prevent runoff from entering highly erodable areas and will reduce rill and gully erosion. For stabilized channel and drainage system specifications and design see Filtrexx® Channel protection. Ultimately, runoff conveyance and drainage should lead to infiltration zones, heavily vegetated areas, or sediment/storm water treatment ponds.

To increase the weight of the Runoff diversion blending GrowingMedia™ with native soil and/or sand is acceptable. Blends should displace no more than 50% (by volume) of the GrowingMedia™ typically used within the Runoff diversion. Blends should consider the potential affects on vegetation if Runoff diversion will be seeded or used to support live stakes.

Design Height

A 4 in. (100mm) minimum vertical distance from the waterline to the top of the Runoff diversion (freeboard) is recommended. For most standard runoff diversion applications, a 18 in (450mm) diameter Runoff diversion is recommended (see Figure 6.1); however, where runoff flow may concentrate or sheet flow may be extreme a 24 in (600mm) or 32 in (800mm) diameter Runoff diversion may be used.

Three or more Runoff diversion Soxx™ may be stacked in a pyramid configuration to achieve a greater height or greater lateral stability, if desired (see Figure 6.1). Vegetation may be direct seeded at the time of installation resulting in enhanced performance and stability (see Figure 6.2 for an example). For a summary of specifications for product/practice use, performance and design see Table 6.1 and Table 6.2.

Slope Degree and Runoff Flow

Runoff diversion must be placed on slopes of at least 1% to effectively divert and convey runoff without ponding. If Runoff diversion is to be used on hill slopes greater than 5% soil stabilization or armoring practices may be necessary to prevent erosion from concentrated flows and/or conveyance channels. Concentrated runoff flows with hydraulic shear stress greater than 3 lbs/ft2 (15 kg/m2) or velocity greater than 6 ft/sec (2 m/sec) should also use stabilization or armoring devices to prevent erosion. Runoff diversion should not be used on slopes steeper than 2:1. Runoff from undisturbed lands should be directed and discharged to an outlet that has been protected by approved practices such as Channel protection, rip rap or turf reinforcement mats. Sediment-laden runoff should be directed to a designed sediment containment or treatment system. Installation and utilization of runoff diversion devices should be done early in the construction process

(Fifield, 2001). Correct installation and maintenance is especially important for proper function and performance.

Land Placement:
Runoff diversion should be placed on smooth ground and even surfaces to prevent undercutting or excessive ponding and overtopping by runoff. Placing Runoff diversion on undisturbed soil will reduce the potential for undercutting.

Directing Flow:
In order to prevent water flowing around the ends of Runoff diversion, 5 ft (1.5m) of the end at highest elevation should be constructed pointing slightly upslope and into any existing vegetation. This will ensure runoff will flow along the down gradient of Runoff diversion.
The trailing edge of the device should point down slope to direct runoff flow to appropriate outlet, containment, or treatment systems already described.

Permanent Application: (Vegetated Filter Strip)
For permanent runoff control, Runoff diversion can be direct-seeded to allow vegetation to establish directly in the device, and seeding may be expanded to 5 ft (1.5m) upslope and downslope from the device, to increase performance. Vegetation on and around the Runoff diversion will assist in slowing runoff velocity, and increase the structural stability and anchoring of the device for long term use. Additionally, runoff control by the device may increase the stability and sustainability of plant establishment and growth where runoff is prone to destabilize vegetation. The option of adding vegetation will be at the discretion of the Engineer. No additional soil amendments or fertilizer are required for vegetation establishment in the Runoff diversion. See Figure 6.2 for an example of a vegetated Runoff diversion.

24 in Runoff Diversion for High Storm Flow

INSTALLATION

1. Runoff diversion used for runoff and erosion control shall meet Filtrexx® FilterSoxx™ Material Specifications and use Filtrexx® GrowingMedia™. Soil and/or sand may be added to the Filtrexx® GrowingMedia™ at percent determined by the Engineer.
2. Contractor is required to be a Filtrexx® Certified™ Installer as determined by Filtrexx® International, LLC (440-926-2607 or visit website at Filtrexx.com). Certification shall be considered current if appropriate identification is shown during time of bid or at time of application (current list can be found at www.filtrexx.com). Look for the Filtrexx Certified™ Installer Seal.
3. Runoff diversion will be placed at locations indicated on plans as directed by the Engineer.
4. Runoff diversion shall be installed above and adjacent to areas of unprotected soil or areas prone to soil erosion.
5. Runoff diversion shall be installed where 5 ft (1.5m) of the end at highest elevation shall be constructed pointing slightly upslope and into any existing vegetation.
6. Runoff diversion shall be installed so trailing end of the device points down slope to prevent ponding of runoff.
7. Runoff diversion shall lead sheet and shallow concentrated runoff from vegetated/stabilized soil areas to stabilized channels, vegetated areas, level areas, high infiltration zones, or collection ponds.
8. Runoff diversion shall be placed on slopes 1% or greater to allow effective runoff conveyance and to prevent ponding.
9. Runoff diversion installed on slopes greater than 5% may require erosion control/soil stabilization practices where runoff flow is concentrated or conveyed.
10. Runoff diversion should not be used on slopes greater than 2:1.
11. Stakes shall be installed through the middle of the Runoff diversion on 10 ft (3m) centers, using 2 in (50mm) by 2 in (50mm) by 3 ft (1m) wooden stakes.
12. Staking depth for sand and silt loam soils shall

be 12 in (300mm), and 8 in (200mm) for clay soils.

13. If the Runoff diversion is to be a permanent runoff diversion device or part of the natural landscape, it may be seeded at time of installation for establishment of permanent vegetation. The Engineer will specify seed requirements.
14. Loose GrowingMedia™ used for backfilling and extension of filter strip may also be seeded. The Engineer will specify seed requirements.

See design drawing details for correct Filtrexx® Runoff diversion installation (Figure 6.1).

INSPECTION

Routine inspection should be conducted within 24 hrs of a runoff event or as designated by the regulating authority. Runoff diversion should be regularly inspected to make sure they maintain their shape and are adequately diverting storm runoff. If ponding becomes excessive, additional Runoff diversion may be required, sediment or debris removal may be necessary, or the device may need to be adjusted to allow gravitational flow of water down slope. A freeboard height of 4 in. (100mm) below the top edge of the device must be maintained at all times.

Runoff diversion shall be inspected until the entire area has been permanently stabilized and construction activity has ceased.

MAINTENANCE

1. The Contractor shall maintain the Runoff diversion in a functional condition at all times and it shall be routinely inspected.
2. If the Runoff diversion has been damaged, it shall be repaired, or replaced if beyond repair.
3. The Contractor shall remove sediment and debris at the base of the upslope side of the Runoff diversion when accumulation has reached 1/2 of the effective height of the Soxx™ or as directed by the Engineer.
4. A freeboard height of 4 in. (100mm) below the top edge of the device must be maintained throughout the life of the device.
5. Runoff diversion shall be maintained until the hill slope has been permanently stabilized and construction activity has ceased.
6. The GrowingMedia™ will be dispersed on site once disturbed area has been permanently stabilized, construction activity has ceased, or as determined by the Engineer.

Caption Please.

For runoff diversion and erosion control exceeding 1 year, Runoff diversion can be seeded at the time of installation to create a permanent runoff and erosion control system. Vegetation will add stability to the device and will reduce UV degradation of the system. The appropriate seed mix shall be determined by the Engineer.

DISPOSAL/RECYCLING

Filtrexx® GrowingMedia™ is an organic, composted product manufactured from locally generated organic, natural, and biologically based materials. Once all soil has been stabilized and construction activity has been completed, the GrowingMedia™ may be dispersed with a loader, rake, bulldozer or similar device and may be incorporated into the soil as an amendment or left on the soil surface to aid in permanent seeding or landscaping. Leaving the GrowingMedia™ on site reduces removal and disposal costs compared to other temporary runoff diversion devices. The mesh netting material will be extracted from the GrowingMedia™ and disposed of properly by the Contractor. The mesh netting material is photodegradable and will decompose in 2 to 5 years if left on site. Biodegradable mesh netting material is available and does not need to be extracted and disposed of, as it will completely decompose in approximately 6 months. Using biodegradable Runoff diversion completely eliminates the need and cost of removal and disposal.
As an alternative, vegetated Runoff diversion can be left on-site as permanent runoff diversion and erosion control devices used to redirect storm runoff and reduce stress from sheet flow on permanent vegetation.

METHOD OF MEASUREMENT

Bid items shall show measurement as 'X inch (X mm) diameter Filtrexx® Runoff diversion per linear ft (linear meter), installed.

Engineer shall notify Filtrexx® of location, description, and details of project prior to the bidding process so that Filtrexx® can provide design aid and technical support.

REFERENCES CITED & ADDITIONAL RESOURCES

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Caption Please.

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support tools for the erosion control industry. www.Filtrexx®library.com.

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Tyler, R.W., J. Hoeck, and J. Giles. 2004. Keys to understanding how to use compost and organic matter. IECA Annual Meeting Presentations published as IECA Digital Education Library, Copyright 2004 Blue Sky Broadcast.

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Tyler, R.W. 2007. US Patent # 7,226,240 "Devices, Systems and Methods for Controlling Erosion" Issue date 6-5-07.

US EPA NPDES Phase II. 2006. Compost Filter Socks: Construction Site Storm Water Runoff Control. National Menu of Best Management Practices for Construction Sites. http://cfpub.epa.gov/npdes/stromwater/menuofbmps/con_site.cfm

ADDITIONAL INFORMATION

For other references on this topic, including trade magazine and press coverage, visit the Filtrexx® Website at: http://www.filtrexx.com/resourcespress.htm.

For research reports not included in the Appendix, visit: http://www.filtrexx.com/resourcesreports.htm.

Filtrexx® International, LLC
Technical Support
35481 Grafton Eastern Rd
Grafton, OH 44044
440-926-2607
440-926-4021 (fax)
Website: www.filtrexx.com
Email: info@filtrexx.com

See website or call for complete list of international installers.

