

March 10, 2022

Mr. Josh D. Hoffman, P.E. Snyder, Secary & Associates, a Division of Pennoni 2000 Linglestown Road, Suite 304 Harrisburg, PA 17110

**RE:** Preliminary Geotechnical Summary Report

2951 Betz Court Development

Lowhill Township, Lehigh County, Pennsylvania Kleinfelder Project Number: 20221785.003A

Dear Mr. Hoffman:

In accordance with your request, Kleinfelder, Inc. (Kleinfelder) has completed a preliminary geotechnical engineering evaluation of the above referenced project site. This correspondence serves to transmit the results of the data obtained and our preliminary conclusions regarding development of the property.

#### SITE AND PROJECT DESCRIPTION

The project site currently consists of commercial, wooded, and agricultural properties located at 2591 Betz Court in Lowhill Township, Lehigh County, Pennsylvania. The project site is bordered to the north by agricultural property, to the east by residential properties and Kernsville Road (4003), to the southwest by Betz Court and to the northwest by woods and agricultural property. Topography across the project site slopes downgradient from east to west, with notable soil, mulch, and construction debris stockpiles and hills located in the eastern and central portions of the site, resulting in approximately 140 feet of grade variation across the project site. Within the building footprint, elevations vary from approximately 640 to 670 feet above mean sea level (amsl), resulting in approximately 30 feet of grade variation. It should be noted that a portion of the subject site is currently being used by a mulch supplier (Stone Haven Supply); therefore, stopckpiles of mulch and other debris (e.g. concrete/rock) are present at the site. The approximate location of the site in relation to the surrounding area is shown on the *Topographic Map* (Figure 1) presented within the Appendix.

Based on *Concept Grading and Drainage Plan* (Plan), prepared by Snyder, Secary & Associates, LLC, dated February 4, 2022, the project will consist of constructing a building measuring approximately 299,880 square feet (SF) in plan area with a finished floor elevation (FFE) situated at 653.00. Based on this information, cuts of fills of approximately 17 and 13 feet, respectively, are anticipated.

At the time of this writing, structural loads were not known. For purposes of this report, it was assumed that column and wall loads are not anticipated to exceed 150 kips and 7 kips per linear foot, respectively. Additionally, slab loads have been assumed to range from about 250 to 500 psf. Development of this project site will also include constructing new parking areas, drive lanes, retaining walls, and stormwater management facilities.

#### **SCOPE OF WORK**

The objective of our work was to complete a preliminary evaluation of the underlying subsurface conditions to provide preliminary recommendations and conclusions regarding development of the site. The scope of work for this project included completion of a subsurface exploration, laboratory testing program, and preliminary engineering analysis of the data obtained. This report summarizes the results of the work performed and provides preliminary geotechnical and construction recommendations, specific to the aforementioned scope of work.

Mr. Josh D. Hoffman, P.E. 2951 Betz Court Development March 10, 2022 Page 2 of 9

#### **SITE GEOLOGY**

According to the <u>Pennsylvania State Geologic Survey Atlas of Preliminary Geologic Quadrangles</u>, 1981, the project site is underlain by the Ordovician Martinsburg Formation (geologic symbol Om). The project site within its geologic setting is presented on the *Geologic Map* (Figure 2) found within the Appendix.

According to the *Engineering Characteristics of the Rocks of Pennsylvania*, Second Edition 1982, the Martinsburg Formation is composed of buff-weathering dark-gray shale, with thin interbeds of siltstone, metabentonite, and fine-grained sandstone. This formation is well bedded with the sandstone being thick to massive, and shale thin to fissile. The rock of this formation is moderately weathered to a moderate depth with small to large platy fragments resulting. Cleavage is dominant and highly developed with jointing present and irregularly spaced, open and nearly vertical.

#### SUBSURFACE EXPLORATION PROGRAM

To evaluate the subsurface conditions across the project site, 15 test borings and 8 test pits were completed on February 15 through 17, 2022 and February 23, 2022. Supervision and monitoring of the subsurface exploration were provided by representatives of Kleinfelder, who field located the test locations based on the previously referenced *Plan*. The approximate test locations are shown on the *Exploration Plan* (Figure 3) presented within the Appendix.

The test borings were advanced using a track-mounted Diedrich D-50 drill rig equipped with an automatic hammer and 3 ¼" hollow-stem augers. Split-spoon samples, conducted in general accordance with ASTM standard D1586, were taken at suitable intervals throughout the entire depth of the borings and the Standard Penetration Test (SPT) values were recorded for each sample obtained. The SPT values, which are a measure of density or consistency, are the number of blows required to drive a 2-inch (outer-diameter) split-barrel sampler 2 feet using a 140-pound weight dropped 30 inches. The number of blows required to advance the sampler over the 12-inch interval from 6 to 18 inches is considered the "N" value.

Data pertaining to the subsurface exploration was documented in the field and is presented on the *Test Boring Profiles* (Figure 4) and *Test Boring Logs* within the Appendix. The *Test Boring Profiles* depict cross-sections of the subsurface conditions encountered within each test boring conducted, including: soil types, depths of individual strata and recorded "N" values. The *Test Boring Logs* contain general information about the subsurface program and specific data regarding each test boring, including: sample depths, hammer blows per 6 inches of penetration and visual classifications of the subsurface materials encountered.

The test pits were excavated utilizing a CAT 416 backhoe and extended to depths ranging from approximately 5.5 to 8.5 feet below existing site grades. A detailed account of the material encountered during the excavation of each test pit, as well as groundwater data and infiltration test data, where applicable, is presented on the *Test Pit Logs* within the Appendix.

#### LABORATORY TESTING

Soil samples retrieved from the site were visually reviewed and classified by Kleinfelder. Representative soil samples were subjected to laboratory analyses to verify visual classifications and aid in establishing the engineering parameters in accordance with the following schedule:

- Natural Moisture Content (ASTM D2216)
- Sieve Analysis (ASTM D422)
- Atterberg Limits Determination (ASTM D4318)

Unified Soil Classification System (USCS) Group Symbols and ASTM Group Names have been assigned to the soils analyzed. The results of the testing conducted are presented within the Appendix and the table below.

Mr. Josh D. Hoffman, P.E. 2951 Betz Court Development March 10, 2022 Page 3 of 9

	LABORATORY TESTING RESULTS													
Location I.D.	Depth (feet)	Soil Type	% Gravel	% Sand	% Fines	LL	LL PL PI		As Received Moisture	USCS Group Symbol	ASTM Group Name			
B-5	2 – 6		42.2	22.8	35.0	No	n-Pla	stic	14.9%	GM	Silty GRAVEL with Sand			
B-9	6 – 8	Stratum I	32.7	56.3	11.0	Non-Plastic			8.9%	SW-SM	Well-Graded SAND with Silt and Gravel			
LL-Liquid Limit; PL-Plastic Limit; PI-Plasticity Index														

#### **DESCRIPTION OF SUBSURFACE CONDITIONS**

#### SOIL

#### **Surficial Material**

The test locations were covered by approximately to 4 to 12 inches of topsoil, 3 to 24 inches of Gravel, or 3 inches of pavement (asphalt and stone subbase); however, the thickness of surficial materials may vary in unexplored areas of the site. Kleinfelder utilized visual classifications in order to field delineate the approximate topsoil and surficial material thicknesses within the test locations completed.

#### Fill - Orangish brown to gray SILT and SAND with secondary amounts of Gravel

Fill was encountered within test locations B-3, B-5, B-6, B-9 and B-10, and extended to depths ranging from approximately 2 to 6 feet below existing site grades. The "N" values, recorded within this soil ranged from 5 to 50 blows per foot (bpf).

Upon review, this soil was found to be poorly to moderately well graded, non-plastic, and predominantly comprised of SILT and SAND with secondary amounts of Gravel.

The existing Fill was found to contain deleterious material in the form of organic debris (i.e. mulch) in test location B-3. It should be noted, a portion of the project site is occupied by a mulch supplier, so several stockpiles of mulch and other debris (e.g. concrete, rock) are present on site. These samples were taken from discrete locations and the possibility does exist for unsuitable materials (e.g. ash, cinder, slag, and topsoil and/or organic debris) to be present in unexplored portions of the site.

## Stratum I – Tan to light brown to gray SAND and GRAVEL with varying amounts of Silt [highly weathered to decomposed rock]

Stratum I was encountered within each test location completed, with the exception of TP-9, and extended to depths ranging from approximately 1 to 20 feet below existing site grades. The "N" value, recorded within this soil was found to range from 4 bpf to 50 blows over 1-inch and shows Stratum I to range from loose to very dense in relative density.

Laboratory testing conducted on representative samples of Stratum I shows this soil to be poorly to moderately well graded and non-plastic, with natural moisture contents ranging from 8.9% to 14.9%. Stratum I is described under the USCS as Silty GRAVEL with Sand (GM) and Well-Graded SAND with Silt and Gravel (SW-SM).

#### Stratum II - Orangish brown to tan SILT with varying amounts of Sand

Stratum II was encountered within test locations B-1, B-2 and B-10, and extended to depths ranging from approximately 3 to 6 feet below existing site grades. The "N" values, recorded within this soil ranged from 4 to 22 bpf and show Stratum II to range from medium stiff to very stiff in consistency.

Mr. Josh D. Hoffman, P.E. 2951 Betz Court Development March 10, 2022 Page 4 of 9

Upon review, Stratum II was found to be poorly graded, slightly plastic, and predominantly comprised of SILT with secondary amounts of Sand.

#### **BEDROCK & REFUSAL**

Bedrock was encountered within each test boring completed, with the exception of B-6, and test pits IT-5 through IT-7, at depths ranging from approximately 1 to 18.5 feet below existing site grades. Bedrock was defined as the depth as which the drilling augers could no longer penetrate or the depth at which the bucket of the backhoe could no longer excavate.

To determine the composition and integrity of the rock present beneath the site, rock coring was conducted in general accordance with ASTM D 2113. Percent Recovery (REC) was calculated by dividing the length of the rock core retrieved from the core barrel by the total length of the core run and multiplying by 100. Rock Quality Designation (RQD) was calculated by summing the length of the rock fragments in the core run which are greater than or equal to 4 inches in length and dividing by the total length of the core run and multiplying by 100. A visual description of the bedrock encountered is provided on the *Test Boring Logs* within the Appendix and provided in the table below.