TABLES & FIGURES:

Table 6.1. Filtrexx Soxx™ Material Specifications

Material Type	3 mil HDPE	5 mil HDPE	5 mil HDPE	Multi-Filament Polypropylene (MFPP)	Multi-Filament Polypropylene "SafetySoxx™"
Material Characteristic	Photodegradable	Photodegradable	Biodegradable	Photodegradable	Photodegradable
Design Diameters	5 in (125mm), 8 in (200mm), 12 in (300mm), 18 in (400mm)	5 in (125mm), 8 in (200mm), 12 in (300mm), 18 in (400mm), 24 in (600mm), 32 in (800mm)	8 in (200mm), 12 in (300mm), 18 in (400mm), 24 in (600mm), 32 in (800mm)	8 in (200mm), 12 in (300mm), 18 in (400mm), 24 in (600mm), 32 in (800mm)	8 in (200mm), 12 in (300mm), 18 in (400mm), 24 in (600mm), 32 in (800mm)
Mesh Opening	3/8 in (10mm)	3/8 in (10mm)	3/8 in (10mm)	3/8 in (10mm)	1/8 in (3mm)
Tensile Strength	ND	26 psi (1.83 kg/cm2)	26 psi (1.83 kg/cm2)	44 psi (3.09 kg/cm2)	202 psi (14.2 kg/cm2)*
Ultraviolet Stability % Original Strength (ASTM G-155)	23% at 1000 hr	23% at 1000 hr	ND	100% at 1000 hr	100% at 1000 hr
Functional Longevity/ Project Duration	6 mo-2 yr	9 mo-3 yr	6-12 months	1-4 yr	2-5 yr

* Tested at Texas Transportation Institute/Texas A&M University (ASTM 5035-95).
** Functional Longevity based on continual UV exposure without vegetation.
Once vegetation is established longevity of the system is greatly increased.

Table 6.2. Filtrexx Runoff Diversion Performance and Design Specifications Summary

Design Diameter / Design & Performance	8 in (200mm)	12 in (300mm)	18 in (450mm)	24 in (600mm)	32 in (800mm)	Testing Lab/ Reference	Publication(s)
Effective Height	6.5 in (160mm)	9.5 in (240mm)	14.5 in (360mm)	19 in (480mm)	26 in (650mm)	The Ohio State University, Ohio Agricultural Research and Development Center	Transactions of the American Society of Agricultural & Biological Engineers, 2006
Effective Circumference	25 in (630mm)	38 in (960mm)	57 in (1450mm)	75 in (1900mm)	100 in (2500mm)		
Density	20 lbs/ft (30 kg/m)	48 lbs/ft (73 kg/m)	110 lbs/ft (167 kg/m)	200 lbs/ft (300 kg/m)	300 lbs/ft (450 kg/m)	Filtrexx International Field Lab	
Air Space	Testing in Progress	Testing in Progress	Testing in Progress	Testing in Progress	Testing in Progress	Soil Control Lab, Inc	
Maximum continuous length	unlimited	unlimited	unlimited	unlimited	unlimited		
Staking Requirement	10 ft (3m)	10 ft (3m)	10 ft (3m)	10 ft (3m)	10 ft (3m)		
Maintenance Requirement (sediment removal at X height)	3.25 in (80mm)	4.75 in (120mm)	7.25 in (180mm)	9.5 in (240mm)	13 in (325mm)		
Functional Longevity	2 – 5 yr	2 – 5 yr	2 – 5 yr	2 – 5 yr	2 – 5 yr	Filtrexx International Field Lab	
Percent Vegetated Cover	Testing in Progress	Testing in Progress	Testing in Progress	Testing in Progress	Testing in Progress	Filtrexx International Field Lab	
Hydraulic Flow Through Rate (sediment-laden water)	< 1 gpm /linear ft (<1 L /min/m)	< 1 gpm /linear ft (<1L/min/m)	< 1 gpm /linear ft (<1L /min/m)	< 1 gpm /linear ft (<1L /min/m)	< 1 gpm /linear ft (<1L /min/m)	Soil Control Lab, Inc	
Max Runoff Flow Height	3 in (75mm)	6 in (150mm)	11 in (275mm)	15 in (375mm)	22 in (550mm)	The Ohio State University, Ohio Agricultural Research and Development Center	Transactions of the American Society of Agricultural & Biological Engineers, 2006
Max Flow Velocity							

APPENDIX B

Preparer Qualifications

STANDARD E&S WORKSHEET # 22
PLAN PREPARER RECORD OF TRAINING AND EXPERIENCE IN EROSION AND SEDIMENT POLLUTION CONTROL METHODS AND TECHNIQUES

NAME OF PLAN PREPARER: Alaric J. Busher, PE, CPESC

FORMAL EDUCATION:

Name of College or Technical Institute: The Pennsylvania State University

Curriculum or Program: Civil Engineering

Dates of Attendance: **From:** 9/1995 **To:** 5/1999

Degree Received Bachelor of Science - Civil Engineering

OTHER TRAINING:

Name of Training:	Annual Oil and Gas Training	Chapter 102 Update Training for the Regulated Community
Presented By:	PADEP	PADEP
Date:	7/10/2013	11/12/2010

EMPLOYMENT HISTORY:

Current Employer: BL Companies

Telephone: 717-651-9850

Former Employer: N/A

Telephone:

RECENT E&S PLANS PREPARED:

Name of Project:	Constitution Pipeline, Access Roads and Meter Station (ES, PCSM)	Reynolds Alford Pipeline (E&S, PCSM)	Annville Medical Office (E&S, PCSM)
County:	Susquehanna	Susquehanna	Lebanon
Municipality:	Multiple	Brooklyn, Harford	Annville Twp
Permit Number:	ESG0011540002	ESX13-115-0152(01)	PAG-02-0038-15-010
Approving Agency:	Susquehanna CCD	PADEP (O&G)	Lebanon CCD

APPENDIX C

Site Characterization Assessment

Field Observation Report

Project Number:	14C4909		
Project Name:	Atlantic Sunrise Project – Compressor Station 605		
Date of Field Visit:	March 4, 2015; March 12, 2015; April 7, 2015		
Weather Conditions:	Overcast; Sunny; Overcast with light rain	Temperature:	Approx 35-40°F; Approx 35-40°F; Approx. 48°F
Prepared By:	Krystal Bealing, APSS and Joseph Kempf		

Copies of Report Have Been Sent To: ☒ Client ☐ Contractor ☐ Other

Client:
Transcontinental Gas Pipe Line Company, LLC
2800 Post Oak Blvd
Houston, TX 77251

Contractor:
BL Companies
4242 Carlisle Pike, Suite 260
Camp Hill, PA 17011

Twelve soil pits were excavated by backhoe and described to varying depths. Pit #4 was not dug due to its location with a graveled staging area. Additionally, infiltration tests using the double ring infiltrometer method were conducted at each pit location, at depths ranging from the surface to 42 inches.

Weather conditions at the original time of testing limited infiltration results for several pits due to frozen ground conditions. Some of these pits were revisited during April 7, 2015 to obtain infiltration testing results.

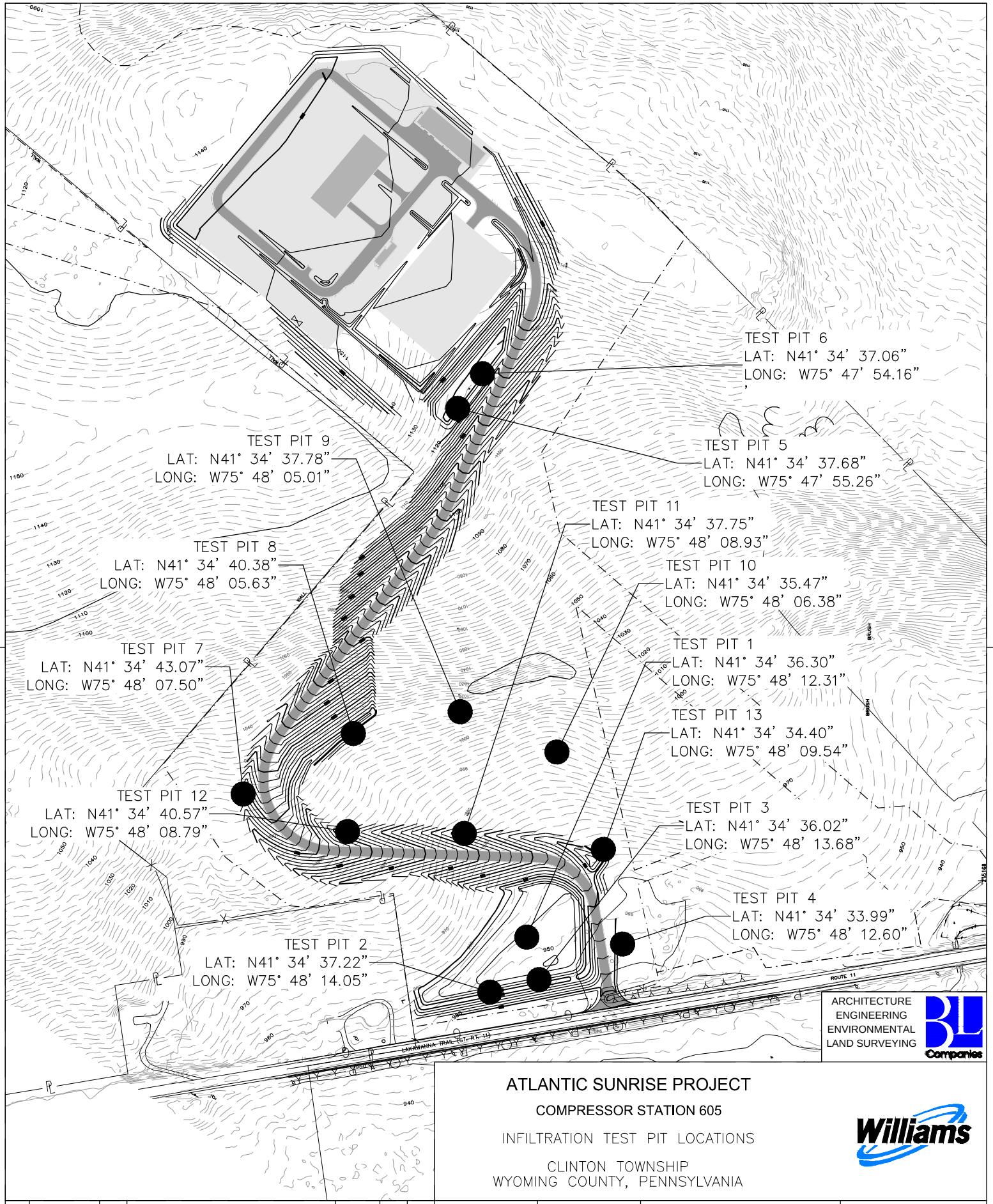
It should be noted that fill material was observed in several test pits. Conversation with the landowner and review of historical aerials suggest the fill has been there for more than five years.

The test pit location map, soil profile descriptions, infiltration worksheet and photographs are attached. Determined limiting layer depths are listed below:

Pit #1: 60 inches deep, Limiting Layer observed at 21 inches
Infiltration conducted at 42 inches, Infiltration Rate = 0.844 inches/hour
Pit #2: 48 inches deep, Limiting Layer observed at 36 inches
Infiltration conducted at 24 inches, Infiltration Rate = 1.375 inches/hour
Pit #3: 38 inches deep, No Limiting Layer observed, pit consisted entirely of fill material.
Infiltration conducted at 6 inches, Infiltration Rate = 8.625 inches/hour

Field Observation Report

Pit #4: Test pit was not dug.
Pit #5: 40 inches deep, Limiting Layer observed at 33 inches
Infiltration conducted at 12 inches, Infiltration Rate = 11.625 inches/hour
Pit #6: 45 inches deep, Limiting Layer observed at 22 inches
Infiltration conducted at 12 inches, Infiltration Rate = 4.313 inches/hour
Pit #7: 49 inches deep, Limiting Layer observed at 25 inches
Infiltration conducted at 24 inches, Infiltration Rate = 0.438 inches/hour
Pit #8: 48 inches deep, Limiting Layer observed at 13 inches
Infiltration conducted at 24 inches, Infiltration Rate = 0.063 inches/hour
Pit #9: 42 inches deep, Limiting Layer observed at 24 inches but could be shallower due to frozen ground. Pit consisted entirely of fill material.
Infiltration conducted at surface, Infiltration Rate = N/A due to failure
Pit #10: 52 inches deep, Limiting Layer observed at 22 inches
Infiltration conducted at surface, Infiltration Rate = N/A due to failure
Pit #11: 48 inches deep, Limiting Layer observed at 3 inches
Infiltration conducted at surface, Infiltration Rate = 0.531 inches/hour
Pit #12: 60 inches deep, Limiting Layer observed at 27 inches
Infiltration conducted at three inches, Infiltration Rate = 1.219 inches/hour
Pit #13: 60 inches deep, Limiting Layer observed at 10 inches
Infiltration conducted at surface, Infiltration Rate = 3.094 inches/hour



ARCHITECTURE
ENGINEERING
ENVIRONMENTAL
LAND SURVEYING

BL Companies

ATLANTIC SUNRISE PROJECT

COMPRESSOR STATION 605

INFILTRATION TEST PIT LOCATIONS

CLINTON TOWNSHIP
WYOMING COUNTY, PENNSYLVANIA

Williams

NO.	DATE	BY	REVISION DESCRIPTION	W.O. NO.	CHK.	APP.

DRAWN BY: AOE	DATE: 3/27/15	ISSUED FOR BID:	SCALE: 1"=300'
CHECKED BY: AJB	DATE: 3/27/15	ISSUED FOR CONSTRUCTION:	
APPROVED BY: AJB	DATE: 3/27/15	DRAWING NUMBER: CS 605 TEST PITS	SHEET 1 OF 1
WO:			

Soil Profile Log

Project 14C4909-A Atlantic Sunrise Project - Compressor Station 605
Test Pit # 1
Name Krystal Bealing
Date March 4, 2015
Weather 35-40°F; Overcast
Equipment Mini Excavator

Elevation 957 AMSL
Soil Type Morris channery loam, 8-18% slopes
Geology Catskill Formation
Landscape Position/Slope Hillslope bench, 2-5%
Land Use Agriculture
Additional Comments Approximately 10" snow; approximately 10" frozen soil

Horizon	Upper Boundary (inches)	Lower Boundary (inches)	Soil Textural Class	Type, Size, Coarse Fragments, etc.	Soil Matrix Color	Color Patterns	Pores, Roots, Structure	Depth to Bedrock	Depth to Water	Comments
Ap	0	11	SiL	15-35% Channery	10YR 3/3	-	Roots present; Weak, Granular	-	-	-
Bw1	11	21	SiL	15-35% Channery	10YR 4/4	-	Roots present; Weak, Granular	-	-	-
Bw2	21	36	SiL	15-35% Channery	10YR 4/3	10% 10YR 5/2 5% 7.5YR 5/8	Weak, Granular	-	-	Limiting Layer - Seasonal High Water Table
Bx	36	60+	SiL	15-35% Channery	7.5YR 4/3	20% 7.5YR 5/2 10% 10YR 5/8	Weak, Subangular Blocky	-	-	Limiting Layer - Fragipan

Note: Unless stated otherwise, horizon strike and dip was not observed to have a significant impact on water flow within the profile.

Soil Profile Log

Project	14C4909-A Atlantic Sunrise Project - Compressor Station 605	**Elevation**	954 AMSL
Test Pit #	2	**Soil Type**	Morris channery loam, 8-18% slopes
Name	Krystal Bealing	**Geology**	Catskill Formation
Date	March 4, 2015	**Landscape Position/Slope**	Hillslope bench, 2-5%
Weather	35-40°F; Overcast	**Land Use**	Agriculture
Equipment	Mini Excavator	**Additional Comments**	Approximately 10" snow; Approximately 10" frozen soil

Horizon	Upper Boundary (inches)	Lower Boundary (inches)	Soil Textural Class	Type, Size, Coarse Fragments, etc.	Soil Matrix Color	Color Patterns	Pores, Roots, Structure	Depth to Bedrock	Depth to Water	Comments
F1	0	5	SiL	-	7.5YR 2.5/1	-	Weak, Granular	-	-	Fill Material
F2	5	16	SiL	60-90% Gravelly	10YR 2/2	-	None	-	-	Fill Material
Ab	16	24	SiL	-	10YR 3/3		Weak, Granular	-	-	-
Bw	36	48+	SiL	15-35% Channery	10YR 5/2	10% 7.5YR 5/8	Weak, Subangular Blocky	-	-	Limiting Layer - Seasonal High Water Table

Note: Unless stated otherwise, horizon strike and dip was not observed to have a significant impact on water flow within the profile.

Soil Profile Log

Project	14C4909-A Atlantic Sunrise Project - Compressor Station 605	**Elevation**	951 AMSL
Test Pit #	3	**Soil Type**	Morris channery loam, 8-18% slopes
Name	Krystal Bealing	**Geology**	Catskill Formation
Date	March 4, 2015	**Landscape Position/Slope**	Hillslope bench, 2-5%
Weather	35-40°F; Overcast	**Land Use**	Agriculture
Equipment	Mini Excavator	**Additional Comments**	Approximately 10" snow; approximately 10" frozen soil

Horizon	Upper Boundary (inches)	Lower Boundary (inches)	Soil Textural Class	Type, Size, Coarse Fragments, etc.	Soil Matrix Color	Color Patterns	Pores, Roots, Structure	Depth to Bedrock	Depth to Water	Comments
F1	0	18	SiL	60-90% Channery	10YR 3/3	-	-	-	-	Fill Material
F2	18	32	*	*	-	-	-	-	-	Fill Material *Consisted of flags and cobbles
F3	32	38+	SiL	60-90% Channery	10YR 3/3	-	-	-	-	Fill Material

Note: Unless stated otherwise, horizon strike and dip was not observed to have a significant impact on water flow within the profile.

Soil Profile Log

Project	14C4909-A Atlantic Sunrise Project - Compressor Station 605	**Elevation**	1128 AMSL
Test Pit #	5	**Soil Type**	Wellsboro channery loam, 15-25% slopes
Name	Krystal Bealing	**Geology**	Catskill Formation
Date	March 4, 2015	**Landscape Position/Slope**	Shoulder 10-15%
Weather	35-40°F; Overcast	**Land Use**	Agriculture
Equipment	Mini Excavator	**Additional Comments**	Approximately 10" snow; approximately 10" frozen soil

Horizon	Upper Boundary (inches)	Lower Boundary (inches)	Soil Textural Class	Type, Size, Coarse Fragments, etc.	Soil Matrix Color	Color Patterns	Pores, Roots, Structure	Depth to Bedrock	Depth to Water	Comments
Ap	0	14	SiL	-	10YR 3/3	-	Roots present; Weak, Granular	-	-	-
Bw1	14	22	SiL	-	7.5YR 4/4	-	Roots present; Weak, Subangular Blocky	-	-	-
Bw2	22	33	SiL	-	7.5YR 5/3	-	Weak, Subangular Blocky	-	-	-
Bx	33	40+	SiL	-	7.5YR 5/2	25% 7.5YR 5/6	Moderate, Subangular Blocky	-	-	Limiting Layer - Seasonal High Water Table

Note: Unless stated otherwise, horizon strike and dip was not observed to have a significant impact on water flow within the profile.

Soil Profile Log

Project	14C4909-A Atlantic Sunrise Project - Compressor Station 605	**Elevation**	1127 AMSL
Test Pit #	6	**Soil Type**	Morris channery loam, 8-18% slopes
Name	Krystal Bealing	**Geology**	Catskill Formation
Date	March 4, 2015	**Landscape Position/Slope**	Shoulder 10-15%
Weather	35-40°F; Overcast	**Land Use**	Agriculture
Equipment	Mini Excavator	**Additional Comments**	Approximately 10" snow; approximately 10" frozen soil

Horizon	Upper Boundary (inches)	Lower Boundary (inches)	Soil Textural Class	Type, Size, Coarse Fragments, etc.	Soil Matrix Color	Color Patterns	Pores, Roots, Structure	Depth to Bedrock	Depth to Water	Comments
Ap	0	15	SiL	-	10YR 3/3	-	Roots present; Weak, Granular	-	-	-
Bw1	15	22	SiL	-	10YR 4/4	-	Roots present; Weak, Subangular Blocky	-	-	-
Bw2	22	30	SiL	-	5YR 3/3	20% 10YR 5/2 10% 7.5YR 5/8	Weak, Subangular Blocky	-	-	Limiting Layer - Seasonal High Water Table
Bx	30	45+	SiL	15-35% Channery	5YR 4/3	10% 10YR 5/2 5% 7.5YR 5/8	Moderate, Subangular Blocky	-	-	-

Note: Unless stated otherwise, horizon strike and dip was not observed to have a significant impact on water flow within the profile.