	ROCK CORING DATA SUMMARY												
Location	Run Number	Rock Core Depth (ft)	REC (%)	RQD (%)	Visual Description								
B-11	R-1	1 – 6	100	0	SHALE: light to dark gray, moderately to highly weathered, intensely fractured								
B-12	R-1	1.5 – 6.5	100	0	SHALE: light to dark gray, moderately to highly weathered, intensely fractured								
B-14	R-1	7 – 12	47	0	SHALE: light to dark gray, moderately to highly weathered, intensely fractured								

#### **GROUNDWATER / SOIL MOTTLING**

Groundwater was encountered within test locations IT-1 through IT-3. IT-1 had an initial groundwater reading of approximately 5.5 feet below existing site grades and a final groundwater reading of 4 feet below existing site grades at the time of completion. IT-2 encountered perched water at depths ranging from approximately 0.5 to 1.5 feet below existing site grades. IT-3 encountered groundwater at a depth of approximately 3 feet below existing site grades. Soil mottling (indication of poorly draining soils and/or seasonal high-water table) was not encountered within the test locations completed. These observations were made at the time of the field exploration and groundwater table elevations will vary with daily, seasonal, and climatological variations as well as anthropogenic activities.

#### PRELIMINARY CONCLUSIONS

Based upon geotechnical engineering review of the data gathered during the field exploration, preliminary conclusions have been formulated regarding the project site and are as follows:

#### **Excavation Considerations**

At the time of this writing, the proposed FFE of the building is expected to be 653.00 feet. Within the building footprint, existing grades vary from approximately 640 to 670 feet amsl, resulting in approximately 30 feet of grade variation. Based on the test locations completed for the proposed improvements, it is expected that construction of the project will likely take place within the existing Fill, naturally occurring soils of Stratum I and II, and the

Mr. Josh D. Hoffman, P.E. 2951 Betz Court Development March 10, 2022 Page 5 of 9

underlying bedrock. The existing Fill and the naturally occurring soils of Stratum I and Stratum II may be removed using conventional earth moving equipment and techniques. However, based on the high SPT values obtained, slow advancement of the drilling augers and heavy bucket resistance observed, portions of Stratum I will be difficult to excavate and require the use of larger equipment and/or hydraulic or pneumatic hammering equipment for removal.

Bedrock removal will be required during development of the project site, including to reach the proposed building finished floor elevation. Bedrock excavation will be difficult and require the use of hydraulic or pneumatic "hammering" equipment or blasting techniques for removal. Should blasting be utilized during site development, it is imperative to minimize charges to avoid "over-blasting" of the bedrock beyond required excavation depths. Upon completion of blasting procedures, all loose rock and "over-blast" must be completely excavated from the area. Excavated bedrock may be utilized as structural fill provided it is sufficiently processed to meet the requirements presented in this report.

It must be understood, the test boring and test pit logs may be used to estimate rock excavation based on the refusal depths; however, refusal should not be considered to be a definite indicator of rock excavation required. There are many geologic factors which effect the difficulty of excavation such as rock hardness, bedding, joint spacing, fracture spacing and degree of weathering. The ease of excavation will also be governed by the type of excavation equipment used and the contractor's willingness to utilize the equipment to its full potential. Rock excavation is expected to vary due to the variability in the rock surface between exploration points.

All excavations should be adequately sloped, benched, or supported to minimize collapse and protect personnel. All excavations should be completed in accordance with OSHA requirements.

#### Reuse of On-Site Soils

**Topsoil** - The topsoil will not be suitable for reuse as structural fill, however, the topsoil may be stockpiled for reuse within landscaping areas, non-structural areas, berms, etc. As written above, Kleinfelder utilized visual classifications to estimate the topsoil thicknesses encountered during the field explorations. The Client or construction team (i.e., general contractor, earthwork contractor, etc.) may consider the topsoil depth information in their evaluation of the project site, however, the we recommend they complete their own evaluation prior to the start of construction. The Geotechnical of Record and/or other professionals (i.e. soil agronomist) should be consulted during the pre-construction process in order to reduce the risk of incorrect estimation of topsoil thickness.

Fill – This soil was found to be poorly to moderately well graded, non-plastic, and predominately comprised of SILT and SAND with secondary amounts of Gravel. The existing Fill was found to be contain deleterious material in the form of organic debris (i.e. mulch) in test location B-3. It should be noted, a portion of the project site is currently occupied by a mulch supplier, so several stockpiles of mulch and other debris (e.g. concrete, rock) are present on site. During grading operations, care should be given to ensure that the mulch, and any other deleterious material, if encountered, not be combined with the on-site soils.

Based on this information, this soil is considered marginally suitable for re-use as structural fill, provided any deleterious materials, if encountered, is removed prior to placement.

**Stratum I** - This soil was found to be poorly to moderately well graded, non-plastic, and predominantly comprised of SAND and GRAVEL with varying amounts of Silt. Based on this information, this soil is considered suitable for reuse as structural fill. It should be noted, portions of this soil Stratum may have to be processed and/or resized prior to placement per the criteria within the **Processed Bedrock** section below.

**Stratum II** - This soil was found to be poorly graded, slightly plastic, and predominantly comprised of SILT with secondary amounts of Sand. Based on this information, this soil is considered to be marginally suitable for reuse as structural fill.

Mr. Josh D. Hoffman, P.E. 2951 Betz Court Development March 10, 2022 Page 6 of 9

Due to the content of fines (SILT), portions of the Fill and Stratum II soils may be moisture sensitive and difficult to place during periods of adverse weather. Additionally, based on our experience with this geologic setting and similar project sites, earthwork activities during construction of the project site may cause the breakdown of weathered rock material within the naturally-occurring soils. Therefore, the amount of fines (clay and/or silt) may be higher post construction than in-situ during the geotechnical field exploration.

**Processed Bedrock** – Bedrock excavation will be required during site development. The excavated bedrock is considered well-suited for use as structural fill provided the following criteria are adhered to:

- Within the <u>upper 4 feet</u> of the proposed building pad subgrade elevation and within the <u>upper 1 foot</u> of the pavement subgrade elevation: Well graded mixture with a maximum particle size of 6 inches.
- <u>4 feet or more</u> below the proposed building pad subgrade elevation and <u>1 foot or more</u> below of the pavement subgrade: *Well graded mixture with a maximum particle size of 12 inches.*

Should consideration be given to processing the rock for use as pavement, concrete slab and/or asphalt pavement subbase material, the bedrock should be crushed and screened to meet PennDot (PADOT) 2A gradation and meet all quality requirements.

Our analysis of the suitability of the on-site soil for use as structural fill is based on data collected from the test locations completed at the site. Soil suitability should be confirmed in the field by Kleinfelder during construction.

#### Removal and Replacement of Existing Fill

According to the subsurface data obtained, portions of the proposed development are underlain by a layer of existing Fill, which extended to depths ranging from approximately 2 to 6 feet below existing site grades. Due to the lack of historical data indicating the fill materials were placed under engineering control, support of the proposed structures on conventional shallow foundations bearing directly on the existing Fill is not recommended due to the potential for intolerable post-construction settlement. Therefore, it is recommended the existing Fill be excavated in it's entirety and replaced under engineering control. Details concerning the removal and replacement of the Fill are presented below.

The existing Fill, where encountered, should be excavated in it's entirety from beneath the proposed structural areas (areas to be covered by the structures or pavement elements). The excavation sidewalls should be adequately sloped or benched, as necessary, to minimize collapse and protect personnel.

- Once excavated, the base of the resulting excavation should be thoroughly compacted utilizing appropriate equipment and reviewed by Kleinfelder. Should any weak or yielding areas be encountered, excavation should continue until suitable stable soils are encountered.
- Following review, the excavation may be backfilled to the prevailing subgrade elevations with structural fill. The previously excavated material may be used provided any deleterious materials are discarded prior to placement. The placement and compaction of structural fill should be completed in accordance with this Report.

#### **Foundation Considerations**

Based on the data obtained during the preliminary subsurface exploration, and engineering review of the conditions encountered, it is estimated that allowable soil bearing capacities ranging from 2,500 to 4,000 psf should be considered for foundation design. Conventional shallow foundations are expected to be suitable for support of the proposed building provided it is founded on stable naturally occurring soils and/or properly compacted structural fill placed under engineering control. Foundation bearing surfaces should be cleaned of loose material or debris immediately prior to the placement of concrete. Localized weak and yielding areas may be encountered during construction. Any weak or yielding areas encountered should be re-compacted in place or

Mr. Josh D. Hoffman, P.E. 2951 Betz Court Development March 10, 2022 Page 7 of 9

removed and replaced with suitable structural fill. To protect against frost heave, spread footing foundations, including those in unheated areas, should extend to depths specified by the building code or local code amendments.

#### Floor Slab

The floor of the proposed structure may be constructed as a conventional slab-on-grade and may be supported on properly placed structural fill or firm and stable existing soils. These soils are expected to exhibit a modulus of subgrade reaction between 95 and 150 pounds per cubic inch (pci), provided they are compacted to a minimum of 95 percent Modified Proctor maximum dry density (ASTM D1557) or 98 percent Standard Proctor maximum dry density (ASTM D698).

#### STORMWATER INFILTRATION ANALYSIS

To evaluate the feasibility of infiltration of stormwater, infiltration tests were conducted within each test pit excavated, with the exception of IT-1 and IT-3, utilizing the "double-ring" infiltrometer method in accordance with the <u>Pennsylvania Stormwater Best Management Practices Manual</u>, latest Edition. The infiltration test pits extended to depths of approximately 2 feet below existing site grades in an effort to review the presence of limiting zones (i.e. bedrock, groundwater and/or soil mottling). Information regarding the results of the infiltration testing is provided within the table below.

	INFILTRATION TEST RESULTS											
Test Location	Actual Test Elevation (ft)	Limiting Zone Depth (ft)	Infiltration Rate (in/hr)*									
IT-1	No Test	Groundwater encountered at 4	No Test									
IT-2	6	0.0										
IT-3	No Test	Groundwater Encountered at 3	No Test									
IT-4	5.5	Not Encountered at 8 feet	15.0									
IT-5	4	Bedrock Encountered at 6	10.8									
IT-6	3.5	Bedrock Encountered at 5.5	15.0									
IT-7	5	Bedrock Encountered at 7	4.2									
IT-8	6	Not Encountered at 8	15.0									
*Infiltration rates re	epresent the rates	recorded in the field and no safety factor h	as been applied									

Based on the results of our field exploration we offer the following comments:

- The final groundwater reading in test pit IT-1 was 4 feet below existing site grades; however, the water
  was percolating in from the side walls between 1.5 to 3 feet below existing site grades. Therefore, no
  infiltration test was conducted.
- In test location IT-2, water was percolating in from the side walls between 0.5 to 1.5 feet below existing site grades. An infiltration test was still conducted to gather data.

Mr. Josh D. Hoffman, P.E. 2951 Betz Court Development March 10, 2022 Page 8 of 9

- Test location IT-3 was excavated to 8 feet below existing site grades; however, groundwater was
  percolating in and caused the collapse of the side walls to 4 feet below existing site grades. A final
  groundwater reading was taken after the collapse, measuring approximately 3 feet below existing site
  grades.
- The bedrock surface was encountered within test pits IT-5 through IT-7 at depths of approximately 5.5 to 7 feet below existing site grades. The bedrock surface was defined as the depth at which the bucket of the backhoe could no longer excavate.
- Soil mottling was not encountered within the test locations completed.
- The unfactored infiltration rates were found to range from 0.0 to 15.0 inches per hour. The PADEP recommended rate for infiltration of stormwater is 0.1 to 10 inches per hour.

It should be noted, these are the field rates obtained from the in-situ soils at the project site. The project site is situated within the Martinsburg Formation, which is comprised of gray to dark gray shale and slate. Based on our experience with this geologic setting and similar project sites, earthwork activities during construction of the project site may cause the breakdown of weathered rock material within the naturally-occurring soils. Therefore, the amount of fines (clay/silt) may be higher post construction than in situ during the geotechnical field exploration. Consequently, infiltration results may vary.

#### FINAL GEOTECHNICAL ENGINEERING SERVICES

The scope of work completed for this report was intended to provide preliminary review of the subsurface conditions beneath the project site for anticipated improvements. It is recommended Kleinfelder review updated design plans and loading data for the proposed structure in order to finalize geotechnical and construction recommendations prior to issuance of final design criteria for the project.

#### **LIMITATIONS**

The conclusions and recommendations contained in this report are preliminary in nature due to the conceptual site layout, structure loading and other site features, and based upon the subsurface data collected and on details stated in this report. Should conditions arise which differ from those specifically stated herein, our office should be notified immediately so that our recommendations can be reviewed and revised, if necessary.

It is emphasized that this preliminary engineering analysis was completed for the proposed development at Betz Court in Lowhill Township, Lehigh County, Pennsylvania. Kleinfelder does not warrant the use of the data presented herein for any other purpose.

This work was performed in a manner consistent with that level of care and skill ordinarily exercised by other members of Kleinfelder's profession practicing in the same locality, under similar conditions and at the date the services are provided. Our conclusions are based on a limited number of observations and data. It is possible that conditions could vary between or beyond the data evaluated. Further, Kleinfelder assumes no liability for interpolation of data between the specific testing locations discussed herein. Kleinfelder makes no other representation, guarantee, or warranty, express or implied, regarding the services, communication (oral or written), report, opinion, or instrument of service provided.

This report may be used only by the Client and the registered design professional in responsible charge and only for the purposes stated for this specific engagement within a reasonable time from its issuance, but in no event later than 2 years from the date of the report.

Our scope of services for this exploration and report did not include environmental assessments or evaluations regarding the presence or absence of wetlands or hazardous substances in the soil, surface water, or groundwater at this site.

Mr. Josh D. Hoffman, P.E. 2951 Betz Court Development March 10, 2022 Page 9 of 9

#### **CLOSING**

We thank you for the opportunity to work on this project with you. Should you have any questions or require any additional information, please do not hesitate to contact us.

Sincerely,

KLEINFELDER, INC.

Bailey Jean Wildown
Bailey J. Wildasin
Project Manager

Mark A. Giunta, P.E. Principal Professional

PA License No: PE-073764

Trevor L. Dombach Program Manager



## **APPENDIX**

FIGURE 1 – TOPOGRAPHIC MAP

FIGURE 2 – GEOLOGIC MAP

FIGURE 3 – EXPLORATION PLAN

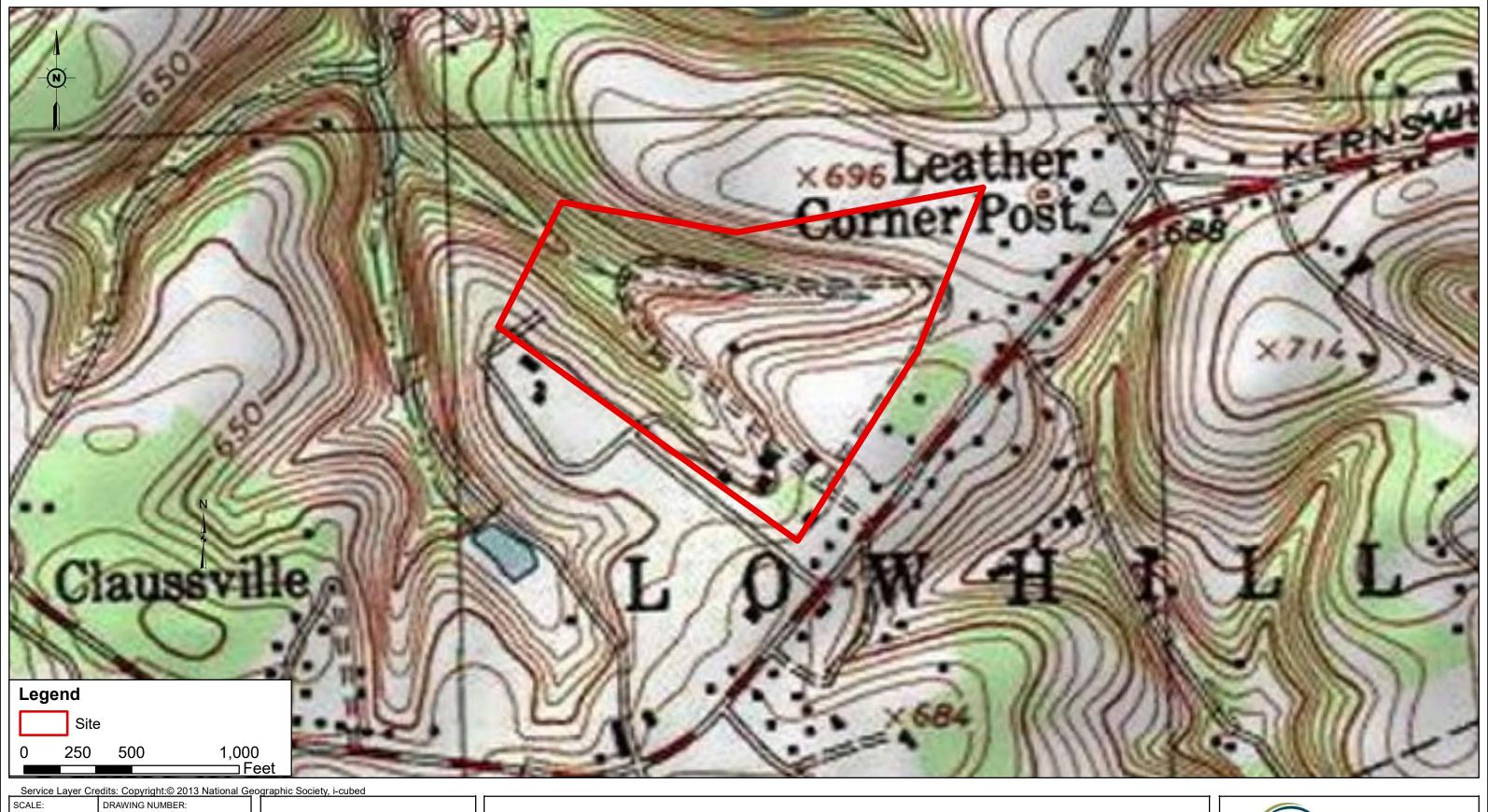
FIGURES 4 & 5 – TEST BORING PROFILES

FIGURE 6 - GRAPHICS KEY

LABORATORY TEST RESULTS

**TEST BORING LOGS** 

**TEST PIT LOGS** 



 Service Layer Credits: Copyright:© 2013 National Geo

 SCALE:
 DRAWING NUMBER:

 AS SHOWN
 FIGURE 1

 DRAWN BY:
 CHECKED BY:

 E. HINKLE
 B. WILDASIN

 APPROVED BY:
 DATE:

 M. GIUNTA
 03-03-2022

BASE PLAN:
N/A
PROVIDED BY:
N/A
DATE:
N/A

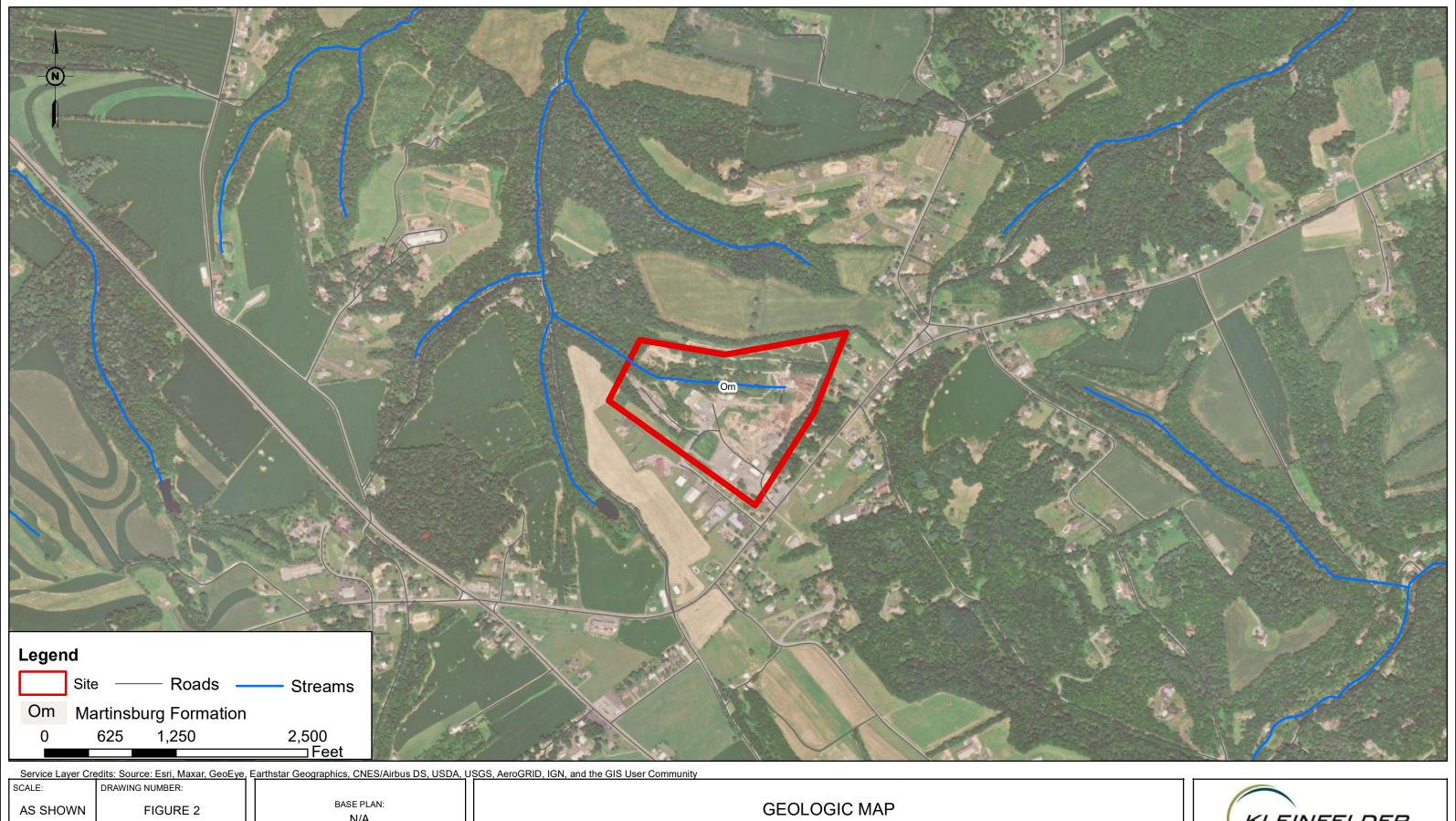
## TOPOGRAPHIC MAP PREPARED FOR

2951 BETZ COURT DEVELOPMENT

LOWHILL TOWNSHIP LEHIGH COUNTY PENNSYLVANIA



6330 HEDGEWOOD DR. SUITE 310 ALLENTOWN, PA, 18106 PH (610) 366-7120 FAX (610) 366-7121



CHECKED BY: DRAWN BY: E. HINKLE B. WILDASIN APPROVED BY: DATE: 03-03-2022 M. GIUNTA

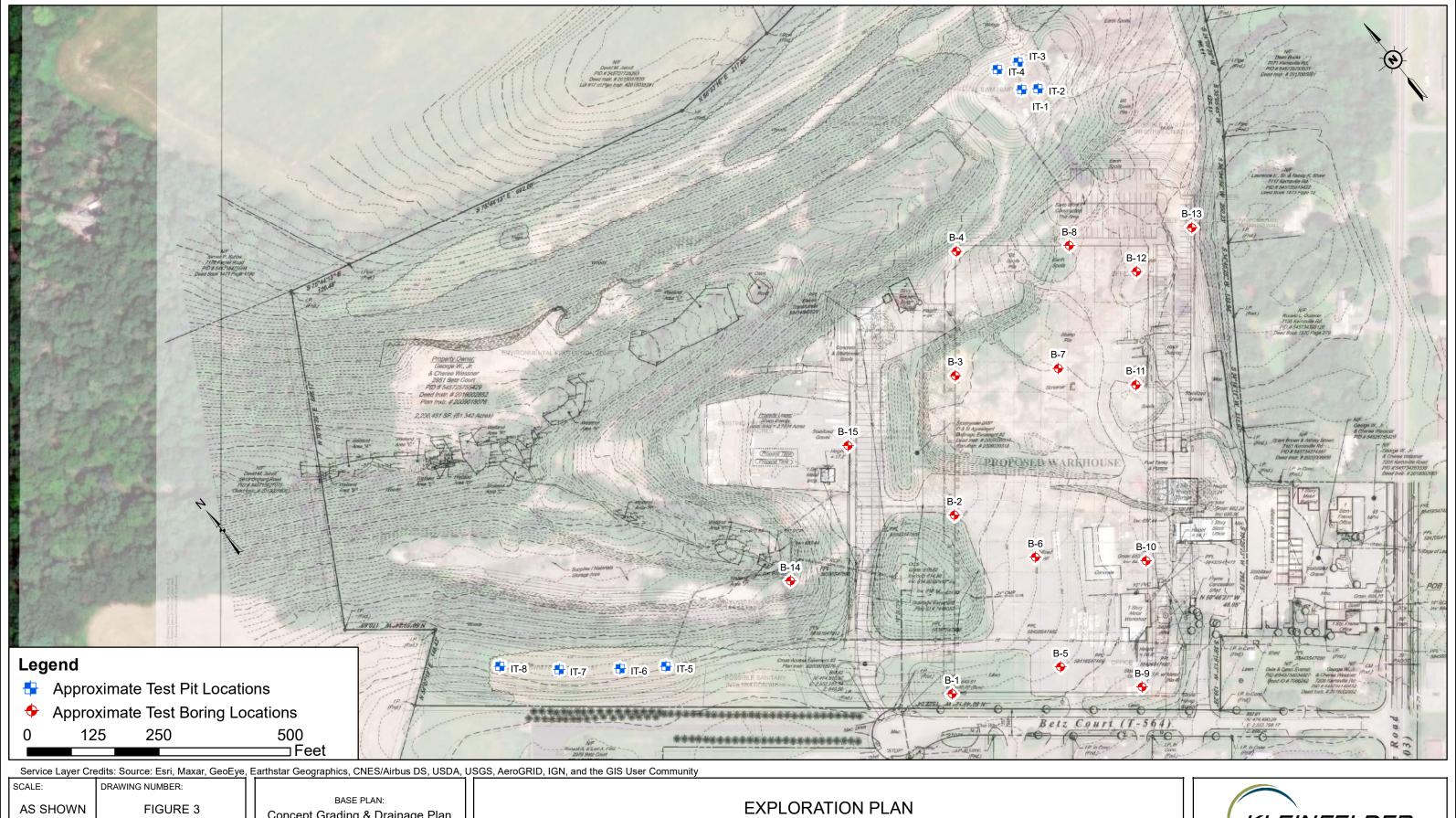
N/A PROVIDED BY: N/A DATE: N/A

PREPARED FOR 2951 BETZ COURT DEVELOPMENT

LOWHILL TOWNSHIP **LEHIGH COUNTY** PENNSYLVANIA



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DRAWN BY: CHECKED BY: B. WILDASIN E. HINKLE APPROVED BY: DATE: 03-03-2022 M. GIUNTA

Concept Grading & Drainage Plan Snyder, Secary & Associates, a Division of Pennoni

February 4, 2022

DATED:

# PREPARED FOR

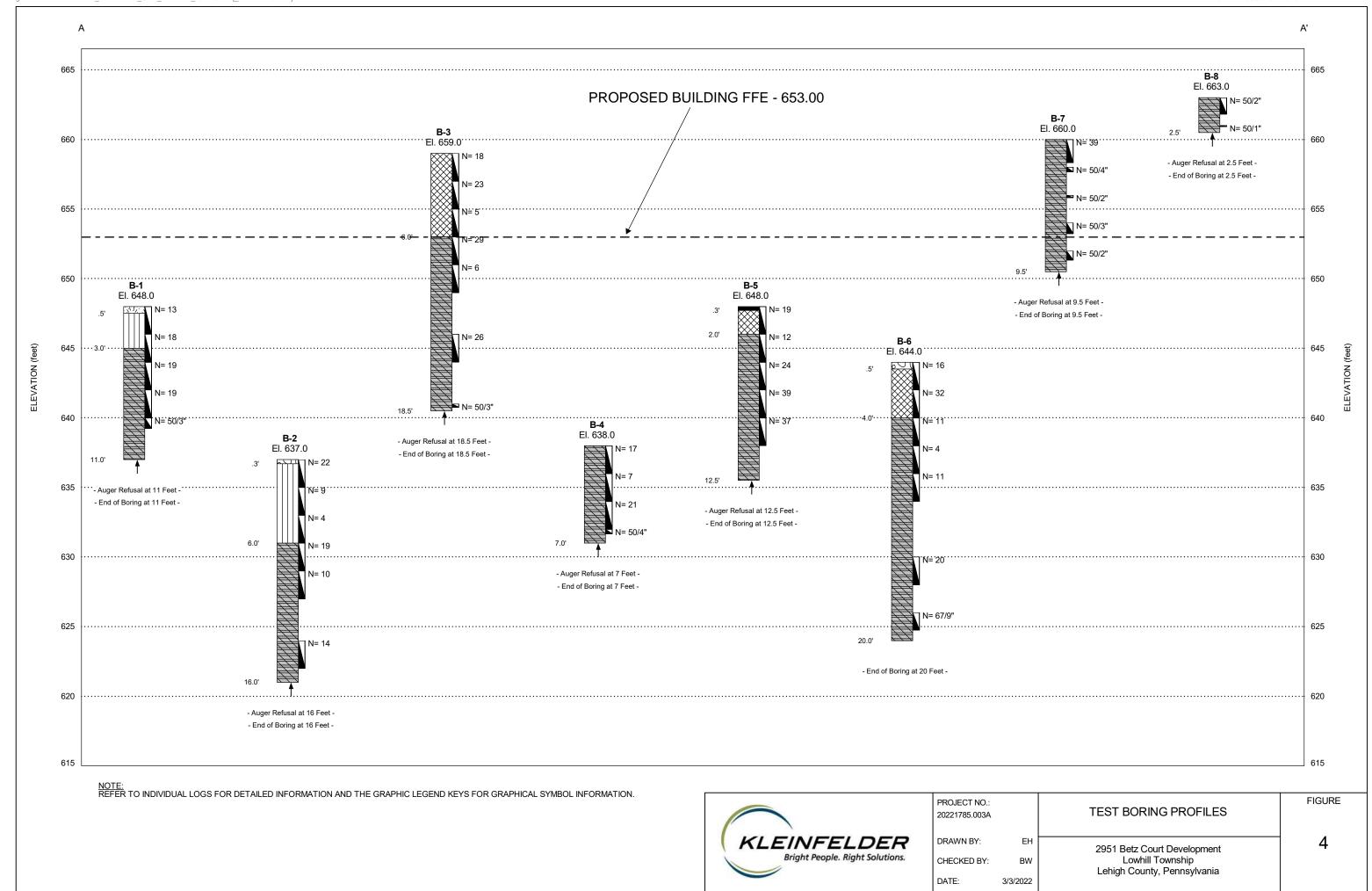
2951 BETZ COURT DEVELOPMENT

**LOWHILL TOWNSHIP LEHIGH COUNTY** PENNSYLVANIA

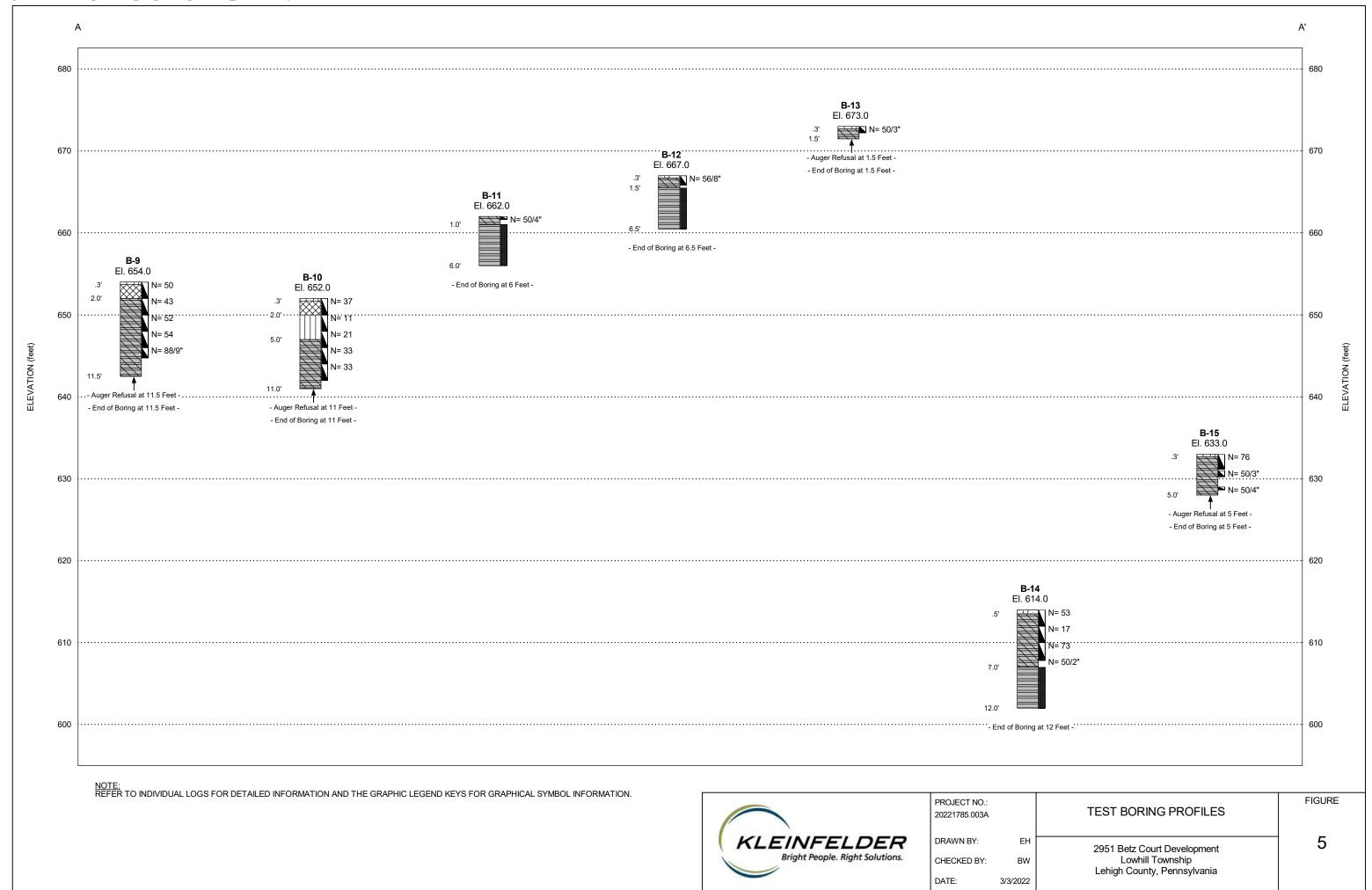


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OFFICE FILTER: ALLENTOWN



OFFICE FILTER: ALLENTOWN



L KLF GEO-LEG1 (GRAPHICS KEY) WITH USCS

#### SAMPLE/SAMPLER TYPE GRAPHICS



NQ CORE SAMPLE (1.874 in. (47.6 mm.) core diameter)

STANDARD PENETRATION SPLIT SPOON SAMPLER (2 in. (50.8 mm.) outer diameter and 1-3/8 in. (34.9 mm.) inner diameter)

#### **ROCK LITHOLOGY GRAPHICS**



SHALE

#### **GROUND WATER GRAPHICS**

- ▼ WATER LEVEL (level after exploration completion)
- ▼ WATER LEVEL (additional levels after exploration)



#### **NOTES**

- The report and graphics key are an integral part of these logs. All data and interpretations in this log are subject to the explanations and limitations stated in the report.
- Lines separating strata on the logs represent approximate boundaries only. Actual transitions may be gradual or differ from those shown.
- No warranty is provided as to the continuity of soil or rock conditions between individual sample locations.
- Logs represent general soil or rock conditions observed at the point of exploration on the date indicated.
- In general, Unified Soil Classification System designations presented on the logs were based on visual classification in the field and were modified where appropriate based on gradation and index property testing.
- Fine grained soils that plot within the hatched area on the Plasticity Chart, and coarse grained soils with between 5% and 12% passing the No. 200 sieve require dual USCS symbols, ie., GW-GM, GP-GM, GW-GC, GP-GC, GC-GM, SW-SM, SP-SM, SW-SC, SP-SC, SC-SM.
- If sampler is not able to be driven at least 6 inches then 50/X indicates number of blows required to drive the identified sampler X inches with a 140 pound hammer falling 30 inches.

#### ABBREVIATIONS WOH - Weight of Hammer WOR - Weight of Rod

#### UNIFIED SOIL CLASSIFICATION SYSTEM (ASTM D 2487)

OIT	ILD C	OIL CLAS	SIFICATION	JIY O I	SILI	VI (A	51 W D 2407)						
	ve)	CLEAN GRAVEL	Cu≥4 and 1≤Cc≤3	Ä	Gl	N	WELL-GRADED GRAVELS, GRAVEL-SAND MIXTURES WITH LITTLE OR NO FINES						
	ger than the #4 sie	WITH <5% FINES	Cu<4 and/ or 1>Cc>3		G	P	POORLY GRADED GRAVELS, GRAVEL-SAND MIXTURES WITH LITTLE OR NO FINES						
			Cu≥4 and		GW-	GM	WELL-GRADED GRAVELS, GRAVEL-SAND MIXTURES WITH LITTLE FINES						
	ction is lar	GRAVELS WITH	1≤Cc≤3		GW-	-GC	WELL-GRADED GRAVELS, GRAVEL-SAND MIXTURES WITH LITTLE CLAY FINES						
ieve)	oarse frac	5% TO 12% FINES	Cu<4 and/		GP-	GM	POORLY GRADED GRAVELS, GRAVEL-SAND MIXTURES WITH LITTLE FINES						
ne #200 s	n half of c		or 1>Cc>3		GP-GC		GP-GC		POORLY GRADED GRAVELS, GRAVEL-SAND MIXTURES WITH LITTLE CLAY FINES				
ger than tl	GRAVELS (More than half of coarse fraction is larger than the #4 sieve)				GI	М	SILTY GRAVELS, GRAVEL-SILT-SAND MIXTURES						
COARSE GRAINED SOILS (More than half of material is larger than the #200 sieve)		GRAVELS WITH > 12% FINES			GC GC-GM		CLAYEY GRAVELS, GRAVEL-SAND-CLAY MIXTURES						
alf of mate	GR GR						CLAYEY GRAVELS, GRAVEL-SAND-CLAY-SILT MIXTURES						
re than ha	ore of coarse fraction is smaller than the #4 sieve)	CLEAN SANDS WITH	Cu≥6 and 1≤Cc≤3		SW		WELL-GRADED SANDS, SAND-GRAVEL MIXTURES WITH LITTLE OR NO FINES						
OILS (Mo		<5% FINES	Cu<6 and/ or 1>Cc>3				POORLY GRADED SANDS, SAND-GRAVEL MIXTURES WITH LITTLE OR NO FINES						
AINED S	er than th	SANDS WITH 5% TO 12% FINES	Cu≥6 and	• • • • • • • • • • • • • • • • • • • •	SW-SM		SW-SM		WELL-GRADED SANDS, SAND-GRAVEL MIXTURES WITH LITTLE FINES				
RSE GR	n is small		1≤Cc≤3		SW-	sc	WELL-GRADED SANDS, SAND-GRAVEL MIXTURES WITH LITTLE CLAY FINES						
COA	se fractio		Cu<6 and/		SP-	SM	POORLY GRADED SANDS, SAND-GRAVEL MIXTURES WITH LITTLE FINES						
	re of coar		or 1>Cc>3		SP-	sc	POORLY GRADED SANDS, SAND-GRAVEL MIXTURES WITH LITTLE CLAY FINES						
	Ε	0.111D0			SI	М	SILTY SANDS, SAND-GRAVEL-SILT MIXTURES						
	SANDS (Half or	SANDS WITH > 12% FINES			S	С	CLAYEY SANDS, SAND-GRAVEL-CLAY MIXTURES						
	o,				SC-	SM	CLAYEY SANDS, SAND-SILT-CLAY MIXTURES						
S			T	N	1L		GANIC SILTS AND VERY FINE SANDS, SILTY OR YEY FINE SANDS, SILTS WITH SLIGHT PLASTICITY						
alf or more of material is smaller than the #200 sieve)		OII === ::::		1	L	INOR	GANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY						
		SILTS AND (Liquid L	imit /////	1			S, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS GANIC CLAYS-SILTS OF LOW PLASTICITY, GRAVELLY						
Ę.	smaller than the #200 sieve)	less than	50)	CL	-ML	CLAY	S, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS						
P P	200		==	C	L		ANIC SILTS & ORGANIC SILTY CLAYS OF PLASTICITY						
<b>9</b> 8	sma e #2			M	IH	INOR	GANIC SILTS, MICACEOUS OR						
in i	″ £	SILTS AND (Liquid L		<b>у</b>	СН		DIATOMACEOUS FINE SAND OR SILT INORGANIC CLAYS OF HIGH PLASTICITY, FAT CI AYS						

SILTS AND CLAYS

(Liquid Limit
50 or greater)

CH

CH

CH

CLAYS

ORGANIC CLAYS & ORGANIC SILTS OF

MEDIUM-TO-HIGH PLASTICITY

NOTE: USE MATERIAL DESCRIPTION ON THE LOG TO DEFINE A GRAPHIC THAT MAY NOT BE

PROVIDED ON THIS LEGEND.