Soil Profile Log

Project	14C4909-A Atlantic Sunrise Project - Compressor Station 605	**Elevation**	1023 AMSL
Test Pit #	7	**Soil Type**	Morris channery loam, 8-18% slopes
Name	Krystal Bealing	**Geology**	Catskill Formation
Date	March 12, 2015	**Landscape Position/Slope**	Hillslope, 5-8%
Weather	35-40°F; Sunny	**Land Use**	Agriculture
Equipment	Mini Excavator	**Additional Comments**	Approximately 2" snow; approximately 7" frozen soil

Horizon	Upper Boundary (inches)	Lower Boundary (inches)	Soil Textural Class	Type, Size, Coarse Fragments, etc.	Soil Matrix Color	Color Patterns	Pores, Roots, Structure	Depth to Bedrock	Depth to Water	Comments
Ap	0	3	SiL	15-35% Channery	10YR 3/2	-	Roots present; Weak, Granular	-	-	-
Bw1	3	25	SiL	35-60% Channery	7.5YR 4/3	-	Roots present; Weak, Subangular Blocky	-	-	-
Bw2	25	31	SiL	15-35% Channery	10YR 5/3	10% 7.5YR 4/6	Weak, Subangular Blocky	-	-	Limiting Layer - Seasonal High Water Table
Bx	31	49+	L	15-35% Channery	5YR 3/3	15% 10YR 6/2 5% 7.5YR 5/8	Moderate, Subangular Blocky	-	-	-

Note: Unless stated otherwise, horizon strike and dip was not observed to have a significant impact on water flow within the profile.

Soil Profile Log

Project	14C4909-A Atlantic Sunrise Project - Compressor Station 605	**Elevation**	1025 AMSL
Test Pit #	8	**Soil Type**	Morris channery loam, 15-25% slopes
Name	Krystal Bealing	**Geology**	Catskill Formation
Date	March 12, 2015	**Landscape Position/Slope**	Hillslope, 5-8%
Weather	35-40°F; Sunny	**Land Use**	Agriculture
Equipment	Mini Excavator	**Additional Comments**	Approximately 12" frozen soil

Horizon	Upper Boundary (inches)	Lower Boundary (inches)	Soil Textural Class	Type, Size, Coarse Fragments, etc.	Soil Matrix Color	Color Patterns	Pores, Roots, Structure	Depth to Bedrock	Depth to Water	Comments
F	0	13	SiL	35-60% Channery	7.5YR 3/2	-	Weak, Granular	-	-	Fill Material
Ab	13	25	SiL	15-35% Channery	10YR 3/3	5% 7.5YR 4/6	Weak,Granular	-	-	Limiting Layer - Seasonal High Water Table
Bw1	25	32	SiL	15-35% Channery	7.5YR 4/3	15% 7.5YR 4/6	Weak, Subangular Blocky	-	-	-
Bw2	32	48+	SiL	15-35% Channery	10YR 4/3	15% 7.5YR 4/6	Weak, Subangular Blocky	-	-	-

Note: Unless stated otherwise, horizon strike and dip was not observed to have a significant impact on water flow within the profile.

Soil Profile Log

Project	14C4909-A Atlantic Sunrise Project - Compressor Station 605	**Elevation**	1020 AMSL
Test Pit #	9	**Soil Type**	Wellsboro channery loam, 15-25% slopes
Name	Krystal Bealing	**Geology**	Catskill Formation
Date	March 12, 2015	**Landscape Position/Slope**	Hillslope, 5-8%
Weather	35-40°F; Sunny	**Land Use**	Agriculture
Equipment	Mini Excavator	**Additional Comments**	Approximately 2" snow; approximately 24" frozen soil

Horizon	Upper Boundary (inches)	Lower Boundary (inches)	Soil Textural Class	Type, Size, Coarse Fragments, etc.	Soil Matrix Color	Color Patterns	Pores, Roots, Structure	Depth to Bedrock	Depth to Water	Comments
F	0	42+	SiL	35-60% Channery	7.5YR 3/2	-	*	-	24*	Fill Material *Frozen to 24 inches; depth to water is potentially shallower

Note: Unless stated otherwise, horizon strike and dip was not observed to have a significant impact on water flow within the profile.

Soil Profile Log

Project 14C4909-A Atlantic Sunrise Project - Compressor Station 605
Test Pit # 10
Name Krystal Bealing
Date March 12, 2015
Weather 35-40°F; Sunny
Equipment Mini Excavator

Elevation 993 AMSL
Soil Type Wellsboro channery loam, 15-25% slopes
Geology Catskill Formation
Landscape Position/Slope Hillslope, 5-8%
Land Use Agriculture
Additional Comments Approximately 9" frozen soil; snow melt infiltration from surface observed

Horizon	Upper Boundary (inches)	Lower Boundary (inches)	Soil Textural Class	Type, Size, Coarse Fragments, etc.	Soil Matrix Color	Color Patterns	Pores, Roots, Structure	Depth to Bedrock	Depth to Water	Comments
Ap	0	22	SiL	15-35% Channery	10YR 3/3	-	Roots present; Weak, Granular	-	9*	*Frozen to 9 inches; depth to water is potentially shallower; however seeps assumed to be due to snow melt
Bw	22	32	SiL	15-35% Channery	10YR 4/3	10% 7.5YR 4/6	Weak, Granular	-	-	Seeps observed; Limiting Layer - Seasonal High Water Table
BE	32	52+	L	15-35% Channery	2.5Y 5/1	40% 10YR 5/8	Strong, Subangular Blocky	-	-	Seeps observed; Limiting Layer - Seasonal High Water Table

Note: Unless stated otherwise, horizon strike and dip was not observed to have a significant impact on water flow within the profile.

Soil Profile Log

Project	14C4909-A Atlantic Sunrise Project - Compressor Station 605	**Elevation**	984 AMSL
Test Pit #	11	**Soil Type**	Morris channery loam, 8-18% slopes
Name	Krystal Bealing	**Geology**	Catskill Formation
Date	March 12, 2015	**Landscape Position/Slope**	Hillslope bench, 2-5%
Weather	35-40°F; Sunny	**Land Use**	Agriculture
Equipment	Mini Excavator	**Additional Comments**	Approximately 9" frozen soil

Horizon	Upper Boundary (inches)	Lower Boundary (inches)	Soil Textural Class	Type, Size, Coarse Fragments, etc.	Soil Matrix Color	Color Patterns	Pores, Roots, Structure	Depth to Bedrock	Depth to Water	Comments
Ap	0	3	SiL	-	10YR 3/3	-	*	-	-	*Frozen to 9 inches
Bw1	3	20	SiL	15-35% Channery	10YR 6/2	30% 7.5YR 5/6	Weak, Subangular Blocky	-	-	Limiting Layer - Seasonal High Water Table
Bw2	20	27	SiL	15-35% Channery	10YR 5/2	30% 7.5YR 4/6	Moderate, Subangular Blocky	-	-	Limiting Layer - Seasonal High Water Table
BE	27	48+	L	-	10YR 6/2	40% 7.5YR 5/8	Moderate, Subangular Blocky	-	-	Limiting Layer - Seasonal High Water Table

Note: Unless stated otherwise, horizon strike and dip was not observed to have a significant impact on water flow within the profile.

Soil Profile Log

Project	14C4909-A Atlantic Sunrise Project - Compressor Station 605	**Elevation**	1006 AMSL
Test Pit #	12	**Soil Type**	Morris channery loam, 8-18% slopes
Name	Joseph Kempf	**Geology**	Catskill Formation
Date	April 7, 2015	**Landscape Position/Slope**	Hillslope, 5-8%
Weather	48°F; Overcast with light rain	**Land Use**	Agriculture
Equipment	Mini Excavator	**Additional Comments**	

Horizon	Upper Boundary (inches)	Lower Boundary (inches)	Soil Textural Class	Type, Size, Coarse Fragments, etc.	Soil Matrix Color	Color Patterns	Pores, Roots, Structure	Depth to Bedrock	Depth to Water	Comments
Ap	0	8	SiL	15-35% Channery	10YR 4/2	-	Roots present; Weak, Granular	-	-	-
Bw1	8	30	SiL	15-35% Channery	7.5YR 5/3	-	Weak, Subangular Blocky	-	27	Seeps observed Limiting Layer - Seasonal High Water Table
Bw2	30	38	SiL	35-60% Channery	7.5YR 5/3	5% 10YR 5/6	Moderate, Subangular Blocky	-	-	Limiting Layer - Seasonal High Water Table
BE	38	60+	L	15-35% Channery	5YR 4/3	10% 10YR 6/2 10% 10YR 5/6	Weak, Subangular Blocky	-	-	Limiting Layer - Seasonal High Water Table

Note: Unless stated otherwise, horizon strike and dip was not observed to have a significant impact on water flow within the profile.

Soil Profile Log

Project	14C4909-A Atlantic Sunrise Project - Compressor Station 605	**Elevation**	962 AMSL
Test Pit #	13	**Soil Type**	Morris channery loam, 8-18% slopes
Name	Joseph Kempf	**Geology**	Catskill Formation
Date	April 7, 2015	**Landscape Position/Slope**	Hillslope bench, 2-5%
Weather	48°F; Overcast with light rain	**Land Use**	Agriculture
Equipment	Mini Excavator	**Additional Comments**	

Horizon	Upper Boundary (inches)	Lower Boundary (inches)	Soil Textural Class	Type, Size, Coarse Fragments, etc.	Soil Matrix Color	Color Patterns	Pores, Roots, Structure	Depth to Bedrock	Depth to Water	Comments
Ap	0	10	SiL	15-35% Channery	10YR 3/3	-	Roots present; Weak, Granular	-	-	-
Bw1	10	22	SiL	15-35% Channery	7.5YR 3/2	5% 10YR 6/1 20% 10YR 5/6	Moderate, Subangular Blocky	-	14	Seeps observed; Limiting Layer - Seasonal High Water Table
Bw2	22	48	SiL	35-60% Channery	7.5YR 5/3	5% 10YR 6/2 5% 10YR 5/6	Moderate, Subangular Blocky	-	-	Limiting Layer - Seasonal High Water Table
Bgx	48	54	CL	-	5G 5/1	-	Moderate, Subangular Blocky	-	-	Limiting Layer - Seasonal High Water Table
Bw3	54	60+	SL	15-35% Channery	10YR 5/1	5% 5G 5/1	Weak, Granular	-	-	Limiting Layer - Seasonal High Water Table

Note: Unless stated otherwise, horizon strike and dip was not observed to have a significant impact on water flow within the profile.

ATLANTIC SUNRISE PROJECT - COMPRESSOR STATION 605													
SOIL INFILTRATION WORKSHEET - DOUBLE RING INFILTROMETER METHOD													
Hole Number	Drop >2 inches after 30 minute presoak?[1]	Reading Interval (minutes)	Reading 1 (Inches of Drop)	Reading 2 (Inches of Drop)	Reading 3 (Inches of Drop)	Reading 4 (Inches of Drop)	Reading 5 (Inches of Drop)	Reading 6 (Inches of Drop)	Reading 7 (Inches of Drop)	Reading 8 (Inches of Drop)	Average Stabilized Reading[2] (Inches of Drop)	Infiltration Rate[3] (in/hr)	Comments
1	No	30	0.625	0.375	0.313	0.500	0.500				0.422	0.844	35-40 degrees, overcast. Test done at 42" below surface. Ground was frozen to approx. 18" below surface.
2	No	30	1.375	0.750	0.750	0.625	0.625				0.688	1.375	35-40 degrees, overcast. Test done at 24" below surface. Ground was frozen to approx. 18" below surface.
3	Yes	10	2.438	2.313	1.500	1.500	1.375	1.375			1.438	8.625	Approximately 48 degrees, overcast with a slight drizzle. Test done at 6" below surface.
4	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	Testing not completed due to location of pit within a graveled staging area.
5	Yes	10	3.250	2.000	1.875	1.875	2.000				1.938	11.625	35-40 degrees, overcast. Test done at 12" below surface. Ground was frozen to approx. 8" below surface.
6	Yes	10	0.750	0.625	0.750	0.750					0.719	4.313	35-40 degrees, overcast. Test done at 12" below surface. Ground was frozen to approx. 10" below surface.
7	No	30	0.188	0.250	0.250	0.188					0.219	0.438	Approximately 35-40 degrees, sunny. Test done at 24" below surface. Ground was frozen to approx. 7" below surface.

ATLANTIC SUNRISE PROJECT - COMPRESSOR STATION 605													
SOIL INFILTRATION WORKSHEET - DOUBLE RING INFILTROMETER METHOD													
Hole Number	Drop >2 inches after 30 minute presoak?[1]	Reading Interval (minutes)	Reading 1 (Inches of Drop)	Reading 2 (Inches of Drop)	Reading 3 (Inches of Drop)	Reading 4 (Inches of Drop)	Reading 5 (Inches of Drop)	Reading 6 (Inches of Drop)	Reading 7 (Inches of Drop)	Reading 8 (Inches of Drop)	Average Stabilized Reading[2] (Inches of Drop)	Infiltration Rate[3] (in/hr)	Comments
8	No	30	0.063	0.063	0.000	0.000					0.031	0.063	Approximately 35-40 degrees, sunny. Test done at 13" below surface. Ground was frozen to approx. 12" below surface.
9	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	Approximately 35-40 degrees, sunny. Test done at surface. Soil Frozen to 24'', infiltrometer was unable to penetrate soil.
10	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	Approximately 35-40 degrees, sunny. Test done at surface. Soil Frozen to 9'', infiltrometer was unable to penetrate soil.
11	30	0.438	0.688	0.250	0.313	0.250	0.250				0.266	0.531	Approximately 48 degrees, overcast with a slight drizzle. Test done at surface.
12	30	0.500	0.750	0.688	0.500						0.609	1.219	Approximately 48 degrees, overcast with a slight drizzle. Test done at 3" below surface..
13	30	1.313	1.500	1.688	1.500	1.500					1.547	3.094	Approximately 48 degrees, overcast with a slight drizzle. Test done at surface.

ATLANTIC SUNRISE PROJECT - COMPRESSOR STATION 605													
SOIL INFILTRATION WORKSHEET - DOUBLE RING INFILTROMETER METHOD													
Hole Number	Drop >2 inches after 30 minute presoak?[1]	Reading Interval (minutes)	Reading 1 (Inches of Drop)	Reading 2 (Inches of Drop)	Reading 3 (Inches of Drop)	Reading 4 (Inches of Drop)	Reading 5 (Inches of Drop)	Reading 6 (Inches of Drop)	Reading 7 (Inches of Drop)	Reading 8 (Inches of Drop)	Average Stabilized Reading[2] (Inches of Drop)	Infiltration Rate[3] (in/hr)	Comments
[1]Inches of drop greater than 2 inches after the 30 minute presoak? Yes, use 10 minute interval; No, use 30 minute interval.													
[2]Calculated as the average of the last four stabilized (less than 0.25-inch difference overall) readings.													
[3]Calculated as the average stabilized reading x 2 for 30 minute intervals; x 6 for 10 minute intervals.													

View of Pit #1.

View of Pit #2.

View of Pit #3.

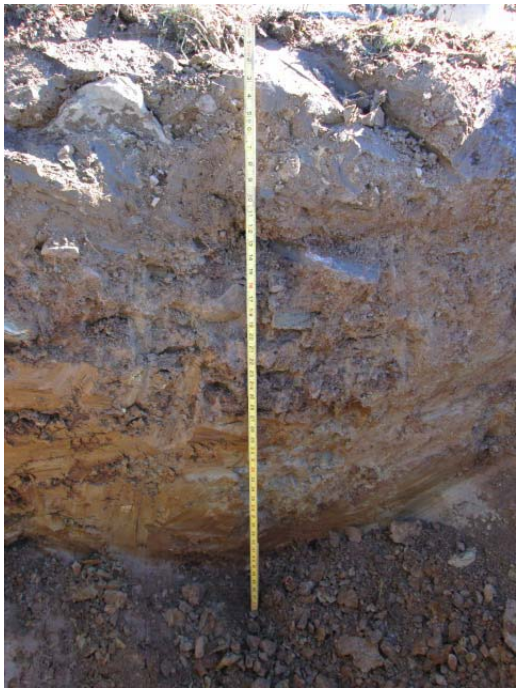
View of Pit #5.

View of Pit #6.

View of Pit #7.

View of Pit #9.

View of Pit #10.



View of Pit #11.

View of Pit #12.

View of Pit #13.

Architecture
Engineering
Environmental
Land Surveying
Companies

An Employee-Owned Company

APPENDIX D

United States Department of Agriculture (USDA)
Natural Resources Conservation Service (NRCS)
Custom Soil Resource Report

United States Department of Agriculture

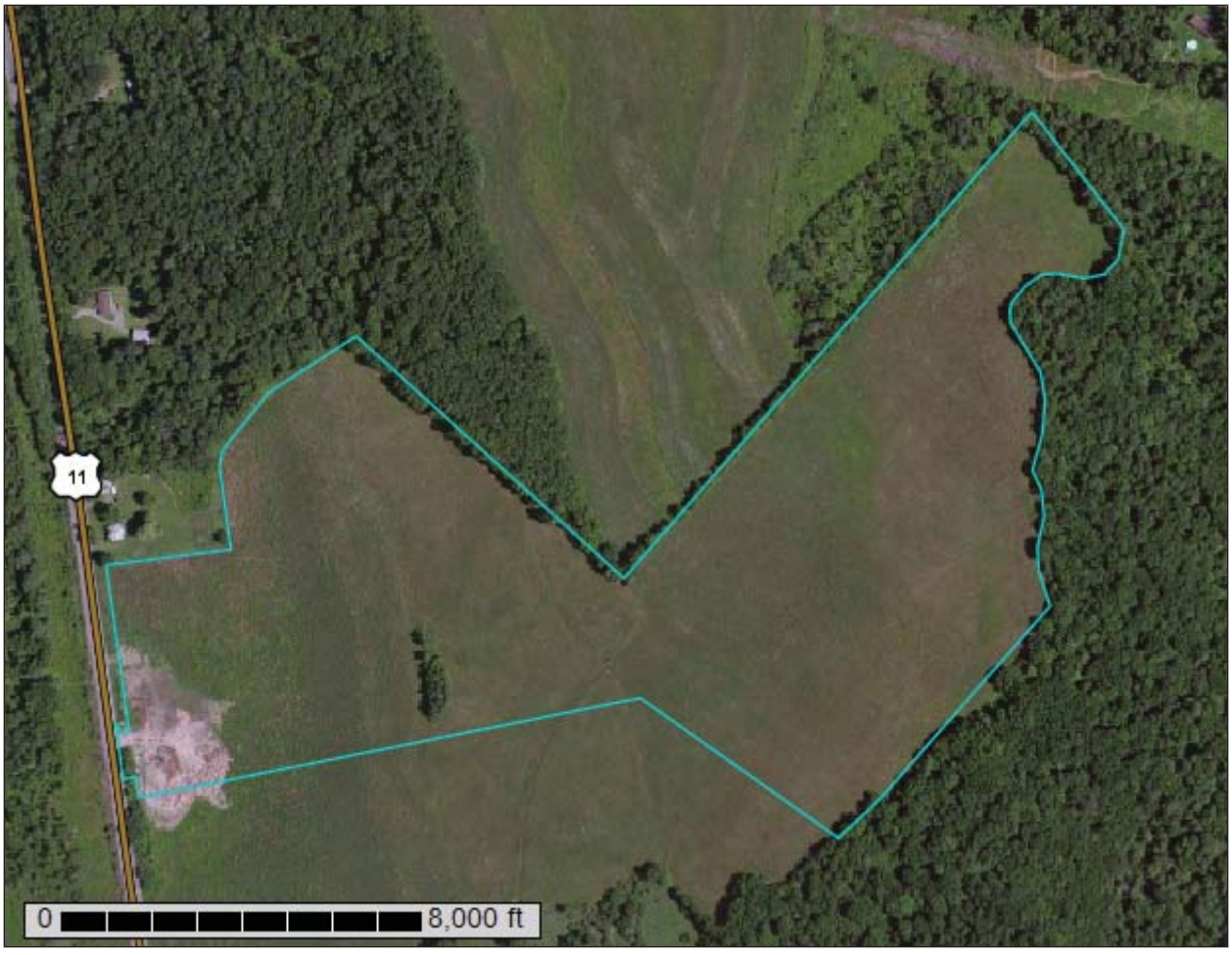
NRCS

Natural Resources Conservation Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Wyoming County, Pennsylvania

Compressor Station 605



July 6, 2015

Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (http://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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Contents