Lehigh County, Pennsylvania

6



DATE:

3/3/2022

PROJECT NO.:
20221785.003A

DRAWN BY:
CHECKED BY:
BW

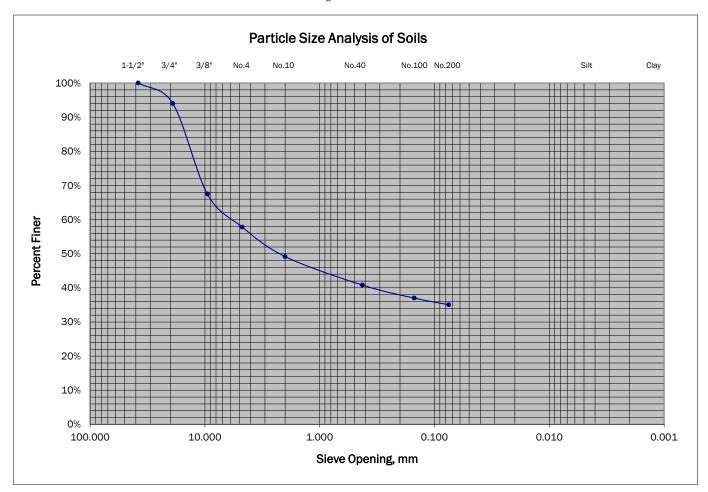
GRAPHICS KEY

2951 Betz Court Development
Lowhill Township



### Soil Classification Report

Per ASTM Designations D 2487 and D 2488

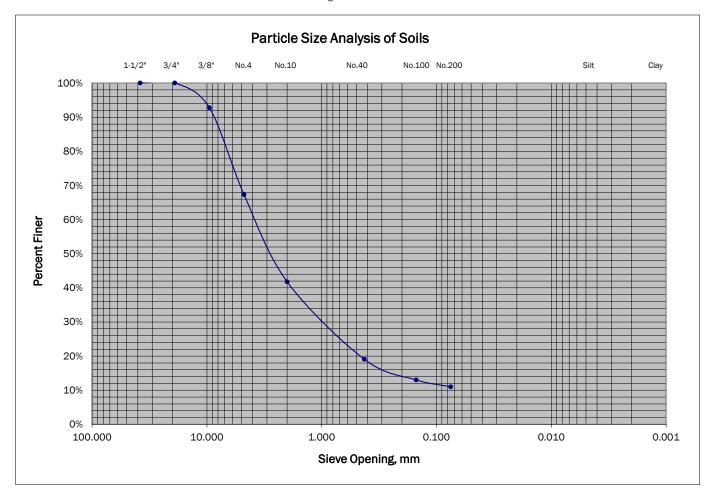


As-Recei	ved Moisture	14.9%				Particle Size Distribution							
USCS Classification: Silty GRAVEL with Sand (GM)								US Standard	Sieve Size	Opening (mm)	(	%Finer	
Gravel:	42.2%	Coarse:	6.0%			Fine:	36.2%	Coarse	1-1/2"	38.0	1	L00.0%	
Sand:	22.8%	Coarse:	8.7%	Medium:	8.3%	Fine:	5.8%	GRAVEL	3/4"	19.0		94.0%	
Fines:	35.0%	Silt:			Clay:			Fine	3/8"	9.50		67.5%	
Gravel D	escription:	Subangu	lar						No. 4	4.75		57.8%	
								Coarse	No. 10	2.00		49.1%	
Sand De	scription:	Subangu	lar					Medium	No. 40	0.425	40.8%		
								SAND	No. 100	0.150	;	37.0%	
Consiste	Consistency: N/A Dry Strength: N/A							Fine	No. 200	No. 200 0.075		35.0%	
Dilatancy	y: N/A			Toughness:		N/A		Hydrometer	Hydrometer Silt Size 0.005				
Structure	e: Homogene	ous	(	Cementatio	n:	Modera	ate	Analysis	Clay Size	0.001			
								D <sub>60</sub> :	D <sub>30</sub> :	D <sub>10</sub> :	Cu:	Cc:	
Boring:	B-5							Atterberg Limits	LL: NP	PL: NP		PI: NP	
Sample: S-2, S-3 Depth: 2' - 6'						Description: Brown to tan Silty GRAVEL with Sand							
Project:	2951 Betz	Court Dev	elopmer	nt									
							Remarks: Stratum I						
Client: Snyder, Secary & Associates, a Division of Pennoni													
Kleinfeld	ler Project Ni	umber:	:	20221785.0	003A			Report Date:	March 3, 2022				