How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil scientists classified and named the soils in the survey area, they compared the

individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

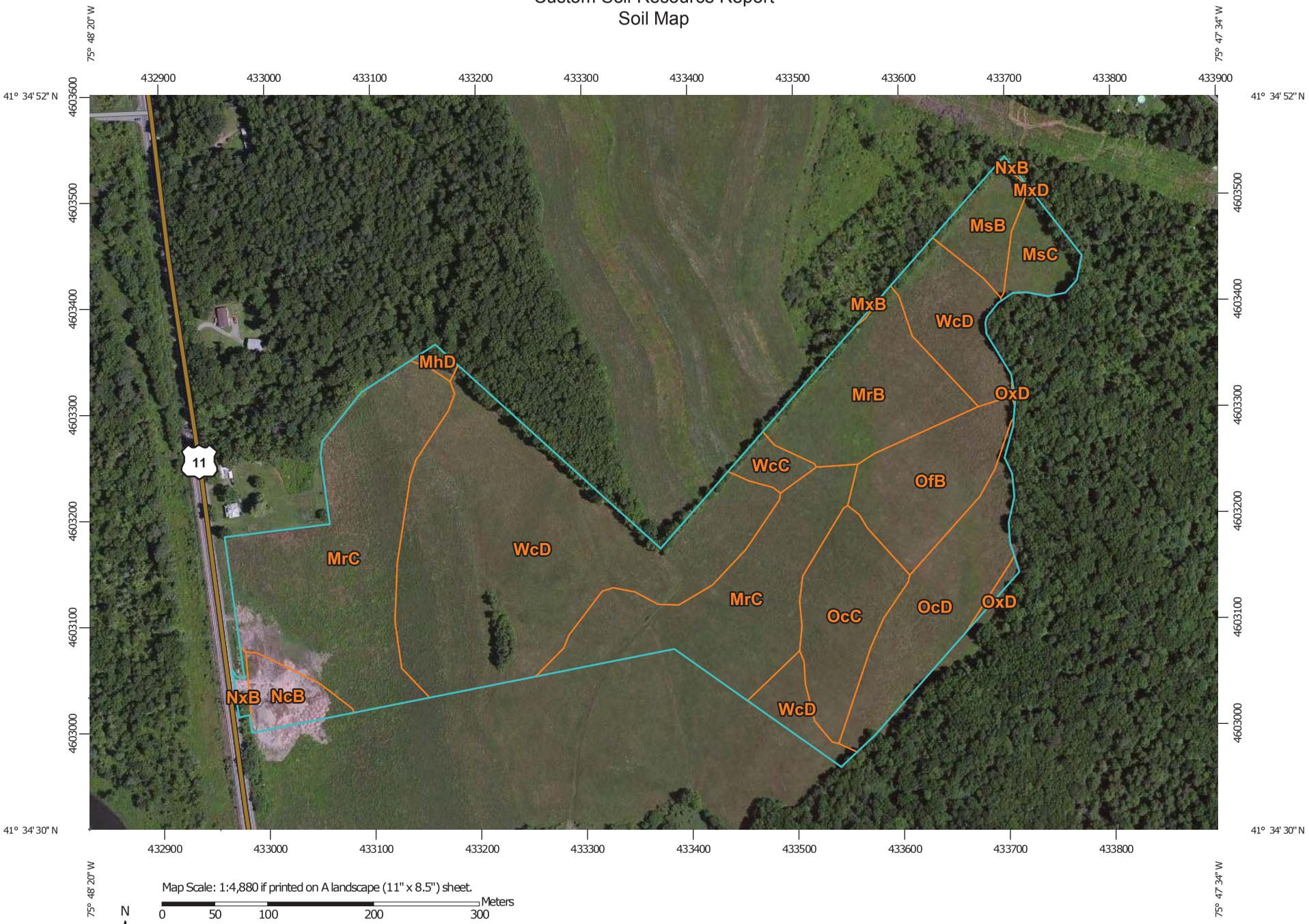
Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

Custom Soil Resource Report
Soil Map



Map Scale: 1:4,880 if printed on A landscape (11" x 8.5") sheet.

N

Meters: 0 50 100 200 300

Feet: 0 200 400 800 1200

Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 18N WGS84

MAP LEGEND

Area of Interest (AOI)
- Area of Interest (AOI)

Soils
- Soil Map Unit Polygons
- Soil Map Unit Lines
- Soil Map Unit Points

Special Point Features
- Blowout
- Borrow Pit
- Clay Spot
- Closed Depression
- Gravel Pit
- Gravelly Spot
- Landfill
- Lava Flow
- Marsh or swamp
- Mine or Quarry
- Miscellaneous Water
- Perennial Water
- Rock Outcrop
- Saline Spot
- Sandy Spot
- Severely Eroded Spot
- Sinkhole
- Slide or Slip
- Sodic Spot
- Spoil Area
- Stony Spot
- Very Stony Spot
- Wet Spot
- Other
- Special Line Features

Water Features
- Streams and Canals

Transportation
- Rails
- Interstate Highways
- US Routes
- Major Roads
- Local Roads

Background
- Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:20,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL: http://websoilsurvey.nrcs.usda.gov
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Wyoming County, Pennsylvania
Survey Area Data: Version 7, Sep 22, 2014

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Mar 20, 2011—Jul 5, 2011

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Wyoming County, Pennsylvania (PA131)			
Map Unit Symbol	**Map Unit Name**	**Acres in AOI**	**Percent of AOI**
MhD	Mardin channery silt loam, 8 to 25 percent slopes, rubbly	0.2	0.3%
MrB	Morris channery loam, 3 to 8 percent slopes	4.1	8.2%
MrC	Morris channery loam, 8 to 18 percent slopes	14.6	28.8%
MsB	Morris flaggy loam, 3 to 8 percent slopes	1.4	2.7%
MsC	Morris flaggy loam, 8 to 15 percent slopes	1.2	2.3%
MxB	Morris extremely stony loam, 0 to 8 percent slopes	0.0	0.0%
MxD	Morris extremely stony loam, 8 to 25 percent slopes	0.0	0.0%
NcB	Norwich and Chippewa channery silt loams, 3 to 8 percent slopes	1.1	2.1%
NxB	Norwich and Chippewa channery silt loams, 0 to 8 percent slopes, rubbly	0.2	0.3%
OcC	Oquaga channery loam, 8 to 15 percent slopes	3.2	6.3%
OcD	Oquaga channery loam, 15 to 25 percent slopes	4.0	7.9%
OfB	Oquaga flaggy loam, 3 to 8 percent slopes	3.4	6.7%
OxD	Oquaga extremely stony loam, 8 to 25 percent slopes	0.1	0.3%
WcC	Wellsboro channery loam, 8 to 15 percent slopes	0.6	1.1%
WcD	Wellsboro channery loam, 15 to 25 percent slopes	16.7	32.9%
Totals for Area of Interest		**50.7**	**100.0%**

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic

class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical

or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Wyoming County, Pennsylvania

MhD—Mardin channery silt loam, 8 to 25 percent slopes, rubbly

Map Unit Setting

National map unit symbol: 2v307
Elevation: 330 to 2,460 feet
Mean annual precipitation: 31 to 70 inches
Mean annual air temperature: 39 to 52 degrees F
Frost-free period: 105 to 180 days
Farmland classification: Not prime farmland

Map Unit Composition

Mardin, rubbly, and similar soils: 85 percent
Minor components: 15 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Mardin, Rubbly

Setting

Landform: Till plains
Landform position (two-dimensional): Backslope, shoulder
Landform position (three-dimensional): Interfluve, side slope, head slope
Down-slope shape: Linear, concave
Across-slope shape: Linear
Parent material: Loamy till

Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material
A - 1 to 3 inches: channery silt loam
BE - 3 to 12 inches: channery silt loam
Bw1 - 12 to 16 inches: channery silt loam
Bw2 - 16 to 20 inches: channery silt loam
Bx1 - 20 to 36 inches: channery silt loam
Bx2 - 36 to 57 inches: channery silt loam
C - 57 to 72 inches: channery silt loam

Properties and qualities

Slope: 8 to 25 percent
Percent of area covered with surface fragments: 20.0 percent
Depth to restrictive feature: 14 to 26 inches to fragipan
Natural drainage class: Moderately well drained
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.14 in/hr)
Depth to water table: About 13 to 24 inches
Frequency of flooding: None
Frequency of ponding: None
Available water storage in profile: Low (about 3.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7s
Hydrologic Soil Group: D

Minor Components

Lordstown, very stony
Percent of map unit: 5 percent
Landform: Ridges
Landform position (two-dimensional): Summit, shoulder
Landform position (three-dimensional): Base slope, side slope
Down-slope shape: Linear, concave
Across-slope shape: Linear

Volusia, rubbly
Percent of map unit: 5 percent
Landform: Hills
Landform position (two-dimensional): Footslope, summit
Landform position (three-dimensional): Base slope, side slope
Down-slope shape: Concave
Across-slope shape: Linear

Bath, rubbly
Percent of map unit: 5 percent
Landform: Drumlinoid ridges, hills, till plains
Landform position (two-dimensional): Backslope, shoulder
Landform position (three-dimensional): Side slope, interfluve, nose slope
Down-slope shape: Concave, linear
Across-slope shape: Linear

MrB—Morris channery loam, 3 to 8 percent slopes

Map Unit Setting
National map unit symbol: b463
Elevation: 50 to 1,800 feet
Mean annual precipitation: 32 to 50 inches
Mean annual air temperature: 45 to 50 degrees F
Frost-free period: 110 to 180 days
Farmland classification: Farmland of statewide importance

Map Unit Composition
Morris and similar soils: 75 percent
Minor components: 25 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Morris

Setting
Landform: Till plains
Landform position (two-dimensional): Toeslope
Landform position (three-dimensional): Base slope
Down-slope shape: Concave
Across-slope shape: Concave

Typical profile

A - 0 to 8 inches: channery loam
Bw - 8 to 17 inches: channery loam
Bx - 17 to 70 inches: channery silt loam
C - 70 to 80 inches: channery silt loam

Properties and qualities

Slope: 3 to 8 percent
Depth to restrictive feature: 11 to 22 inches to fragipan
Natural drainage class: Somewhat poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately high (0.00 to 0.20 in/hr)
Depth to water table: About 3 to 10 inches
Frequency of flooding: None
Frequency of ponding: None
Available water storage in profile: Very low (about 2.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 3w
Hydrologic Soil Group: D

Minor Components

Norwich

Percent of map unit: 20 percent
Landform: Depressions
Down-slope shape: Concave
Across-slope shape: Concave