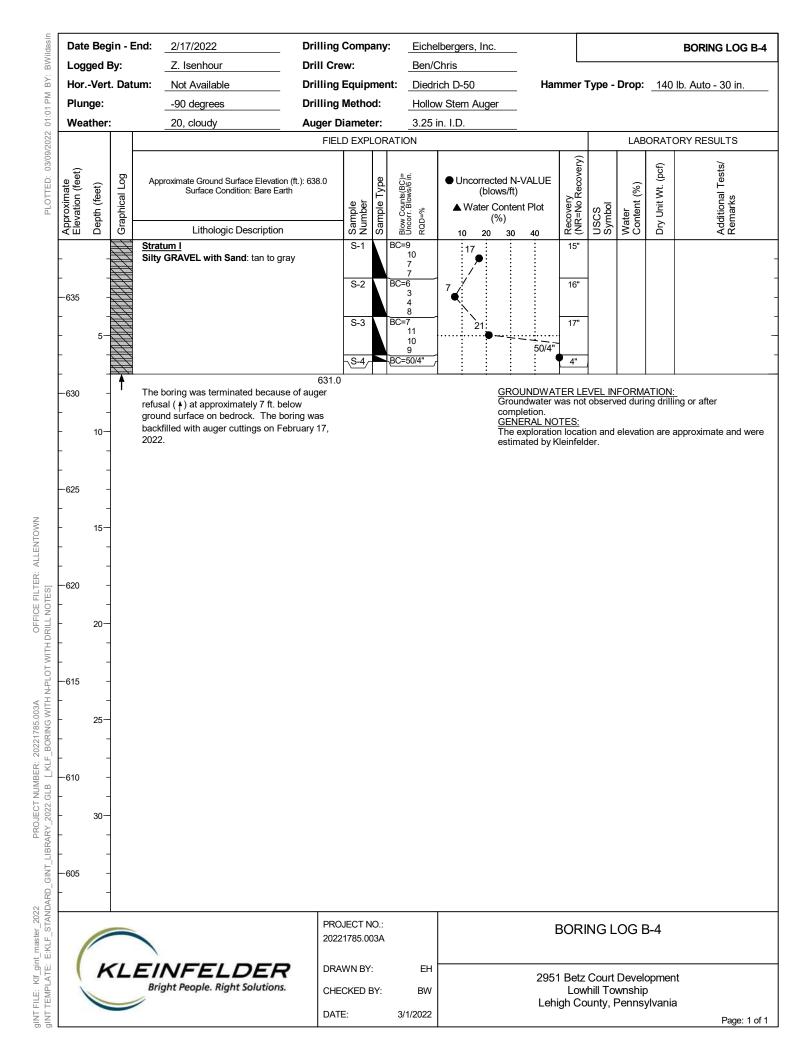
### Soil Classification Report

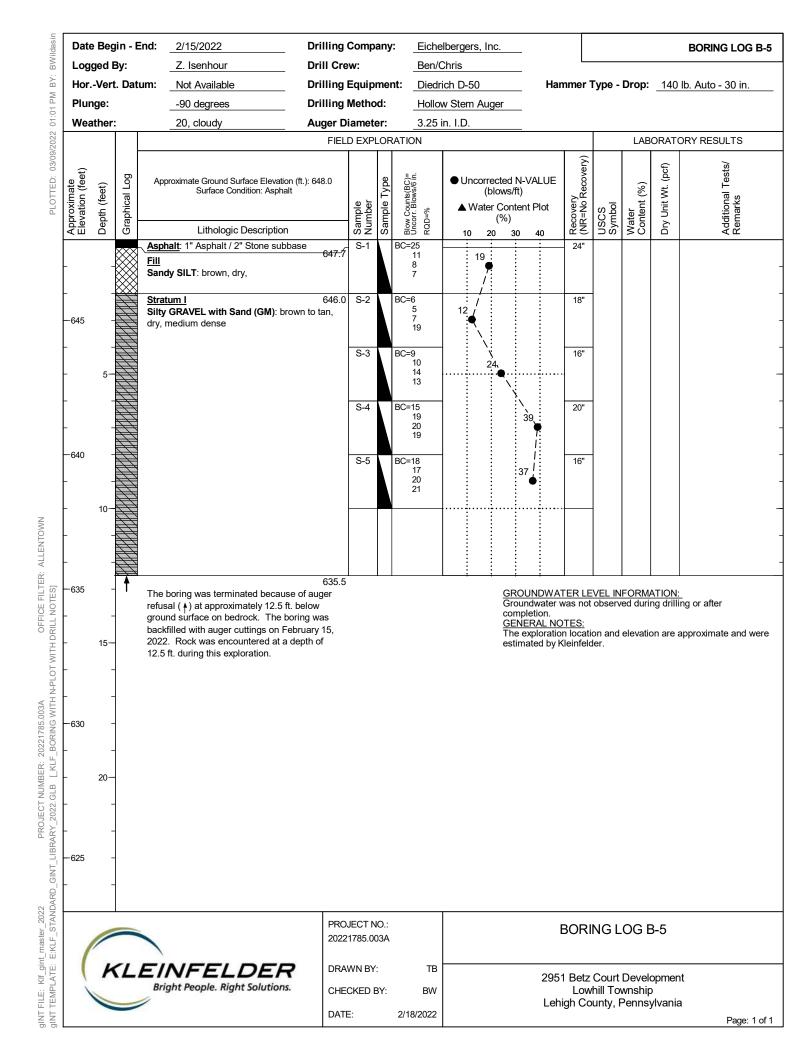
Per ASTM Designations D 2487 and D 2488

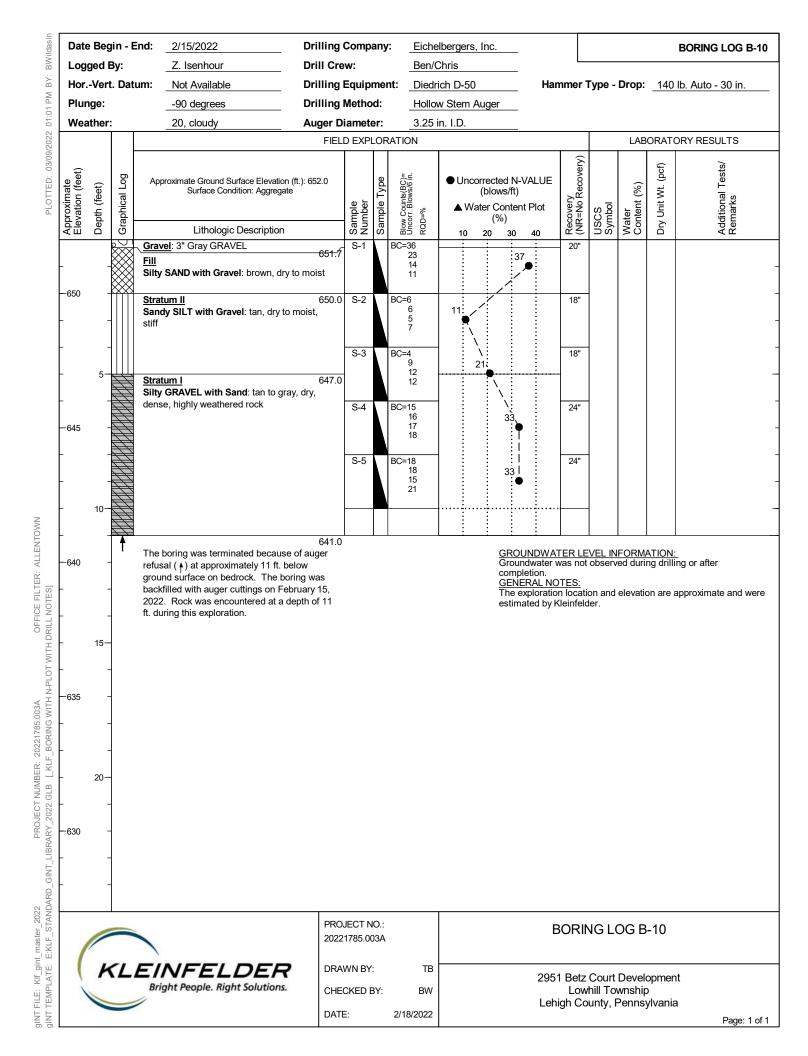


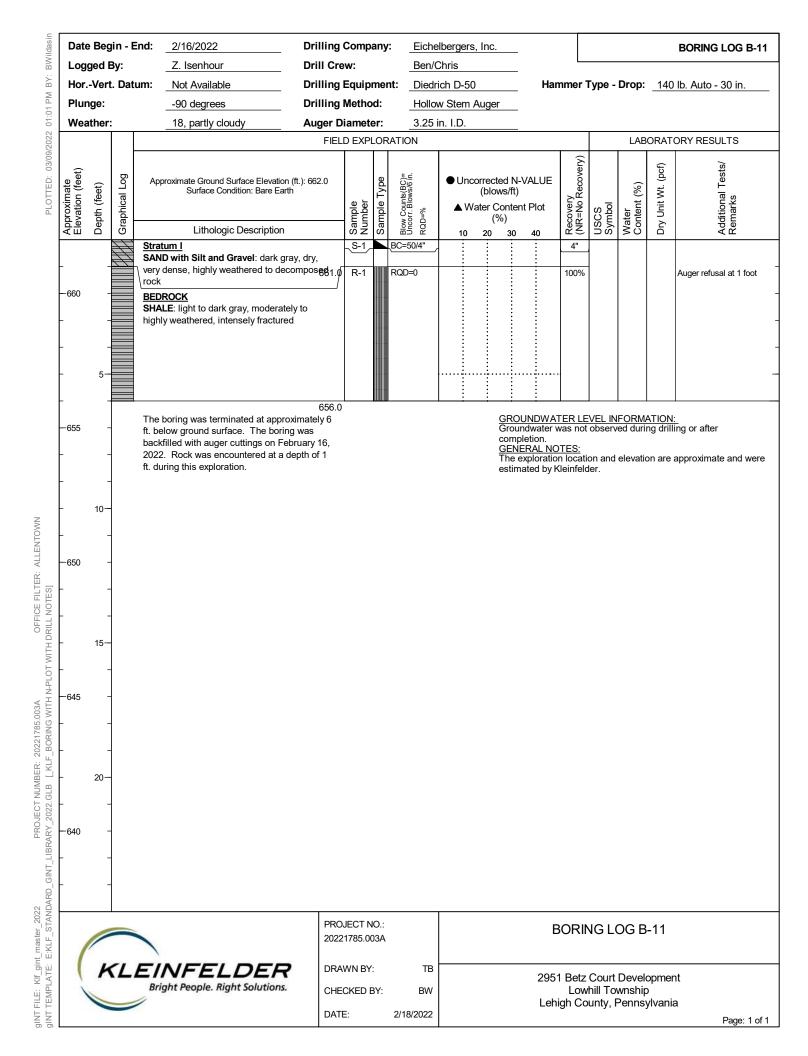
As-Recei	ved Moisture	8.9%			Particle Size Distribution							
USCS CI	assification:	Well-graded SA	ND with Silt	and Grav	US Standard	Sieve Size	Opening (mm)	%	Finer			
Gravel:	32.7%	<b>Coarse:</b> 0.0%			Fine:	32.7%	Coarse	1-1/2"	38.0	10	00.0%	
Sand:	56.3%	Coarse: 25.5%	Medium:	22.8%	Fine:	8.0%	GRAVEL	3/4"	19.0	10	00.0%	
Fines:	11.0%	Silt:		Clay:			Fine	3/8"	9.50	9	2.8%	
Gravel D	escription:	Subangular						No. 4	4.75	67.3%		
							Coarse	No. 10	2.00	41.8%		
Sand De	scription:	Subangular to s	subrounded				Medium	No. 40 0.425		19.0%		
							SAND	No. 100	0.150	13.0%		
Consiste	Consistency: N/A Dry Strength: N/A						Fine	No. 200 0.075		1	1.0%	
Dilatancy	y: N/A		Toughness	:	N/A		Hydrometer	rometer Silt Size 0.005				
Structure	e: Homogene	ous	Cementatio	on:	Weak		Analysis	Clay Size	0.001			
							D <sub>60</sub> : 4.7	D <sub>30</sub> : 1	D <sub>10</sub> : 0.077	Cu: 61	Cc: 2.76	
Boring:	B-9						Atterberg Limits	LL: NP	PL: NP	Р	l: NP	
Sample: S-4 Depth: 6' - 8'						Description: Tan SAND with Silt and Gravel						
Project:	2951 Betz	Court Developm	ent									
						Remarks:	Stratum I					
Client: Snyder, Secary & Associates, a Division of Pennoni												
Kleinfeld	ler Project Ni	umber:	20221785	.003A			Report Date:	March 3, 2022				

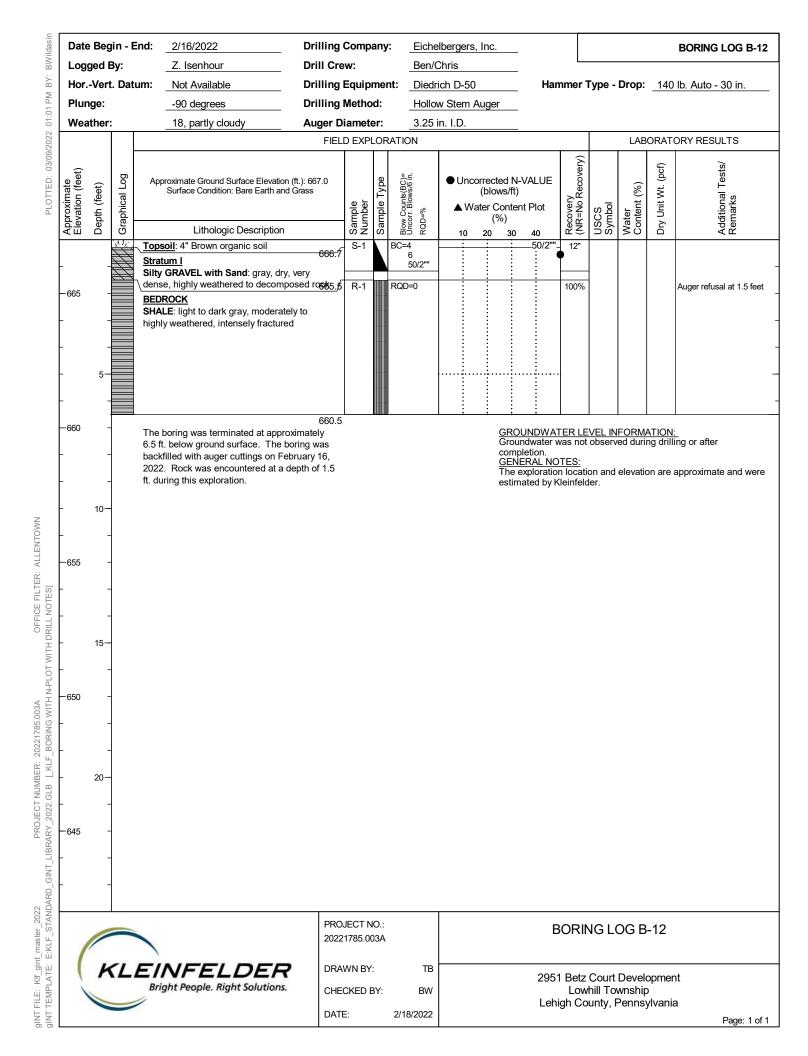
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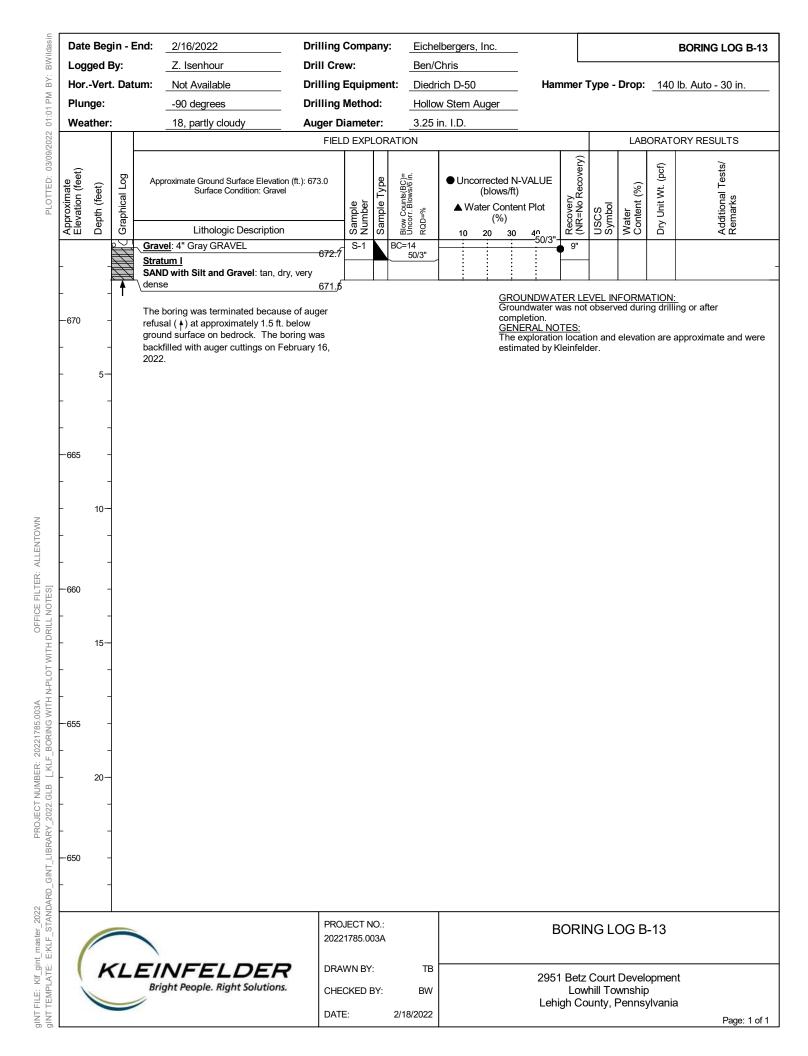