Wellsboro

Percent of map unit: 5 percent

MrC—Morris channery loam, 8 to 18 percent slopes

Map Unit Setting

National map unit symbol: b464
Elevation: 50 to 1,800 feet
Mean annual precipitation: 32 to 50 inches
Mean annual air temperature: 45 to 50 degrees F
Frost-free period: 110 to 180 days
Farmland classification: Farmland of statewide importance

Map Unit Composition

Morris and similar soils: 80 percent
Minor components: 20 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Morris

Setting

Landform: Till plains
Landform position (two-dimensional): Toeslope
Landform position (three-dimensional): Base slope
Down-slope shape: Concave
Across-slope shape: Concave

Typical profile

A - 0 to 8 inches: channery loam
Bw - 8 to 17 inches: channery loam
Bx - 17 to 70 inches: channery silt loam
C - 70 to 80 inches: channery silt loam

Properties and qualities

Slope: 8 to 18 percent
Depth to restrictive feature: 11 to 22 inches to fragipan
Natural drainage class: Somewhat poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately high (0.00 to 0.20 in/hr)
Depth to water table: About 3 to 10 inches
Frequency of flooding: None
Frequency of ponding: None
Available water storage in profile: Very low (about 2.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 3e
Hydrologic Soil Group: D

Minor Components

Norwich

Percent of map unit: 12 percent
Landform: Depressions
Down-slope shape: Concave
Across-slope shape: Concave

Wellsboro

Percent of map unit: 8 percent

MsB—Morris flaggy loam, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: b465
Elevation: 600 to 1,800 feet
Mean annual precipitation: 30 to 50 inches
Mean annual air temperature: 45 to 50 degrees F
Frost-free period: 110 to 165 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Morris and similar soils: 75 percent
Minor components: 25 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Morris

Setting

Landform: Till plains
Landform position (two-dimensional): Toeslope
Landform position (three-dimensional): Base slope
Down-slope shape: Concave
Across-slope shape: Concave

Typical profile

A - 0 to 8 inches: flaggy loam
Bw - 8 to 17 inches: flaggy loam
Bx - 17 to 70 inches: channery silt loam
C - 70 to 80 inches: channery silt loam

Properties and qualities

Slope: 3 to 8 percent
Depth to restrictive feature: 11 to 22 inches to fragipan
Natural drainage class: Somewhat poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately high (0.00 to 0.20 in/hr)
Depth to water table: About 3 to 10 inches
Frequency of flooding: None
Frequency of ponding: None
Available water storage in profile: Very low (about 2.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 3w
Hydrologic Soil Group: D

Minor Components

Chippewa

Percent of map unit: 20 percent
Landform: Depressions
Down-slope shape: Concave
Across-slope shape: Concave

Wellsboro

Percent of map unit: 5 percent

MsC—Morris flaggy loam, 8 to 15 percent slopes

Map Unit Setting

National map unit symbol: b466
Elevation: 600 to 1,800 feet
Mean annual precipitation: 30 to 50 inches
Mean annual air temperature: 45 to 50 degrees F
Frost-free period: 110 to 165 days
Farmland classification: Farmland of statewide importance

Map Unit Composition

Morris and similar soils: 83 percent
Minor components: 17 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Morris

Setting

Landform: Till plains
Landform position (two-dimensional): Toeslope
Landform position (three-dimensional): Base slope
Down-slope shape: Concave
Across-slope shape: Concave

Typical profile

A - 0 to 8 inches: flaggy loam
Bw - 8 to 17 inches: flaggy loam
Bx - 17 to 70 inches: channery silt loam
C - 70 to 80 inches: channery silt loam

Properties and qualities

Slope: 8 to 15 percent
Depth to restrictive feature: 11 to 22 inches to fragipan
Natural drainage class: Somewhat poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately high (0.00 to 0.20 in/hr)
Depth to water table: About 3 to 10 inches
Frequency of flooding: None
Frequency of ponding: None
Available water storage in profile: Very low (about 2.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 3e
Hydrologic Soil Group: D

Minor Components

Chippewa

Percent of map unit: 12 percent
Landform: Depressions
Down-slope shape: Concave
Across-slope shape: Concave

Wellsboro

Percent of map unit: 5 percent

MxB—Morris extremely stony loam, 0 to 8 percent slopes

Map Unit Setting

National map unit symbol: b467
Elevation: 600 to 1,800 feet
Mean annual precipitation: 32 to 50 inches
Mean annual air temperature: 45 to 50 degrees F
Frost-free period: 110 to 165 days
Farmland classification: Not prime farmland

Map Unit Composition

Morris and similar soils: 75 percent
Minor components: 25 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Morris

Setting

Landform: Till plains
Landform position (two-dimensional): Toeslope
Landform position (three-dimensional): Base slope
Down-slope shape: Concave
Across-slope shape: Concave

Typical profile

A - 0 to 8 inches: channery loam
Bw - 8 to 17 inches: channery loam
Bx - 17 to 70 inches: channery silt loam
C - 70 to 80 inches: channery silt loam

Properties and qualities

Slope: 0 to 8 percent
Percent of area covered with surface fragments: 9.0 percent
Depth to restrictive feature: 11 to 22 inches to fragipan
Natural drainage class: Somewhat poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately high (0.00 to 0.20 in/hr)
Depth to water table: About 3 to 10 inches

Frequency of flooding: None
Frequency of ponding: None
Available water storage in profile: Very low (about 2.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7s
Hydrologic Soil Group: D

Minor Components

Norwich

Percent of map unit: 20 percent
Landform: Depressions
Down-slope shape: Concave
Across-slope shape: Concave

Wellsboro

Percent of map unit: 5 percent

MxD—Morris extremely stony loam, 8 to 25 percent slopes

Map Unit Setting

National map unit symbol: b468
Elevation: 600 to 1,800 feet
Mean annual precipitation: 32 to 50 inches
Mean annual air temperature: 45 to 50 degrees F
Frost-free period: 110 to 165 days
Farmland classification: Not prime farmland

Map Unit Composition

Morris and similar soils: 80 percent
Minor components: 20 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Morris

Setting

Landform: Till plains
Landform position (two-dimensional): Toeslope
Landform position (three-dimensional): Base slope
Down-slope shape: Concave
Across-slope shape: Concave

Typical profile

A - 0 to 8 inches: channery loam
Bw - 8 to 17 inches: channery loam
Bx - 17 to 70 inches: channery silt loam
C - 70 to 80 inches: channery silt loam

Properties and qualities

Slope: 8 to 25 percent

Percent of area covered with surface fragments: 9.0 percent
Depth to restrictive feature: 11 to 22 inches to fragipan
Natural drainage class: Somewhat poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately high (0.00 to 0.20 in/hr)
Depth to water table: About 3 to 10 inches
Frequency of flooding: None
Frequency of ponding: None
Available water storage in profile: Very low (about 2.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7s
Hydrologic Soil Group: D

Minor Components

Wellsboro

Percent of map unit: 12 percent

Norwich

Percent of map unit: 8 percent
Landform: Depressions
Down-slope shape: Concave
Across-slope shape: Concave

NcB—Norwich and Chippewa channery silt loams, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: 2vcjd
Elevation: 330 to 2,460 feet
Mean annual precipitation: 31 to 70 inches
Mean annual air temperature: 39 to 52 degrees F
Frost-free period: 105 to 180 days
Farmland classification: Not prime farmland

Map Unit Composition

Norwich and similar soils: 45 percent
Chippewa and similar soils: 35 percent
Minor components: 20 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Norwich

Setting

Landform: Depressions
Landform position (two-dimensional): Toeslope
Landform position (three-dimensional): Base slope
Down-slope shape: Concave
Across-slope shape: Concave

Parent material: Loamy till dominated by reddish sandstone, siltstone and shale fragments

Typical profile

A - 0 to 6 inches: channery silt loam
Eg - 6 to 10 inches: channery silt loam
Bg - 10 to 16 inches: channery silt loam
Bgx - 16 to 46 inches: channery silt loam
C - 46 to 72 inches: channery silt loam

Properties and qualities

Slope: 3 to 8 percent
Percent of area covered with surface fragments: 0.0 percent
Depth to restrictive feature: 10 to 24 inches to fragipan
Natural drainage class: Poorly drained
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.14 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: None
Frequency of ponding: None
Available water storage in profile: Low (about 3.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 4w
Hydrologic Soil Group: D

Description of Chippewa

Setting

Landform: Depressions
Landform position (two-dimensional): Toeslope
Landform position (three-dimensional): Base slope
Down-slope shape: Concave
Across-slope shape: Concave
Parent material: Loamy till dominated by siltstone, sandstone, and shale fragments

Typical profile

Ap - 0 to 7 inches: channery silt loam
Eg - 7 to 15 inches: channery silt loam
Bgx - 15 to 45 inches: channery silt loam
C - 45 to 72 inches: channery silt loam

Properties and qualities

Slope: 3 to 8 percent
Percent of area covered with surface fragments: 0.0 percent
Depth to restrictive feature: 8 to 20 inches to fragipan
Natural drainage class: Poorly drained
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.14 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 15 percent
Available water storage in profile: Low (about 3.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4w
Hydrologic Soil Group: D

Minor Components

Volusia
Percent of map unit: 5 percent
Landform: Hills
Landform position (two-dimensional): Footslope, summit
Landform position (three-dimensional): Base slope, side slope
Down-slope shape: Concave
Across-slope shape: Linear

Morris
Percent of map unit: 5 percent
Landform: Hills
Landform position (two-dimensional): Footslope, summit
Landform position (three-dimensional): Base slope, side slope
Down-slope shape: Concave
Across-slope shape: Linear

Chippewa, very poorly drained
Percent of map unit: 5 percent
Landform: Depressions
Landform position (two-dimensional): Toeslope
Landform position (three-dimensional): Base slope
Down-slope shape: Concave
Across-slope shape: Concave

Norwich, very poorly drained
Percent of map unit: 5 percent
Landform: Depressions
Landform position (two-dimensional): Toeslope
Landform position (three-dimensional): Base slope
Down-slope shape: Concave
Across-slope shape: Concave

NxB—Norwich and Chippewa channery silt loams, 0 to 8 percent slopes, rubbly

Map Unit Setting
National map unit symbol: 2vcjq
Elevation: 330 to 2,460 feet
Mean annual precipitation: 31 to 70 inches
Mean annual air temperature: 39 to 52 degrees F
Frost-free period: 105 to 180 days
Farmland classification: Not prime farmland

Map Unit Composition

Norwich, rubbly, and similar soils: 45 percent
Chippewa, rubbly, and similar soils: 40 percent
Minor components: 15 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Norwich, Rubbly