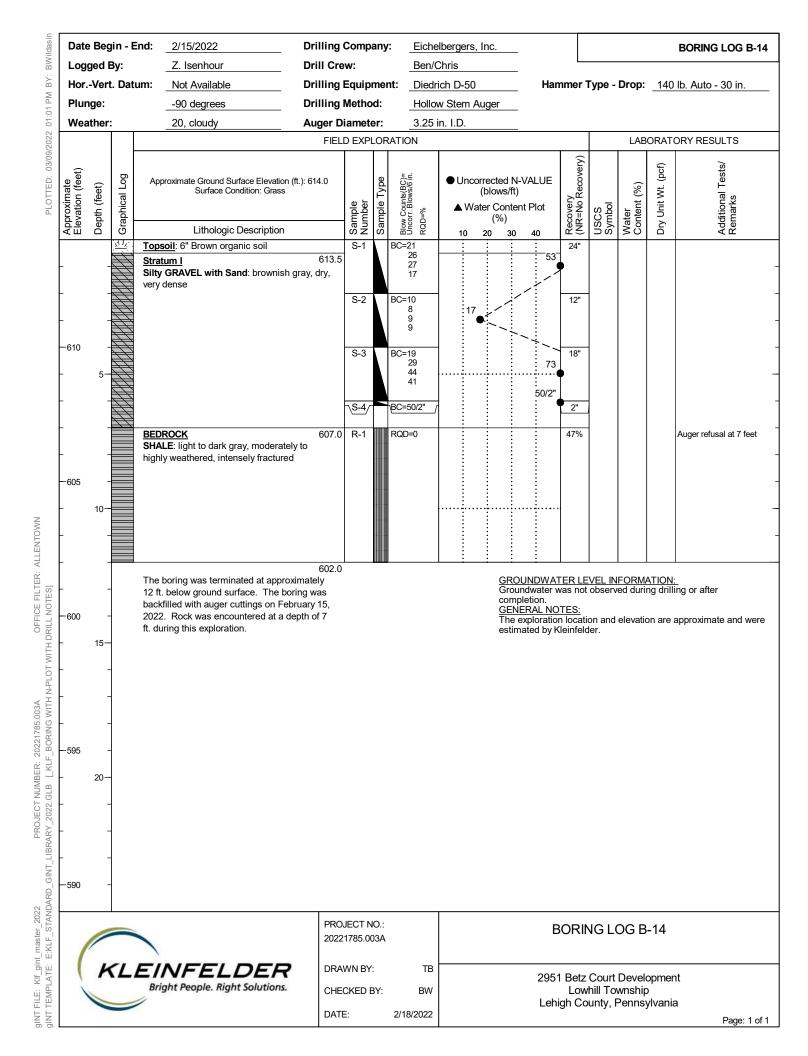


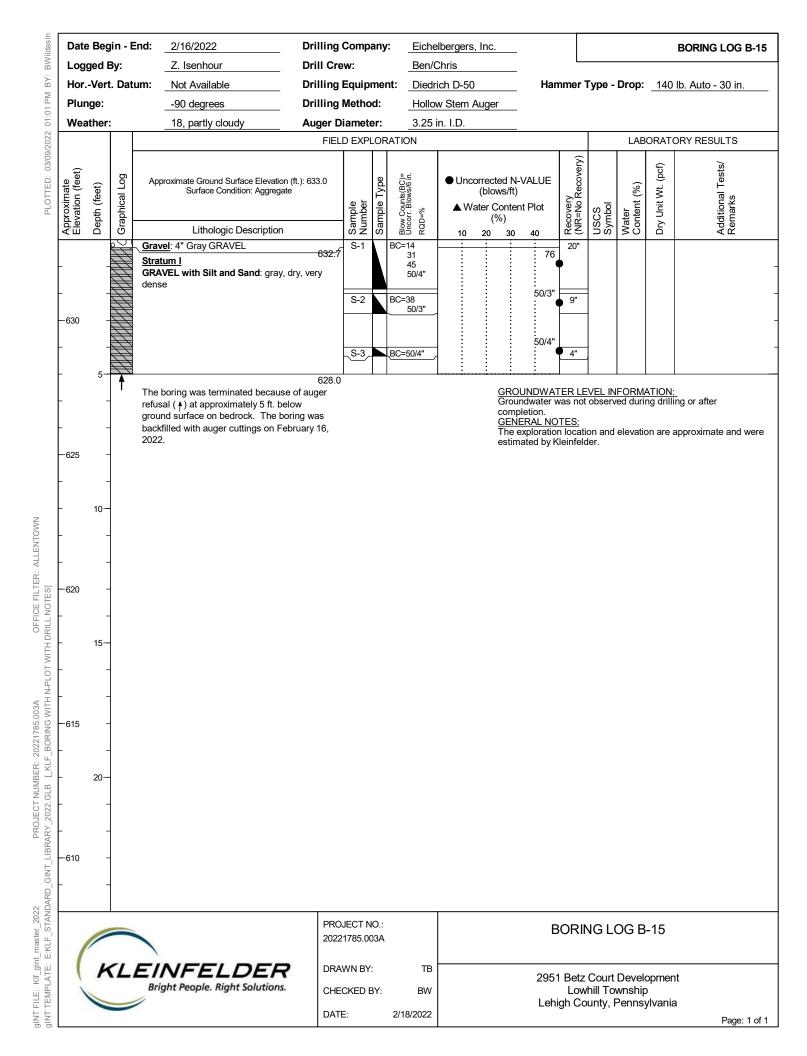












PROJECT NUMBER: 20221785.003A Klf\_gint\_master\_2022 gINT FILE:



DRAWN BY: EΗ

CHECKED BY: BW DATE: 2/25/2022

2951 Betz Court Lowhill Township Lehigh County, Pennsylvania

GROUNDWATER LEVEL INFORMATION:

Perched groundwater was observed at approximately 0.5 ft. below ground surface during excavation.

below ground surface during excavation.



PROJECT NO .: 20221785.003A

DATE:

DRAWN BY: EΗ

CHECKED BY: BW

2/25/2022

2951 Betz Court Lowhill Township Lehigh County, Pennsylvania

**TEST PIT LOG IT-2** 

Page: 1 of 1

**TEST PIT LOG IT-2** 

Additional Tests/ Remarks

Basin side walls collapsing

Infiltration test at 6 ft Presoak 1 (30min): 0.0" Presoak 2 (30min): 0.0" Reading 1 (30min): 0.0" Reading 2 (30min): 0.0" Reading 3 (30min): 0.0" Reading 4 (30min): 0.0"

Field Rate = 0.0 in/hr

Idasii	Date Begin - End: Logged By:		2/23/2022	<b>Excavation Company</b>	Excavation Company: Joma Excavating						TEST PIT LOG IT-3				
D V			E. Hinkle	<b>Excavation Crew:</b>	J. Santo	s Sı				ı					
□	HorVert.	Vert. Datum: Not Available		Excavation Equip.:	416 CAT	AT Backhoe									
0	Plunge:		N/A degrees	Excav. Dimensions:	_ft										
. 08.	Weather:		60 degrees, cloudy												
1/202/			FIELD E	EXPLORATION						LA	BORA	TORY	RESU	JLTS	
PLOTIED: US/U	Depth (feet)	Graphical Log		Condition: Gravel		Sample Type	USCS Symbol	Water Content (%)	Dry Unit Wt. (pcf)	Passing #4 (%)	Passing #200 (%)	Liquid Limit	Plasticity Index (NP=NonPlastic)	Additional Tests/ Remarks	
				c Description		Sa	US Sy	>္ဂိပိ	٥٦	Ра	Ра	Liq	₩Ž	Ad	
DARU-GINI_LIBRARI_2022.5LB	<b>▼</b>	Str. Silt	e test pit was terminated at appretest pit was backfilled with except the test pit was backfilled with except pit was backfilled with except pit was backfilled with except pi	, wet, highly weathered bedro	-8.0 surface.		₹	GROU Groun surfac GENE	e 3 hou	ırs afte	er exca	INFO d at a a vation	RMAT pproxin compl	Basin side walls collapsing to 4' below exisiting site grades	
E.NLF_OIAIN				PROJECT NO.: 20221785.003A						TES <sup>-</sup>	T PIT	LO	G IT-	-3	
GINI LEMPLAIE	K	LEI	NFELDER	CHECKED BY:	EH BW 25/2022	2951 Betz Court Lowhill Township Lehigh County, Pennsylvania Page: 1 of 1									

-8.5 The test pit was terminated at approximately 8.5 ft. below ground surface. The test pit was backfilled with excavated material on February 23, 2022.

GROUNDWATER LEVEL INFORMATION: Groundwater was not observed during excavation or after completion. **GENERAL NOTES:** 



PROJECT NO .: 20221785.003A

CHECKED BY:

DRAWN BY: EΗ

BW

DATE: 2/25/2022 **TEST PIT LOG IT-4** 

2951 Betz Court Lowhill Township Lehigh County, Pennsylvania

Page: 1 of 1

**TEST PIT LOG IT-4** 

Additional Tests/ Remarks

PROJECT NUMBER: 20221785.003A Klf\_gint\_master\_2022 gINT FILE:

Bright People. Right Solutions.

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2951 Betz Court Lowhill Township Lehigh County, Pennsylvania

Page: 1 of 1



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EΗ CHECKED BY: BW DATE: 2/25/2022

2951 Betz Court Lowhill Township Lehigh County, Pennsylvania

gINT FILE:

Bright People. Right Solutions.

CHECKED BY: BW

2/25/2022

DATE:

Lowhill Township Lehigh County, Pennsylvania



Klf\_gint\_master\_2022

gINT FILE:

PROJECT NO .: 20221785.003A

DRAWN BY: EΗ CHECKED BY: BW

DATE: 2/25/2022 **TEST PIT LOG IT-8** 

2951 Betz Court Lowhill Township Lehigh County, Pennsylvania