Setting

Landform: Depressions
Landform position (two-dimensional): Toeslope
Landform position (three-dimensional): Base slope
Down-slope shape: Concave
Across-slope shape: Concave
Parent material: Loamy till dominated by reddish sandstone, siltstone and shale fragments

Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material
A - 1 to 5 inches: channery silt loam
Eg - 5 to 10 inches: channery silt loam
Bg - 10 to 16 inches: channery silt loam
Bgx - 16 to 46 inches: channery silt loam
C - 46 to 72 inches: channery silt loam

Properties and qualities

Slope: 0 to 8 percent
Percent of area covered with surface fragments: 20.0 percent
Depth to restrictive feature: 10 to 24 inches to fragipan
Natural drainage class: Poorly drained
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.14 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: None
Frequency of ponding: None
Available water storage in profile: Low (about 3.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7s
Hydrologic Soil Group: D

Description of Chippewa, Rubbly

Setting

Landform: Depressions
Landform position (two-dimensional): Toeslope
Landform position (three-dimensional): Base slope
Down-slope shape: Concave
Across-slope shape: Concave
Parent material: Loamy till dominated by siltstone, sandstone, and shale fragments

Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material
A - 1 to 5 inches: channery silt loam
Eg - 5 to 15 inches: channery silt loam

Bgx - 15 to 45 inches: channery silt loam
C - 45 to 72 inches: channery silt loam

Properties and qualities

Slope: 0 to 8 percent
Percent of area covered with surface fragments: 20.0 percent
Depth to restrictive feature: 8 to 20 inches to fragipan
Natural drainage class: Poorly drained
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.14 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 15 percent
Available water storage in profile: Low (about 3.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7s
Hydrologic Soil Group: D

Minor Components

Chippewa, rubbly, very poorly drained

Percent of map unit: 5 percent
Landform: Depressions
Landform position (two-dimensional): Toeslope
Landform position (three-dimensional): Base slope
Down-slope shape: Concave
Across-slope shape: Concave

Norwich, rubbly, very poorly drained

Percent of map unit: 5 percent
Landform: Depressions
Landform position (two-dimensional): Toeslope
Landform position (three-dimensional): Base slope
Down-slope shape: Concave
Across-slope shape: Concave

Morris, extremely stony

Percent of map unit: 3 percent
Landform: Hills
Landform position (two-dimensional): Footslope, summit
Landform position (three-dimensional): Base slope, side slope
Down-slope shape: Concave
Across-slope shape: Linear

Volusia, extremely stony

Percent of map unit: 2 percent
Landform: Hills
Landform position (two-dimensional): Footslope, summit
Landform position (three-dimensional): Base slope, side slope
Down-slope shape: Concave
Across-slope shape: Linear

OcC—Oquaga channery loam, 8 to 15 percent slopes

Map Unit Setting

National map unit symbol: b46f
Elevation: 600 to 1,800 feet
Mean annual precipitation: 32 to 50 inches
Mean annual air temperature: 45 to 52 degrees F
Frost-free period: 110 to 180 days
Farmland classification: Farmland of statewide importance

Map Unit Composition

Oquaga and similar soils: 85 percent
Minor components: 15 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Oquaga

Setting

Landform: Hillslopes
Landform position (two-dimensional): Shoulder
Landform position (three-dimensional): Side slope
Down-slope shape: Linear
Across-slope shape: Linear

Typical profile

Ap - 0 to 7 inches: channery loam
Bw - 7 to 30 inches: extremely channery silt loam
R - 30 to 42 inches: unweathered bedrock

Properties and qualities

Slope: 8 to 15 percent
Depth to restrictive feature: 20 to 40 inches to lithic bedrock
Natural drainage class: Well drained
Runoff class: Medium
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 2.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water storage in profile: Very low (about 2.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 3e
Hydrologic Soil Group: C

Minor Components

Arnot
Percent of map unit: 5 percent

Lordstown
Percent of map unit: 5 percent

Lackawanna
Percent of map unit: 5 percent

OcD—Oquaga channery loam, 15 to 25 percent slopes

Map Unit Setting
National map unit symbol: b46g
Elevation: 600 to 1,800 feet
Mean annual precipitation: 32 to 50 inches
Mean annual air temperature: 45 to 52 degrees F
Frost-free period: 110 to 180 days
Farmland classification: Not prime farmland

Map Unit Composition
Oquaga and similar soils: 90 percent
Minor components: 10 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Oquaga

Setting
Landform: Hillslopes
Landform position (two-dimensional): Shoulder
Landform position (three-dimensional): Side slope
Down-slope shape: Linear
Across-slope shape: Linear

Typical profile
Ap - 0 to 7 inches: channery loam
Bw - 7 to 30 inches: extremely channery silt loam
R - 30 to 42 inches: unweathered bedrock

Properties and qualities
Slope: 15 to 25 percent
Depth to restrictive feature: 20 to 40 inches to lithic bedrock
Natural drainage class: Well drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 2.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water storage in profile: Very low (about 2.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 4e
Hydrologic Soil Group: C

Minor Components

Arnot

Percent of map unit: 5 percent

Lackawanna

Percent of map unit: 5 percent

OfB—Oquaga flaggy loam, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: b46h
Elevation: 600 to 1,800 feet
Mean annual precipitation: 32 to 50 inches
Mean annual air temperature: 45 to 52 degrees F
Frost-free period: 110 to 180 days
Farmland classification: Farmland of statewide importance

Map Unit Composition

Oquaga and similar soils: 85 percent
Minor components: 15 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Oquaga

Setting

Landform: Hillslopes
Landform position (two-dimensional): Shoulder
Landform position (three-dimensional): Side slope
Down-slope shape: Linear
Across-slope shape: Linear

Typical profile

Ap - 0 to 7 inches: flaggy loam
Bw - 7 to 30 inches: extremely channery silt loam
R - 30 to 42 inches: unweathered bedrock

Properties and qualities

Slope: 3 to 8 percent
Depth to restrictive feature: 20 to 40 inches to lithic bedrock
Natural drainage class: Well drained
Runoff class: Medium
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 2.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None

Frequency of ponding: None
Available water storage in profile: Very low (about 2.7 inches)

Interpretive groups
Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 2e
Hydrologic Soil Group: C

Minor Components

Arnot
Percent of map unit: 5 percent

Lordstown
Percent of map unit: 5 percent

Lackawanna
Percent of map unit: 5 percent

OxD—Oquaga extremely stony loam, 8 to 25 percent slopes

Map Unit Setting
National map unit symbol: b46l
Elevation: 700 to 1,800 feet
Mean annual precipitation: 32 to 50 inches
Mean annual air temperature: 45 to 52 degrees F
Frost-free period: 110 to 180 days
Farmland classification: Not prime farmland

Map Unit Composition
Oquaga and similar soils: 85 percent
Minor components: 15 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Oquaga

Setting
Landform: Hillslopes
Landform position (two-dimensional): Shoulder
Landform position (three-dimensional): Side slope
Down-slope shape: Linear
Across-slope shape: Linear

Typical profile
A - 0 to 7 inches: channery loam
Bw - 7 to 30 inches: extremely channery silt loam
R - 30 to 42 inches: unweathered bedrock

Properties and qualities
Slope: 8 to 25 percent
Percent of area covered with surface fragments: 9.0 percent
Depth to restrictive feature: 20 to 40 inches to lithic bedrock

Natural drainage class: Well drained
Runoff class: Medium
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 2.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water storage in profile: Very low (about 2.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7s
Hydrologic Soil Group: C

Minor Components

Arnot

Percent of map unit: 5 percent

Lordstown

Percent of map unit: 5 percent

Lackawanna

Percent of map unit: 5 percent

WcC—Wellsboro channery loam, 8 to 15 percent slopes

Map Unit Setting

National map unit symbol: b47g
Elevation: 50 to 1,800 feet
Mean annual precipitation: 32 to 50 inches
Mean annual air temperature: 45 to 50 degrees F
Frost-free period: 110 to 180 days
Farmland classification: Farmland of statewide importance

Map Unit Composition

Wellsboro and similar soils: 85 percent
Minor components: 15 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Wellsboro

Setting

Landform: Valley sides
Landform position (two-dimensional): Footslope
Landform position (three-dimensional): Base slope
Down-slope shape: Concave
Across-slope shape: Linear

Typical profile

A - 0 to 8 inches: channery loam
Bw - 8 to 17 inches: channery loam

BE - 17 to 21 inches: channery loam
Bx - 21 to 60 inches: channery silt loam
C - 60 to 80 inches: channery loam

Properties and qualities

Slope: 8 to 15 percent
Depth to restrictive feature: 14 to 26 inches to fragipan
Natural drainage class: Moderately well drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: About 11 to 22 inches
Frequency of flooding: None
Frequency of ponding: None
Available water storage in profile: Very low (about 2.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 3e
Hydrologic Soil Group: D

Minor Components

Morris

Percent of map unit: 5 percent

Lackawanna

Percent of map unit: 5 percent

Norwich

Percent of map unit: 5 percent
Landform: Depressions
Down-slope shape: Concave
Across-slope shape: Concave

WcD—Wellsboro channery loam, 15 to 25 percent slopes

Map Unit Setting

National map unit symbol: b47h
Elevation: 600 to 1,800 feet
Mean annual precipitation: 32 to 50 inches
Mean annual air temperature: 45 to 50 degrees F
Frost-free period: 110 to 165 days
Farmland classification: Not prime farmland

Map Unit Composition

Wellsboro and similar soils: 90 percent
Minor components: 10 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Wellsboro

Setting

Landform: Valley sides
Landform position (two-dimensional): Footslope
Landform position (three-dimensional): Base slope
Down-slope shape: Concave
Across-slope shape: Linear

Typical profile

A - 0 to 8 inches: channery loam
Bw - 8 to 17 inches: channery loam
BE - 17 to 21 inches: channery loam
Bx - 21 to 60 inches: channery silt loam
C - 60 to 80 inches: channery loam

Properties and qualities

Slope: 15 to 25 percent
Depth to restrictive feature: 14 to 26 inches to fragipan
Natural drainage class: Moderately well drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: About 11 to 22 inches
Frequency of flooding: None
Frequency of ponding: None
Available water storage in profile: Very low (about 2.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 4e
Hydrologic Soil Group: D

Minor Components

Lackawanna

Percent of map unit: 5 percent

Morris

Percent of map unit: 5 percent

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